STORMWATER POLLUTION PREVENTION PLAN (SWPPP)

For

MARMEN-WELCON TOWER MANUFACTURING PLANT

PREPARED FOR:



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FINAL SITE PLAN SUBMISSION

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1. INTRODUCTION

A stormwater management assessment has been conducted for the proposed project in order to protect the waters of the State of New York from the adverse impacts of stormwater runoff. This report presents an analysis of the project in accordance with the *New York State Department of Environmental Conservation SPDES General Permit for Stormwater Discharges from Construction Activity Permit No. GP-0-20-001.* A separate Drainage Design Report (included as Appendix C of this report) has been developed to address the *New York State Stormwater Management Design Manual* ("The Manual"). As required, the Stormwater Pollution Prevention Plan is designed, where appropriate, to incorporate green infrastructure techniques that preserve natural resources and utilize the existing hydrology of the site, provide runoff reduction practices, water quality treatment practices, apply volume and peak control practices for channel protection, overbank flood control, and extreme flood control as appropriate.

In accordance with Appendix B, Table 2 of the SPDES General Permit for Construction Activity, GP-0-20-001 (included as Appendix E of this report), industrial facilities that involve a soil disturbance of one or more acres require the preparation of a full SWPPP that includes post-construction stormwater management practices. In total, approximately 72.7 acres of soil disturbance is expected during the construction of this project. Therefore, this project includes the development of erosion and sediment controls, green infrastructure site planning techniques, runoff reduction volume practices and post-construction stormwater management practices.

The general contractor and subcontractors performing any activity that involves soil disturbance will be required to comply with the terms and conditions of the SWPPP for the project identified as a condition of authorization to discharge stormwater. The Contractor shall provide signed certifications (Form CONR 5) for itself and all applicable subcontractors at the preconstruction meeting. These signed certifications shall be included as part of the SWPPP. The SPDES General Permit and SWPPP must be kept on file at the Project Field Office. As required by the conditions described in the SPDES general permit, the SWPPP shall be kept current, and updates will be made to reflect changes in the design, construction and operation, or maintenance of the project.

The complete set of construction drawings and specifications are provided as separate documents; however, they should be considered an integral component of the SWPPP and are referenced throughout this document. Prior to the start of construction activities, a Notice of Intent (NOI) must be filed and accepted by the NYSDEC. A Draft NOI has been included in this document as Appendix J. The applicant must retain all documentation for 5 years after NYSDEC accepts the Notice of Termination (NOT).

1.1 Scope of the Project

The proposed development is an offshore wind (OSW) manufacturing operation that will produce wind turbine tower components. The site development includes 603,500 +/- square feet of OSW manufacturing spread over four (4) buildings with ancillary impervious areas including parking for automobiles and trucks, roadway, bridge, and a maritime wharf. The remainder of the site will be used for tower storage and be made up of dense graded aggregate (compacted gravel). There will also be small pervious areas of grass and unaltered brush and trees.

1.2 Location of Project

The Project is situated on 81.62 acres of land on Beacon Island ("Expansion Site"), located at the confluence of the Normans Kill and Hudson River. The project also includes development within 4.4 acres



of the adjoining parcel owned by National Grid, the extension and improvement of Normanskill Street (Normanskill Street Improvements) and widening of Rt. 144 (Offsite Improvements). The project owner, Albany Port District Commission (APDC), is proposing to develop the vacant parcels of land (tax parcels 98.00-2-10.23 and 98.01-2-1.0) to expand the existing Port of Albany in the Town of Bethlehem, Albany County, New York. Refer to the Location Map in Appendix A.

The project is not located within a TMDL and does not discharge into a 303(d) listed waterbody.

Table 1 - Location Table

Approximate Coordinate Position @ Center of Project		
Latitude 42° 36′ 10.8″ N		
Longitude	73° 45′ 57.0″ W	

1.3 Project Type and Size

The project is a new development construction project that has a disturbance area of approximately 72.7 +/- acres. The new impervious area is approximately 65.9 acres.

1.4 Project Description

The proposed project will include development of an OSW tower manufacturing (Marmen-Welcon) facility consisting of five (5) separate buildings totaling up to 625,539+/- square feet of floor space. The following is a breakdown of the function and size of each building:

- Building A Plate Preparation & Welding (299,250 SF)
- Building B Welding Finishing (111,023 SF)
- Building C Blast Metallization Plant (131,968 SF)
- Building D Internal Assembly Finishing (61,550 SF)
- Building E Material Receiving (21,748 SF)

Tower production will occur within four (4) buildings (Buildings A-D) at the main facility on the Port Expansion property located in the Town of Bethlehem. The 5th building (Building E) will be located at 700 Smith Boulevard within the existing Port District in the City of Albany. A proposed gated bridge over the Normans Kill will provide a truck transportation route in and out of the main facility, by connecting Beacon Island and the 14.7-acre offsite parcel at 700 Smith Boulevard. In conjunction with the proposed bridge, Normanskill Street is to be extended from its existing end point to the bridge. The existing pavement will be improved to accommodate the proposed trucking route. River Road (Rt. 144) will be widened to accommodate the employee entrance. Employee parking will be situated on the adjoining land owned by National Grid with access from River Road. A proposed 500 LF wharf and associated dredging along the Hudson River will be used to load and ship completed tower sections. A separate stormwater analysis and SWPPP has been prepared for the 14.7-acre Building E site at 700 Smith Boulevard and the portion of Normanskill Street. located in the City of Albany, as the sites are separated by approximately 1-mile and are under separate MS4 jurisdictions.

The purpose of this report is to assess the stormwater quality, quantity, and erosion and sediment control for the development of the site. This report has been developed in accordance with the New York State Department of Environmental Conservation (NYSDEC) State Pollution Discharge Elimination System (SPDES) General Permit for Stormwater Discharges from Construction Activity, GP-0-20-001 (Permit) and the NYSDEC Stormwater Management Design Manual (The Manual). The project site is located within the



Town of Bethlehem, Albany County, New York, which is an MS4 community, requiring this report and project to receive approval from the Town.

The soil disturbance area addressed in this is report is contained within the Town of Bethlehem. This report does not include coverage for work within the Mean High Water (MHW) elevation of the Hudson River or the Normans Kill. Work within the MHW line will be covered under a separate permit.

The total disturbance area is 72.7 +/- acres and includes the Expansion Site, Normanskill Street Improvements and Offsite Improvement. The existing impervious area is approximately 5.16 +/- acres, 7.09% of the total disturbance area. The proposed site development will consist of 65.9 +/- acres of impervious cover, 90.6% of the total disturbance area.

Due to the amount of soil disturbance proposed for this project, a 5-acre disturbance waiver is being requested. The 5-acre waiver request along with all required documentation is included as Appendix L of this report.

1.5 Cultural Resources

A Supplemental Environmental Impact Statement (SEIS) has been developed as part of the SEQR process for the Port of Albany Expansion Project. A SHPO review was conducted, and the current status reflects "No Adverse Effect". The SHPO review letter for the GEIS review process, dated September 13, 2019. A follow up SEIS SHPO review letter, dated December 9, 2021, resulted in a follow up noise study and coordination with the Stockbridge-Munsee Tribal Historic Preservation (SMTHP). Multiple coordination meetings were conducted resulting in some modifications to the site design and additional information provided. As a result, the SMTHP provided a follow up letter dated March 3, 2022, confirming the project has "No Adverse Effect". In response to the SMTHP letter, SPHO has issued a letter of "No Adverse Effect" dated March 25, 2022, contingent upon a deed restriction to be filed by the Owner to protect the Tree and Vegetation buffer area during the construction phase as well as permanently after construction is completed. All referenced letters have been included in Appendix F of this report.

1.6 On-site Wetlands

As part of the Draft Generic Environmental Impact Statement (DGEIS) and SEIS, impact to aquatic resources, including wetlands, were evaluated. The New York State Freshwater Wetland and Tidal Wetlands mapping of the project site indicates there are no NYSDEC jurisdictional wetlands within or adjacent to the project area. Review of USFWS National Wetlands Inventory (NWI) mapping of the project site indicates that the majority of the project area is mapped as palustrine emergent wetlands (PEM) and palustrine forested wetlands (PFO). It should be noted that NWI mapping does not have any regulatory consequence, but rather indicates areas that may meet federal wetland criteria as identified by the USFWS using aerial photography.

A wetland delineation was conducted in April 2019 by McFarland Johnson (MJ) for the FGEIS. The results of the delineation indicated that there are 8 freshwater wetlands located within the project limits. These wetlands are hereafter referred to as Wetlands 1, 3, 4, 5, 6, 7, 8, and 9. Wetlands within the original study area totaled approximately 2.33 acres. A Supplemental Wetland Delineation was performed by MJ in April 2021 within the 18.22 acres on the National Grid Parcel. One contiguous wetland, comprising of approximately 7.13 acres, was delineated within the 18.22-acre area. The delineated wetland represents an extension of the 2019 wetland delineation and previously identified as Wetland 1. Wetland 1 drains in a northerly direction into 40-inch corrugated metal pipe (CMP) which discharges directly to the Normans Kill.



The Project will result in direct impacts to 0.81 acres of Wetland 1 located in Beacon Island (original Project Area) and 0.01 acres of direct impact to Wetland 1 on National Grid property for the construction of a retaining wall. In addition, there is a 0.04-acre impact to Wetland 9 for the bridge over the Normans Kill and a 0.02-acre impact to Wetland 7 for roadway improvements. There will also be approximately 0.33 acres of temporary impacts to wetlands during construction. Total permanent wetland impacts are estimated to be approximately 0.86 acre.

Compensatory wetland mitigation will be satisfied through a federally approved In-Lieu Fee Mitigation Program or off-site mitigation bank (The Wetland Trust). Mitigation in accordance with USACE rules and regulations will ensure no net loss of wetlands and will be included as part of the Joint application Permit submitted to the USACE and NYSDEC.

2. PROJECT MAPS AND PLANS

2.1 Location Map

See Appendix A

2.2 Soil Maps

See Appendix E of the Drainage Design Report (included as Appendix C of this report)

2.3 Erosion and Sediment Control Plans

See Appendix B of this report

2.4 Existing and Proposed Subcatchment Maps

See Appendix A and B of the Drainage Design Report (included as Appendix C of this report)

3. PROJECT SOILS

3.1 NRCS Soil Map

See Appendix E of the Drainage Design Report (included as Appendix C of this report)

3.2 Soil Types

The following soil type(s) and hydrologic group(s) are present within the project area of disturbance:

Table 2 – Soil Types

Symbol	Soil Name	Hydrologic Soil Group
HuE	Hudson silt loam, 25 to 45 percent slopes	C/D
NrD	Nassau very channery silt loam, hilly, very rocky	D
Ug	Udorthents, loamy	А
Ur	Urban land	
Wo Wayland soils complex, non-calcareous substratum 0 to 3 percent slopes, frequently flooded		B/D



3.3 Discussion of Soil Characteristics and Soil Erosion Hazard Potential

According to the Natural Resources Conservation Service (NRCS) web soil survey, there are five (5) mapped soil units identified within the project boundary. See Appendix E of the Drainage Design Report (included as Appendix C of this report). The majority of the soil at the expansion site falls within the hydrologic soil group B/D. The first letter corresponds to drained soil's properties under drained conditions and the second to saturated conditions. Group B soils have moderate infiltration and runoff rates while group D have a low infiltration rate and a high runoff rate. The soils with dual group identifiers have been modeled with the more conservative of the two, in this case a D soils group. Most of the soil adjacent to Normanskill Street is within soil group A. Group A soils have a high infiltration rate.

Geotechnical studies have been undertaken to evaluate the subsurface conditions of the site. These investigations have been summarized in the following reports:

- Preliminary Geotechnical Evaluation and Interpretive Report, CME Associates, Inc., April 5, 2017
- Supplemental Geotechnical Report, Dente Group, July 20, 2017

Copies of these reports were included in the TOWN OF BETHLEHEM PLANNING BOARD, DRAFT GENERIC ENVIRONMENTAL IMPACT STATEMENT For ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY EXPANSION PROJECT, Appendix E.

Draft Geotechnical Engineering Report, Terracon, October 15, 2021

A copy of this reports is included in the TOWN OF BETHLEHEM PLANNING BOARD, SUPPLEMENTAL ENVIRONMENTAL IMPACT STATEMENT FOR ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY EXPANSION PROJECT.

Based on these previous investigations, the subsurface conditions of the Expansion site are generally characterized by historic fills of various depths overlying, in sequence with depth; river sediments, alluvial sands, glaciolacustrine silt/ clay, glacial till, and shale bedrock. The fill was noted at specific boring locations ranging from 6 to 23 feet below existing grade. The fill material is characterized as a random landfill deposit containing natural and solid waste deposits such as, but not limited to, foundry sand waste, sand, silt, coal ash, gravel, and organic matter. A predominant component of the fill was reported as coal ash.

Shale bedrock was found beneath the glacial till soils at select boring locations. The depth to rock ranged from approximately 61 feet below grade near the northwest portion of the site, to greater than 148 feet at the southeast portion of the site. The rock depths appear shallowest on the north and west sides of the site and increase to the east towards the Hudson River and in a south direction across the site. Based on the New York State Museum and Science Service's Geologic Map of New York: State Hudson-Mohawk Sheet, and the geotechnical rock core samples, the bedrock appears to be consistent with the Normans kill Shale Formation.

According to the geotechnical reports, shallow groundwater was observed at depths ranging from approximately 1.5 to 13.7 feet below existing grade. However, due to the subsurface conditions, the shallower observations could be representative of perched groundwater zones due to discontinuous impermeable layers. Shallow groundwater fluctuations should be expected to occur at this site depending on several factors such as rainfall, seasonal changes, prevailing climate, ambient weather conditions, and the tidal influences of the Hudson River.

Historically, the project site was composed of small islands and river channels subject to natural shifts due



to flows associated with the Hudson River and the former Island Creek, a side channel of the Hudson River. Island Creek historically flowed along the western side of the site through the current power line corridor and discharged to the Hudson River at the southern end of the site. Based on available mapping, sometime between 1936 and 1961, Island Creek channel was diverted at the north end of the site directly to the Hudson River, whereupon it was referred to solely as Normans Kill, the main tributary to this former channel. The site was subject to historic filling operations to create usable lands and a portion of the site was operated as a coal ash (fly ash) disposal site by Niagara Mohawk from approximately 1952 to 1970. As such, there are large areas of fly ash deposits on the site that must be considered during the design and construction of the site infrastructure and stormwater management facilities. Excavated fly ash material will need to be appropriately handled and properly disposed of.

Due to the presence of fly ash on the Expansion Site, in addition to a NYSDEC SPDES, a Site Management Plan (SMP) has been prepared in accordance with 6 NYCRR Part 375 and DER Technical Guidance for Site Investigation and Remediation and submitted to the NYSDEC, Division of Environmental Remediation and the NYSDOH. The SMP includes: a Health and Safety Plan (HASP), to inform and protect the contractor and their work force; a Community Air Monitoring Plan (CAMP), to monitor and protect the surrounding communities; and an Excavation Work Plan (EWP), to direct the activities of the contractor during construction. The EWP includes a detailed description of the work to be performed, the anticipated environmental conditions, and engineering controls to mitigate the movement of fly ash. The SMP pertains only to the Expansion Site portion of the project (see Appendix H of this report).

3.4 Soil Infiltration Test

Supplemental to the above noted geotechnical reports, additional subsurface investigation and infiltration testing was completed by Terracon on May 12, 13, and 18, 2022. Test pit locations were selected based on the potential for stormwater infiltration practices to be utilized. Test locations were along the shore of the Hudson River and Normans Kill as well as within the boundary of Infiltration Basin #1 and #2. The testing locations are shown on a map included in Appendix F of the Drainage Report (included as Appendix C to this report).

The subsurface investigation and infiltration testing concluded that locations IT-1, IT-1A, IT-7, IT-7A, IT-8, IT-10, IT-12, IT-12A, and IT-15 can provide an infiltration rate of 0.5 in/hr or greater. The remaining locations had test results below 0.5 in/hr which is not sufficient for infiltration chambers or infiltration basins. In addition to infiltration rate, a soil classification was also provided at the test depth. The soil classifications found were fill (coal ash with crushed stone and slag), sandy silt (ML), silt (ML), silt and clay (CL-ML), silt (ML), silt with sand (ML), silty sand (ML), silty clay (CL-ML), fill (sandy silt), and fill (coal ash). The entire subsurface investigation report including soil profiles is located in Appendix F of the Drainage Report (included as Appendix C to this report).

4. CONSTRUCTION PHASING

4.1 Sequence of Construction Activities

The Contractor's work schedule and methods shall be consistent with the SWPPP or amended SWPPP. Once approved, the progress schedule shall become a part of the SWPPP. It should be noted that there is a NYSDEC approved SMP for this site, which is included as Appendix H of this report. Any disturbance of the site must comply with the SMP.



The following list is a suggested sequence of major construction activities for the project to meet the NYSDEC Phase II erosion control requirements:

- 1. Conduct a pre-construction meeting with the MS4, Engineer, and Contractor to review the SWPPP.
- 2. Notify the NYSDEC within 14 days, and no less than 3 days, prior to commencing work activities that may affects areas of the subject site that are impacted with ash, as required by Section 3.2 of the SMP.
- 3. Clearly identify project work limits, identifying all areas where construction disturbance shall be permitted.
- 4. Install erosion control measures prior to commencing earthwork operations. Construct temporary earthen berms, diversion swales, sediment control dams and associated erosion control measures necessary to divert runoff from entering planned areas of disturbance and to protect the adjacent waterway.
- 5. All installed erosion and sediment control measures are to be inspected and certified as correctly installed by the owner's qualified inspector and Town of Bethlehem staff.
- 6. Establish temporary/permanent storm water management ponds/erosion control basins.
 - a. Consult the SMP for the appropriate measures to handle or dispose of any encountered contaminated soils.
- 7. Remove vegetation and dispose of off-site.
- 8. Strip and stockpile topsoil from proposed pavement, structural fill and cut areas (stockpile materials in locations as directed by owner's representative).
 - a. Consult the SMP for appropriate measures to handle or dispose of any encountered contaminated soils.
- 9. Establish mass earthwork subgrade elevations.
 - a. Consult the SMP the appropriate measures to handle or dispose of any encountered contaminated soils.
- 10. All temporary erosion and sediment control measures as well as stockpiles are to be mulched and seeded for temporary vegetative cover immediately following grading.
- 11. Import the aggregate fill material to serve as a surcharge for the proposed building and concrete pad areas.
- 12. After surcharging compaction is completed, places fabric and geogrid on the subgrade and spread the aggregate material in layers with additional geogrid as specified.
- 13. Construct utility lines (water/electric/gas/communications/sanitary sewers/storm sewers), construct building and install infrastructure improvements.
- 14. Box out roadway and pavement areas and install concrete curbing.
- 15. Construct asphalt pavement section, up to binder course.
- 16. Fine grade and spread topsoil, install landscaping plantings and hardscapes, site amenities and permanent seeding.
- 17. Town of Bethlehem (MS4) shall conduct a site inspection to determine (1) that the site has achieved 80% stabilization and (2) the installed stormwater facilities are operational.
- 18. Remove temporary erosion and sediment control features upon establishment of permanent ground cover and inspection/approval from a Town official or representative.
- 19. Notify owner's representative of completion of final site stabilization.
- 20. File Notice of Termination.



5. EROSION AND SEDIMENT CONSTROL MEASURES

5.1 Erosion Control Plan

An erosion control plan has been developed in accordance with the "New York Standards and Specifications for Erosion and Sediment Control". The erosion control plan employs permanent and temporary erosion and sediment control methods including silt fence, erosion control matting, construction entrances, and other appropriate measures. It should be noted that there is a NYSDEC approved SMP for the Expansion Site, which is included as Appendix H of this report. Any disturbance of this area must comply with the SMP. As stated in Section 3.2 of the SMP, NYSDEC must be notified within 14 days, and no less than 3 days, prior to commencing work activities that may affect areas of the subject site that are impacted with ash.

5.1.1 Temporary Surface Stabilization

All work and prior NYSDEC notification shall be in accordance with the SMP. Areas within the project limits that may be disturbed more than once during the construction activities will be stabilized using temporary seed and mulch item or as directed by the Engineer. Areas remaining unpaved and undisturbed for more than seven (7) days during construction operations shall be stabilized temporarily. Other areas that might need to be stabilized temporarily will be at the discretion of the Engineer.

5.1.2 Drainage Pipe Inlet / Outlet Stabilization

As part of the permanent erosion control measure, the inlet and outlet of the culvert pipes will be provided with either stone riprap apron or an apron consisting of erosion control product with vegetation to provide the required erosion control which blends in with the surrounding natural features and topography. The location and type of stabilization to be provided is shown on project plans.

5.1.3 De-watering

Any groundwater that is suspected of being contaminated shall be handled in accordance with Section 4.2 of the SMP. If required, de-watering of miscellaneous areas within the site will be performed utilizing a pump and filter bag system. The filter bags should be made of non-woven geotextile material capable of trapping particles larger than 150 microns. Filter bags should be replaced when they are half full or a no longer functioning per the manufacturer's requirements. Filter bags should be located in a well vegetated/grassy area and discharge into stable erosions resistant areas. Where this is not possible a geotextile flow path should be established. Bags shall not be placed on slopes greater than 5%. The pump discharge hose shall be inserted into the bags in the manner specified by the manufacturer and securely clamped. Pumping rate shall not be greater than 750 GPM or ½ the maximum specified by the manufacturer, whichever is less. Pump intakes shall be floated and screened.

5.1.4 Construction Entrance

As required, at least one (1) stabilized construction entrance will be constructed to access the Contractors Staging/Storage Area. This entrance/area shall conform to the details. Refer to the Erosion and Sediment Control (E&SC) Plans (included as Appendix B of this report) for location of construction entrance(s).

5.1.5 Concrete Truck Washout / Concrete Batch Plant Protection

As required, a temporary excavated or above ground lined pit where concrete truck mixers and equipment can be washed after their loads have been discharged, to prevent highly alkaline runoff from entering storm drainage systems or leaching into soil shall be constructed. See E&SC Plans (included Appendix B of



this report) for location of concrete washout. If a concrete batch plant is installed at the site, temporary containment to prevent discharge of runoff from entering storm drainage systems or leaching into soil shall be constructed.

5.1.6 Permanent Stabilization

Stabilization of the graded surfaces will be accomplished by using various seed mixtures for establishing permanent vegetation.

5.1.7 Dust Control

Dust shall be controlled and monitored in accordance with Section 4.3 of the SMP. The contractor will be required to minimize dust generation during the construction activities. Provisions such as applying water on haul roads, wetting equipment, and excavation faces, spraying water on buckets during excavation and dumping, hauling materials in properly tarped or watertight containers, restricting vehicle speeds to 10 mph, covering excavated areas and material after excavation activity ceases, and reducing the excavation size and/or number of excavations have proven effective in dust control.

5.1.8 Silt Fence

Silt fence will be placed per the E&SC Plans (Appendix B of this report), down slope of all disturbed areas, soil stockpiles, and spoil areas. Along the bank of the Normans Kill, two layers of silt fence are to be installed due to the proximity to the Mean Higher High Water (MHHW) level. The purpose of the silt fence is to remove sediment from sheet flow in these areas. Silt fence shall remain in place and functional until the contributing area has been permanently stabilized. Sediment socks or mulch dikes may be used in lieu of silt fence, where approved by the Engineer of Record. Erosion Control shall be in accordance with the SMP.

5.1.9 Temporary Sediment Basins

Temporary sediment basins have been designed to store sediment runoff from the Expansion Site. Basin #1 will be converted into a permanent stormwater quality pond. All basins have been designed in accordance with Section 5 of the NYS Standards and Specifications for Erosion and Sediment Control (Blue Book). Calculations for the basins are included as Appendix I to this report. Locations and a detail of the basins are included in the E&SC Plans (Appendix B of this report).

5.1.10 Weekly Inspections

A qualified inspector shall conduct site inspections at least once every seven (7) calendar days. After a 5-acre waiver is granted; site inspections shall occur at least twice every seven (7) calendar days while there are more than 5 acres of soil disturbance. The qualified inspector shall inspect all erosion and sediment control practices and pollution prevention measures to ensure integrity and effectiveness; all post-construction stormwater management practices under construction to ensure that they are constructed in conformance with the SWPPP; all areas of disturbance that have not achieved final stabilization, all points of discharge to natural surface waterbodies located within, or immediately adjacent to, the property boundaries of the construction site; and all points of discharge from the construction site. The qualified construction inspector shall also prepare an inspection report after every inspection. Complete inspection and maintenance requirements can be found in Part IV of the SPDES General Permit GP-0-20-001 (included as Appendix E of this report). Inspection reports shall be submitted to the Town's Stormwater Program Manager.



5.1.11 Final Inspection

Prior to the project being finally accepted, it shall be inspected for any evidence of erosion or slope failure. If any such condition becomes apparent upon final inspection, temporary soil erosion and sediment controls shall be installed immediately as directed by the Engineer. The situation shall be corrected per a schedule agreed to by the MS4 (Town of Bethlehem).

5.1.12 Wharf E&SC

Erosion and sediment control measures associated with the construction of the wharf and dredging of the Hudson River are to be designed and approved prior to disturbance below the Mean High High Water (MHHW) elevation. These E&SC measures are being designed in conjunction with the NYSDEC, USACE and other State agencies through a separate permitting process. All additional permits required for the wharf and dredging will also be in place prior to disturbance below the MHHW. Draft conceptual E&SC Plans associated with the wharf construction and dredging are included in Appendix G of this report.

5.2 Permanent Erosion and Sediment Control Measures

ruble 3 – List of Permanent Erosion & Sealment Control Measures				
Permanent Feature	Converted	Location: ESC Plan	Receiving Waterbody Protected	
	Temporary		(where applicable)	
	Practice?			
Riprap outlet protection	Yes	See Plans	Hudson River, Normans Kill	
Soil Stabilization	Yes	See Plans	Hudson River, Normans Kill	
Check Dam	Yes	See Plans	N/A	
Diversion Dike	Yes	See Plans	N/A	

Table 3 - List of Permanent Erosion & Sediment Control Measures

5.3 Installation Sequence

See the intended sequence of construction activities noted in Section 4 above.

5.4 Maintenance Schedule

The Contractor is required to inspect all E&SC devices in their active work area daily and after each rain event; and repair any deficiencies in accordance with the SPDES permit.

5.5 SWPPP Implementation Responsibilities

Implementation of all E&SC devices will be by the Contractor as indicated in the contract documents.

6. POLLUTION PREVENTION MEASURES

6.1 Material Management Practices

All waste materials, including construction debris and trash that occur onsite shall be handled and disposed of in a lawful manner that is in accordance with state and local regulations. No waste material shall be buried on site.

- An effort will be made to store only enough products required for the project.
- All materials stored within the site will be stored in a neat orderly manner in their appropriate containers and if possible, an enclosed area.
- o Products shall be kept in their original containers with the original manufacturer's labels.



Manufacturer's recommendations for proper use and disposal shall be followed.

- Hazardous materials shall be disposed of in a lawful manner and in accordance with State and Local regulations.
- Sanitary waste will be collected from portable units as required and shall be disposed of in a lawful manner.

The following materials are expected to be on-site during construction:

- o Concrete
- o Asphalt
- o Paints (Enamel and Latex)
- o Petroleum based products
- o Fertilizers
- Metal building components
- o Detergents
- o Cleaning Solvents
- o Roofing Materials
- o Tar

These materials and other materials used during construction with the potential to impact stormwater will be stored, managed, used, and disposed of in a lawful manner that minimizes the potential for releases to the environment and especially into stormwater.

Emergency contacts for the project will be posted at the project office and are included at the end of this section.

6.2 Spill Control Practices

The contractor will be responsible for preparing a project area specific spill control plan in accordance with Local and NYSDEC regulations. At a minimum, this plan shall:

- 1. Stop the source of the spill.
- 2. Contain the spill.
- 3. Reduce stormwater contact if there is a spill.
- 4. Dispose of contaminated material in lawful manner and in accordance with manufacturer's procedures and NYSDEC regulations.
- 5. Identify responsible trained personnel.
- 6. Ensure spill area is well ventilated.

For any work within National Grid property, the National Grid Environmental Guidance EG 501 regarding reporting of a release of oil, chemical or hazardous material must be followed. National Grid EG 501 has been included as Appendix M of this document.

6.3 General Material Handling Practices

The following general practices will be used throughout the project to reduce the potential for spills:

Potential pollutants will be stored and used in a manner consistent with the manufacturer's
instructions in a secure location. To the extent practicable, material storage areas should not be
located near storm drain inlets and should be equipped with covers, roofs, or secondary
containment as needed to prevent stormwater from contacting stored materials. Potential
pollutants should not be stored within 100 feet of a water course or wetland. Chemicals that are



not compatible shall be stored in segregated areas so that spilled materials cannot combine and react.

- 2. Materials disposal will be in accordance with manufacturer's instructions and applicable local state and federal regulations.
- 3. Materials no longer required for construction will be removed from the site as soon as practicable.
- 4. Adequate garbage, construction waste, and sanitary waste handling and disposal facilities will be provided/utilized to the extent necessary to keep the site clear of obstruction and Best Management Practices (BMPs) clear and functional.

6.4 Product Specific Practices

The following product specific practices will be followed within the project area.

6.4.1 Petroleum Products

All project related vehicles shall be monitored for leaks and receive regular preventative maintenance to reduce the potential of leakage. Petroleum products shall be stored in tightly sealed containers, which are clearly labeled. Any asphalt substances used during construction shall be applied according to manufacturer's recommendations.

6.4.2 Fertilizers

Fertilizers used shall be applied only in the minimum amounts recommended by the manufacturer. Once applied, fertilizer shall be worked into the soil to limit exposure to stormwater. Fertilizers shall be stored in covered or other contained areas.

6.4.3 *Paints*

All containers shall be tightly sealed and stored when not required for use. Excess paint shall not be discharged into the storm sewer system but shall be disposed of according to manufacturer's instructions or State regulations.

6.4.4 Concrete Trucks

Concrete Trucks shall be allowed to wash out within project areas that the contractor provides an area which collects and contains any concrete / slurry material washed from trucks for recovery and disposal at a later time. No concrete or slurry shall be discharged from the property at any time of construction. The concrete washout area shall conform to the detail found on sheet ESC-06 (Appendix B of this report).

6.5 Spill Response

The primary objective in responding to a spill is to quickly contain the material(s) and prevent or minimize their migration into stormwater runoff or conveyance systems. If the release has impacted on-site stormwater, it is critical to contain the released material on-site and prevent their release into receiving waters.

If a spill of pollutants threatens stormwater on-site, the spill response procedures outline below must be implemented in a timely manner to prevent release of the pollutant:

- 1. The site superintendent will be notified immediately when a spill or the threat of a spill is observed. The superintendent will assess the situation and determine the appropriate response.
- If spills represent an imminent threat of escaping E&SC facilities and entering the receiving waters, facility personnel will respond immediately to contain the release and notify the superintendent after the situation has been stabilized.
- 3. Spill kits containing materials and equipment for spill response and clean-up will be maintained



onsite. Each spill kit may contain:

- Oil absorbent pads (one bale)
- Oil absorbent booms (40 feet)
- o 55-gallon drums (2)
- o 9-mil plastic bags (10)
- Personal protective equipment including gloves and goggles
- 4. If an oil sheen is observed on surface water, absorbent pads and/or booms will be applied to contain and remove the oil. The source of the oil sheen will also be identified and removed or repaired as necessary to prevent further releases.
- 5. The site superintendent, or their designee, will be responsible for completing a spill reporting form to the appropriate state or local agency.
- 6. Spill response equipment will be inspected and maintained as necessary to replace any materials used in spill response activities.

6.6 Notification

In the event of a spill, make the appropriate notification(s) consistent with the following procedures:

- 1. Any spill of oil which a) violates water quality standards, b) produces a sheen on a surface water, c) causes a sludge or emulsion must be reported immediately by telephone to the National Response Center Hotline at (800) 424-8802.
- Any oil, hazardous substance, or hazardous waste release which exceeds the reportable quantity
 must be reported immediately by telephone to the National Response Center Hotline at (800)
 424-8802.
- 3. Any spill of oil or hazardous substance to waters of the state must be reported immediately by telephone to the NYSDEC.
- 4. Any release of hazardous substance that may be a threat to human health or the environment must be reported to the NYSDEC immediately upon discovery.

7. EXISTING SITE CONDITIONS

The existing site is Beacon Island, located in the Town of Bethlehem, Albany County, New York. The site is currently vacant and consists primarily of brush and trees with a small gravel area as well as abandoned railroad tracks.

7.1 Existing Watershed Information

The project area is in close proximity and includes shorelines to both the Hudson River and Normans Kill, which are the receiving waterbodies for runoff from the current site.

The existing drainage condition is split up into seven (7) drainage areas. Drainage area DR-A drains to analysis point #1A, drainage areas DR-B and DR-F drain to analysis point #1, drainage areas DR-D and DR-E drain to analysis point #2. Drainage area DR-G drains to analysis point #3. Drainage area DR-C drains to a self-contained depression for storage. See Appendix A of the Drainage Design Report (included as Appendix C of this report) for the Pre-Development Site Drainage Areas Map.

Runoff from DR-A travels via sheet and shallow concentrated flow directly to a wetland located in the northwest corner of the site (Wetland 1). During large storm events the wetland overflows into an existing 40" pipe with direct outlet to the Normans Kill. Analysis of the existing capacity of the outlet pipe is



provided in section IV of the Drainage Design Report (included as Appendix C of this report). Runoff from areas DR-B, DR-D, DR-E, and DR-F travel via sheet and concentrated flow to low areas with eventual outfall directly to the Normans Kill and Hudson River. An approximately 30-acre internal portion of the site (DR-C) was determined to be self-contained within the site capable of storing and infiltrating the 100-year storm event. Runoff from area DR-G sheet flows to the west side of River Road and travels to a low spot adjacent to the roadway where it is stored and eventually infiltrated.

The existing site falls within the Normans Kill watershed of the Middle Hudson Sub-Basin for the Lower Hudson River Basin (HUC10: 0202000602, Water Index No H-221-4) which is listed as a Class C water. Neither the Normans Kill nor the Hudson River are listed in the Manual's Appendix C as a watershed where enhanced phosphorus removal standards are required. Additionally, neither are listed in the Manual's Appendix E as a watershed impaired by pollutants related to construction activity.

7.2 Table of Receiving Waterbodies

Table 4: Receiving Waterbodies

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Stormwater Structure	Receiving Waterbody	NYSDEC Regulated
None	Hudson River	Yes – Class C
40" Outlet Pipe	Normans Kill	Yes – Class C

8. STORMWATER MANAGEMENT ASSESSMENT

8.1 Methodology

To analyze the hydrologic impacts of the proposed development, a storm water management model was developed in accordance with the Manual. HydroCAD™, by HydroCAD Software Solutions LLC was used to model both the existing and proposed conditions: soil data from the NRCS Web Soil Survey was entered into the software; land coverage areas were estimated using aerial photography and site visits; watershed areas were developed using the surveyed topography; time of concentrations were estimated using USDA, Urban Hydrology for Small Watersheds, TR-55 (TR-55) methodology; and finally runoff and routing calculations were performed using the SCS Unit Hydrograph method.

Green Infrastructure practices were designed in accordance with the Manual using the NYSDEC Runoff Reduction Worksheets available through the NYSDEC's Construction Stormwater Toolbox, available on their website.

The following general steps are followed when conducting a stormwater design:

- 1. **Site Planning:** The existing natural resource areas and drainage patterns including wetlands, waterways, floodplains, and soils are identified. Conservation of natural resources are maximized given the proposed site.
- Pre and Post-Development Conditions Analysis: The pre and post-development stormwater runoff conditions for the 1, 10, and 100-year storm events are determined using HydroCAD (detailed HydroCAD reports for this project can be found in Appendix A and B or the Drainage Design Report, provided in Appendix C of this report).
- 3. **Water Quality:** The Water Quality Volume and Runoff Reduction Volume are calculated using Chapter 4 of the Manual and Green Infrastructure Worksheets (see Appendix C of the Drainage Design Report, provided in Appendix C of this report).



4. Water Quantity: Peak runoff and stormwater retention/detention are evaluated using the Manual.

8.1.1 Water Quality Volume (WQv) / Runoff Reduction Volume (RRv)

Section 4.2 of the Manual states that Water Quality Volume (WQv) is intended to improve the water quality by capturing and treating runoff from small, frequent storm events that contain higher pollutant levels created through the increase of impervious surfaces. Impervious surfaces accumulate pollutants that quickly wash off and rapidly enter downstream waters as well as prevent natural groundwater recharge.

The WQv required for the proposed site is based upon the 90% rainfall event number, percent of impervious cover, and the total site area. Calculations were done using the Green Infrastructure worksheets and can be found in Appendix C of the Drainage Report (included as Appendix C of this report). The total WQv required is 273,874 cubic feet.

Runoff Reduction Volume (RRv) is the reduction of the total WQv by application of green infrastructure techniques and stormwater management practices to replicate pre-development hydrology more closely. The intent of RRv is to recognize the water quality benefits of certain site design practices to address flow as a pollutant of concern. Calculations were done using the Green Infrastructure worksheets and can be found in Appendix C of the Drainage Report (included as Appendix C of this report). The minimum RRv was determined to be 57,313 cubic feet.

Due to the level of contamination present in the existing soils across the Expansion Site, stormwater infiltration practices were located only in areas along the Hudson River and Normans Kill where contamination is not expected to be present. However, the Normanskill Street project area does not contain contaminated soils, so all treatment practices selected in this area utilize infiltration and therefore include RRv.

The total Water Quality Volume and Runoff Reduction Volume requirements are met for this project.

8.1.2 Channel Protection Volume (CPv)

Stream Channel Protection Volume Requirements (CPv) are designed to protect stream channels from erosion. The Manual was used to determine the water quantity requirements of CPv; specifically, providing 24-hour extended detention for the 1-year storm event or discharging directly to tidal waters.

According to Section 4.4 of the Manual, the Stream Channel Protection Volume (CPV) requirement does not apply when the site discharges to a tidal waterbody.

The CPv requirement does not apply in certain conditions, including the following:

- Reduction of the entire CPv volume is achieved at a site through green infrastructure or infiltration systems.
- The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, 24-hour extended detention of the 1-year storm event is not required for drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and



analyzed as Analysis Point #1A. Hydrologic analysis for the 1-year storm event from existing to proposed is provided in Appendix A and B of the Drainage Report (included as Appendix C of this report) and summarized in Table 8.

8.1.3 Overbank Flood Control (Qp)

The primary purpose of the overbank flood control sizing criterion is to prevent an increase in the frequency and magnitude of out-of-bank flooding generated by urban development. The Manual was used to determine the water quantity requirements of Qp; specifically, providing sufficient retention volume to discharge all runoff from the proposed 10-year storm event at a rate equal to or less than the existing peak 10-year runoff rate or discharging directly to tidal waters.

According to Section 4.5 of the Manual, the Overbank Flood Control Criteria (Qp) requirement does not apply when the site discharges to a tidal waterbody.

The overbank flood control requirement (Qp) does not apply in certain conditions, including:

• The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, 24-hour extended detention of the 10-year storm event is not required for drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and analyzed as Analysis Point #1A. Hydrologic analysis for the 10-year storm event from existing to proposed is provided in Appendix A and B of the Drainage Report (included as Appendix C of this report) and summarized in Table 8.

8.1.4 Extreme Flood Control (Qf)

The intent of the extreme flood criteria is to prevent the increased risk of flood damage from large storm events, maintain the boundaries of the predevelopment 100-year floodplain, and protect the physical integrity of stormwater management practices. The Manual was used to determine the water quantity requirements of Qf; specifically, providing sufficient retention volume to discharge all runoff from the proposed 100-year storm event at a rate equal to or less than the existing peak 100-year runoff rate or discharging directly to tidal waters.

According to Section 4.6 of the Manual, the Extreme Flood Control Criteria (Qf) requirement does not apply when the site discharges to a tidal waterbody.

The 100-year storm control requirement can be waived if:

 The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, 24-hour extended detention of the 100-year storm event is not required for drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and



analyzed as Analysis Point #1A. Hydrologic analysis for the 100-year storm event from existing to proposed is provided in Appendix A and B of the Drainage Report (included as Appendix C of this report) and summarized in Table 8.

8.2 Evaluation of Green Infrastructure

According to Section 4.3 of the Manual, meeting the RRv (through green infrastructure) may not be feasible due to limitations that prevent the use of an infiltration technique and/or infiltration of the total WQv. The Beacon Island portion of the project site does not allow for the infiltration of any stormwater runoff due to the presence of fly ash across the site. However, green infrastructure practices were evaluated for potential use.

8.2.1 Conservation of Natural Areas

The existing vegetation located along the bank of the Hudson River is conserved in a deed restricted area in the proposed plan. Credit has been applied.

8.2.2 Sheetflow to Riparian Buffers and Filter Strips

Riparian Buffers and Filter Strips were not utilized, due to the lack of space on the Port Authority owned land.

8.2.3 Vegetated Swales

The developed site contains vegetated swales where there is sufficient room. Due to the SMP not recommending infiltration within the Expansion Site, no credit has been applied.

8.2.4 Tree Planting / Tree Pits

New landscaping will complement the existing environment and provide aesthetics for the buildings and parking areas. No credit has been applied for proposed tree plantings.

8.2.5 Disconnection of Rooftop Runoff

Rooftop disconnection was not considered for this project, as the buildings will have large, sloped roofs in a single direction and would have to discharge to the compacted gravel areas that would potentially cause erosion and instability of the dense graded aggregate due to over saturation; as well as encourage infiltration into the fly ash sub-surface layer which is not recommended by the SMP.

8.2.6 Stream Daylighting

Stream daylighting is not available for the proposed project.

8.2.7 Bioretention

The developed site does not have sufficient area to accommodate Bioretention. The proposed stormwater treatment ponds designed for this site are located either partially or fully on the adjacent National Grid property. As required by National Grid, the treatment on their property must hold at least the 10-year storm. There is not adequate space to use bioretention systems instead of stormwater ponds in these locations given the quantity of water required to retain. This practice promotes infiltration into the fly ash sub-surface layer which is not recommended by the SMP.

8.2.8 Green Roofs

Green roofs were not considered to be feasible as pre-engineered metal buildings are proposed for this project.



8.2.9 Stormwater Planter

Stormwater Planters were not considered due to the poor soils, excessive rooftop runoff volume, and would promote infiltration into the fly ash sub-surface layer which is not recommended by the SMP.

8.2.10 Rain Barrels and Cisterns

The developed site does not have sufficient area for Rain Barrels or Cisterns to accommodate the storage of the roof runoff volume.

8.2.11 Porous Pavement

Porous pavement was not considered due to the large loads associated with the Tower sections being moved and stored on site that would cause the porous pavement surface to crumble. This practice also promotes infiltration, which is not recommended by the SMP.

8.2.12 Infiltration System

Two infiltration basins were designed to treat runoff from a portion of the Normanskill Street Improvements. Two dry swales were designed to treat runoff from the Offsite and a portion of the Normanskill Street Improvements. Three infiltration chamber systems were designed to provide runoff reduction along the Hudson River and Normans Kill.

POST CONSTRUCTION STORMWATER CONTROL PRACTICES

9.1 Table of Post Construction Practices

See Table 5 below.

9.2 Post Construction Practices Plan

Locations of Post Construction Practices are found in the Erosion & Sediment Control Plans and Details (included as Appendix B of this report).

To best mitigate the water quality requirements of the proposed site, two (2) stormwater quality ponds, six (6) manufactured stormwater filtering systems, three (3) infiltration chamber systems, two (2) infiltration basins, and two (2) dry swales were designed. All practices were designed in accordance with the Manual. Each practice was sized to provide WQv; however, they do not all provide storm event flow mitigation (see sections 8.1.2 through 8.1.4 above).

Drainage Areas DR-1 through DR-7 will provide WQv using manufactured water quality systems. Drainage Areas DR-8 and DR-9 will drain to stormwater ponds providing WQv. The total of all practices providing water quality volume is 211,395 cubic feet (cf). A full description of the designed stormwater treatment practices is provided in Section III.B of the Drainage Design Report (included as Appendix C of this report). The WQv is summarized in Table 5 below:



Table 5 – Water Quality Volume Practice Summary

Drainage Area	Stormwater Practice	WQv (cf)
DR-1	Filter Type 2	18,005
DK-1	Infiltration Chamber	2,802
DR-2	Filter Type 1	21,971
DR-3	Filter Type 1	43,939
DD 4	Filter Type 3	14,989
DR-4	Infiltration Chamber	2,052
DR-5	Infiltration Chamber	2,047
DR-6	Filter Type 1	48,060
DR-7	Filter Type 2	34,826
DR-8	Stormwater Pond #1	8,437
DR-9	Stormwater Pond #2	13,361
DR-14	Infiltration Basin #2	141
DR-15	Dry Swale #1	129
DR-17	Dry Swale #2	636
	Total WQv	211,395

Due to the presence of fly ash across the Expansion Site, infiltration practices were located in areas not expected to be contaminated. However, the Normanskill Street and Offsite Improvement portions of this project are in an area of uncontaminated soil with high infiltration rates. Therefore, all treatment practices selected infiltrate into the ground and provide RRv. The total RRv provided is 63,333 CF. The RRv is summarized in Table 6 below:

Table 6 – Runoff Reduction Practice Summary

Drainage Area	Stormwater Practice	RRv (cf)
DR-1	Infiltration Chamber	21,248
DR-4	Infiltration Chamber	18,464
DR-5	Infiltration Chamber	18,426
DR-11	Conservation of Natural Areas	868
DR-13	Infiltration Basin #1	1,995
DR-14	Infiltration Basin #2	2,245
DR-15	Dry Swale #1	87
	Total RRv	63,333

Drainage Areas DR-10, DR-11, DR-12, and DR-16 are to remain as naturally vegetated and therefore do not require water quality treatment.

However, Drainage Area DR-11 will be deed restricted to ensure the perpetual protection of the proposed area. Therefore, this area qualifies under the "Conservation of Natural Areas" volume reduction practice shown in the chart above.

9.3 Hydraulic Analysis of Pre- and Post-Development Conditions

The site was analyzed in both the pre- and post-construction stormwater conditions. Water quantity controls were required for drainage areas contributing to analysis point #1A as it is a Wetland. Using Chapter 4 of the Manual for new development, the project meets the total water quality volume required. Table 7 below summarizes the impervious cover of the pre- and post-development conditions.

Table 7 – Impervious Cover

	Pre-Development	Post-Development
Impervious Area	5.16 ac	65.9 ac
% Impervious Cover	7.1%	90.6%

The existing site has no water quality treatment measures. A portion of all stormwater not stored within the site is directly discharged into the Hudson River and Normans Kill. Per Chapter 4 of the Manual, new development projects are required to provide water quality treatment. As shown below, the project can meet the total water quality volume required. The peak discharge for all storm events draining to Analysis Point #1A is decreased in the post-development condition. The post-development peak discharge rates for the 1-year, 10-year and 100-year storm events exceed the pre-development peak discharge rates for the remaining analysis points; however, as described in Section 8.1 above, this requirement is waived when discharging directly to tidal waters. A summary of the peak discharge and stormwater management plan is shown in Table 8 below.

Table 8 – Peak Discharge and Stormwater Management Plan Summary

Storm Event	Pre-Development	Post-Development
Analysis Point #1A (Wetland #1)		
1-yr Discharge	27.32 cfs	4.77 cfs
10-yr Discharge	73.24 cfs	12.46 cfs
100-yr Discharge	163.60 cfs	30.97 cfs
Ana	alysis Point #1	
1-yr Discharge	3.25 cfs	58.54 cfs
10-yr Discharge	14.96 cfs	124.96 cfs
100-yr Discharge	43.20 cfs	205.59 cfs
Ana	alysis Point #2	
1-yr Discharge	7.17 cfs	82.79 cfs
10-yr Discharge	20.65 cfs	166.00 cfs
100-yr Discharge	48.06 cfs	290.19 cfs
Analysis Point #3		
1-yr Discharge	0.60 cfs	1.20 cfs
10-yr Discharge	1.84 cfs	2.62 cfs
100-yr Discharge	4.39 cfs	5.25 cfs
Total Area of Soil Disturbance	72.7 acres	
WQv Target	273,874 cf	
WQv Provided	274,728 cf	
RRv Target	57,313 cf	
RRv Provided	63,33	33 cf

Analysis Point #1A analyzes the peak discharge at Wetland #1. In larger storm events, stormwater quality ponds #1 and #2 will provide a "first flush" treatment for up to a 10-year storm event with stabilized emergency spillways to direct flow to the surrounding area for storms greater than the 10-year event. Due to the topography of the surrounding undisturbed area, water will flow toward Wetland #1. In the post-development condition, Analysis Point #1A has a peak discharge less than the pre-development condition during all storm events, therefore the required water quantity controls are met.

In the post-development condition, Analysis Point #1 has a total drainage area of 0.12 square miles (75.28 acres). This point drains to the Normans Kill with a drainage area of 162 square miles (103,680 acres). The project area makes up approximately 0.07% of the total drainage area of the Normans Kill. With an overall project time of concentration of around 10 minutes, the proposed project will have a negligible impact on the total Normans Kill hydrology as the site-produced runoff will be conveyed prior to the Normans Kill peak and will not impact the overall flood conditions of the Normans Kill.

In the post-development condition, Analysis Point #2 has a total drainage area of 0.04 square miles (23.6 acres). This point drains to the Hudson River with a drainage area of 8,090 square miles (5,177,600 acres). The project area makes up approximately 0.0005% of the total drainage area of the Hudson. With an overall project time of concentration of around 10 minutes, the proposed project will have a negligible impact on the total Hudson River hydrology, as the site-produced runoff will be conveyed prior to the Hudson River peak and will not impact the overall flood conditions of the Hudson River.

At Analysis Point #3, the post-development discharge rates are higher than the pre-development condition. However, analysis point #3 drains to the surrounding area which stores runoff to be gradually infiltrated. Runoff from this analysis point does not flow to a stream or wetland.

9.4 Deviation from NYS Stormwater Management Design Manual

The proposed stormwater management design deviates from The Manual by utilizing manufactured stormwater filtering systems for new development.

The need for alternative stormwater management practices is rooted in the extremely limited space available as well as the current site conditions. The proposed Offshore Wind Manufacturing Facility requires 85 acres of usable manufacturing and storage space along the Hudson River. It also requires close proximity to an existing port. Such requirements narrow the available project locations to a select few plots of unoccupied land in the entire state and this site was selected through a solicitation process by the state for off-shore wind development. This site was chosen given it is located adjacent to the existing Port of Albany and is directly on the Hudson River. However, the usable portion of the site adjacent to the Hudson River, is only 66-acres. Therefore, the entirety of the site is needed for the OSW manufacturing process, with an ancillary receiving site located at 700 Smith Boulevard.

The Expansion Site also extends onto the adjacent National Grid property from which APDC is leasing approximately 4.4 acres. However, National Grid has prohibited the installation of permanent stormwater infiltration practices within their property.

In addition to space limitations, the existing soils conditions prevent infiltration from being utilized as a stormwater management practice over most of the site. The existing soils are classified as Hydrologic Group D and B/D which provide little to no infiltration and are underlaid by fly ash. Infiltration practices were utilized in the areas where greater than 0.5 in/hr infiltration rates were achieved.



To adequately satisfy the WQv requirements of the Manual, manufactured systems are needed. The Contech Jellyfish units designed meet both the performance and sizing requirements of Chapter 4 of the Manual. The units are also certified by Washington State Department of Ecology (TAPE) and the Maryland Department of the Environment, adequate sources accepted by the NYSDEC. Specifications and details for the proposed units are provided in Appendix D of the Design Report (included as Appendix C of this report).

9.5 Maintenance Schedule of Post-Construction Stormwater Control Practices

See Appendix D of this report for the maintenance inspection checklists and requirement for the facilities to be maintained as summarized below in Table 9.

Table 9 – Maintenance Schedule of Post-Construction Stormwater Management Facilities

Maintained By	Name of Entity
Name, Address, Phone of Responsible Party	Albany Port District Commission 106 Smith Boulevard Albany, NY 12202 (518) 463-8763
Facilities to be Maintained	Jellyfish Filter (9 units at 6 locations) Infiltration Chamber (3 systems) Stormwater Quality Ponds (2) Infiltration Basins (2) Dry Swales (2) Stormwater Collection & Conveyance Systems
Description of Maintenance Activity for each Facility and Frequency	See Appendix D for maintenance guidelines, as recommended by the manufacturer and NYSDEC.
Description of Applicable Easements	N/A
Access and Safety Issues	Maintenance forces have access to all drainage facilities within the site.
Local and Non-Local Permits	Joint Permit Application
Legal Agreements	N/A

9.6 Drainage Structure Catchment Areas

See Appendix C of the Drainage Design Report (included as Appendix C of this report).

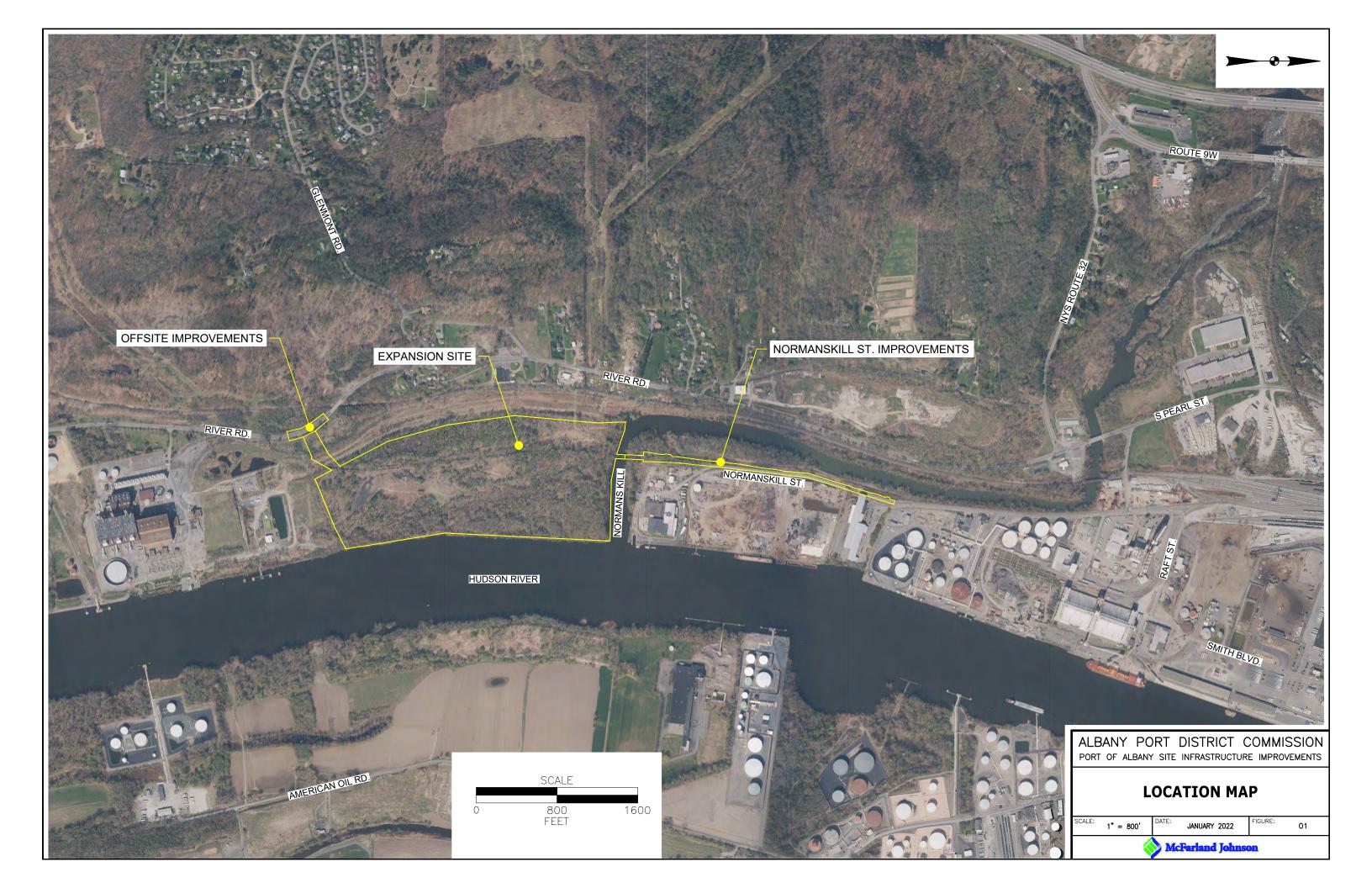
9.7 Hydraulic Analysis of Stormwater Sewer System

All elements of the closed drainage system have been designed to be non-erosive during a 2-year storm event and capable of conveying a 10-year storm event. The profiles were created in AutoCAD Civil 3D which incorporates the rational method and Manning's Equation to iteratively calculate the hydraulic capacity, grade lines, and inlet spreads. Printouts of the closed drainage system analysis are in Appendix C of the Drainage Design Report (included as Appendix C of this report).



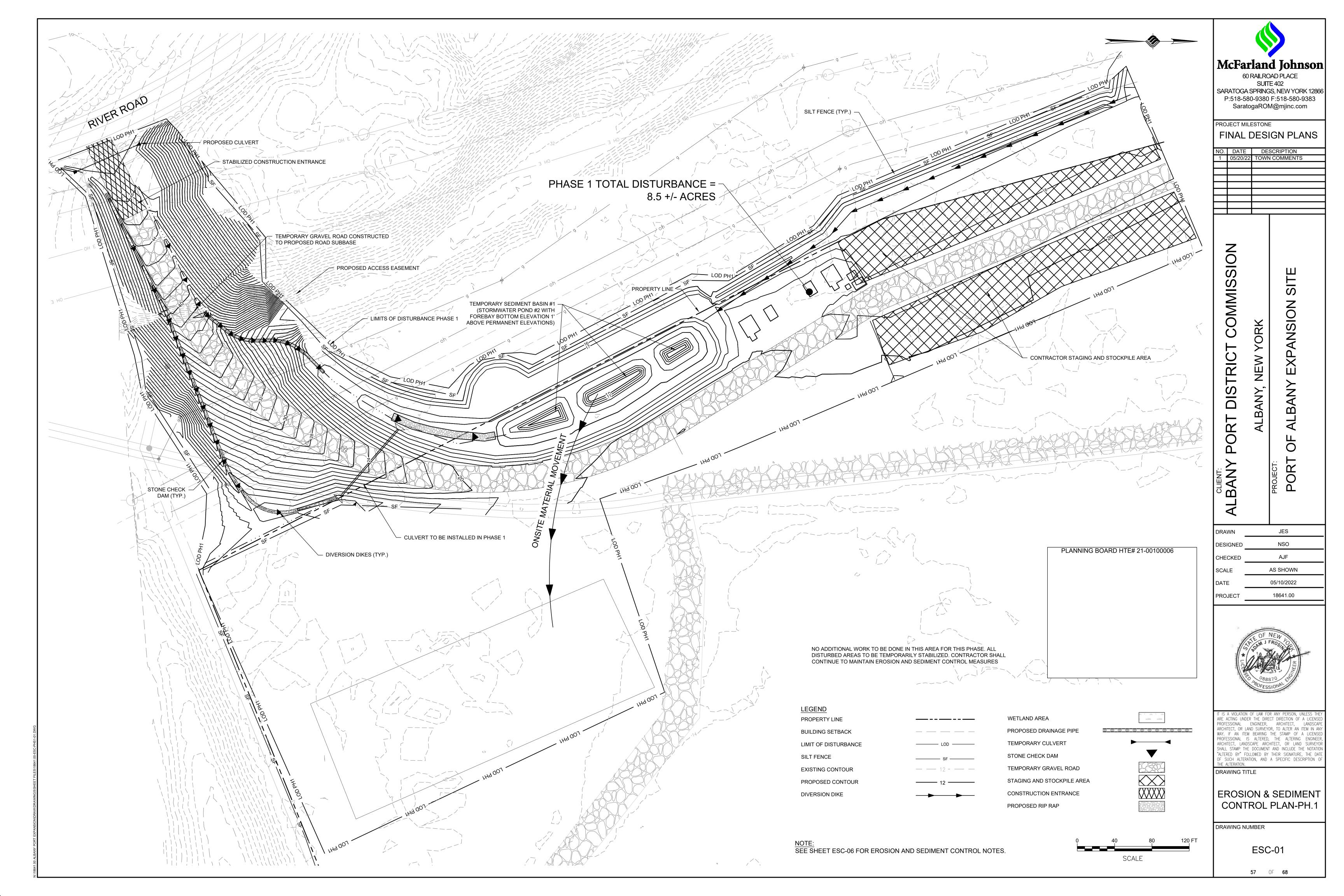
APPENDIX A

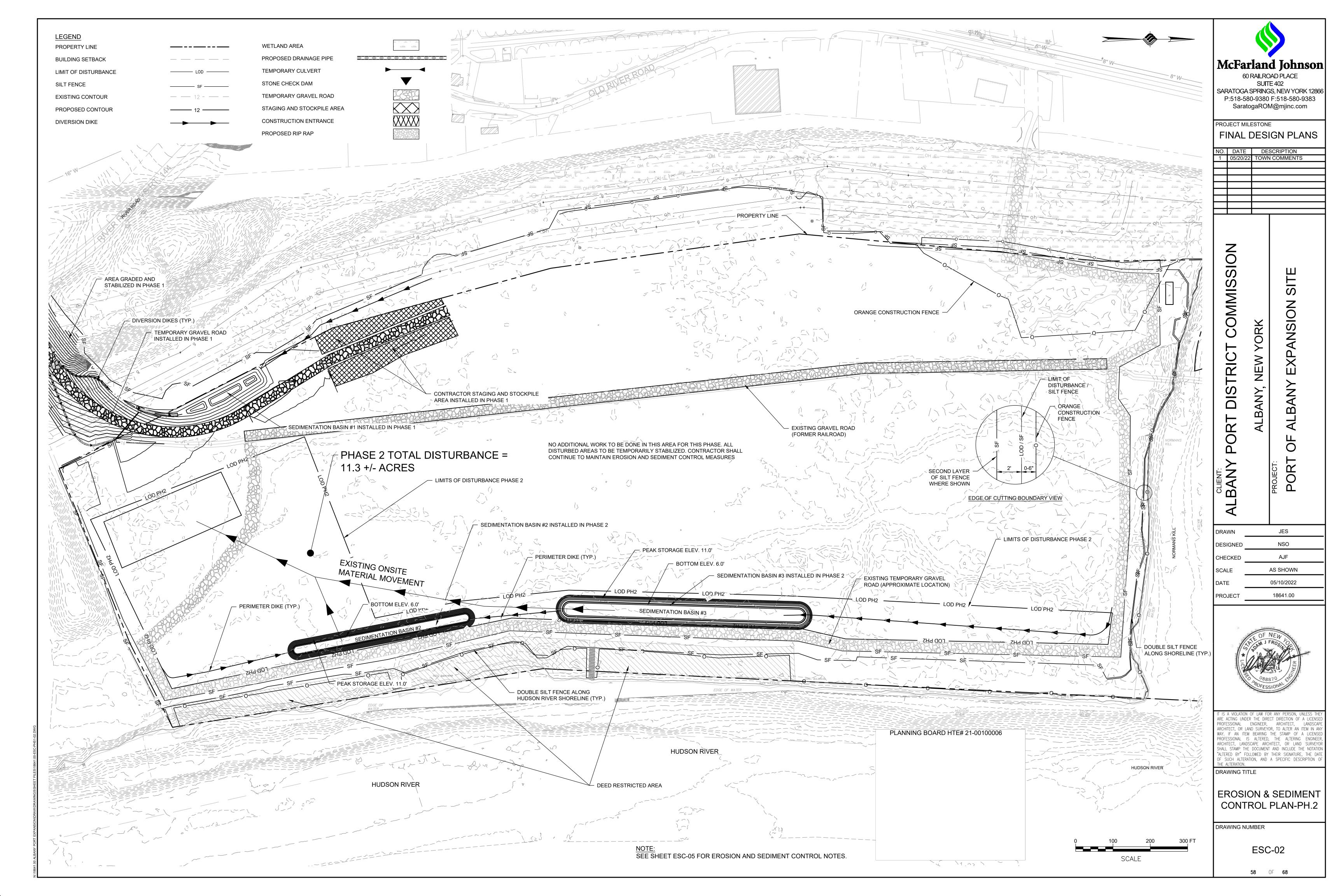
LOCATION MAP

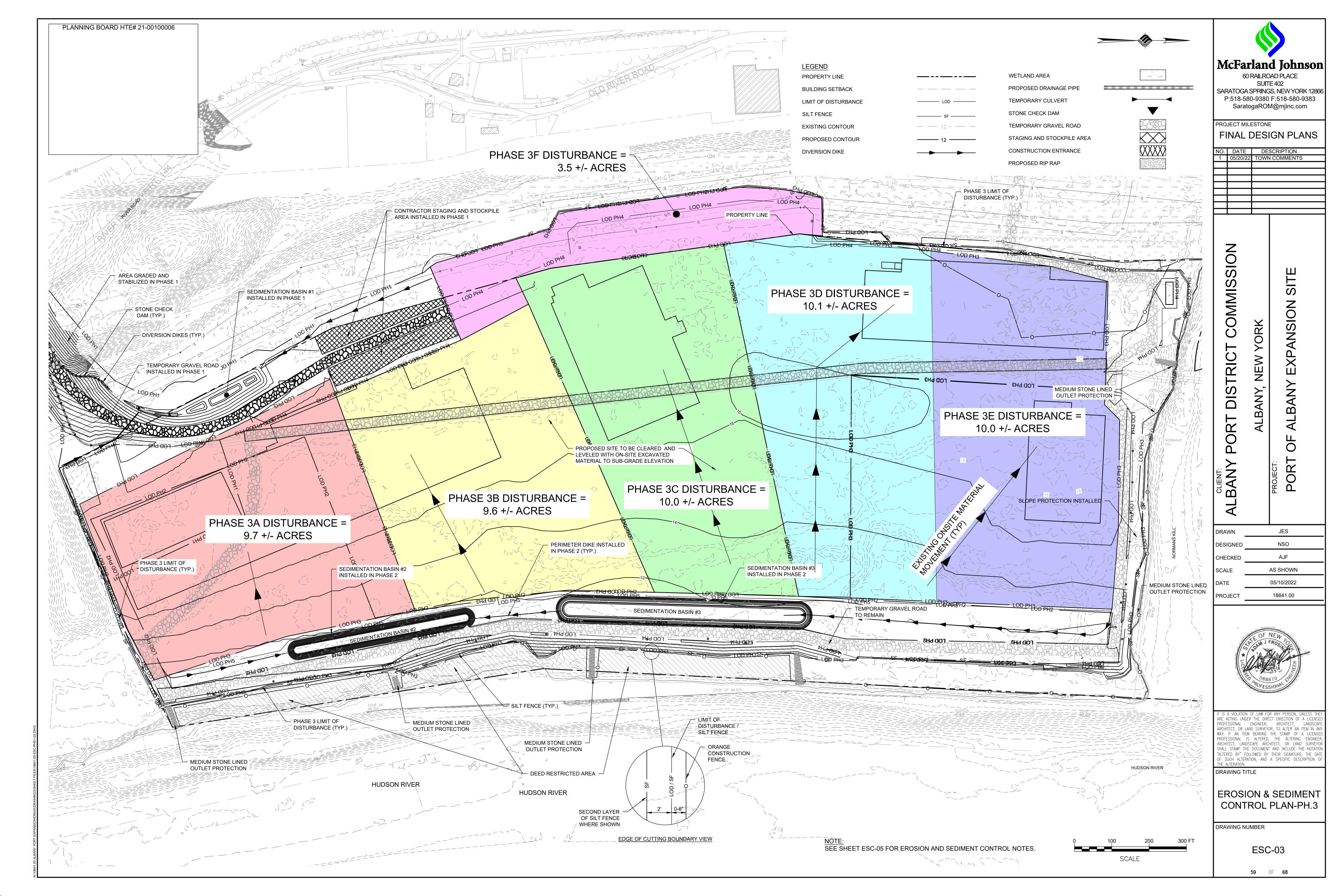


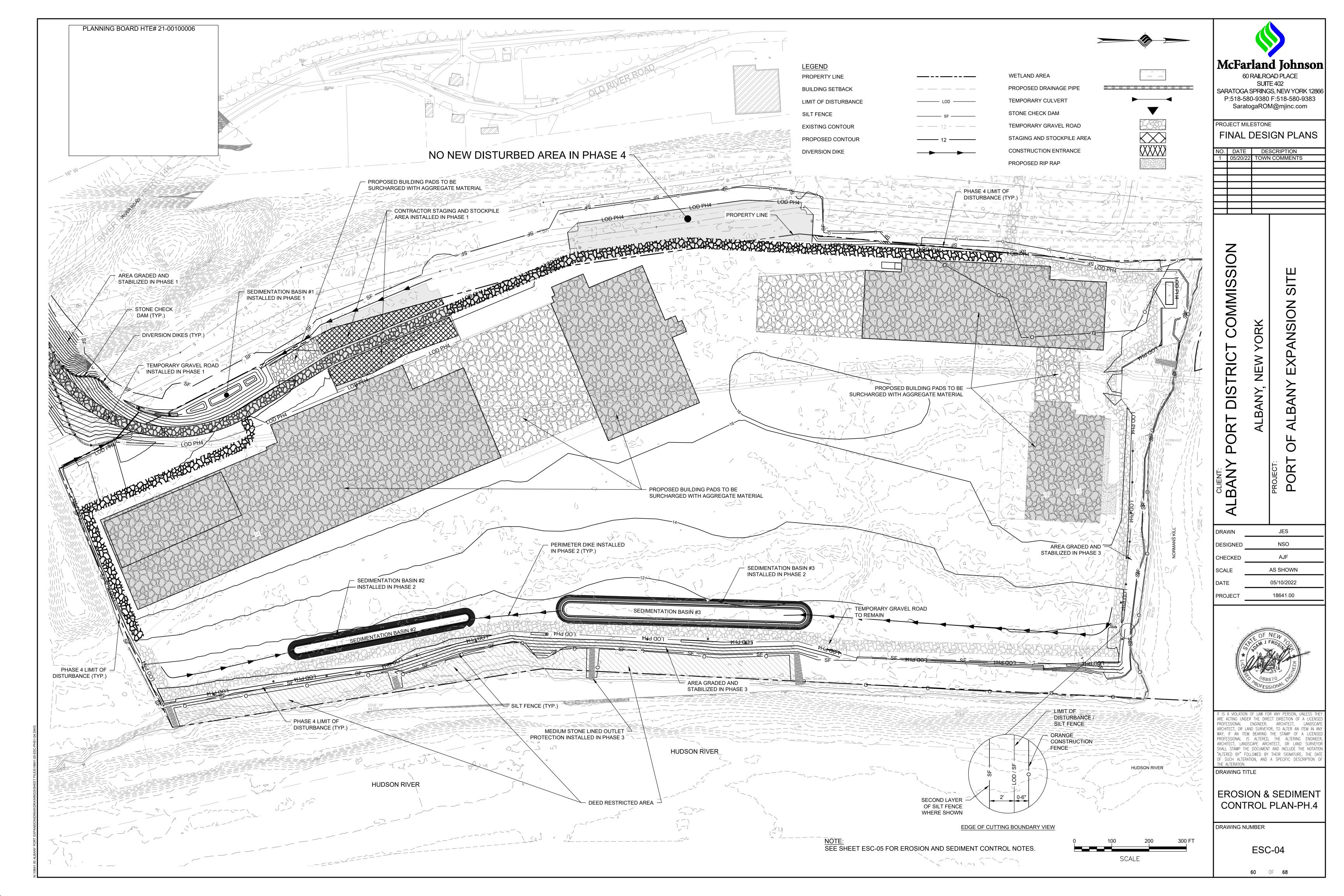
APPENDIX B

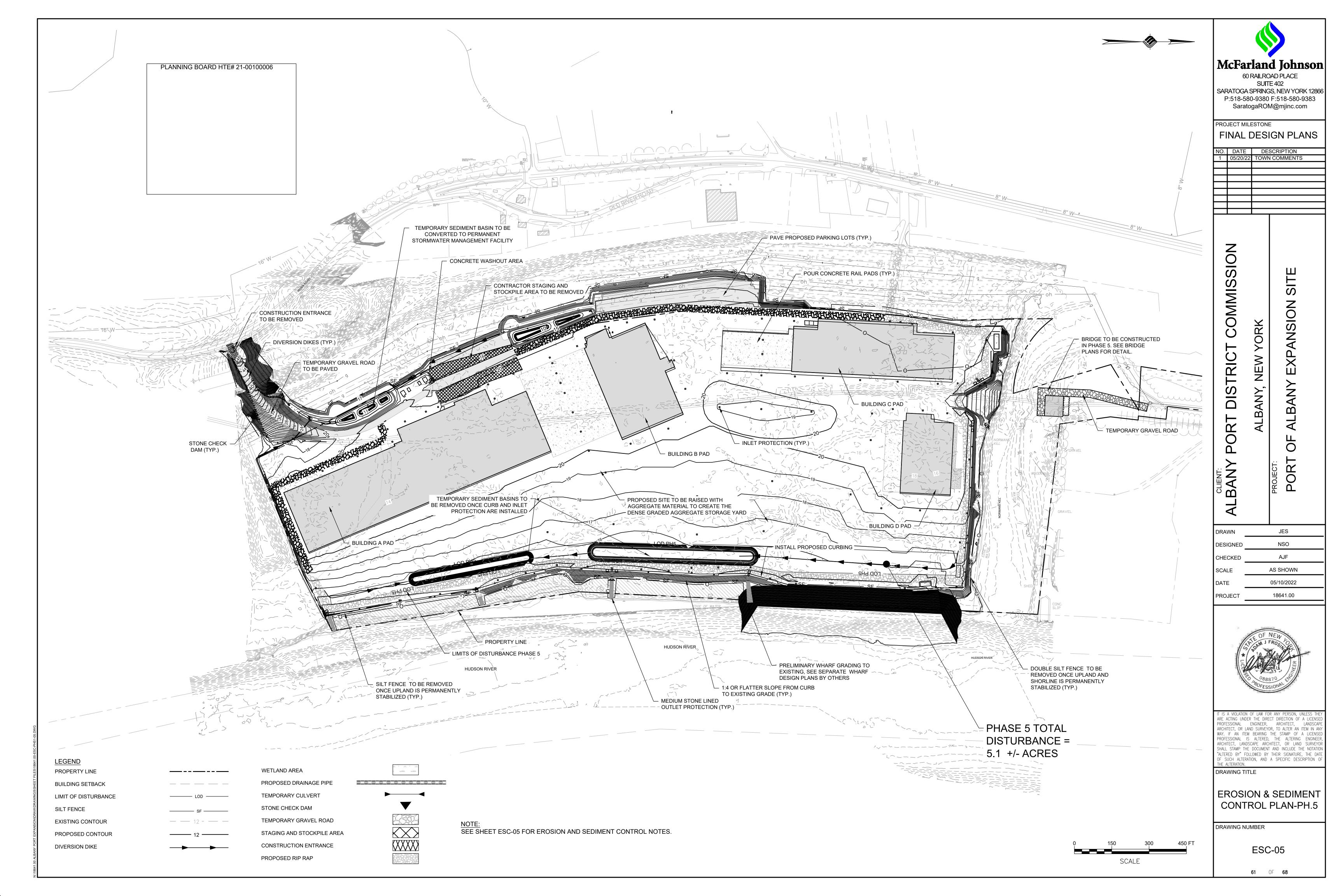
EROSION & SEDIMENT CONTROL PLANS, DETAILS & NOTES











EROSION AND SEDIMENT CONTROL PLAN NOTES:

- 1. THE EROSION AND SEDIMENT CONTROL PLAN IS INTENDED TO REPRESENT A CONCEPTUAL APPROACH TO EROSION AND SEDIMENT CONTROL. IT IS FURTHER INTENDED THAT THE OWNER AND CONTRACTOR SHALL IMPLEMENT PRACTICES, AS REQUIRED, TO CONTROL EROSION AND SEDIMENT IN ACCORDANCE WITH THE NEW YORK STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL AND
- 2. INSTALL SILT FENCE, AND ALL OTHER EROSION CONTROL MEASURES AS INDICATED ON THE PLAN PRIOR TO THE START OF ANY EXCAVATION WORK. EROSION CONTROL MEASURES WILL BE IMPLEMENTED IN ACCORDANCE WITH THE NEW YORK STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL, NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION AND THE GOVERNING MUNICIPALITY REQUIREMENTS.
- REMOVE AND STOCKPILE TOPSOIL IN ACCORDANCE WITH THE EROSION AND SEDIMENT CONTROL PLAN. REPLACE TOPSOIL TO A MINIMUM 4" DEPTH. ALL DISTURBED AREAS ARE TO BE HYDROSEEDED IN ACCORDANCE WITH THE EROSION AND SEDIMENT CONTROL PLANS.
- 4. CONTRACTOR SHALL BE RESPONSIBLE FOR THE MAINTENANCE AND REMOVAL OF TEMPORARY SEDIMENTATION CONTROLS, INCLUDING INLET PROTECTION AND SILT FENCE. EROSION CONTROL MEASURES SHALL NOT BE REMOVED BEFORE AREAS HAVE BEEN PROPERLY STABILIZED.
- 5. CONTRACTOR SHALL MAINTAIN A STOCK PILE OF EROSION AND SEDIMENT CONTROL MEASURES ON SITE AS INDICATED ON THE PLAN.
- 6. NO PETROLEUM PRODUCTS ARE TO BE STORED ON SITE WITHOUT PRIOR APPROVAL OF THE LOCAL STORMWATER INSPECTOR. ANY PETROLEUM ON SITE WILL COMPLY WITH ALL LOCAL, STATE, AND FEDERAL GOVERNMENT REGULATIONS.
- 7. WRAP YARD INLET GRATES IN FILTER FABRIC PROGRESSIVELY AS STORM SEWER AND YARD INLETS ARE INSTALLED.
- 8. ALL EROSION CONTROL MEASURES ARE TO BE REPLACED WHENEVER THEY BECOME CLOGGED OR INOPERABLE AND SHALL BE REPLACED AT A MINIMUM OF EVERY 3
- 9. JUTE MESH WILL BE USED ON SLOPES STEEPER THAN 3:1 AND WHEREVER NECESSARY TO CONTROL EROSION AND SILTATION OF EXISTING DRAINAGE SYSTEMS AS ORDERED BY THE ENGINEER.
- 10. ALL DISTURBED AREAS SHALL BE FINISH GRADED TO PROMOTE VEGETATION ON ALL EXPOSED AREAS AS SOON AS PRACTICABLE. STABILIZATION PRACTICES (TEMPORARY/PERMANENT SEEDING, MULCHING, GEOTEXTILES, ETC.) MUST BE IMPLEMENTED WITHIN SEVEN (7) DAYS WHERE CONSTRUCTION ACTIVITIES HAVE TEMPORARILY OR PERMANENTLY CEASED, AND NOT EXPECTED TO RESUME WITHIN FOURTEEN (14) DAYS.
- 11. ALL RIP-RAP OUTLET PROTECTION TO BE CONSTRUCTED PER NYSDEC STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL.
- 12. CONTRACTOR SHALL TAKE THE NECESSARY MEASURES, INCLUDING WATER SPRINKLING, TO PROVIDE DUST CONTROL DURING CONSTRUCTION.
- 13. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE MAINTENANCE OF ALL TEMPORARY AND PERMANENT EROSION CONTROL FEATURES THROUGHOUT THE DURATION OF CONSTRUCTION.
- A. ALL SEDIMENT TRAPPING DEVICES AND INLET PROTECTION DEVICES SHALL BE CLEANED OF ACCUMULATED SILT WHEN STORAGE CAPACITY HAS BEEN REDUCED BY 50% OF THEIR DESIGN CAPACITY.
- B. ALL SEDIMENT SHALL BE REMOVED FROM BEHIND SILT FENCE AND STRAW BALES WHEN IT ACCUMULATES TO A MAXIMUM HEIGHT OF 6".
- C. AFTER VEGETATION HAS BEEN SUBSTANTIALLY ESTABLISHED, EXCAVATE SWALES OF
- ACCUMULATED SILT. RE-ESTABLISHED VEGETATION ON DISTURBED AREAS. D. SEDIMENT COLLECTED BY EROSION CONTROL MEASURES SHALL BE DISPOSED OF BY SPREADING ON-SITE OR HAULED AWAY IF DETERMINED TO BE UNSUITABLE FOR FILL.
- 12. ALL DISTURBED AREAS SHALL BE STABILIZED, SEEDED AND MULCHED WITHIN 7 DAYS OF CEASED CONSTRUCTION ACTIVITY.
- 13. TOTAL PROJECT DISTURBANCE AREA PER THE NYSDEC SPDES STANDARDS IS 79 ACRES.
- 14. ALL AREAS TO REMAIN AS PERVIOUS VEGETATED AREAS SHALL BE RESTORED IN ACCORDANCE WITH THE NYS STORMWATER MANAGEMENT DESIGN MANUAL TABLE 5.3

PERMANENT SEEDING NON-SLOPED AREAS:

SOIL RESTORATION REQUIREMENTS.

- 1. IF SOILS ARE COMPACTED, SCARIFY UPPER TWO INCHES BY BACKBLADING WITH DOZER, RAKING, OR DISKING.
- 2. PLACE TOPSOIL TO A MINIMUM DEPTH OF 4 INCHES.
- 3. SEED PER SCHEDULE SPECIFIED ON LANDSCAPE PLANS.
- 4. FERTILIZE WITH 600 POUNDS PER ACRE OF 10-10-10. LIME TO ACHIEVE A PH OF NOT LESS THAN 5.5 OR GREATER THAN 7.6. IF HYDROSEEDER IS NOT USED, SEED AND FERTILIZER SHOULD BE LIGHTLY RAKED INTO SOIL.
- 5. MULCH WITH CLEAN (WEED FREE) STRAW IF SPECIFIED ON PLANS.

PERMANENT SEEDING SLOPED AREAS:

- 1. IF SOILS ARE COMPACTED, SCARIFY UPPER TWO INCHES BY BACKBLADING WITH DOZER, RAKING, OR DISKING.
- 2. PLACE TOPSOIL TO A MINIMUM DEPTH OF 4 INCHES.
- 3. FERTILIZE WITH 600 POUNDS PER ACRE OF 10-10-10. LIME TO ACHIEVE A PH OF NOT LESS THAN 5.5 OR GREATER THAN 7.6. IF HYDROSEEDER IS NOT USED, SEED AND FERTILIZER SHOULD BE LIGHTLY RAKED INTO SOIL.
- 4. IMMEDIATELY SEED PER SEED SCHEDULE SPECIFIED ON LANDSCAPE PLAN.
- 5. PROVIDE JUTE MESH IF SPECIFIED ON PLANS OR MULCH WITH CLEAN (WEED FREE) STRAW.

EROSION AND SEDIMENT CONTROL SEQUENCE:

THE TOWN OF BETHLEHEM SHOULD BE NOTIFIED PRIOR TO CONSTRUCTION ACTIVITIES STARTING AND CEASING DISTURBANCE OF OVER 5 ACRES AT ONE TIME.

- INSTALL CONSTRUCTION ENTRANCE ROADS
- ESTABLISH THE PROJECT CONSTRUCTION STAGING/OFFICE AREA
- USE ANY ACCESS ROAD CUT MATERIAL AS FILL FOR THE CONSTRUCTION STAGING AREA TEMPORARILY STABILIZE ALL DISTURBED AREAS
- INSTALL SILT FENCE DOWNSTREAM OF ALL DISTURBED AREAS • CONSTRUCT SEDIMENTATION BASIN #1 FOREBAYS TO 1' HIGHER THEN PROPOSED GRADING
- FOR THE PERMANENT STORM WATER MANAGEMENT POND #2 FOREBAYS. MATERIAL FROM THE POND EXCAVATION TO BE PLACED AND COMPACTED AS PART OF THE BUILDING A EMBANKMENT.
- BASED ON THE POTENTIAL FOR PROPOSED ROCK CUT WHEN EXCAVATING THE ROADWAY SECTION PHASE II MAY PROGRESS PRIOR TO THE COMPLETION OF PHASE I. THE PHASE I AREA SHALL BE STABILIZED TO THE MINIMIZE DISTURBANCE AREA PRIOR TO PROGRESSION TO PHASE II

PHASE II:

- INSTALL PERIMETER CONTROLS
- INSTALL ADDITIONAL CONSTRUCTION ACCESS ROAD
- CONSTRUCT SEDIMENTATION BASINS AND DIVERSION DIKES TO BASINS
- THE PROPOSED TEMPORARY STORM WATER TREATMENT FACILITIES SHALL BE INSTALLED BEFORE PROGRESSING INTO PHASE III

- SITE TO BE GRUBBED AND GRADED TO THE TOP OF SUB-GRADE ELEVATION IN SUB-PHASES
- BALANCE CUT AND FILLS IN THE SITE. COMPACT/IMPROVE EXISTING GROUND CONDITIONS ACCORDING TO GEOTECHNICAL REPORT
- IMPORT MATERIAL TO RAISE THE SITE TO PROPOSED SUB-GRADE ELEVATIONS
- LIMITS OF DISTURBANCE DISTURBANCE TO BE MINIMIZED IN EACH SUB-PHASE BY STABILIZING AREAS WITHIN 2 DAYS AFTER FINAL GRADE IS ACHIEVED
- THE SUB-PHASE AREAS WILL BE DISTURBED AND STABILIZE IN A ROLLING OPERATION AS THE EARTHWORK PROGRESSES FROM THE SOUTH END OF THE SITE TO THE NORTH END. TO AVOID STOCKPILING AVAILABLE CUT MATERIAL FROM ONE SUB-PHASE AREA MAY BE DEPOSITED AND STABILIZED WITHIN ANOTHER SUB-PHASE AREA; HOWEVER THE OVERALL TOTAL DISTURBED AREA SHALL NOT EXCEED 11 ACRES.
- PHASE IV AGGREGATE PLACEMENT WORK WILL OCCUR SIMULTANEOUSLY AND PROVIDE STABILIZATION ONCE SUB-GRADE ELEVATIONS HAVE BEEN ACHIEVED.

- HAUL IN PROPOSED AGGREGATE MATERIAL TO SURCHARGE THE BUILDING FOOTPRINTS AND
- MAINTAIN EXISTING PHASE III EROSIONAL AND SEDIMENT CONTROL MEASURES
- MONITOR SETTLEMENT OF THE SUB-GRADE MATERIAL IN ACCORDANCE WITH THE GEOTECHNICAL REPORT.

- INSTALL STORM SEWER SYSTEM WITH INLET PROTECTION FOR DRAINAGE STRUCTURES AND
- STONE LINING OUTLET PROTECTION INSTALL SITE UTILITIES
- SPREAD AGGREGATE MATERIAL TO STORAGE AREAS
- INSTALL INFILTRATION CHAMBERS
- POUR ALL PROPOSED CONCRETE RAIL PADS AND SIDEWALKS
- INSTALL PROPOSED CONCRETE CURBING
- PAVE PARKING LOT AREAS REMOVE CONSTRUCTION STAGING AREA
- CONVERT TEMPORARY SEDIMENT BASIN TO PERMANENT STORM WATER MANAGEMENT FACILITIES BY EXCAVATING THE PERMANENT POOL AND FOREBAYS DOWN TO FINAL GRADE AND CONVERTING THE OUTLET STRUCTURE.
- REMOVE TEMPORARY SEDIMENT BASINS, WHICH ARE NOT TO BE CONVERTED TO PERMANENT PRACTICES
- FINAL STABILIZATION FOR EMBANKMENT SLOPES ALONG THE NORMANS KILL AND HUDSON

TEMPORARY SEEDING

- 1. IF SOILS ARE COMPACTED, SCARIFY UPPER TWO INCHES BY BACKBLADING WITH DOZER, RAKING, OR DISKING. FERTILIZE WITH 300 POUNDS PER ACRE OF 10-10-10.
- NOTE: NO FERTILIZER SHOULD BE USED AFTER OCTOBER 1ST IF THERE IS DANGER OF LEACHING INTO WATER RESOURCE.
- IMMEDIATELY SEED PER SEED SCHEDULE SPECIFIED ON LANDSCAPE PLAN.
- APPLY STRAW MULCH AS NECESSARY TO HOLD IN MOISTURE, PROTECT SOIL FROM EROSION, HOLD SEED IN PLACE, AND KEEP SOIL TEMPERATURES MORE CONSTANT; 2 TONS PER ACRE.

SOIL RESTORATION NOTES:

SOIL RESTORATION PROCEDURE:

DURING PERIODS OF RELATIVELY LOW TO MODERATE SUBSOIL MOISTURE, THE DISTURBED SUBSOILS ARE RETURNED TO ROUGH GRADE AND THE FOLLOWING SOIL RESTORATION STEPS APPLIED:

- 1. APPLY 3 INCHES OF COMPOST OVER SUBSOIL
- 2. TILL COMPOST INTO SUBSOIL TO A DEPTH OF AT LEAST 12 INCHES USING A CAT-MOUNTED RIPPER, TRACTOR-MOUNTED DISC, OR TILLER, MIXING, AND CIRCULATING AIR AND COMPOST INTO SUBSOILS
- 3. ROCK-PICK UNTIL UPLIFTED STONE/ROCK MATERIALS OF FOUR INCHES AND LARGER SIZE ARE CLEANED OFF THE SITE
- 4. APPLY TOPSOIL TO A DEPTH OF 6 INCHES
- 5. VEGETATE AS REQUIRED BY APPROVED PLAN.
- AT THE END OF THE PROJECT AN INSPECTOR SHOULD BE ABLE TO PUSH A 3/8" METAL BAR 12 INCHES INTO THE SOIL JUST WITH BODY WEIGHT. TILLING (STEP 2 ABOVE) SHOULD NOT BE PERFORMED WITHIN THE DRIP LINE OF ANY EXISTING TREES OR OVER UTILITY INSTALLATIONS THAT ARE WITHIN 24 INCHES OF THE SURFACE.

COMPOST SPECIFICATIONS:

COMPOST SHALL BE AGED, FROM PLANT DERIVED MATERIALS, FREE OF VIABLE WEED SEEDS, HAVE NO VISIBLE FREE WATER OR DUST PRODUCED WHEN HANDLING, PASS THROUGH A HALF INCH SCREEN AND HAVE A PH SUITABLE TO GROW DESIRED PLANTS.

WINTER STABILIZATION:

- PREPARE A SNOW MANAGEMENT PLAN WITH ADEQUATE STORAGE FOR SNOW AND CONTROL OF MELT WATER, REQUIRING CLEARED SNOW TO BE STORED IN A MANNER NOT AFFECTING ONGOING CONSTRUCTION ACTIVITIES.
- TO ENSURE ADEQUATE STABILIZATION OF DISTURBED SOIL IN ADVANCE OF A MELT EVENT, AREAS OF DISTURBED SOIL SHOULD BE STABILIZED AT THE END OF EACH WORK DAY UNLESS:
 - A. WORK WILL RESUME WITHIN 24 HOURS IN THE SAME AREA AND NO PRECIPITATION IS FORECAST OR;
 - B. THE WORK IS IN DISTURBED AREAS THAT COLLECT AND RETAIN RUNOFF, SUCH AS OPEN UTILITY TRENCHES, FOUNDATION EXCAVATIONS, OR WATER MANAGEMENT AREAS.
- IF THE SITE WILL NOT HAVE EARTH DISTURBING ACTIVITIES ONGOING DURING THE "WINTER SEASON", ALL BARE EXPOSED SOIL MUST BE STABILIZED BY ESTABLISHED VEGETATION, STRAW OR OTHER ACCEPTABLE MULCH, MATTING, ROCK OR OTHER APPROVED MATERIAL SUCH AS ROLLED EROSION CONTROL PRODUCTS. SEEDING OF AREAS WITH MULCH COVER IS PREFERRED BUT

SEEDING ALONE IS NOT ACCEPTABLE FOR PROPER STABILIZATION.

SOIL DISTURBANCE PHASING		
PHASE	DISTURBANCE AREA	
1	8.5 ACRES	
2	11.3 ACRES	
3	11 ACRES MAX.	
3A	9.7 ACRES	
3B	9.6 ACRES	
3C	10.0 ACRES	
3D	10.1 ACRES	
3E	10.0 ACRES	
3F	3.5 ACRES	
4	NO NEW AREAS (MAY OCCUR SIMULTANEOUSLY WITH PHASE 3)	
5	5.1 ACRES	

NOTE: A 5-ACRE WAIVER REQUEST MUST BE APPROVED BY THE TOWN OF BETHLEHEM (MS4) PRIOR TO DISTURBING MORE THAN 5 ACRES.

McFarland Johnson

60 RAILROAD PLACE SARATOGA SPRINGS, NEW YORK 12866 P:518-580-9380 F:518-580-9383 SaratogaROM@mjinc.com

ROJECT MILESTONE

FINAL DESIGN PLANS

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ARE ACTING UNDER THE DIRECT DIRECTION OF A LICENS PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAP ARCHITECT. OR LAND SURVEYOR. TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSI PROFESSIONAL IS ALTERED, THE ALTERING ENGINEE ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYO SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATIO "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION

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PROJECT

PLANNING BOARD HTE# 21-00100006

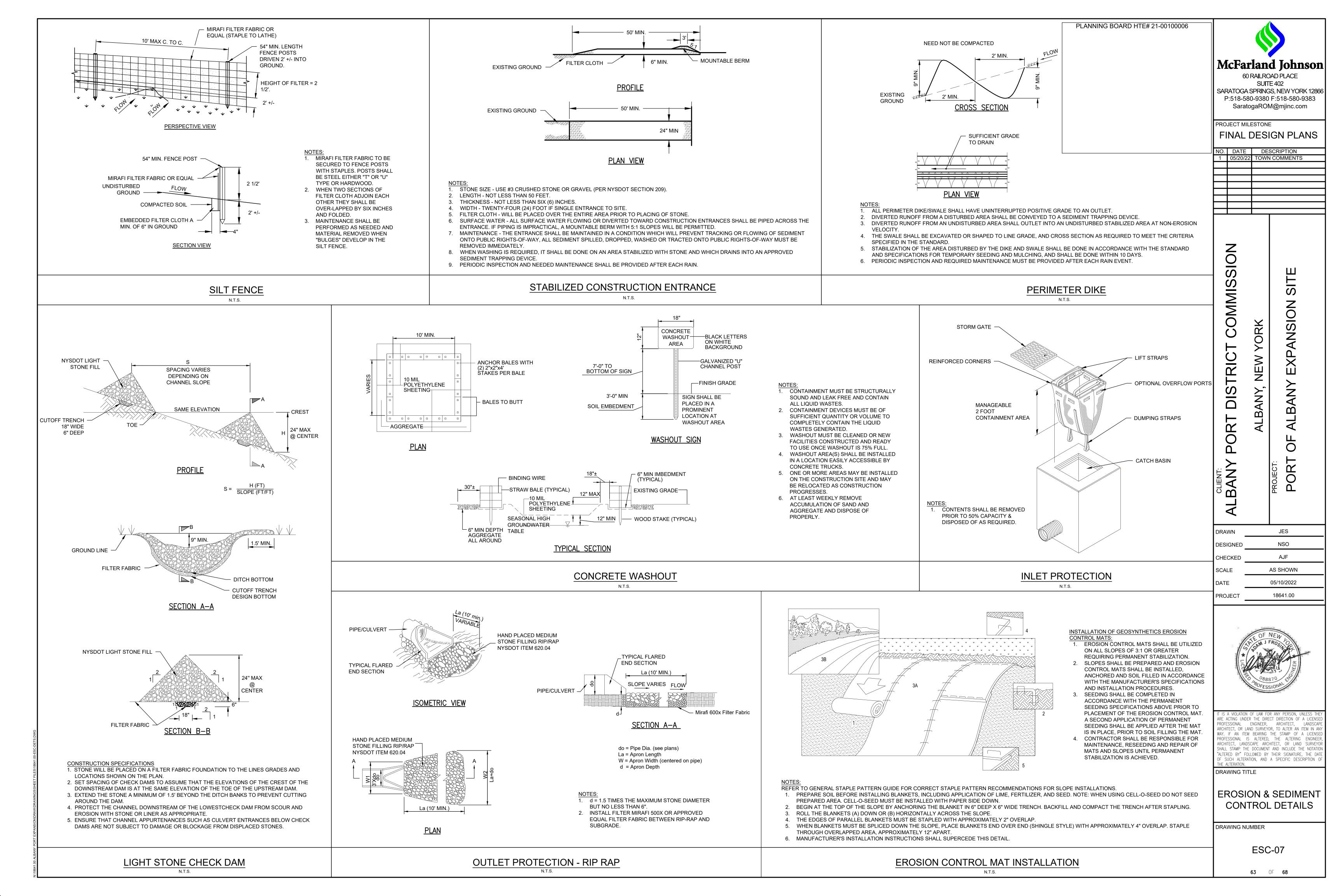
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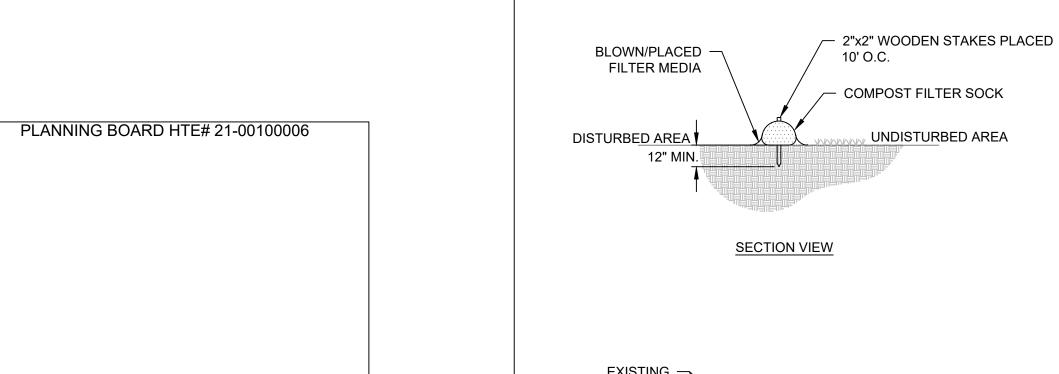
EROSION & SEDIMENT CONTROL NOTES

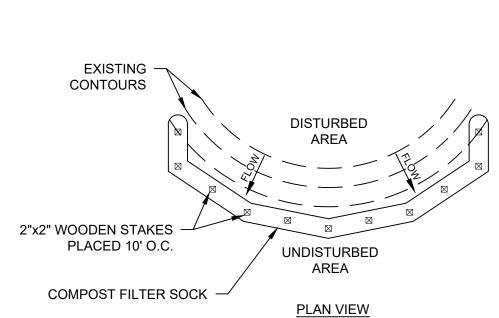
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62 OF **68**







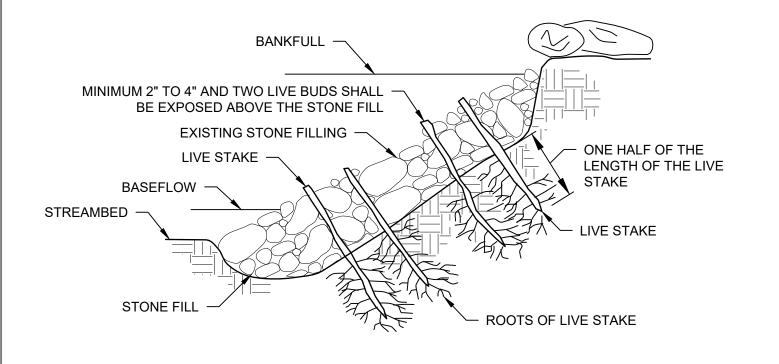
- 1. SOCK FABRIC SHALL MEET STANDARDS OF TABLE 5.1 OF NYS STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL. COMPOST SHALL MEET THE STANDARDS LISTED ON TABLE 5.2 OF NYS STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL.
- 2. COMPOST FILTER SOCK SHALL BE PLACED AT EXISTING LEVEL GRADE. BOTH ENDS OF THE SOCK SHALL BE EXTENDED AT LEAST 8 FEET UP SLOPE AT 45° TO THE MAIN SOCK ALIGNMENT. MAXIMUM SLOPE LENGTH ABOVE ANY SOCK SHALL NOT EXCEED THAT SHOWN ON FIGURE X.X OF NYS STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL. STAKES MAY BE INSTALLED IMMEDIATELY DOWNSLOPE OF THE SOCK IF SO SPECIFIED BY THE MANUFACTURER.
- 3. TRAFFIC SHALL NOT BE PERMITTED TO CROSS FILTER SOCKS. 4. ACCUMULATED SEDIMENT SHALL BE REMOVED WHEN IT REACHES HALF THE ABOVEGROUND
- HEIGHT OF THE SOCK AND DISPOSED IN THE MANNER DESCRIBED ELSEWHERE IN THE PLAN. 5. SOCKS SHALL BE INSPECTED WEEKLY AND AFTER EACH RUNOFF EVENT. DAMAGED SOCKS SHALL BE REPAIRED ACCORDING TO MANUFACTURER'S

SPECIFICATIONS OR REPLACED WITHIN 24 HOURS

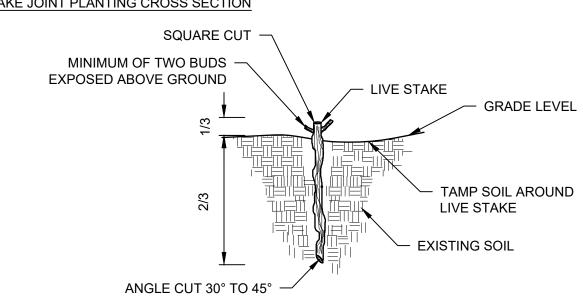
- OF INSPECTION. 6. BIODEGRADABLE FILTER SOCKS SHALL BE REPLACED AFTER 6 MONTHS; PHOTODEGRADABLE SOCKS AFTER 1 YEAR. POLYPROPYLENE SOCKS SHALL BE REPLACED ACCORDING TO MANUFACTURER'S RECOMMENDATIONS.
- 7. UPON STABILIZATION OF THE AREA TRIBUTARY TO THE SOCKS. STAKES SHALL BE REMOVED. THE SOCK MAY BE LEFT IN PLACE AND VEGETATED OR REMOVED. IN THE LATTER CASE, THE MESH SHALL BE CUT OPEN AND THE MULCH SPREAD AS A SOIL SUPPLEMENT.

END VIEW

VERTICAL TRAVEL GUIDE RAILS



LIVE STAKE JOINT PLANTING CROSS SECTION

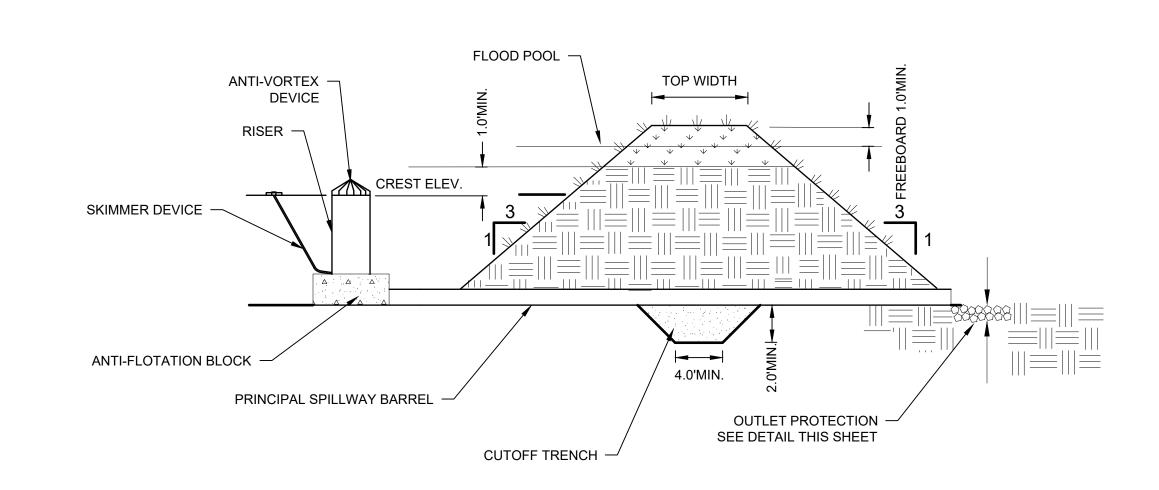


LIVE STAKE CROSS SECTION

- 1. CARE SHALL BE TAKEN NOT TO DAMAGE THE LIVE STAKES DURING INSTALLATION. THOSE DAMAGED SHALL BE LEFT IN PLACE AND SUPPLEMENTED WITH AN INTACT LIVE STAKE.
- 2. THE LENGTHS OF LIVE STAKES DEPENDS UPON THE APPLICATION. THE LENGTH SHALL EXTEND THROUGH THE SURFACE OF THE STONE FILL AT LEAST HALF THE LENGTH SHALL BE INSERTED IN TO THE SOIL, BELOW THE STONE FILL.
- 3. A PILOT HOLE IS REQUIRED TO ENSURE THAT THE LIVE STAKE IS NOT DAMAGED WHEN DRIVEN THROUGH THE STONE FILLING. ACCESS SHALL BE MADE THROUGH THE USE OF A DIBBLE BAR, OR SIMILAR TOOL TO WORK AN OPENING THROUGH THE ROCK LAYER.
- 4. MINIMUM 2" TO 4" AND TWO LIVE BUDS OF THE LIVE STAKE SHALL BE EXPOSED ABOVE THE STONE FILLING.
- 5. LIVE STAKES SHALL RANGE FROM 1" TO 4" IN DIAMETER AND BE FROM 5' TO 6' IN LENGTH.
- 6. LIVE STAKES SHALL BE CUT TO A POINT ON THE BASAL END FOR INSERTION IN THE GROUND.
- 7. USE A DEAD BLOW HAMMER TO DRIVE STAKES INTO THE GROUND. (HAMMER HEAD FILLED WITH SHOT OR SAND). A DIBBLE, IRON BAR, OR SIMILAR TOOL SHALL BE USED TO MAKE A PILOT HOLE TO PREVENT DAMAGING THE MATERIAL DURING INSTALLATION.
- 8. WHEN POSSIBLE, TAMP SOIL AROUND LIVE STAKES.

COMPOST FILTER SOCK

LIVE STAKE

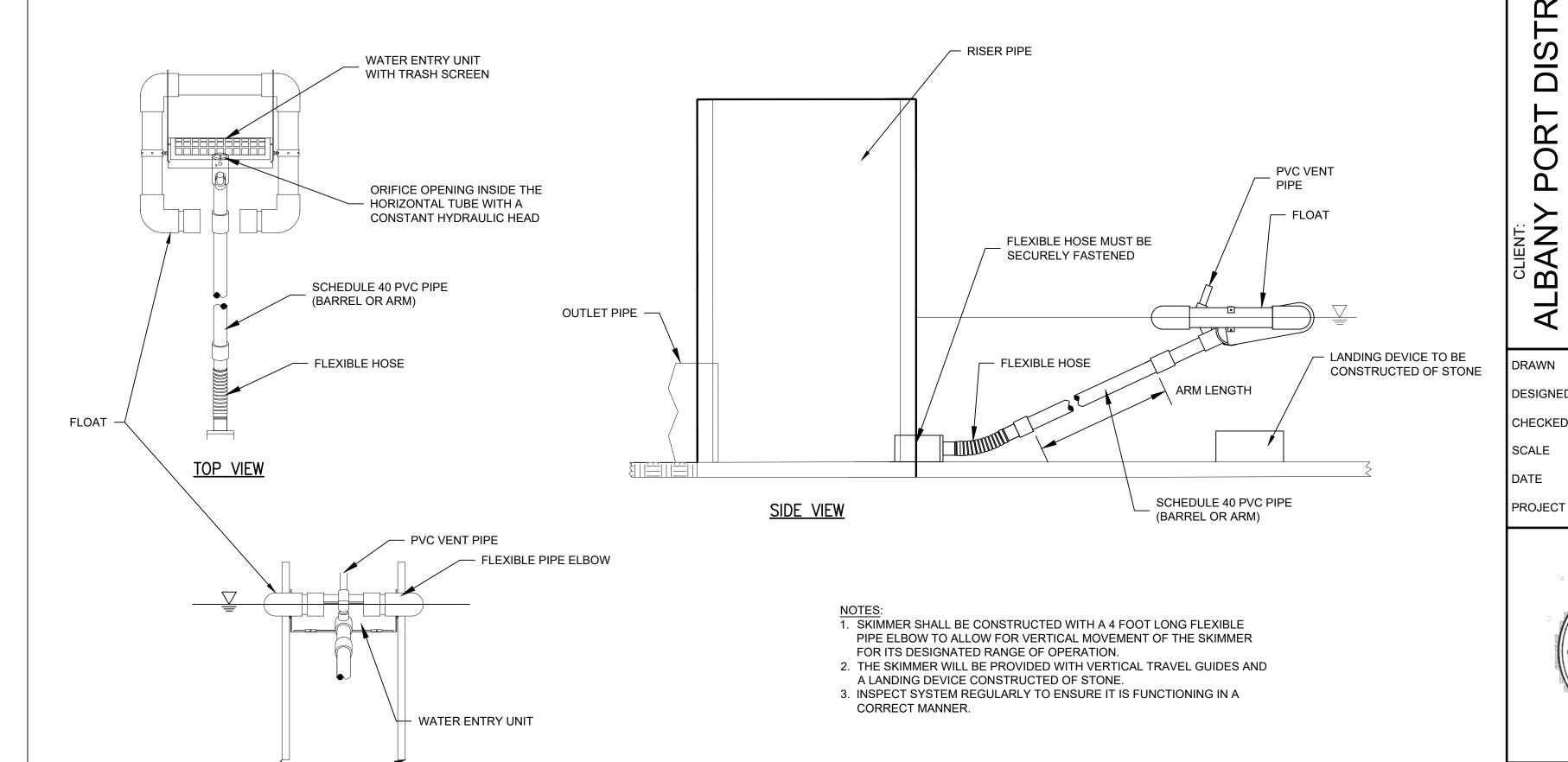


SEDIMENT BASIN CHART											
BASIN NUMBER	BOTTOM ELEV. (FT)	TOP OF DAM ELEV. (FT)	TOP OF RISER ELEV. (FT)	INV. OUT (FT)	SEDIMENT STORAGE ZONE VOLUME REQ'D (FT³)	SEDIMENT STORAGE ZONE VOLUME PROVIDED (FT³)	SEDIMENT STORAGE ZONE ELEV. (FT)	DEWATERING ZONE VOLUME REQ'D (FT³)	DEWATERING ZONE VOLUME PROVIDED (FT³)	DEWATERING ZONE ELEV. (FT)	CLEANOUT ELEVATION (FT.)
1	10	14	-	-	5300	5300	-	19080	19080	-	-
2	6	14	11	6.5	15200	16370	7.5	54720	55416	11	6.75
3	6	14	11	6.5	33000	36859	7.5	118800	119226	11	6.75

- 1. TEMPORARY SEDIMENT BASIN 1 CALCULATIONS HAVE BEEN SHOWN FOR CAPACITY VERIFICATION
- 2. BASIN 1 WILL BE GRADED OUT PER WQV POND DETAIL ON SHEET GR-14. ALL OUTLET STRUCTURES ARE TO BE COVERED WITH FILTER FABRIC DURING CONSTRUCTION. EXCAVATION OF BASIN 1 TO FINAL GRADE ELEVATIONS SHALL OCCUR ONCE FINAL STABILIZATION HAS BEEN REACHED.
- 3. EMBANKMENT MUST BE COMPACTED TO DESIGN SPECIFICATIONS. 4. EROSION PROTECTION MUST BE INSTALLED ALONG THE EMBANKMENT AND AT THE DISCHARGE END

TEMPORARY SEDIMENT BASIN

OF THE PIPE.



SKIMMER DEWATERING DEVICE							
BASIN NUMBER	WATER SURFACE ELEVATION (FT)	ARM LENGTH (FT)	ARM DIA. (in)	ORIFICE SIZE (in)	TOP OF LANDING DEVICE ELEVATION (FT)	FLEXIBLE HOSE LENGTH (in)	FLEXIBLE HOSE ATTACHMENT ELEVATION (FT)
2	11	16	5	5	7.5	12	6
3	11	16	7	7	7.5	12	6

N.T.S.

SKIMMER DEWATERING DEVICE DETAILS

PROJECT MILESTONE FINAL DESIGN PLANS NO. DATE DESCRIPTION

TOWN COMMENTS

McFarland Johnson

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SaratogaROM@mjinc.com

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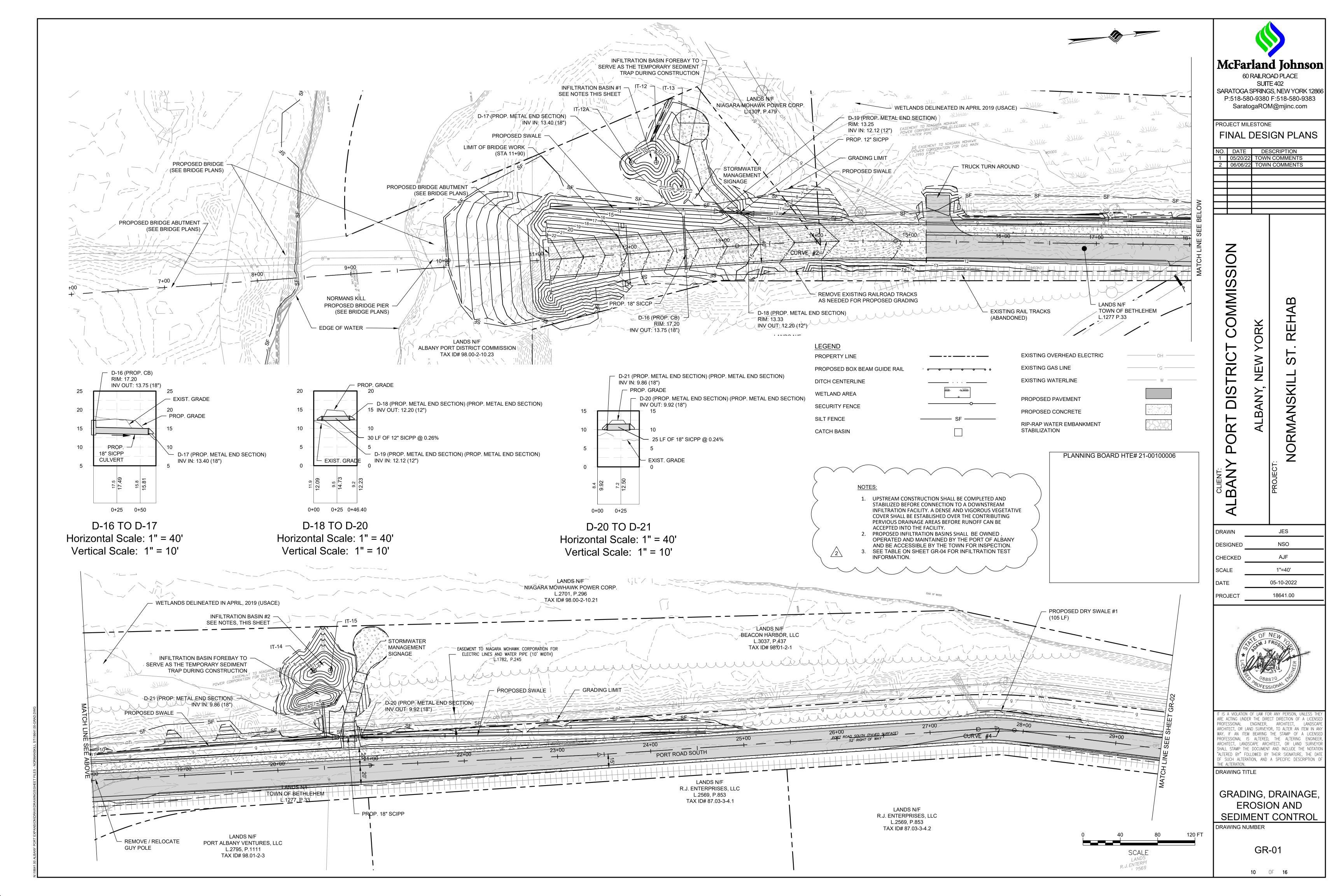
EROSION & SEDIMENT CONTROL DETAILS

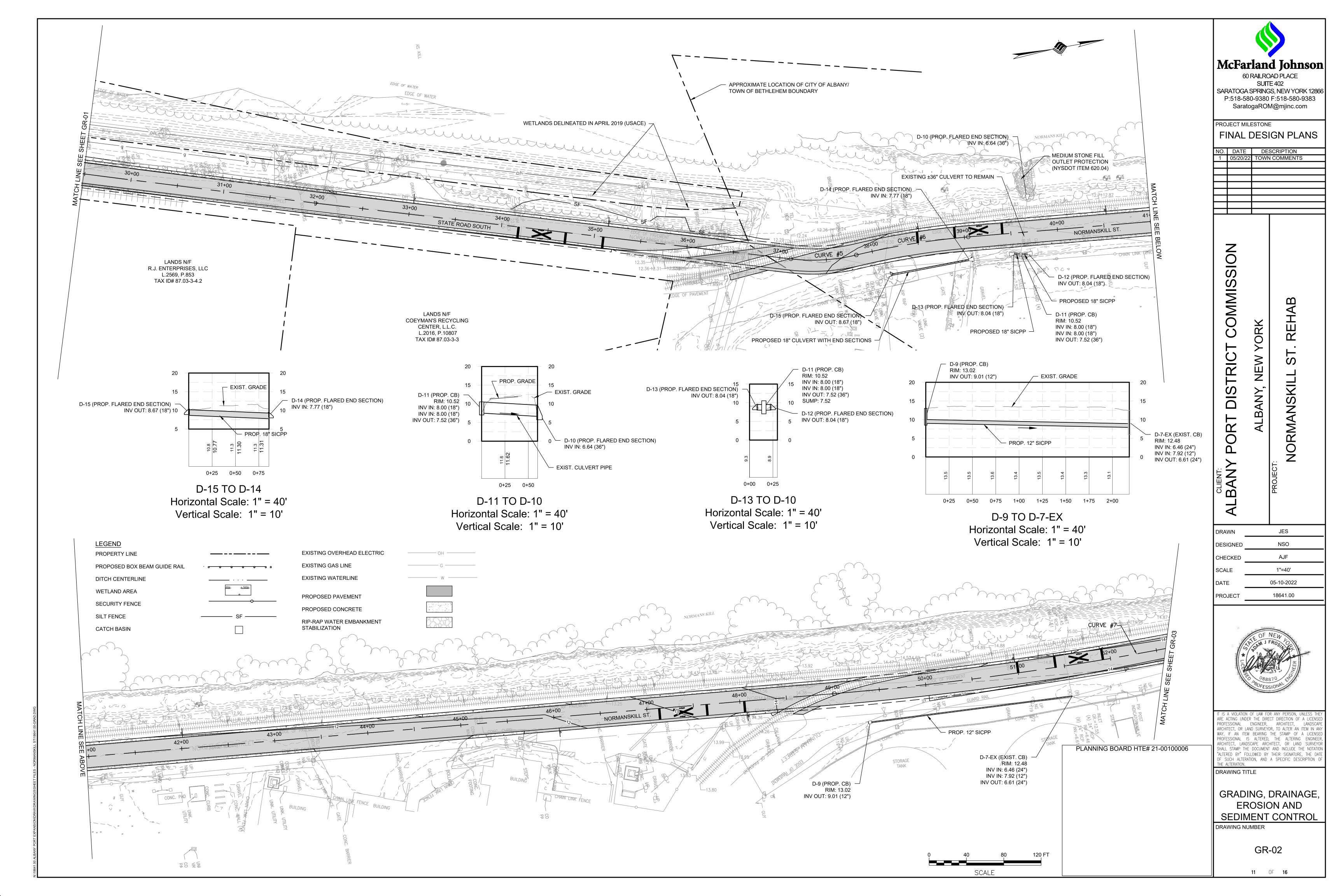
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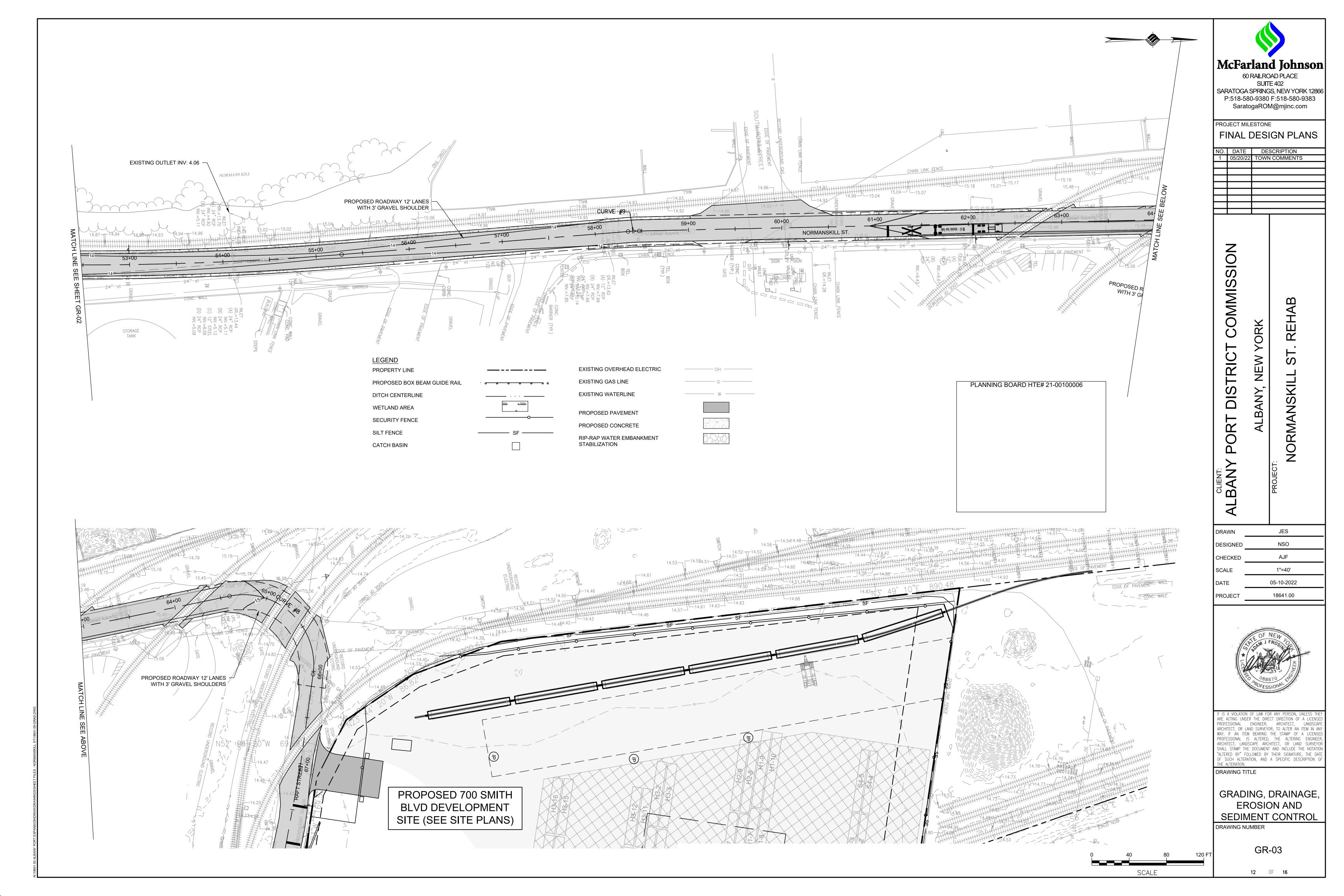
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APPENDIX C

DRAINAGE DESIGN REPORT

DRAINAGE DESIGN REPORT

FOR

MARMEN-WELCON TOWER MANUFACTURING PLANT

TOWN OF BETHLEHEM ALBANY COUNTY NEW YORK

FINAL SUBMISSION JUNE 20, 2022

CREATED FOR:



ALBANY PORT DISTRICT COMMISSION 106 Smith Boulevard Albany, NY 12202 518-463-8763 www.portofalbany.us

CREATED BY:



60 Railroad Place, Suite 402 Saratoga Springs, NY 12866 518-580-9380 www.mjinc.com

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- B. Water Quality Volume (WQv) / Runoff Reduction Volume (RRv)
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I. General Information

A. Project Description

This Stormwater Management Report has been developed for a Supplemental Environmental Impact Statement (SEIS) regarding a proposed development at the Port of Albany. The proposed development is an offshore wind (OSW) manufacturing facility that will produce wind turbine tower components. The Project is situated on 81.62 acres of land at the Beacon Island site, located at the confluence of the Normans Kill and Hudson River. The project also includes development within 4.4 acres of the adjoining parcel owned by National Grid, the extension and improvement of Normanskill Street, and widening of Rt. 144. The project owner, Albany Port District Commission (APDC), is proposing to develop the vacant parcels of land (tax parcels 98.00-2-10.23 and 98.01-2-1.0) to expand the existing Port of Albany in the Town of Bethlehem, Albany County, New York.

The proposed project will include development of an OSW tower manufacturing (Marmen-Welcon) facility consisting of five (5) separate buildings totaling up to 625,539+/- square feet of floor space. The following is a breakdown of the function and size of each building:

- Building A Plate Preparation & Welding (299,250 SF)
- Building B Welding Finishing (111,023 SF)
- Building C Blast Metallization Plant (131,968 SF)
- Building D Internal Assembly Finishing (61,550 SF)
- Building E Material Receiving (21,748 SF)

Tower production will occur within four (4) buildings (Buildings A-D) at the main facility on the Port Expansion property located in the Town of Bethlehem. The 5th building (Building E) will be located at 700 Smith Boulevard within the existing Port District in the City of Albany. A proposed gated bridge over the Normans Kill will provide a truck transportation route in and out of the main facility, by connecting Beacon Island and the 14.7-acre offsite parcel at 700 Smith Boulevard. In conjunction with the proposed bridge, Normanskill Street is to be extended from its existing end point to the bridge. The existing pavement will be improved to accommodate the proposed trucking route. River Road (Rt. 144) will be widened to accommodate the employee entrance. Employee parking will be situated on the adjoining land owned by National Grid with access from River Road. A proposed 500 LF wharf and associated dredging along the Hudson River will be used to load and ship completed tower sections. A separate stormwater analysis and SWPPP has been prepared for the 14.7-acre Building E site at 700 Smith Boulevard and the portion of Normanskill Street located in the City of Albany, as the sites are separated by approximately 1-mile and are under separate MS4 jurisdictions.

Historically, the Port Expansion site was composed of small islands and river channels subject to natural shifts due to flows associated with the Hudson River and the former Island Creek, a side channel of the Hudson River. Island Creek historically flowed along the western side of the site



through the current power line corridor and discharged to the Hudson River at the southern end of the site. Based on available mapping, sometime between 1936 and 1961, Island Creek channel was diverted at the north end of the site directly to the Hudson River, whereupon it was referred to solely as Normans Kill, the main tributary to this former channel. The site was subject to historic filling operations to create usable lands and a portion of the site was operated as a coal ash (fly ash) disposal site by Niagara Mohawk from approximately 1952 to 1970. As such, there are large areas of fly ash deposits on the site that must be considered during the design and construction of the site infrastructure and stormwater management facilities. Excavated fly ash material will need to be appropriately handled and properly disposed of as discussed in Section B below. A soil management plan has been developed and will require a cap over the site.

The purpose of this report is to assess the stormwater quality, quantity, and erosion and sediment control for the development of the site. This report has been developed in accordance with the New York State Department of Environmental Conservation (NYSDEC) State Pollution Discharge Elimination System (SPDES) General Permit for Stormwater Discharges from Construction Activity, GP-0-20-001 (Permit) and the NYSDEC Stormwater Management Design Manual (The Manual). The project site is located within the Town of Bethlehem, Albany County, New York, which is an MS4 community, requiring this report and project to receive approval from the Town. A separate stormwater analysis and SWPPP has been prepared for the 14.7-acre Building E site at 700 Smith Boulevard and the portion of Normanskill Street located in the City of Albany, as the sites are separated by approximately 1-mile and are under separate MS4 jurisdictions.

The overall project limits analyzed in this Drainage Report are broken up into three (3) areas, hereafter referred to as (1) "Expansion Site", (2) "Normanskill Street Improvements", (3) "Offsite Improvements". See Existing Conditions Map (Appendix A) for the location of each of these areas. The Expansion Site is the portion of the project area that is located on Beacon Island. The Normanskill Street Improvement portion begins on the north end of the proposed bridge over the Normans Kill and extends north to the border of the Town of Bethlehem and City of Albany. The Offsite Improvements portion refers to the widening of Rt. 144 adjacent to the employee entrance.

B. Soil Classification

According to the Natural Resources Conservation Service (NRCS) web soil survey, there are five (5) mapped soil units identified within the project boundary (see Appendix E). The majority of the soil at the expansion site falls within the hydrologic soil group B/D. The first letter corresponds to drained soil's properties under drained conditions and the second to saturated conditions. Group B soils have moderate infiltration and runoff rates while group D have a low infiltration rate and a high runoff rate. The soils with dual group identifiers have been modeled with the more conservative of the two, in this case a D soils group. Most of the soil adjacent to Normanskill Street Improvements is within soil group A. Group A soils have a high infiltration rate.



The complete list of soils found on the project site is identified in the table below (see Appendix E for NRCS Soils Report).

Table I – Soils Summary

Symbol	Soil Name	Hydrologic Soil Group
HuE	Hudson silt loam, 25 to 45 Percent slopes	C/D
NrD	Nassau very channery silt loam, hilly, very rocky	D
Ug	Udorthents, loamy	Α
Ur	Urban land	-
Wo	Wayland soils complex, non- calcareous substratum, 0 to 3 percent slopes, frequently flooded	B/D

Geotechnical studies have been undertaken to evaluate the subsurface conditions of the site. These investigations have been summarized in the following reports:

- Preliminary Geotechnical Evaluation and Interpretive Report, CME Associates, Inc., April 5, 2017
- Supplemental Geotechnical Report, Dente Group, July 20, 2017

Copies of these reports were included in the TOWN OF BETHLEHEM PLANNING BOARD, DRAFT GENERIC ENVIRONMENTAL IMPACT STATEMENT For ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY EXPANSION PROJECT, Appendix E.

• Draft Geotechnical Engineering Report, Terracon, October 15, 2021

A copy of this reports is included in the TOWN OF BETHLEHEM PLANNING BOARD, SUPPLEMENTAL ENVIRONMENTAL IMPACT STATEMENT FOR ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY EXPANSION PROJECT.

Based on these previous investigations, the subsurface conditions of the Expansion Site portion of the project site are generally characterized by historic fills of various depths overlying, in sequence with depth; river sediments, alluvial sands, glaciolacustrine silt/ clay, glacial till, and shale bedrock. The fill was noted at specific boring locations ranging from 6 to 23 feet below existing grade. The fill material is characterized as a random landfill deposit containing natural and solid waste deposits such as, but not limited to, foundry sand waste, sand, silt, coal ash, gravel, and organic matter. A predominant component of the fill was reported as coal ash.

Shale bedrock was found beneath the glacial till soils at select boring locations. The depth to rock ranged from approximately 61 feet below grade near the northwest portion of the site, to greater than 148 feet at the southeast portion of the site. The rock depths appear shallowest on the north and west sides of the site and increase to the east towards the Hudson River and in a south



direction across the site. Based on the New York State Museum and Science Service's Geologic Map of New York: State Hudson-Mohawk Sheet, and the geotechnical rock core samples, the bedrock appears to be consistent with the Normans kill Shale Formation.

According to the geotechnical reports, shallow groundwater was observed at depths ranging from approximately 1.5 to 13.7 feet below existing grade. However, due to the subsurface conditions, the shallower observations could be representative of perched groundwater zones due to discontinuous impermeable layers. Shallow groundwater fluctuations should be expected to occur at this site depending on several factors such as rainfall, seasonal changes, prevailing climate, ambient weather conditions, and the tidal influences of the Hudson River.

A soil management plan (SMP) has been prepared in accordance with the NYSDEC regulations. The SMP is included in SWPPP. The SMP pertains only to the Expansion Site portion of the project.

II. Hydrology

A. Existing Conditions

The existing drainage area totals 108.4 +/- acres, separated by the Normans Kill. The drainage area is bordered by the Hudson River to the east. At the south boundary there is a Public Service Energy Group (PSEG) power plant, and to the west a parcel owned by National Grid that conveys overhead electric transmission lines as well as an underground gas main. The Port Expansion site consists primarily of brush and trees with a small gravel area as well as abandoned railroad tracks. The Normanskill Street Improvement site consists of an existing road as well as brush and trees to the west. The Offsite Improvements consist of the existing roadway as well as brush and trees to the east and west.

The existing drainage condition is split up into seven (7) drainage areas. Drainage area DR-A drains to analysis point #1A, drainage areas DR-B and DR-F drain to analysis point #1, drainage areas DR-D and DR-E drain to analysis point #2. Drainage area DR-G drains to analysis point #3. Drainage area DR-C drains to a self-contained depression for storage. See Appendix A for the Existing Conditions Drainage Map.

Runoff from DR-A travels via sheet and shallow concentrated flow directly to a wetland located in the northwest corner of the site (Wetland 1). During large storm events the wetland overflows into an existing 40" pipe with direct outlet to the Normans Kill. Analysis of the existing capacity of the outlet pipe is provided in section IV below. Runoff from areas DR-B, DR-D, DR-E, and DR-F travel via sheet and concentrated flow to low areas with eventual outfall directly to the Normans Kill and Hudson River. An approximately 30-acre internal portion of the site (DR-C) was determined to be self-contained within the site capable of storing and infiltrating the 100-year storm event. Runoff from area DR-G sheet flows to the west side of River Road and travels to a low spot adjacent to the roadway where it is stored and eventually infiltrated.



A wetland delineation was conducted in April 2019 by McFarland Johnson for the FGEIS. The results of the delineation indicated that there are 8 freshwater wetlands located within the project limits. These wetlands are hereafter referred to as Wetlands 1, 3, 4, 5, 6, 7, 8, and 9. Wetlands within the original study area totaled approximately 2.33 acres.

A Supplemental Wetland Delineation was performed by MJ in April 2021 of the 18.22 acres on the National Grid Parcel. One contiguous wetland, comprising of approximately 7.13 acres, was delineated within the 18.22-acre area. The delineated wetland represents an extension of the 2019 wetland delineation and previously identified as Wetland 1. Wetland 1 drains in a northerly direction into a 40-inch corrugated metal pipe (CMP) which discharges directly to the Normans Kill.

The existing site falls within the Normans Kill watershed of the Middle Hudson Sub-Basin for the Lower Hudson River Basin (HUC10: 0202000602, Water Index No H-221-4) which is listed as a Class C water. Neither the Normans Kill nor the Hudson River are listed in the Manual's Appendix C as a watershed where enhanced phosphorus removal standards are required. Additionally, neither are listed in the Manual's Appendix E as a watershed impaired by pollutants related to construction activity.

B. Proposed Conditions

The proposed Port Expansion Site development includes 603,791 +/- square feet of OSW manufacturing facility space spread out over four (4) separate buildings. Ancillary impervious areas include parking for automobiles and trucks, a roadway, bridge, and a maritime wharf. The remainder of the site will be used for tower storage and be made up of dense graded aggregate. There will also be small pervious areas of grass and unaltered brush and trees.

The Normanskill Street Improvements are along a 0.52 mile stretch of roadway within the Town of Bethlehem. A new portion of Normanskill Street is to be constructed from the proposed vehicle bridge north to the existing roadway. This extension is approximately 925 feet long and will be dense graded aggregate. The existing portion of Normanskill Street will be widened on the west side of the roadway. The remaining portion of the existing roadway will be re-paved and not disturbed, as subbase will remain. A top course mill and fill of 1.11 acres is proposed. The improvements also include the required corresponding stormwater conveyance and treatment.

The Offsite Improvements consist of widening an approximately 600 LF stretch of Rt. 144 adjacent to the expansion site employee entrance. The roadway is to be widened by 7 +/- ft on the east side. The new impervious area is 0.14 acres. Corresponding grading is also part of the offsite improvements.

The total post-development drainage area will be 108.6 acres. The post-development drainage area is larger than the pre-development area by 0.2 acres due to the proposed bridge over the Normans Kill. The total disturbance for construction of the site will be approximately 72.7 +/-



acres.

The proposed drainage condition is split up into seventeen (17) drainage areas. Drainage Areas DR-8, DR-9, and DR-10 drain to analysis point #1A. Drainage Areas DR-5, DR-6, DR-7, DR-12, DR-13, DR-14, DR-15, and DR-16 drain directly to analysis point #1. Drainage areas DR-1, DR-2, DR-3, DR-4, and DR-11 drain to analysis point #2. Drainage area DR-17 drains to analysis point #3. Each analysis point remains the same in the pre- and post-development condition for comparison. See Appendix B for the Proposed Conditions Drainage Map.

On the Expansion Site, runoff from the proposed impervious areas will travel via sheet and shallow concentrated flow to one of seven (7) closed drainage networks. Drainage networks 1-7 will be conveyed through a NYSDEC approved stormwater filtering system and/or an off-line infiltration chamber system which will provide water quality volume treatment and runoff reduction prior to being discharged into the Normans Kill or Hudson River.

Runoff from DR-8 and DR-9 will be conveyed via vegetated swales to Micropool Extended Detention Ponds (Type P-1 per the Manual). The ponds will provide water quality volume treatment. The portion of the water held above the wet pool will be slowly discharged to the surrounding area over a 24-hour period. The ponds will also hold larger storm events up to the 10-year storm. During the 10-year storm and larger, emergency spillways outlet to the surrounding vegetated area, eventually flowing to Wetland #1.

Drainage Areas DR-10, DR-11, and DR-12 maintain their existing drainage patterns.

Drainage areas DR-13 and DR-14 correspond to sections of new Normanskill Street roadway. In each area, stormwater is collected via roadside swales and directed into a sedimentation basin which overflows into Infiltration Basin #1. The basins are designed to infiltrate the WQv as well as smaller storm events. During large storm events water will overflow to the Normans Kill.

Drainage area DR-15 corresponds to a section of Normanskill Street that is being expanded to the west. Stormwater is collected via a roadside swale with a dry swale at the end. In large storm events, water will flow through the dry swale to an overflow trench to be discharged to the surrounding vegetated area, eventually flowing into the Normans Kill. Drainage Area DR-16 will not be disturbed in the development of this project and will continue to drain into the Normans Kill.

Drainage area DR-17 will collect runoff on Rt. 144 via a roadside swale with a dry swale at the end. In large storm events, water will flow through the dry swale to an overflow trench to be discharged to the surrounding area. The surround area is self-contained and eventually infiltrates stormwater runoff.

The overall drainage plan incorporates multiple separate systems with outlets to the Normans Kill and/or Hudson River to avoid a more concentrated larger outlet for the site. See Appendix B



for proposed conditions plans and watershed mapping.

III. Stormwater Management & SPDES Requirements

The Proposed Development Project will have land disturbance of more than 1-acre, a full SPDES permit will be required, and a Stormwater Pollution Prevention Plan (SWPPP) will be developed in accordance with the Permit regulations and MS4 requirements as part of the Town of Bethlehem site plan approval process. A 5-acre waiver will also be requested in order to disturb more than 5 acres at one time.

Due to the presence of fly ash on the Expansion Site, in addition to a NYSDEC SPDES, a Site Management Plan (SMP) has been prepared in accordance with 6 NYCRR Part 375 and DER Technical Guidance for Site Investigation and Remediation and submitted to the NYSDEC, Division of Environmental Remediation and the NYSDOH. The SMP includes: a Health and Safety Plan (HASP), to inform and protect the contractor and their work force; a Community Air Monitoring Plan (CAMP), to monitor and protect the surrounding communities; and an Excavation Work Plan (EWP), to direct the activities of the contractor during construction. The EWP includes a detailed description of the work to be performed, the anticipated environmental conditions, and engineering controls to mitigate the movement of fly ash. The SMP has been included in the SEIS and SWPPP.

The SWPPP will be prepared in coordination with the Manual and meet the following criteria as the principal objectives contained in an approved SWPPP:

- Reduction or elimination of erosion and sediment loading to waterbodies during construction activities. Controls will be designed in accordance with the NYSDEC's New York State Standards and Specifications for Erosion and Sediment Control.
- Mitigate the impact of stormwater runoff on the water quality of the receiving waters.
- Maintenance of stormwater controls during and after completion of construction.

These objectives will be accomplished by incorporating design criteria outlined within the Technical Guidelines provided by The Manual and summarized below.

A. Methodology

To analyze the hydrologic impacts of the proposed development, a storm water management model was developed in accordance with the Manual. HydroCAD™, by HydroCAD Software Solutions LLC was used to model both the existing and proposed conditions: soil data from the NRCS Web Soil Survey was entered into the software; land coverage areas were estimated using aerial photography and site visits; watershed areas were developed using the surveyed topography; time of concentrations were estimated using USDA, Urban Hydrology for Small Watersheds, TR-55 (TR-55) methodology; and finally runoff and routing calculations were performed using the SCS Unit Hydrograph method.



The following rainfall depths were utilized in the analysis of the 1, 10, and 100-year storm events:

Table II - Hydrologic Analysis Data

Storm Event	Rainfall Depth (in.)
1-year	2.20
10-year	3.63
100-year	6.11

Rainfall depths were determined using the Northeast Regional Climate Center (NRCC) data for Albany County. The rainfall intensity utilized is the Type II-24 hour storm. This data is preprogramed in the HydroCAD software.

Green Infrastructure practices were designed in accordance with the Manual using the NYSDEC Runoff Reduction Worksheets available through the NYSDEC's Construction Stormwater Toolbox, available on their website.

The following general steps are followed when conducting a stormwater design:

- 1. **Site Planning:** The existing natural resource areas and drainage patterns including wetlands, waterways, floodplains, and soils are identified. Conservation of natural resources are maximized given the proposed site.
- 2. **Pre and Post-Development Conditions Analysis:** The pre and post-development stormwater runoff conditions for the 1, 10, and 100-year storm events are determined using HydroCAD (detailed HydroCAD reports for this project can be found in Appendices A and B).
- 3. **Water Quality:** The Water Quality Volume and Runoff Reduction Volume are calculated using Chapter 4 of the Manual and Green Infrastructure Worksheets (provided in Appendix C).
- 4. Water Quantity: Peak runoff and stormwater retention/detention are evaluated using the Manual.

B. Water Quality Volume (WQv) / Runoff Reduction Volume (RRv)

Section 4.2 of the Manual states that Water Quality Volume (WQv) is intended to improve the water quality by capturing and treating runoff from small, frequent storm events that contain higher pollutant levels created through the increase of impervious surfaces. Impervious surfaces accumulate pollutants that quickly wash off and rapidly enter downstream waters as well as prevent natural groundwater recharge.

The WQv required for the proposed site is based upon the 90% rainfall event number, percent of impervious cover, and the total site area. Calculations were done using the Green Infrastructure worksheets and can be found in Appendix C. The total WQv required is 273,874 cubic feet.

Runoff Reduction Volume (RRv) is the reduction of the total WQv by application of green infrastructure techniques and stormwater management practices to replicate pre-development



hydrology more closely. The intent of RRv is to recognize the water quality benefits of certain site design practices to address flow as a pollutant of concern.

According to Section 4.3 of the Manual, RRv may be calculated based on three methods:

- 1. Reduction of the practice contributing area in WQv
- 2. Reduction of runoff volume by storage capacity of the practice
- 3. Reduction using standard SMPs with runoff reduction capacity

The minimum RRv required by the proposed site is based on the total area of new impervious cover and the Hydrologic Soil Group (HSG) Specific Reduction Factor (S). The specific reduction factor is based on the HSGs present at the existing site. Calculations were done using the NYSDEC Green Infrastructure worksheets and can be found in Appendix C. The minimum RRv was determined to be 57,313 cubic feet.

Due to the level of contamination present in the existing soils across the Expansion Site, stormwater infiltration practices were located only in areas along the Hudson River and Normans Kill where contamination is not expected to be present. However, the Normanskill Street extension project area does not contain contaminated soils, so all treatment practices selected utilize infiltration and therefore include RRv. Infiltration testing has been performed at all proposed infiltration practices. Test results are included as Appendix F.

The following stormwater treatment practices were designed to meet the WQv and RRv requirements of the Manual:

Stormwater Ponds

Two stormwater quality ponds (Pond #1 and Pond #2) have been designed as Micropool Extended Detention Ponds (P-1) in accordance with the Manual. Ponds #1 and #2 treat stormwater runoff from drainage areas DR-8 and DR-9 respectively. Runoff from these areas sheet flow to a vegetated swale and outlet into the forebay of the pond. As required by the manual, the permanent pool volume is a minimum 20% of the WQv. Any stormwater held above the permanent pool elevation will be slowly discharged from the pond over a period of 24 hours. In larger storm events, the ponds will provide a "first flush" treatment for up to a 10-year storm event with stabilized emergency spillways to direct flow from larger event greater than a 10-year event to the surrounding area. Due to the topography of the surrounding undisturbed area, water will flow toward Wetland #1. A pre- and post-development analysis of the inflow to Wetland #1 (Analysis Point #1A) has been included in Section IV below. The post-development runoff going to Wetland #1 does not exceed the pre-development condition. Detailed design of the stormwater ponds can be found on page GR-14 of the Expansion Site plan set.

Manufactured Stormwater Filtering Units

Six stormwater filtering systems have been designed to treat runoff from drainage areas DR-1, DR-2, DR-3, DR-4, DR-6, and DR-7. Runoff from these areas sheet flow to its respective closed drainage system and is treated through a filtering manhole unit(s) before the outfall. Details of



the proposed systems are located on sheet GR-15 of the Expansion Site plan set. All systems meet the minimum criteria as defined in Chapter 4 of the Manual and are certified by Washington State Department of Ecology (TAPE) the Maryland Department of the Environment. The systems provide 89% TSS removal and 40% TP removal, which exceed the performance requirements defined in section 3.3.2 of the Manual. Usage of the manufactured stormwater systems is documented in section 9 of the SWPPP. The design and sizing calculations for the manufactured stormwater filtering units is provided in the GI Worksheets (Appendix C).

Infiltration Chamber Systems

Three infiltration chamber systems have been designed to provide runoff reduction volume. For drainage areas DR-1 and DR-4 the infiltration chambers work in conjunction with Stormwater Filtering Units in order to treat the entire water quality volume. For drainage area DR-5 the infiltration chamber system provides sufficient volume to provide runoff reduction as well as treat the entire water quality volume. After flowing through the stormwater filtering units, runoff flows into the infiltration chambers and is stored until infiltrated into the ground. During large storm events, a diversion manhole allows runoff to bypass the infiltration chambers and flow to the Hudson River or Normans Kill. The design and sizing calculations for the chambers is provided in the GI Worksheets under the Infiltration Basin tab (Appendix C). Specifications for the chamber systems utilized are provided in Appendix D.

Infiltration Basins

Two infiltration basins (Basin #1 and Basin #2) have been designed in accordance with the manual. Basin #1 and #2 treat stormwater runoff from drainage areas DR-13 and DR-14 respectively. Runoff from these areas sheet flow to an open roadside swale which outlets into the forebay of the pond. Both ponds have been designed to infiltrate the WQv as required by each catchment area. Because both ponds outlet directly to the Normans Kill, detention of large storm events is not required (see section III.C through III.E below). The basins do not have additional capacity for the Channel Protection Volume (CPv), Overbank Flood Control (Qp), or Extreme Flood Control (Qf). In large storm events, the basin will provide a "first flush" treatment with stabilized emergency spillways to direct flow to the Normans Kill. All stormwater within the basin will be infiltrated within 48 hours of a rain event. Design of the infiltration basins is provided in the GI Worksheets (Appendix C).

Dry Swale

Two dry swales have been designed to treat the new impervious area within DR-15 and DR-17 respectively. Runoff from each area will sheet flow to a roadside swale with the end segment constructed as a dry swale. In large storm events, water not infiltrated into the swale will overflow to a stabilized outlet which drains to the surrounding area. Dry swale #2 has been designed without infiltration, and therefore will only take credit for WQv. Design of the dry swales is provided in the GI Worksheets (Appendix C).



Conservation of Natural Areas

Drainage Area DR-11 will be deed restricted to ensure the perpetual protection of the proposed area to remain vegetated along the Hudson River. Therefore, this area qualifies under the "Conservation of Natural Areas" volume reduction practice.

The RRv provided in the designed practices are summarized in Table III below:

Table III - Practices Providing Runoff Reduction

Drainage Area	Stormwater Practice	RRv (cf)
DR-1	Infiltration Chamber	21,248
DR-4	Infiltration Chamber	18,464
DR-5	Infiltration Chamber	18,426
DR-11	Conservation of Natural Areas	868
DR-13	Infiltration Basin #1	1,995
DR-14	Infiltration Basin #2	2,245
DR-15	Dry Swale #1	87
	Total RRv	63,333

The WQv provided for each drainage area is summarized in Table IV below:

Table IV – Practices Providing Water Quality Volume

Drainage Area	Stormwater Practice	WQv (cf)
DR-1	Filter Type 2	18,005
DK-1	Infiltration Chamber	2,802
DR-2	Filter Type 1	21,971
DR-3	Filter Type 1	43,939
DD 4	Filter Type 3	14,989
DR-4	Infiltration Chamber	2,052
DR-5	Infiltration Chamber	2,047
DR-6	Filter Type 1	48,060
DR-7	Filter Type 2	34,826
DR-8	Stormwater Pond #1	8,437
DR-9	Stormwater Pond #2	13,361
DR-14	Infiltration Basin #2	141
DR-15	.5 Dry Swale #1	
DR-17	Dry Swale #2	636
	Total WQv	211,395

C. Channel Protection Volume (CPv)

Stream Channel Protection Volume Requirements (CPv) are designed to protect stream channels from erosion. The Manual was used to determine the water quantity requirements of CPv; specifically, providing 24-hour extended detention for the 1-year storm event or discharging directly to tidal waters.

According to Section 4.4 of the Manual, the Stream Channel Protection Volume (CPV) requirement does not apply when the site discharges to a tidal waterbody.

The CPv requirement does not apply in certain conditions, including the following:

- Reduction of the entire CPv volume is achieved at a site through green infrastructure or infiltration systems.
- The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, 24-hour extended detention of the 1-year storm event is not required for all drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and analyzed as Analysis Point #1A. The existing 40" outlet pipe from the existing wetland 1 was also analyzed to confirm that adequate capacity was present for the proposed drainage conditions prior to being discharged to the Normans Kill. See Section IV.

The change in hydrology for the 1-year storm event from existing to proposed is shown in the HydroCAD Report printouts provided in Appendix A and B and summarized in Table VI.

D. Overbank Flood Control (Qp)

The primary purpose of the overbank flood control sizing criterion is to prevent an increase in the frequency and magnitude of out-of-bank flooding generated by urban development. The Manual was used to determine the water quantity requirements of Qp; specifically, providing sufficient retention volume to discharge all runoff from the proposed 10-year storm event at a rate equal to or less than the existing peak 10-year runoff rate or discharging directly to tidal waters.

According to Section 4.5 of the Manual, the Overbank Flood Control Criteria (Qp) requirement does not apply when the site discharges to a tidal waterbody.

The overbank flood control requirement (Qp) does not apply in certain conditions, including:

• The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams. Refer to Section 4.3 of the Manual for instructions.



The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, retention the 10-year storm event is not required for all drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls A pre-and post-development analysis of the inflow to Wetland #1 was performed and analyzed as Analysis Point #1A. The existing 40" outlet pipe from the existing wetland 1 was also analyzed to confirm that adequate capacity was present for the proposed drainage conditions prior to being discharged to the Normans Kill. See Section IV.

The change in hydrology for the 10-year storm event from existing to proposed is shown in the HydroCAD Report printouts provided in Appendix A and B and summarized in Table VI.

E. Extreme Flood Control (Qf)

The intent of the extreme flood criteria is to prevent the increased risk of flood damage from large storm events, maintain the boundaries of the predevelopment 100-year floodplain, and protect the physical integrity of stormwater management practices. The Manual was used to determine the water quantity requirements of Qf; specifically, providing sufficient retention volume to discharge all runoff from the proposed 100-year storm event at a rate equal to or less than the existing peak 100-year runoff rate or discharging directly to tidal waters.

According to Section 4.6 of the Manual, the Extreme Flood Control Criteria (Qf) requirement does not apply when the site discharges to a tidal waterbody.

The 100-year storm control requirement can be waived if:

• The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams. Refer to Section 4.3 of the Manual for instructions.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, retention the 100-year storm event is not required for all drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and analyzed as Analysis Point #1A. The existing 40" outlet pipe from the existing wetland 1 was also analyzed to confirm that adequate capacity was present for the proposed drainage conditions prior to being discharged to the Normans Kill. See Section IV.

The change in hydrology for the 100-year storm event from existing to proposed is shown in the HydroCAD Report printouts provided in Appendix A and B and summarized in Table VI.



IV. Summary of Findings

A. Summary of Results

Table V lists the required and provided RRv and WQv for the project. As shown, the project meets both the total water quality volume and runoff reduction volume required by the Manual.

Table V – Stormwater Management Practice Summary

Di la la ci									
Drainage Area	Stormwater Practice	RRv (cf)	WQv (cf)	Total (RRv + WQv)					
DR-1	Filter Type 2	-	18,005	42,055					
DK-1	Infiltration Chamber	21,248	2,802	42,033					
DR-2	Filter Type 1	-	21,971	21,971					
DR-3	Filter Type 1	-	43,939	43,939					
DR-4	Filter Type 3	ı	14,989	25 505					
DR-4	Infiltration Chamber	18,464	2,052	35,505					
DR-5	Infiltration Chamber	18,426	2,047	20,473					
DR-6	Filter Type 1	1	48,060	48,060					
DR-7	Filter Type 2	1	34,826	34,826					
DR-8	Stormwater Pond #1	-	8,437	8,437					
DR-9	Stormwater Pond #2	-	13,361	13,361					
DR-11	Conservation of Natural Areas	868	-	868					
DR-13	Infiltration Basin #1	1,995	-	1,995					
DR-14	Infiltration Basin #2	2,245	141	2,386					
DR-15	Dry Swale #1	87	129	216					
DR-17	Dry Swale #2	-	636	636					
Totals -		63,333	211,395	274,728					
Required	-	57,313	-	273,874					

Table VI below depicts the peak discharge in the existing and proposed conditions for the 1-year, 10-year and 100-year design storms. The peak discharge for all storm events draining to Analysis Point #1A is decreased in the post-development condition. The peak discharge for all storm events for the remaining analysis points exceed the existing value; however, as described in Sections III, C through E above, this requirement does not apply to analysis points 1 (Hudson River) and 2 (Normans Kill).



Table VI - Peak Discharge Storm Analysis

Analysis Point	Storm Event	Existing (cfs)	Proposed (cfs)
	1-year	27.32	4.77
1A	10-year	73.24	12.46
	100-year	163.60	30.97
	1-year	3.25	58.54
1	10-year	14.96	124.96
	100-year	43.20	205.59
	1-year	7.17	82.79
2	10-year	20.65	166.00
	100-year	48.06	290.19
	1-year	0.60	1.20
3	10-year	1.84	2.62
	100-year	4.39	5.25

Analysis Point #1A analyzes the peak discharge at Wetland #1. In large storm events, stormwater quality ponds #1 and #2 will overflow to an emergency spillway that outlets to the area surrounding Wetland #1. In the post-development condition, Analysis Point #1A has a peak discharge less than the pre-development condition during all storm events, therefore the required water quantity controls are met.

In the post-development condition, Analysis Point #1 has a total drainage area of 0.12 square miles (75.28 acres). This point drains to the Normans Kill with a drainage area of 162 square miles (103,680 acres). The project area makes up approximately 0.07% of the total drainage area of the Normans Kill. With an overall project time of concentration of around 10 minutes, the proposed project will have a negligible impact on the total Normans Kill hydrology as the site-produced runoff will be conveyed prior to the Normans Kill peak and will not impact the overall flood conditions of the Normans Kill.

In the post-development condition, Analysis Point #2 has a total drainage area of 0.04 square miles (23.6 acres). This point drains to the Hudson River with a drainage area of 8,090 square miles (5,177,600 acres). The project area makes up approximately 0.0005% of the total drainage area of the Hudson. With an overall project time of concentration of around 10 minutes, the proposed project will have a negligible impact on the total Hudson River hydrology, as the site-produced runoff will be conveyed prior to the Hudson River peak and will not impact the overall flood conditions of the Hudson River.

In the post-development condition, Analysis Point #3 discharge rates are higher than the predevelopment condition. However, analysis point #3 drains to the surrounding area which stores runoff to be gradually infiltrated. Runoff from this analysis point does not flow to a stream or wetland.



The existing 40" outlet pipe from Wetland #1 was also analyzed for capacity. The analysis is summarized in table VII below.

Table VII - Outlet Pipe Capacity Comparison

Storm Event	Existing (cfs)	Proposed (cfs)	Capacity (cfs)		
1-year	3.19	1.61	70.83		
10-year	14.53	5.17	70.83		
100-year	41.52	18.15	70.83		

B. Deviation from NYS Stormwater Management Design Manual

The proposed stormwater management design deviates from The Manual by utilizing manufactured stormwater filtering systems for new development.

The need for alternative stormwater management practices is rooted in the extremely limited space available as well as the current site conditions. The proposed Offshore Wind Manufacturing Facility requires 85 acres of usable manufacturing and storage space along the Hudson River. It also requires close proximity to an existing port. Such requirements narrow the available project locations to a select few plots of unoccupied land in the entire state and this site was selected through a solicitation process by the state for off-shore wind development. This site was chosen given it is located adjacent to the existing Port of Albany and is directly on the Hudson River. However, the usable portion of the site adjacent to the Hudson River, is only 66-acres. Therefore, the entirety of the site is needed for the OSW manufacturing process, with an ancillary receiving site located at 700 Smith Boulevard.

The Expansion Site extends also onto the adjacent National Grid property from which APDC is leasing approximately 4.4 acres. However, National Grid has prohibited the installation of permanent stormwater practices within their property.

In addition to space limitations, the existing soils conditions prevent infiltration from being utilized as a stormwater management practice over most of the site. The existing soils are classified as Hydrologic Group D and B/D which provide little to no infiltration and are underlaid by fly ash. Infiltration practices were utilized in the areas where greater than 0.5 in/hr infiltration rates were achieved.

To adequately satisfy the WQv requirements of the Manual, manufactured systems are needed. The Contech Jellyfish units designed meet both the performance and sizing requirements of Chapter 4 of the Manual. The units are also certified by Washington State Department of Ecology (TAPE) and the Maryland Department of the Environment, adequate sources accepted by the NYSDEC. Specifications for the proposed units are provided in Appendix D.

C. Conclusion

Based upon the analysis provided in this report, the proposed development can meet the sizing and performance requirements as defined in Chapter 4 of the Manual. During construction, Erosion and Sediment Control activities will be designed and enforced in accordance with the NYSDEC New York State Standards and Specifications for Erosion and Sediment Control. Stormwater management practices can provide the required RRv and WQv for the proposed conditions. The elements of the Manual and the SPDES Permit that relate to stormwater quantity controls, specifically CPv (1-year), Qp (10-year), and Qf (100-year), are not applicable for portions of the site that discharge directly to a tidal water. For the remaining areas, the peak discharge for the 1-year, 10-year, and 100-year storm events are reduced in the post-development condition. A downstream analysis was completed for the existing Wetland #1 (Analysis Point #1A) and its outlet pipe to confirm adequate capacity prior to discharging into the tidal waters of the Normans Kill. All elements of the closed drainage system have been designed to be non-erosive during a 2-year storm event and capable of conveying a 10-year storm event. Analysis of all closed drainage pipe networks is included in Appendix C. After construction, a maintenance and operation report program and agreement will be made between the site operator and MS4 (Town of Bethlehem) to ensure all stormwater management practices are maintained over the life of the site's operations.

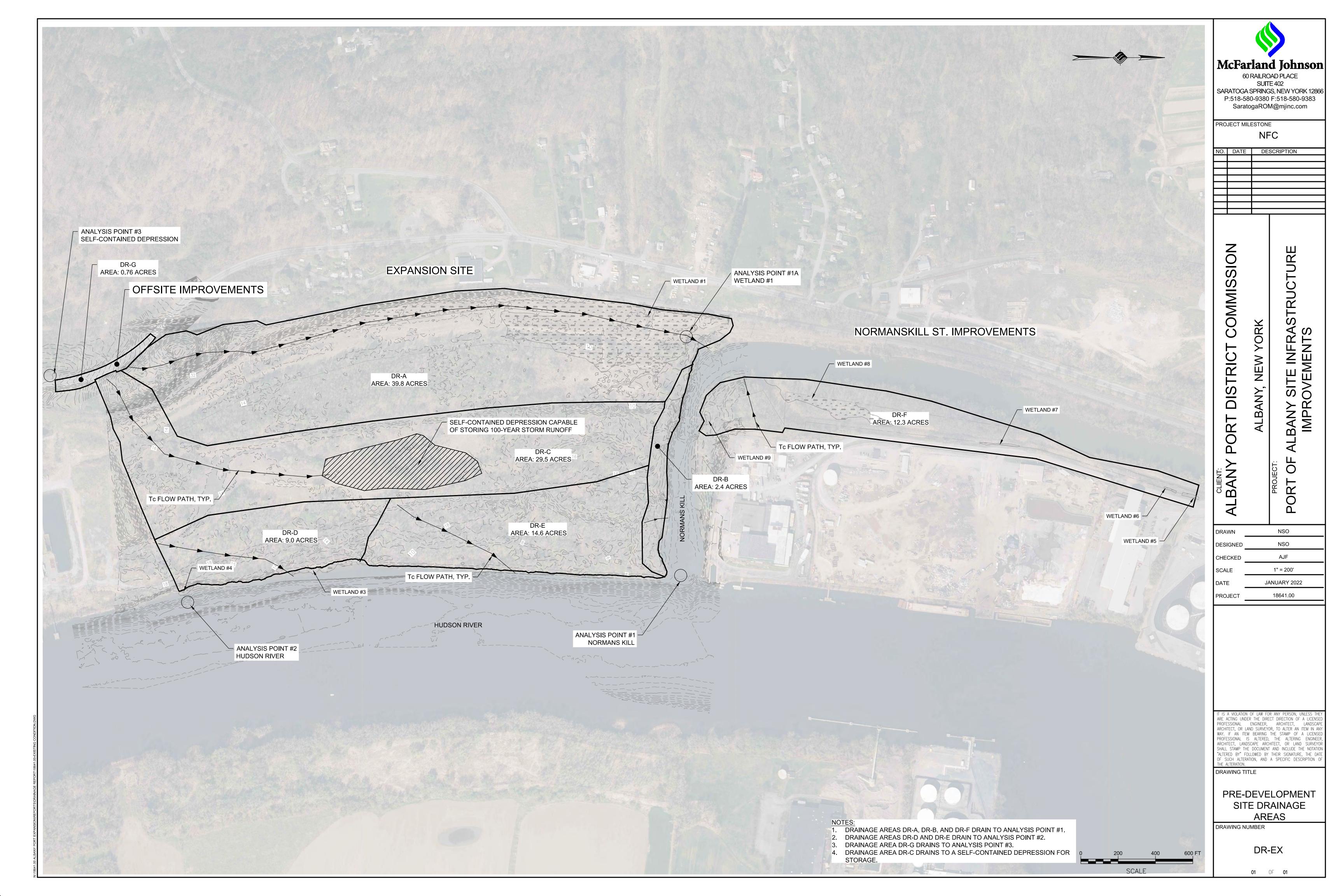


Port of Albany Drainage Site Infrastructure Design Report

Appendix A

Existing Conditions Drainage Map and HydroCAD Report





EXPANSION SITE NORMANSKILL ST. Wetland #1 / Analysis Outlet Pipe Overland Point 1A Overland Analysis Point #1 Overland Depression Infiltration Overland Analysis Point #2 Overland **OFFSITE IMPROVEMENTS** Roadway Analysis Point #3 Routing Diagram for 18641.00-Existing Condition Subcat Reach Pond Link Prepared by McFarland Johnson, Printed 5/6/2022 HydroCAD® 10.10-5a s/n 02401 © 2020 HydroCAD Software Solutions LLC

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Area Listing (all nodes)

Area	CN	Description
 (acres)		(subcatchment-numbers)
0.300	39	>75% Grass cover, Good, HSG A (DR-G)
3.970	77	Brush, Fair, HSG D (DR-C)
1.100	98	Existing Railroad (DR-A)
2.500	96	Gravel surface, HSG D (DR-C)
1.100	98	Pavement (DR-F)
0.460	98	Roadway (DR-G)
87.730	79	Woods, Fair, HSG D (DR-A, DR-B, DR-C, DR-D, DR-E)
11.200	43	Woods/grass comb., Fair, HSG A (DR-F)
108.360	76	TOTAL AREA

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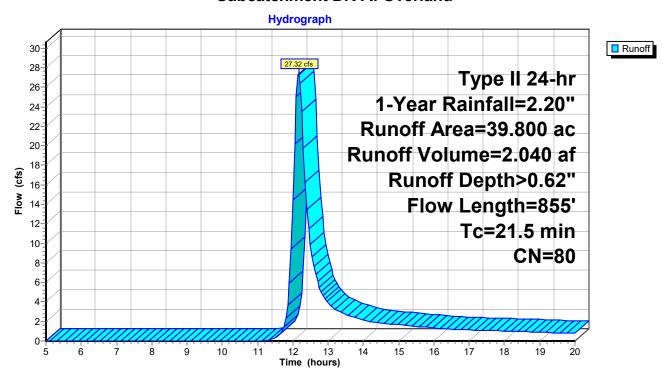
Summary for Subcatchment DR-A: Overland

Runoff = 27.32 cfs @ 12.16 hrs, Volume= 2.040 af, Depth> 0.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac) C	N Desc	cription		
*	38.700 79 Woods, Fair, HSG D * 1.100 98 Existing Railroad					
_						
	39.	800 8		ghted Aver		
	38.	700	97.2	4% Pervio	us Area	
	1.	100	2.76	% Impervi	ous Area	
			•			
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	14.5	150	0.1500	0.17	, ,	Sheet Flow, Sheet Flow
						Woods: Light underbrush n= 0.400 P2= 2.67"
	4.8	575	0.1600	2.00		Shallow Concentrated Flow, Shallow Concentrated
	1.0	0.0	0.1000	2.00		Woodland Kv= 5.0 fps
	2.2	130	0.0400	1.00		Shallow Concentrated Flow, Shallow Concentrated
	۷.۷	130	0.0400	1.00		· · · · · · · · · · · · · · · · · · ·
_						Woodland Kv= 5.0 fps
	21.5	855	Total			

Subcatchment DR-A: Overland



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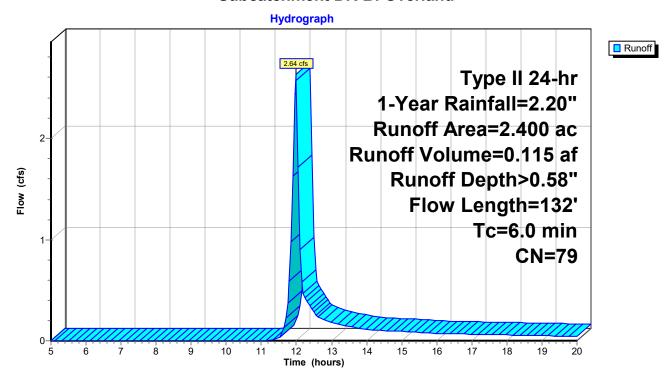
Summary for Subcatchment DR-B: Overland

Runoff = 2.64 cfs @ 11.98 hrs, Volume= 0.115 af, Depth> 0.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

_	Area	(ac)	CN	Desc	cription		
	2.400 79 Woods, Fair, HSG D				ds, Fair, H	ISG D	
_	2.400 100.00% Pervious Area				00% Pervi	ous Area	
	Tc	Lengt	:h :	Slope	Velocity	Capacity	Description
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
	6.0	13	2		0.37		Direct Entry, Sheet Flow

Subcatchment DR-B: Overland



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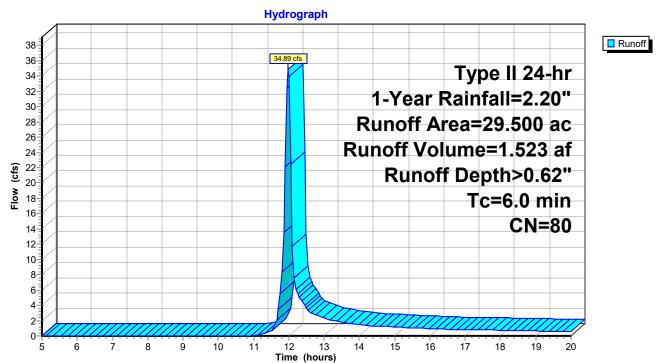
Summary for Subcatchment DR-C: Depression

Runoff = 34.89 cfs @ 11.98 hrs, Volume= 1.523 af, Depth> 0.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

Area	Area (ac) CN Description					
3	.970	77	Brus	h, Fair, HS	G D	
2	.500	96	Grav	el surface	, HSG D	
23	.030	79	Woo	ds, Fair, H	ISG D	
29	.500	80	Weig	hted Aver	age	
29	.500		100.	00% Pervi	ous Area	
-			01		.	D
Tc	Leng	tn :	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
6.0	•			•		Direct Entry, Min

Subcatchment DR-C: Depression



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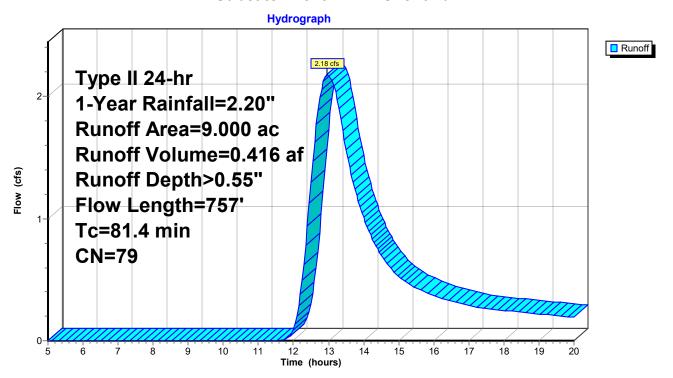
Summary for Subcatchment DR-D: Overland

Runoff = 2.18 cfs @ 12.96 hrs, Volume= 0.416 af, Depth> 0.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac) C	N Des	cription		
	9.	000 7	'9 Woo	ds, Fair, F	ISG D	
_	9.	000	100.	00% Pervi	ous Area	
	Tc Length Slope Velocity Capacity (min) (feet) (ft/ft) (ft/sec) (cfs)					Description
	56.6	150	0.0050	0.04		Sheet Flow, Sheet Flow
	23.9	507	0.0050	0.35		Woods: Light underbrush n= 0.400 P2= 2.67" Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
	0.9	100	0.1300	1.80		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
	81.4	757	Total			

Subcatchment DR-D: Overland



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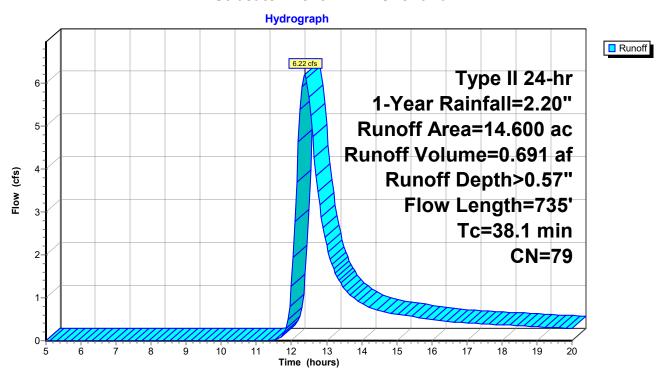
Summary for Subcatchment DR-E: Overland

Runoff = 6.22 cfs @ 12.38 hrs, Volume= 0.691 af, Depth> 0.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

_	Area	(ac) C	N Des	cription		
	14.	600 7	79 Woo	ds, Fair, F	ISG D	
	14.	600	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	27.6	150	0.0300	0.09		Sheet Flow, Sheet Flow
	9.8	510	0.0300	0.87		Woods: Light underbrush n= 0.400 P2= 2.67" Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
	0.7	75	0.1200	1.73		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
_	38.1	735	Total			

Subcatchment DR-E: Overland



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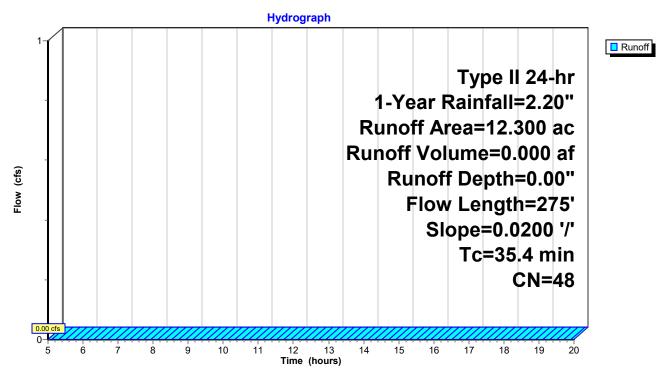
Summary for Subcatchment DR-F: Overland

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac)	CN	Description						
*	1.	100	98	Pave	ement					
	11.200 43			Woods/grass comb., Fair, HSG A						
	12.300 48 Weighted Average					age				
	11.200				91.06% Pervious Area					
	1.100 8.94% Impervious Area					ous Area				
	Tc (min)	Length (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	32.5	150	0.0	0200	0.08		Sheet Flow,			
	2.9	125	5 0.0	0200	0.71		Woods: Light underbrush n= 0.400 P2= 2.67" Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
	35.4	275	5 To	otal						

Subcatchment DR-F: Overland



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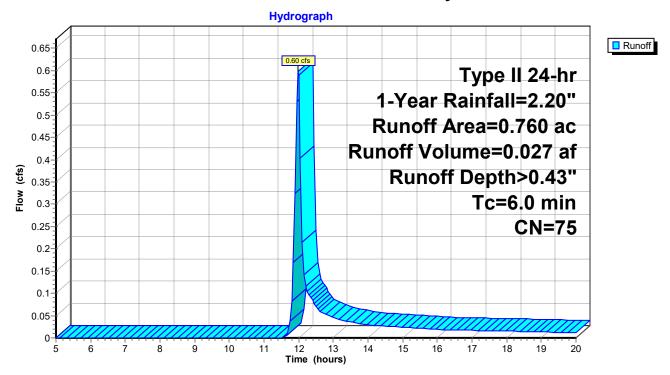
Summary for Subcatchment DR-G: Roadway

Runoff = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af, Depth> 0.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area (ac) CN Description									
*	0.	460	98	Roadway						
	0.	300	39	>759	√ Grass co	over, Good	, HSG A			
	0.760 75 Weighted Average					age				
	0.300 0.460			39.4	39.47% Pervious Area					
				60.53% Impervious Area						
	Тс	Leng	th :	Slope	Velocity	Capacity	Description			
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	6.0						Direct Entry, Minimum			

Subcatchment DR-G: Roadway



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Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 0.62" for 1-Year event

Inflow = 27.32 cfs @ 12.16 hrs, Volume= 2.040 af

Outflow = 3.19 cfs @ 17.12 hrs, Volume= 0.898 af, Atten= 88%, Lag= 297.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.07 fps, Min. Travel Time= 232.8 min Avg. Velocity = 0.05 fps, Avg. Travel Time= 304.0 min

Peak Storage= 44,519 cf @ 13.24 hrs

Average Depth at Peak Storage= 0.22', Surface Width= 201.33' Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

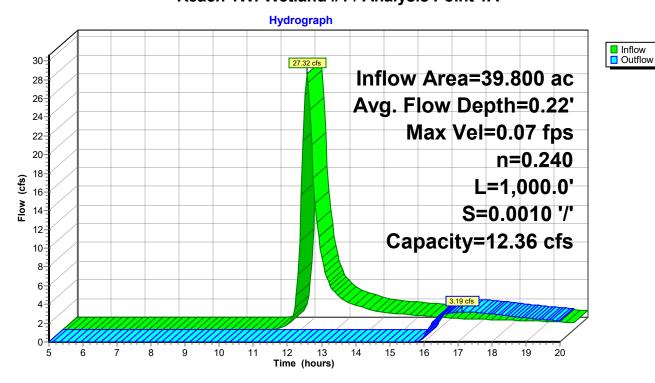
200.00' x 0.50' deep channel, n= 0.240 Sheet flow over Dense Grass

Side Slope Z-value= 3.0 '/' Top Width= 203.00'

Length= 1,000.0' Slope= 0.0010 '/'

Inlet Invert= 6.00', Outlet Invert= 5.00'

Reach 1W: Wetland #1 / Analysis Point 1A



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Summary for Reach 2R: Outlet Pipe

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 0.27" for 1-Year event

Inflow = 3.19 cfs @ 17.12 hrs, Volume= 0.898 af

Outflow = 3.19 cfs @ 17.13 hrs, Volume= 0.896 af, Atten= 0%, Lag= 0.5 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.10 fps, Min. Travel Time= 0.3 min Avg. Velocity = 3.35 fps, Avg. Travel Time= 0.3 min

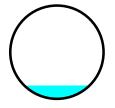
Peak Storage= 54 cf @ 17.12 hrs

Average Depth at Peak Storage= 0.48', Surface Width= 2.34' Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

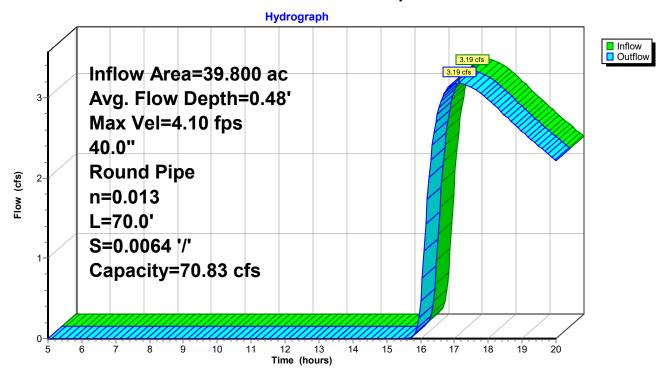
40.0" Round Pipe

n= 0.013 Corrugated PE, smooth interior Length= 70.0' Slope= 0.0064 '/'

Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 2R: Outlet Pipe



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Summary for Pond 1P: Infiltration

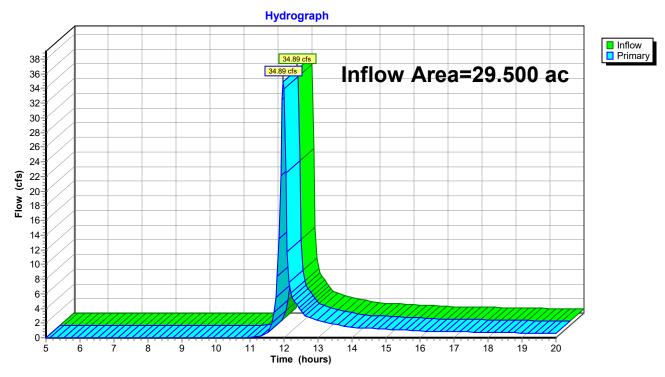
Inflow Area = 29.500 ac, 0.00% Impervious, Inflow Depth > 0.62" for 1-Year event

Inflow = 34.89 cfs @ 11.98 hrs, Volume= 1.523 af

Primary = 34.89 cfs @ 11.98 hrs, Volume= 1.523 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond 1P: Infiltration



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Summary for Pond AP-1: Analysis Point #1

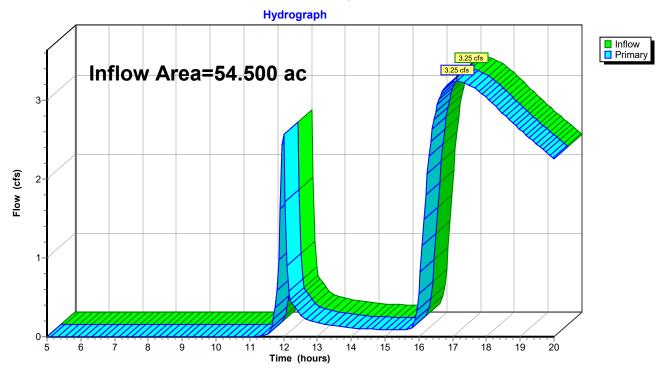
Inflow Area = 54.500 ac, 4.04% Impervious, Inflow Depth > 0.22" for 1-Year event

Inflow = 3.25 cfs @ 17.12 hrs, Volume= 1.012 af

Primary = 3.25 cfs @ 17.12 hrs, Volume= 1.012 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1



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Summary for Pond AP-2: Analysis Point #2

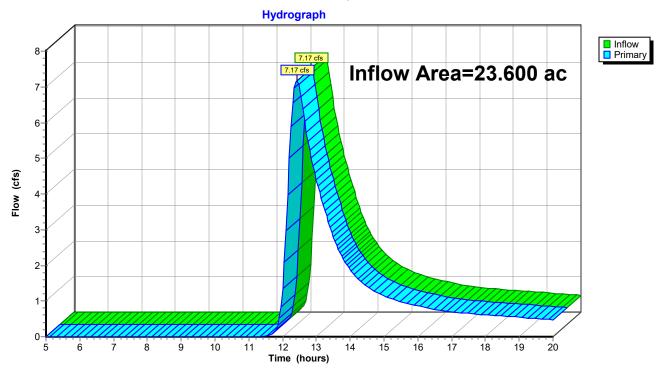
Inflow Area = 23.600 ac, 0.00% Impervious, Inflow Depth > 0.56" for 1-Year event

Inflow = 7.17 cfs @ 12.42 hrs, Volume= 1.107 af

Primary = 7.17 cfs @ 12.42 hrs, Volume= 1.107 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2



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Summary for Pond AP-3: Analysis Point #3

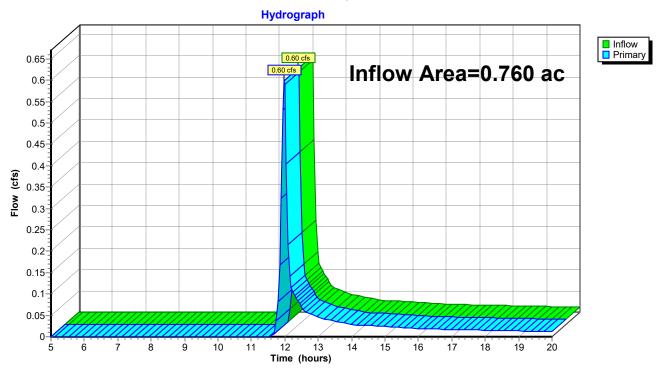
Inflow Area = 0.760 ac, 60.53% Impervious, Inflow Depth > 0.43" for 1-Year event

Inflow = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af

Primary = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3



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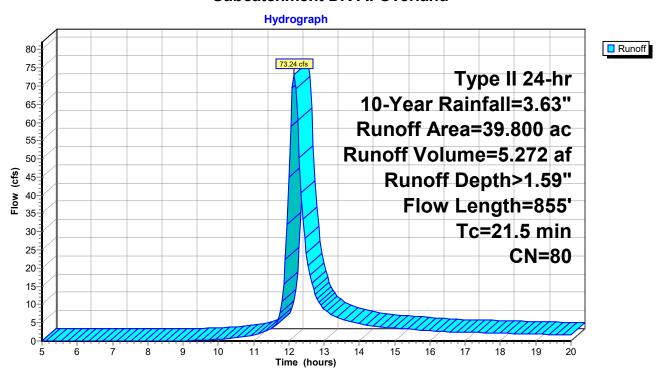
Summary for Subcatchment DR-A: Overland

Runoff = 73.24 cfs @ 12.15 hrs, Volume= 5.272 af, Depth> 1.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac) C	N Desc	cription		
*				ds, Fair, F		
_	ı.			ting Railro		
	39.	800 8	80 Weig	ghted Aver	age	
	38.	700	97.2	4% Pervio	us Area	
	1.	100	2.76	% Impervi	ous Area	
			•			
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
	14.5	150	0.1500	0.17		Sheet Flow, Sheet Flow
						Woods: Light underbrush n= 0.400 P2= 2.67"
	4.8	575	0.1600	2.00		Shallow Concentrated Flow, Shallow Concentrated
		0.0	0.1000	2.00		Woodland Kv= 5.0 fps
	2.2	130	0.0400	1.00		Shallow Concentrated Flow, Shallow Concentrated
	2.2	100	0.0400	1.00		Woodland Kv= 5.0 fps
_						vvoodiand itv- 3.0 ips
	21.5	855	Total			

Subcatchment DR-A: Overland



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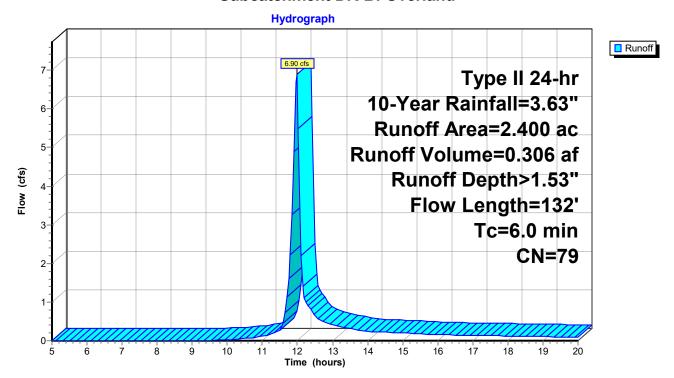
Summary for Subcatchment DR-B: Overland

Runoff = 6.90 cfs @ 11.97 hrs, Volume= 0.306 af, Depth> 1.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	cription		
_	2.	400	79	Woo	ds, Fair, F	ISG D	
	2.400 100.00% Pervious Area					ous Area	
	Tc	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	6.0	13	32	•	0.37	•	Direct Entry. Sheet Flow

Subcatchment DR-B: Overland



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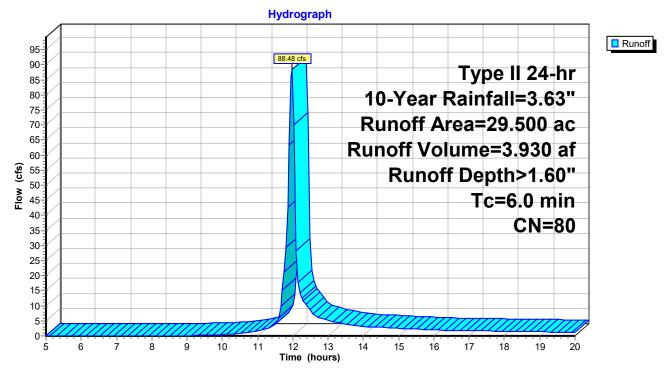
Summary for Subcatchment DR-C: Depression

Runoff = 88.48 cfs @ 11.97 hrs, Volume= 3.930 af, Depth> 1.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

Area (ac) CN Description						
3	.970	77	Brus	h, Fair, HS	G D	
2.500 96 Gravel surface, HSG D						
23	.030	79	Woo	ds, Fair, H	ISG D	
29	29.500 80 Weighted Average					
29	.500		100.	00% Pervi	ous Area	
-			01		.	D
Tc	Leng	tn :	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
6.0	•			•		Direct Entry, Min

Subcatchment DR-C: Depression



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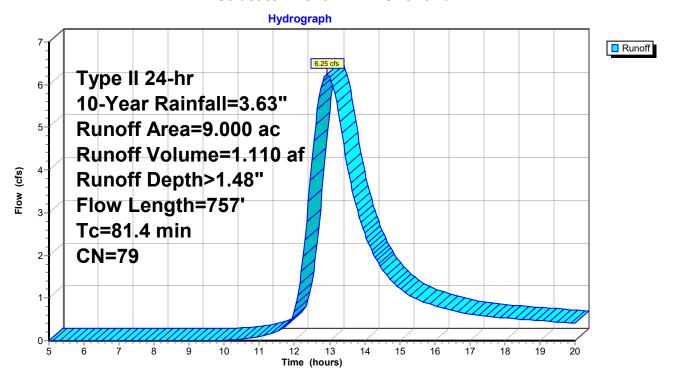
Summary for Subcatchment DR-D: Overland

Runoff = 6.25 cfs @ 12.93 hrs, Volume= 1.110 af, Depth> 1.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area	(ac) C	N Des	cription		
	9.	.000 7	79 Woo	ds, Fair, F	ISG D	
	9.	000	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	56.6	150	0.0050	0.04		Sheet Flow, Sheet Flow
	00.0	507	0.0050	0.05		Woods: Light underbrush n= 0.400 P2= 2.67"
	23.9	507	0.0050	0.35		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
_	0.9	100	0.1300	1.80		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
_	81.4	757	Total			

Subcatchment DR-D: Overland



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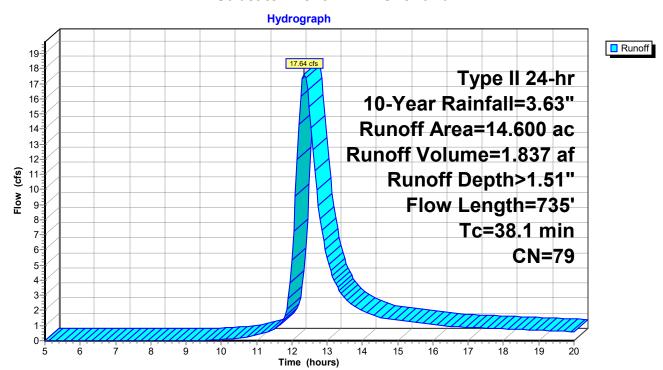
Summary for Subcatchment DR-E: Overland

Runoff = 17.64 cfs @ 12.35 hrs, Volume= 1.837 af, Depth> 1.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac) C	N Des	cription		
	14.	.600 7	79 Woo	ds, Fair, F	ISG D	
	14.	.600	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	27.6	150	0.0300	0.09		Sheet Flow, Sheet Flow
	9.8	510	0.0300	0.87		Woods: Light underbrush n= 0.400 P2= 2.67" Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
_	0.7	75	0.1200	1.73		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
_	38.1	735	Total		•	

Subcatchment DR-E: Overland



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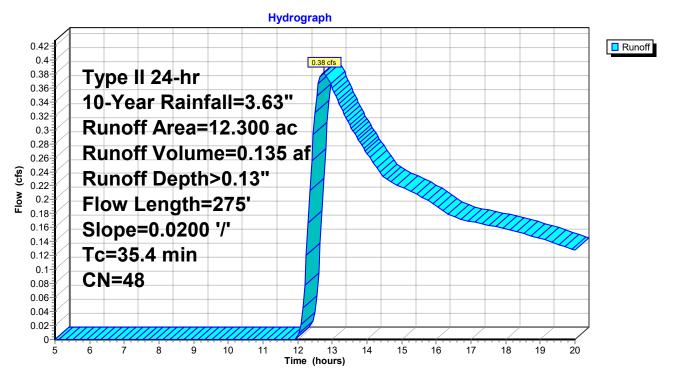
Summary for Subcatchment DR-F: Overland

Runoff = 0.38 cfs @ 12.75 hrs, Volume= 0.135 af, Depth> 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area	(ac)	CN I	Desc	ription		
*	* 1.100 98 Pavement			ment			
_	11.	200	43 \	Woo	ds/grass c	omb., Fair,	, HSG A
12.300 48 Weighted Average					hted Aver	age	
11.200 91.06% Pervious Area					6% Pervio	us Area	
1.100 8.94% Impervious Area				8.949	% Impervi	ous Area	
	Tc (min)	Length (feet		ope t/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	32.5	150	0.02	200	0.08		Sheet Flow,
	2.9	125	5 0.02	200	0.71		Woods: Light underbrush n= 0.400 P2= 2.67" Shallow Concentrated Flow, Woodland Kv= 5.0 fps
	35.4	275	Tota	al			

Subcatchment DR-F: Overland



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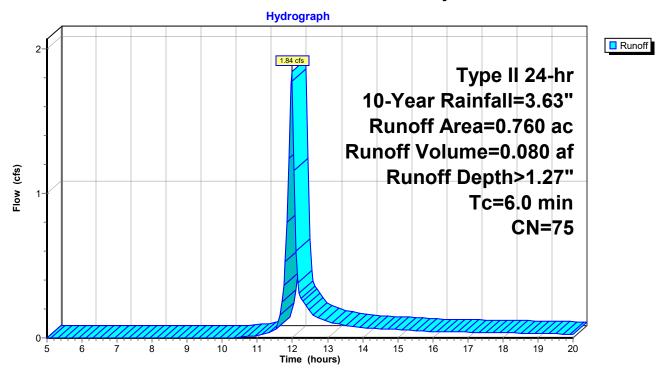
Summary for Subcatchment DR-G: Roadway

1.84 cfs @ 11.98 hrs, Volume= 0.080 af, Depth> 1.27" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

Area (ac) CN Description					ription		
*	0.460 98 Roadway						
	0.	300	39	>759	√ Grass co	over, Good	, HSG A
0.760 75 Weighted Average						age	
0.300 39.47% Pervious Area						us Area	
	0.	460		60.5	3% Imperv	ious Area	
	Tc Length		th :	Slope	Velocity	Capacity	Description
_	(min) (feet) (ft/ft) (ft/sec) (cf			(ft/sec)	(cfs)		
	6.0						Direct Entry, Minimum

Subcatchment DR-G: Roadway



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Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 1.59" for 10-Year event

Inflow = 73.24 cfs @ 12.15 hrs, Volume= 5.272 af

Outflow = 14.53 cfs @ 14.82 hrs, Volume= 3.841 af, Atten= 80%, Lag= 160.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.13 fps, Min. Travel Time= 127.8 min Avg. Velocity = 0.07 fps, Avg. Travel Time= 239.5 min

Peak Storage= 111,494 cf @ 12.69 hrs

Average Depth at Peak Storage= 0.55', Surface Width= 203.32' Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240 Sheet flow over Dense Grass

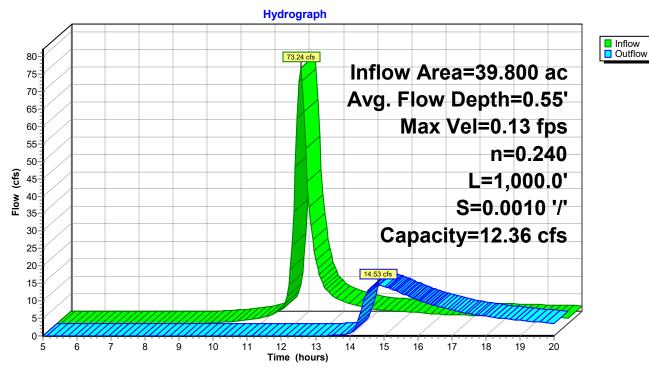
Side Slope Z-value= 3.0 '/' Top Width= 203.00'

Length= 1,000.0' Slope= 0.0010 '/'

Inlet Invert= 6.00', Outlet Invert= 5.00'



Reach 1W: Wetland #1 / Analysis Point 1A



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Summary for Reach 2R: Outlet Pipe

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 1.16" for 10-Year event

Inflow = 14.53 cfs @ 14.82 hrs, Volume= 3.841 af

Outflow = 14.53 cfs @ 14.83 hrs, Volume= 3.838 af, Atten= 0%, Lag= 0.3 min

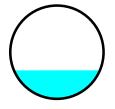
Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.38 fps, Min. Travel Time= 0.2 min Avg. Velocity = 3.89 fps, Avg. Travel Time= 0.3 min

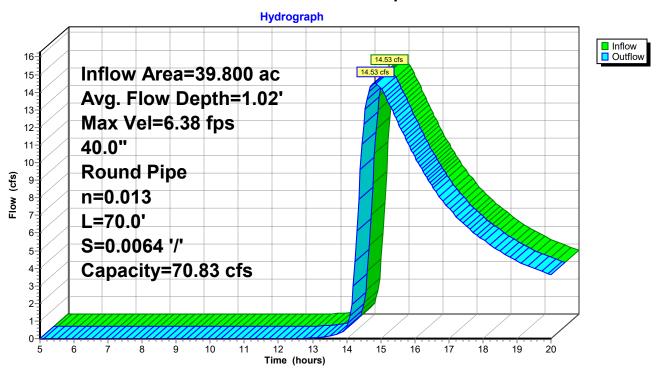
Peak Storage= 159 cf @ 14.82 hrs

Average Depth at Peak Storage= 1.02', Surface Width= 3.08' Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe n= 0.013 Corrugated PE, smooth interior Length= 70.0' Slope= 0.0064 '/' Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 2R: Outlet Pipe



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Summary for Pond 1P: Infiltration

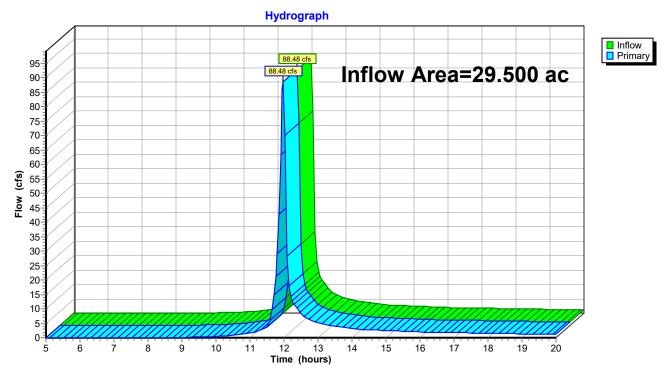
Inflow Area = 29.500 ac, 0.00% Impervious, Inflow Depth > 1.60" for 10-Year event

Inflow = 88.48 cfs @ 11.97 hrs, Volume= 3.930 af

Primary = 88.48 cfs @ 11.97 hrs, Volume= 3.930 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond 1P: Infiltration



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Summary for Pond AP-1: Analysis Point #1

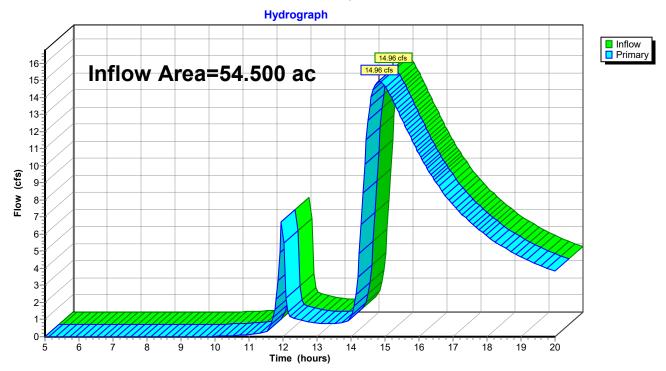
Inflow Area = 54.500 ac, 4.04% Impervious, Inflow Depth > 0.94" for 10-Year event

Inflow = 14.96 cfs @ 14.82 hrs, Volume= 4.279 af

Primary = 14.96 cfs @ 14.82 hrs, Volume= 4.279 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1



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Summary for Pond AP-2: Analysis Point #2

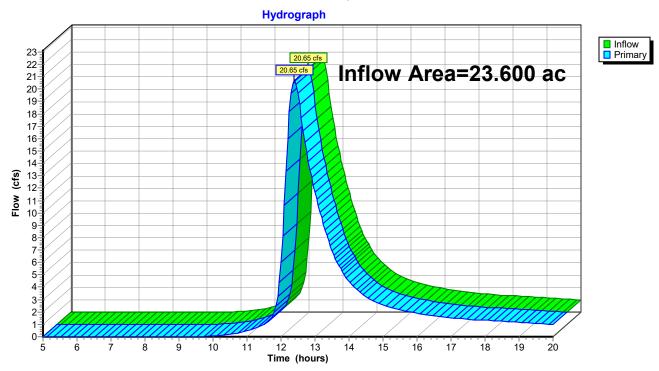
Inflow Area = 23.600 ac, 0.00% Impervious, Inflow Depth > 1.50" for 10-Year event

Inflow = 20.65 cfs @ 12.40 hrs, Volume= 2.947 af

Primary = 20.65 cfs @ 12.40 hrs, Volume= 2.947 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2



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Summary for Pond AP-3: Analysis Point #3

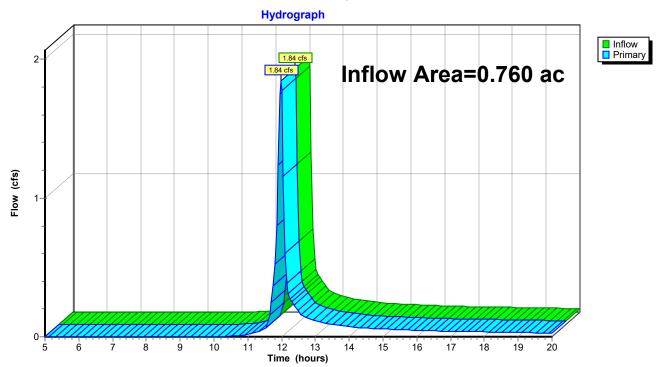
Inflow Area = 0.760 ac, 60.53% Impervious, Inflow Depth > 1.27" for 10-Year event

Inflow = 1.84 cfs @ 11.98 hrs, Volume= 0.080 af

Primary = 1.84 cfs @ 11.98 hrs, Volume= 0.080 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3



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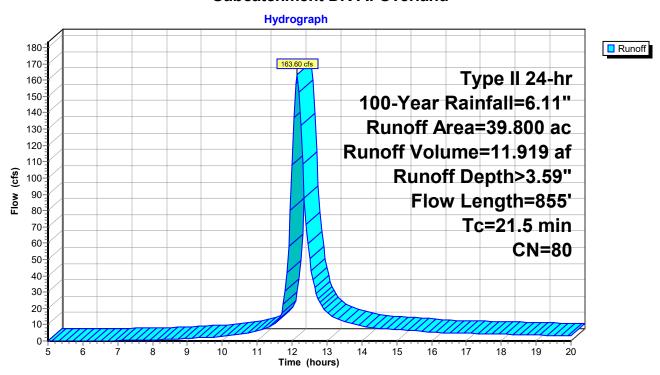
Summary for Subcatchment DR-A: Overland

Runoff = 163.60 cfs @ 12.14 hrs, Volume= 11.919 af, Depth> 3.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

_	Area	(ac) C	N Desc	cription		
	38.700 79 Woods, Fair, HSG D				ISG D	
*	1.	100 9	8 Exis	ting Railro	ad	
	39.	800	0 Weig	ghted Aver	age	
	38.	700	97.2	4% Pervio	us Area	
	1.	100	2.76	% Impervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	14.5	150	0.1500	0.17		Sheet Flow, Sheet Flow
						Woods: Light underbrush n= 0.400 P2= 2.67"
	4.8	575	0.1600	2.00		Shallow Concentrated Flow, Shallow Concentrated
						Woodland Kv= 5.0 fps
	2.2	130	0.0400	1.00		Shallow Concentrated Flow, Shallow Concentrated
						Woodland Kv= 5.0 fps
	21.5	855	Total			

Subcatchment DR-A: Overland



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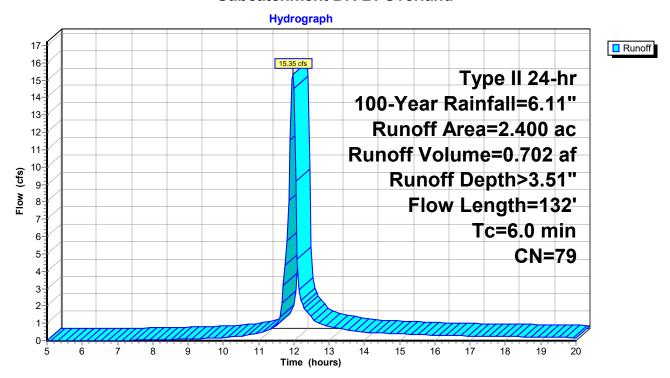
Summary for Subcatchment DR-B: Overland

Runoff = 15.35 cfs @ 11.97 hrs, Volume= 0.702 af, Depth> 3.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
2.400 79 Woods, Fair, HSG D							
_	2.	400		100.	00% Pervi	ous Area	
	Tc	Lengt	:h :	Slope	Velocity	Capacity	Description
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
	6.0	13	2		0.37		Direct Entry, Sheet Flow

Subcatchment DR-B: Overland



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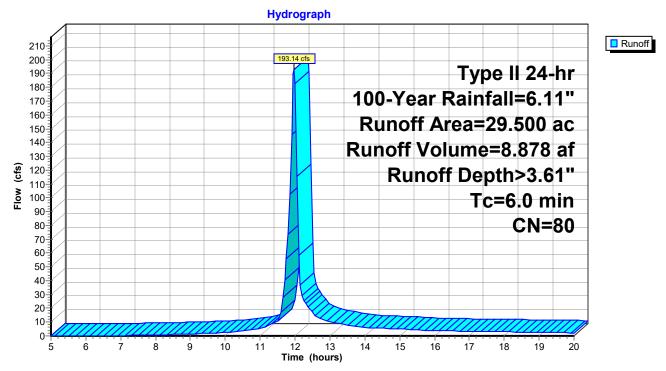
Summary for Subcatchment DR-C: Depression

Runoff = 193.14 cfs @ 11.97 hrs, Volume= 8.878 af, Depth> 3.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

Area (ac) CN Description						
3	.970	77	Brus	h, Fair, HS	G D	
2.500 96 Gravel surface, HSG D						
23	.030	79	Woo	ds, Fair, H	ISG D	
29	29.500 80 Weighted Average					
29	.500		100.	00% Pervi	ous Area	
-			01		.	D
Tc	Leng	tn :	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
6.0	•			•		Direct Entry, Min

Subcatchment DR-C: Depression



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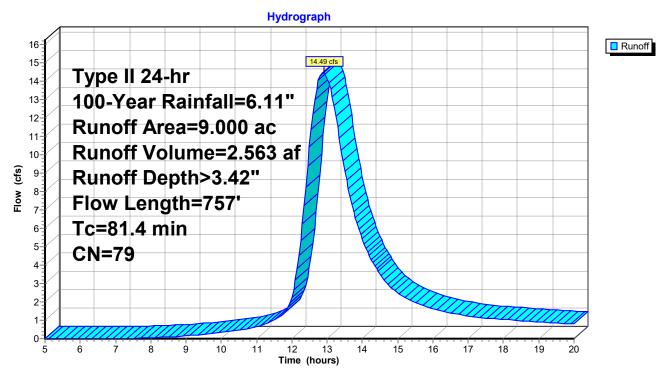
Summary for Subcatchment DR-D: Overland

Runoff = 14.49 cfs @ 12.90 hrs, Volume= 2.563 af, Depth> 3.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

_	Area	(ac) C	N Des	cription		
	9.	.000 7	79 Woo	ds, Fair, F	ISG D	
	9.	000	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	56.6	150	0.0050	0.04		Sheet Flow, Sheet Flow
	00.0	507	0.0050	0.05		Woods: Light underbrush n= 0.400 P2= 2.67"
	23.9	507	0.0050	0.35		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
_	0.9	100	0.1300	1.80		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
_	81.4	757	Total			

Subcatchment DR-D: Overland



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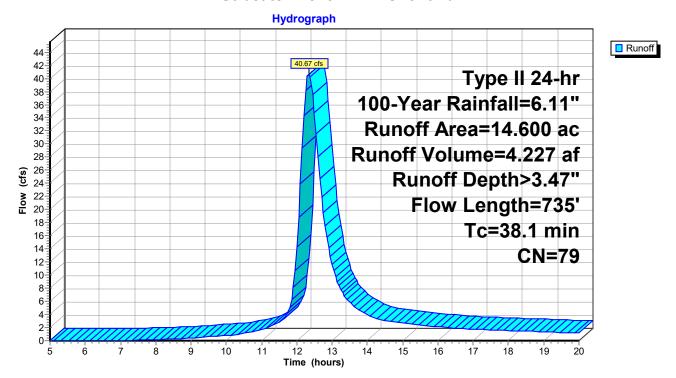
Summary for Subcatchment DR-E: Overland

Runoff = 40.67 cfs @ 12.34 hrs, Volume= 4.227 af, Depth> 3.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

Area	(ac) C	N Des	cription		
14.	.600 7	79 Woo	ds, Fair, F	ISG D	
14.	.600	100.	00% Pervi	ous Area	
Tc (min) 27.6	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
27.6	150	0.0300	0.09		Sheet Flow, Sheet Flow
9.8	510	0.0300	0.87		Woods: Light underbrush n= 0.400 P2= 2.67" Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
0.7	75	0.1200	1.73		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
38 1	735	Total			

Subcatchment DR-E: Overland



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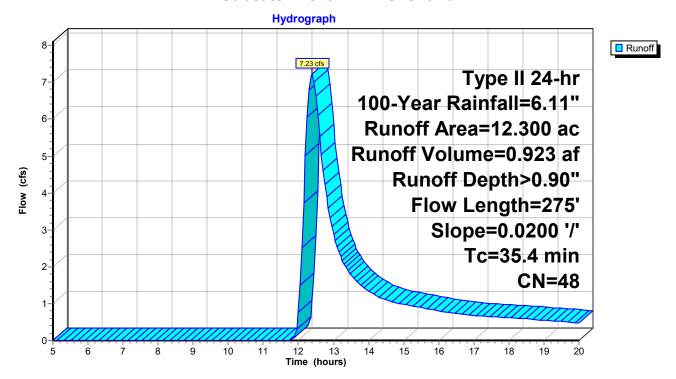
Summary for Subcatchment DR-F: Overland

Runoff = 7.23 cfs @ 12.39 hrs, Volume= 0.923 af, Depth> 0.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

_	Area	(ac)	CN E	Desc	ription			
*	* 1.100 98 Pavement							
_	11.200 43			Woods/grass comb., Fair, HSG A				
12.300 48 Weighted Average					hted Aver	age		
11.200 91.06% Pervious Area						us Area		
	1.100 8.94% Impervious Area							
_	Tc (min)	Length (feet)		pe /ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	32.5	150	0.02	00	0.08		Sheet Flow,	
_	2.9 125		0.02	00	0.71		Woods: Light underbrush n= 0.400 P2= 2.67" Shallow Concentrated Flow, Woodland Kv= 5.0 fps	
	35.4	275	Tota		•	•		

Subcatchment DR-F: Overland



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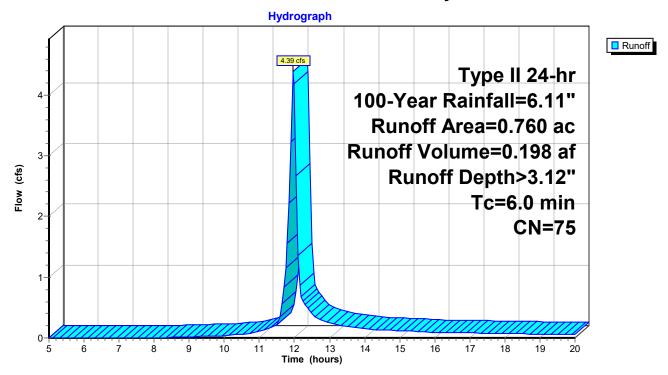
Summary for Subcatchment DR-G: Roadway

Runoff = 4.39 cfs @ 11.97 hrs, Volume= 0.198 af, Depth> 3.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area (ac) CN Description								
*	0.	460	98	Road	dway				
	0.	300	39	>759	√ Grass co	over, Good	, HSG A		
	0.760 75 Weighted Average					age			
	0.300			39.4	39.47% Pervious Area				
	0.460		60.53% Impervious Area			ious Area			
	Тс	Leng	th :	Slope	Velocity	Capacity	Description		
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)			
	6.0						Direct Entry, Minimum		

Subcatchment DR-G: Roadway



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Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 3.59" for 100-Year event

Inflow = 163.60 cfs @ 12.14 hrs, Volume= 11.919 af

Outflow = 41.52 cfs @ 14.21 hrs, Volume= 9.967 af, Atten= 75%, Lag= 123.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.17 fps, Min. Travel Time= 98.2 min Avg. Velocity = 0.08 fps, Avg. Travel Time= 203.6 min

Peak Storage= 244,871 cf @ 12.57 hrs

Average Depth at Peak Storage= 1.21', Surface Width= 207.26' Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240 Sheet flow over Dense Grass

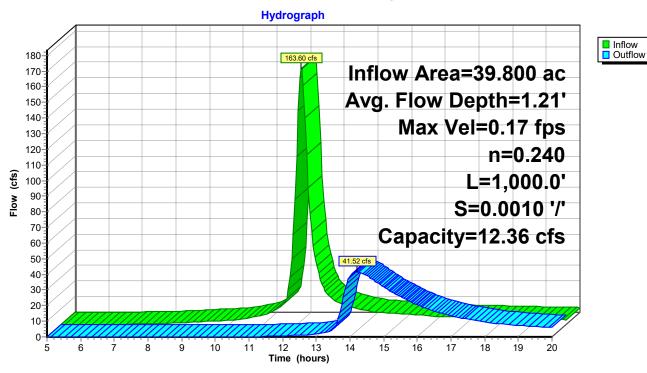
Side Slope Z-value= 3.0 '/' Top Width= 203.00'

Length= 1,000.0' Slope= 0.0010 '/'

Inlet Invert= 6.00', Outlet Invert= 5.00'



Reach 1W: Wetland #1 / Analysis Point 1A



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Summary for Reach 2R: Outlet Pipe

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 3.01" for 100-Year event

Inflow = 41.52 cfs @ 14.21 hrs, Volume= 9.967 af

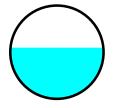
Outflow = 41.52 cfs @ 14.21 hrs, Volume= 9.964 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

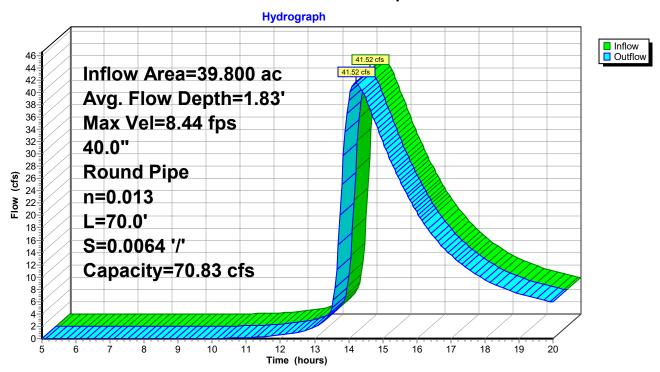
Max. Velocity= 8.44 fps, Min. Travel Time= 0.1 min Avg. Velocity = 4.38 fps, Avg. Travel Time= 0.3 min

Peak Storage= 345 cf @ 14.21 hrs Average Depth at Peak Storage= 1.83', Surface Width= 3.32' Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe n= 0.013 Corrugated PE, smooth interior Length= 70.0' Slope= 0.0064 '/' Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 2R: Outlet Pipe



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Summary for Pond 1P: Infiltration

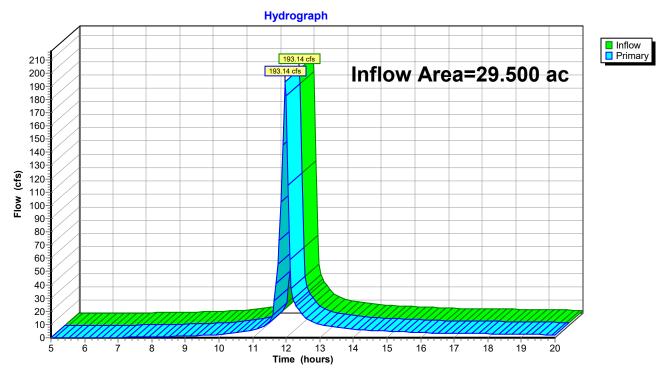
Inflow Area = 29.500 ac, 0.00% Impervious, Inflow Depth > 3.61" for 100-Year event

Inflow = 193.14 cfs @ 11.97 hrs, Volume= 8.878 af

Primary = 193.14 cfs @ 11.97 hrs, Volume= 8.878 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond 1P: Infiltration



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Summary for Pond AP-1: Analysis Point #1

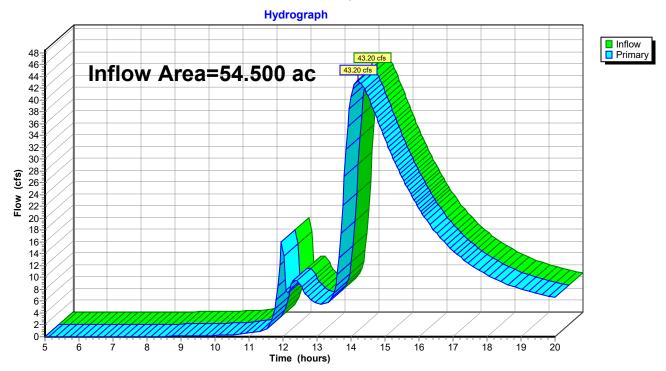
Inflow Area = 54.500 ac, 4.04% Impervious, Inflow Depth > 2.55" for 100-Year event

Inflow = 43.20 cfs @ 14.20 hrs, Volume= 11.589 af

Primary = 43.20 cfs @ 14.20 hrs, Volume= 11.589 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1



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Summary for Pond AP-2: Analysis Point #2

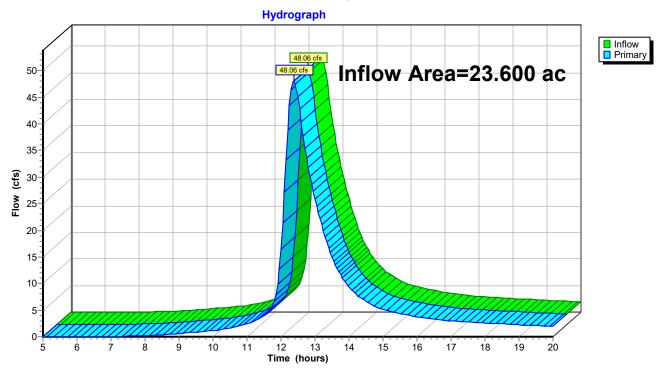
Inflow Area = 23.600 ac, 0.00% Impervious, Inflow Depth > 3.45" for 100-Year event

Inflow = 48.06 cfs @ 12.38 hrs, Volume= 6.789 af

Primary = 48.06 cfs @ 12.38 hrs, Volume= 6.789 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2



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Summary for Pond AP-3: Analysis Point #3

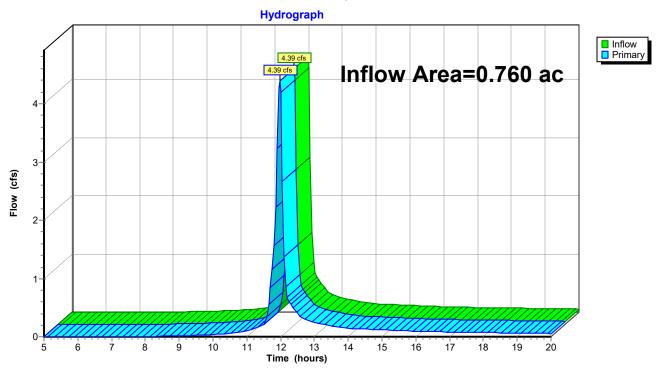
Inflow Area = 0.760 ac, 60.53% Impervious, Inflow Depth > 3.12" for 100-Year event

Inflow = 4.39 cfs @ 11.97 hrs, Volume= 0.198 af

Primary = 4.39 cfs @ 11.97 hrs, Volume= 0.198 af, Atten= 0%, Lag= 0.0 min

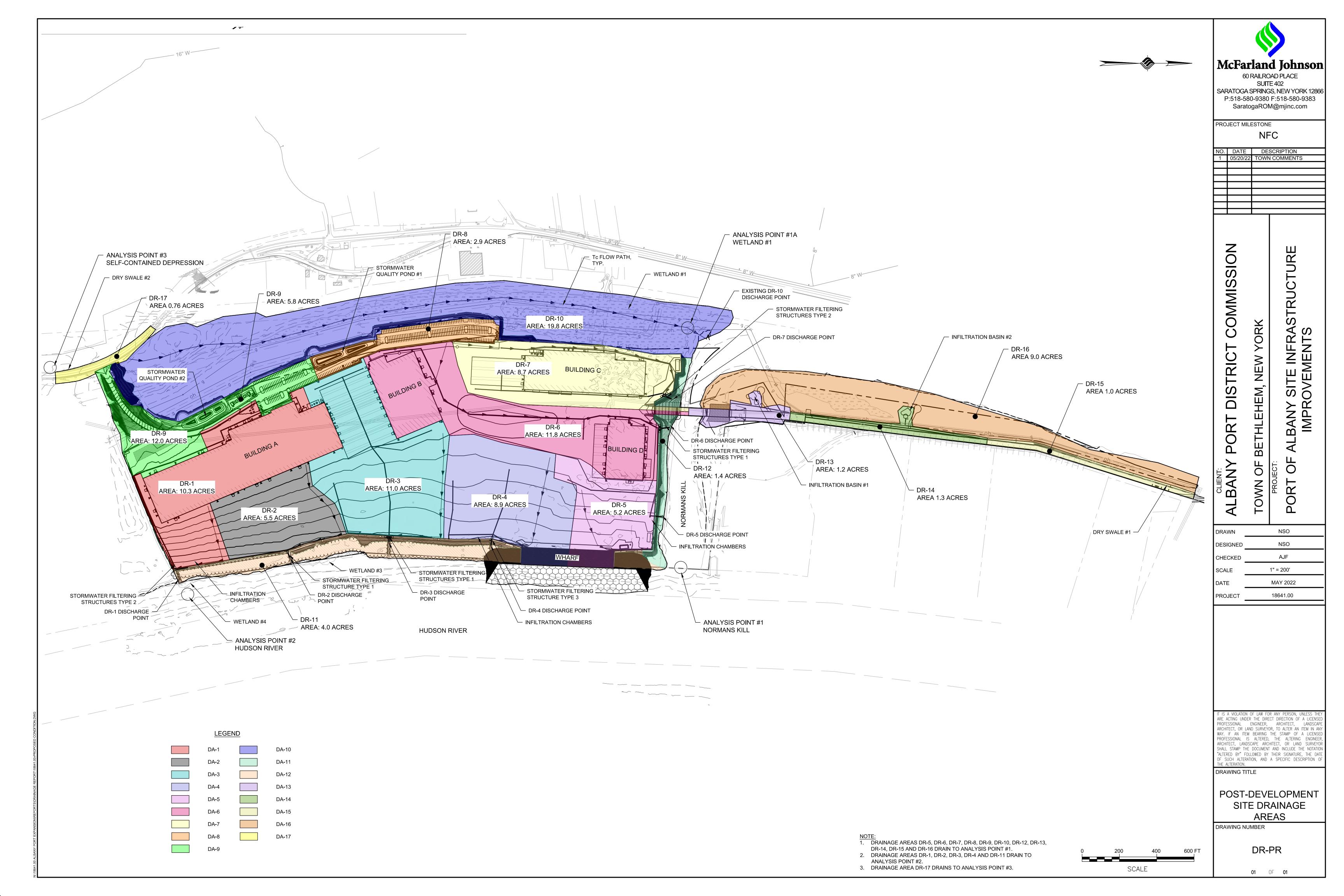
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

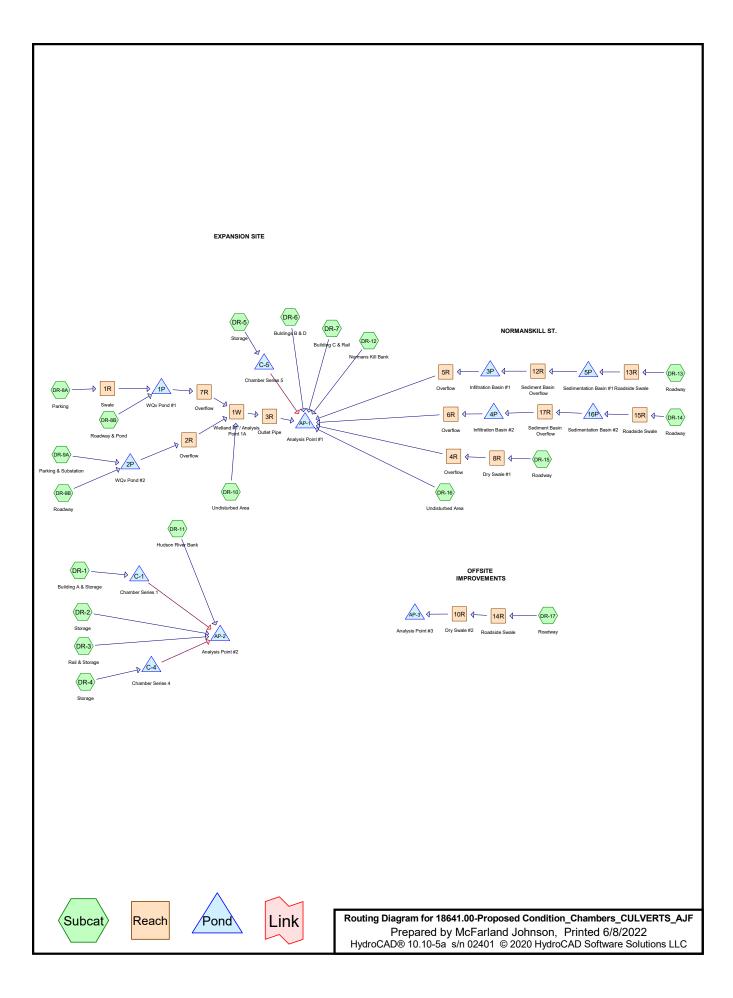
Pond AP-3: Analysis Point #3



Appendix B

Proposed Conditions Drainage Map and HydroCAD Report





18641.00-Proposed Condition_Chambers_CULVERTS_AJF Prepared by McFarland Johnson HydroCAD® 10.10-5a s/n 02401 © 2020 HydroCAD Software Solutions LLC

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Rainfall Events Listing (selected events)

Event#		Event	Storm Type	Curve	Mode	Duration	B/B	Depth	AMC
		Name				(hours)		(inches)	
	1	1-Year	Type II 24-hr		Default	24.00	1	2.20	2
	2	10-Year	Type II 24-hr		Default	24.00	1	3.63	2
	3	100-Year	Type II 24-hr		Default	24.00	1	6.11	2

18641.00-Proposed Condition_Chambers_CULVERTS_AJF
Prepared by McFarland Johnson
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Area Listing (all nodes)

Area	CN	Description			
(acres)		(subcatchment-numbers)			
1.510	39	>75% Grass cover, Good, HSG A (DR-13, DR-14, DR-15, DR-17)			
5.500	80	>75% Grass cover, Good, HSG D (DR-1, DR-2, DR-3, DR-4, DR-5, DR-6, DR-7,			
		DR-8A, DR-8B, DR-9A, DR-9B)			
6.870	98	Building A (DR-1)			
2.549	98	Building B (DR-6)			
3.030	98	Building C (DR-7)			
1.413	98	Building D (DR-6)			
16.900	95	Compacted Gravel (DR-3, DR-4)			
0.200	92	Compacted Gravel (DR-9A)			
26.618	95	Dense Graded Aggregate (DR-1, DR-2, DR-5, DR-6, DR-7, DR-9B)			
0.970	96	Gravel surface, HSG D (DR-12)			
1.100	98	Mill & Fill of Old Pavement (DR-14, DR-15)			
0.600	98	New Pavement (DR-14, DR-15)			
1.600	98	Parking (DR-8A)			
1.200	98	Parking and Road (DR-9A)			
0.450	98	Pavement (DR-13)			
3.270	98	Rail (DR-3, DR-7)			
0.140	98	Road Widening (DR-17)			
1.240	98	Roadway (DR-17, DR-8B, DR-9B)			
0.170	98	Substation (DR-9A)			
24.230	79	Woods, Fair, HSG D (DR-10, DR-11, DR-12)			
9.000	43	Woods/grass comb., Fair, HSG A (DR-16)			
108.560	86	TOTAL AREA			

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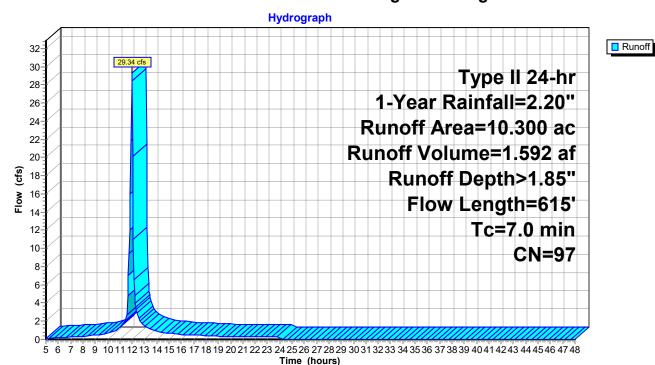
Summary for Subcatchment DR-1: Building A & Storage

Runoff = 29.34 cfs @ 11.98 hrs, Volume= 1.592 af, Depth> 1.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac) (CN D	escription				
*	6.	870 98 Building A						
	0.100 80 >75% Grass cover, Good, HSG D							
*	3.	330	95 D	Dense Graded Aggregate				
	10.300 97		97 W	eighted Ave	rage			
	3.	430		3.30% Pervi	0			
	6.	870	60	6.70% Imper	vious Area			
				·				
	Tc	Length	Slop	e Velocity	Capacity	Description		
	(min)	(feet)	(ft/	t) (ft/sec)	(cfs)			
	3.3	100	0.010	0.50		Sheet Flow,		
						n= 0.023 P2= 2.40"		
	3.1	300	0.010	0 1.61		Shallow Concentrated Flow,		
						Unpaved Kv= 16.1 fps		
	0.6	215	0.005	5.91	29.00	Pipe Channel,		
						30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'		
						n= 0.013		
	7.0	615	Total					

Subcatchment DR-1: Building A & Storage



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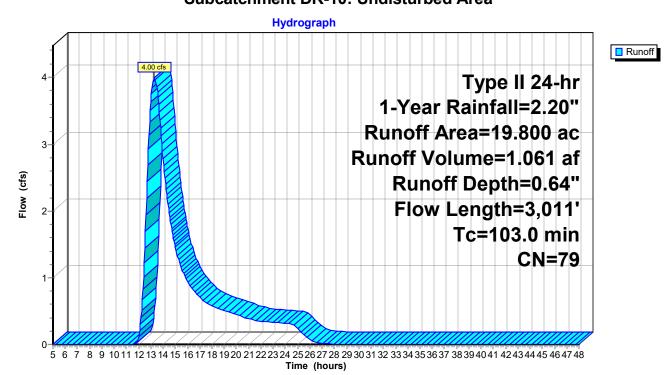
Summary for Subcatchment DR-10: Undisturbed Area

Runoff = 4.00 cfs @ 13.29 hrs, Volume= 1.061 af, Depth= 0.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

Area (ac) CN Description							
19.	800 7	'9 Woo	ds, Fair, F	ISG D			
19.	800	100.	00% Pervi	ous Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
19.7	150	0.0800	0.13		Sheet Flow,		
3.0	200	0.0500	1.12		Woods: Light underbrush n= 0.400 P2= 2.40" Shallow Concentrated Flow,		
0.0	200	0.0000	1.12		Woodland Kv= 5.0 fps		
1.6	250	0.2600	2.55		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
78.7	2,361	0.0100	0.50		Shallow Concentrated Flow, Wetland Flow		
0.0	50	0.0500	22.86	161.57	Woodland Kv= 5.0 fps Pipe Channel,		
0.0	30	0.0300	22.00	101.57	36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'		
					n= 0.012 Corrugated PP, smooth interior		
103.0	3,011	Total					

Subcatchment DR-10: Undisturbed Area



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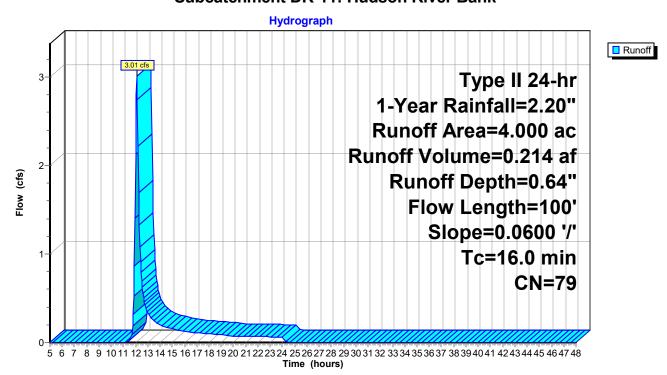
Summary for Subcatchment DR-11: Hudson River Bank

Runoff = 3.01 cfs @ 12.10 hrs, Volume= 0.214 af, Depth= 0.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac) C	N Desc	cription					
	4.000 79 Woods, Fair, HSG D								
_	4.	000	100.	00% Pervi					
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	16.0	100	0.0600	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"			

Subcatchment DR-11: Hudson River Bank



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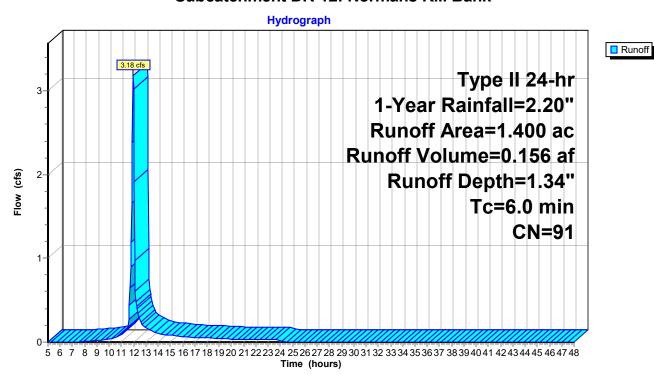
Summary for Subcatchment DR-12: Normans Kill Bank

Runoff = 3.18 cfs @ 11.97 hrs, Volume= 0.156 af, Depth= 1.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

_	Area	(ac)	CN	Desc	cription		
	0.	430	79	Woo	ds, Fair, H	ISG D	
_	0.	.970	96	Grav	el surface	, HSG D	
	1.	400	91	Weig	ghted Aver	age	
	1.	.400		100.	00% Pervi	ous Area	
	Tc	Leng	th	Slope	Velocity	Capacity	Description
_	(min) (feet)		(ft/ft)	(ft/sec)	(cfs)		
	6.0						Direct Entry, Minimum

Subcatchment DR-12: Normans Kill Bank



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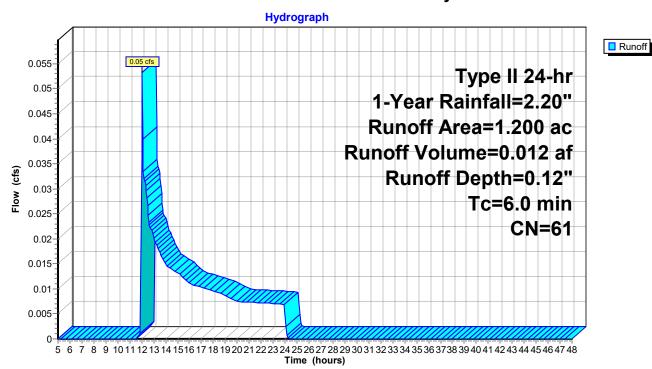
Summary for Subcatchment DR-13: Roadway

Runoff = 0.05 cfs @ 12.05 hrs, Volume= 0.012 af, Depth= 0.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac)	CN	Desc	cription						
*	0.	450	98	Pave	Pavement						
	0.	750	39	>75%	√ Grass co	over, Good	, HSG A				
	1.200 61 Weighted Average										
	0.750 62.50% Pervious Area										
	0.450			37.5	0% Imperv	ious Area					
	Тс	Leng	th :	Slope	Velocity	Capacity	Description				
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)					
	6.0						Direct Entry, Min				

Subcatchment DR-13: Roadway



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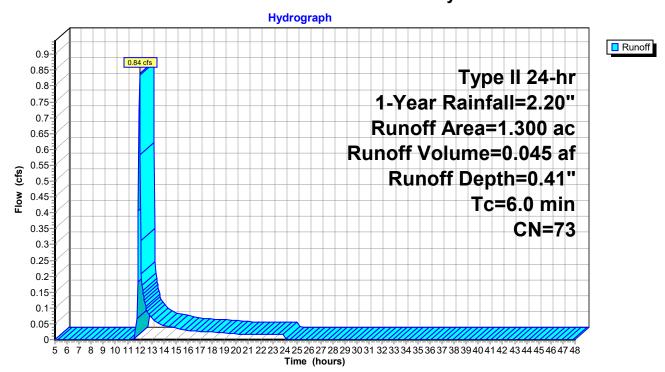
Summary for Subcatchment DR-14: Roadway

Runoff = 0.84 cfs @ 11.99 hrs, Volume= 0.045 af, Depth= 0.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac)	CN	Desc	cription							
*	0.	550	98	New	New Pavement							
	0.	550	39	>75%	75% Grass cover, Good, HSG A							
*	0.	200	98	Mill 8	lill & Fill of Old Pavement							
	1.	300	73	Weig	ghted Aver	age						
	0.	550		42.3	1% Pervio	us Area						
	0.	750		57.69	9% Imperv	ious Area						
	т.		41.	01	V/-126	0	D					
	Tc	Leng		Slope	Velocity	Capacity	Description					
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
	6.0						Direct Entry, Min					

Subcatchment DR-14: Roadway



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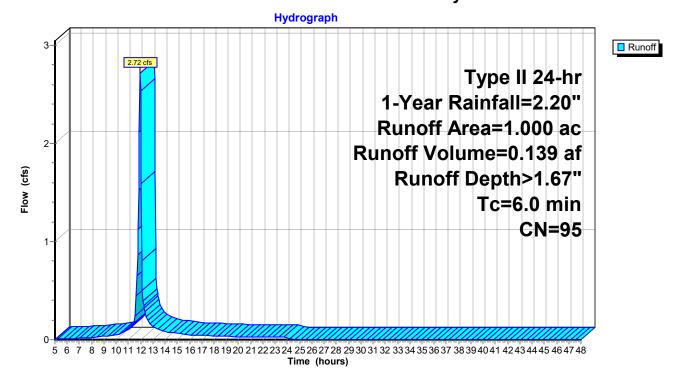
Summary for Subcatchment DR-15: Roadway

Runoff = 2.72 cfs @ 11.96 hrs, Volume= 0.139 af, Depth> 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac)	CN	Desc	cription							
*	0.	050	98	New	New Pavement							
	0.	050	39	>75%	75% Grass cover, Good, HSG A							
*	0.	900	98	Mill 8	ill & Fill of Old Pavement							
	1.	.000 95 Weighted Average										
	0.	050		5.00	% Perviou	s Area						
	0.	950		95.0	0% Imperv	ious Area						
	_											
	Tc	Leng	ıth	Slope	Velocity	Capacity	Description					
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
	6.0						Direct Entry, Min					

Subcatchment DR-15: Roadway



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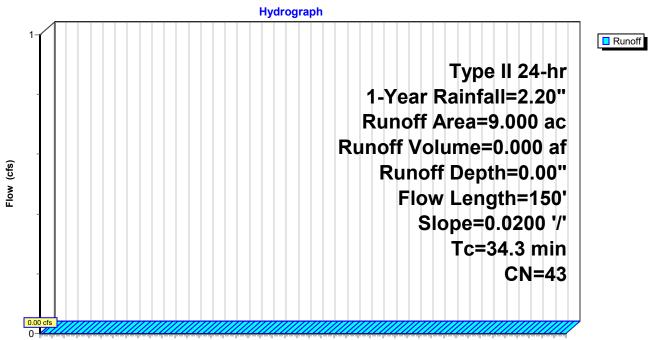
Summary for Subcatchment DR-16: Undisturbed Area

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac) C	N Desc	cription				
	9.000 43 Woods/grass comb., Fair, HSG A							
	9.000 100.00% Pervious Area							
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	_	
	34.3	150	0.0200	0.07		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"		

Subcatchment DR-16: Undisturbed Area



5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 Time (hours)

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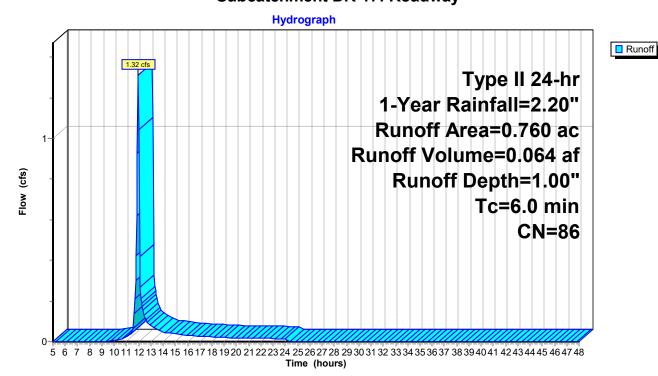
Summary for Subcatchment DR-17: Roadway

Runoff = 1.32 cfs @ 11.97 hrs, Volume= 0.064 af, Depth= 1.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

_	Area	(ac)	CN	Desc	Description							
*	0.	140	98	Road	Road Widening							
*	0.	460	98	Road	Roadway							
	0.	160	39	>75%	% Grass co	over, Good	, HSG A					
	0.	760	86	Weig	ghted Aver	age						
	0.	160		21.0	5% Pervio	us Area						
	0.	600		78.9	5% Imperv	ious Area						
	_	_										
	Тс	Leng		Slope	Velocity	Capacity	Description					
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
	6.0						Direct Entry, Minimum					

Subcatchment DR-17: Roadway



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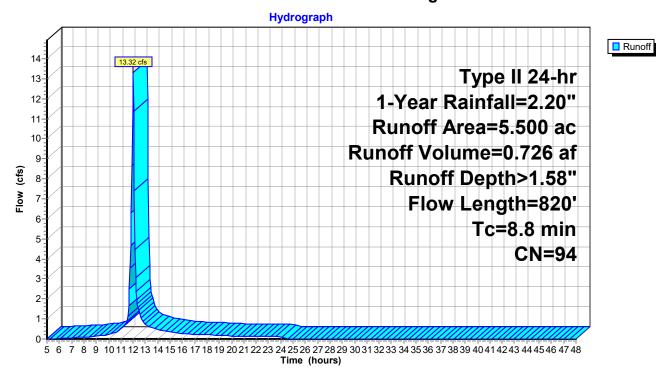
Summary for Subcatchment DR-2: Storage

Runoff = 13.32 cfs @ 12.00 hrs, Volume= 0.726 af, Depth> 1.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

_	Area (ac)		N Desc	I Description		
*	5.	300	5 Dens	se Graded	Aggregate	
	0.	200 8	30 >759	% Grass co	over, Good	, HSG D
	5.	500 9	4 Weig	ghted Aver	age	
	5.	500	100.	00% Pervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	100	0.0100	0.50		Sheet Flow,
						n= 0.023 P2= 2.40"
	4.9	470	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.6	250	0.0050	6.67	47.16	Pipe Channel,
						36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
_						n= 0.013
	8.8	820	Total			

Subcatchment DR-2: Storage



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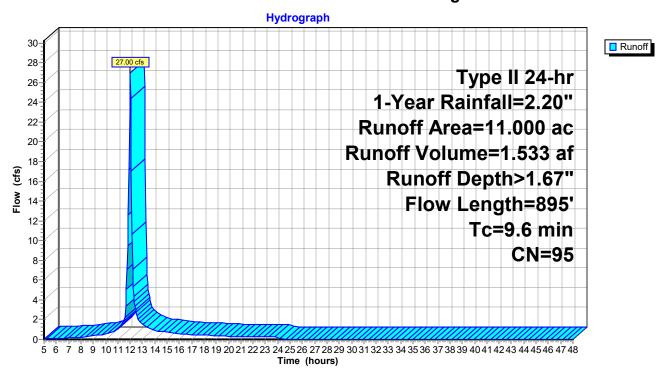
Summary for Subcatchment DR-3: Rail & Storage

Runoff = 27.00 cfs @ 12.01 hrs, Volume= 1.533 af, Depth> 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac) (CN Des	cription						
*	8.	300	95 Cor	Compacted Gravel						
	0.	400	80 >75	>75% Grass cover, Good, HSG D						
*	2.	300		Rail						
	11.	000	95 We	Weighted Average						
	8.	700	79.0	9% Pervio	us Area					
	2.	300	20.9	91% Imperv	vious Area					
				•						
	Tc	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.3	100	0.0100	0.50		Sheet Flow,				
						n= 0.023 P2= 2.40"				
	5.4	525	0.0100	1.61		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0.9	270	0.0050	5.09	16.00	Pipe Channel,				
						24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'				
						n= 0.013				
	9.6	895	Total							

Subcatchment DR-3: Rail & Storage



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Runoff

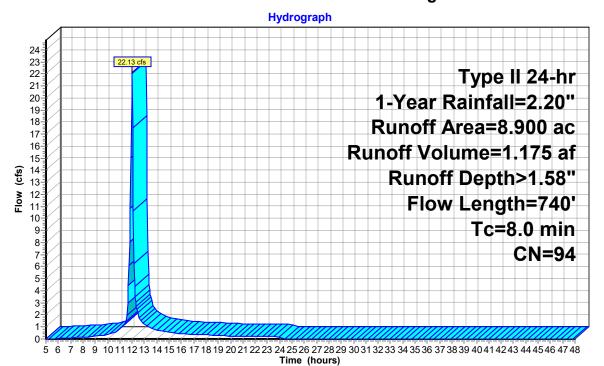
Summary for Subcatchment DR-4: Storage

Runoff = 22.13 cfs @ 11.99 hrs, Volume= 1.175 af, Depth> 1.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

_	Area	(ac) C	N Desc	Description		
*	8.	600 9	5 Com	pacted Gr	avel	
	0.	300 8	30 >759	∕⁄ Grass co	over, Good	, HSG D
	8.	900 9	4 Weig	ghted Aver	age	
	8.	900	100.	00% Pervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	100	0.0100	0.50		Sheet Flow,
						n= 0.023 P2= 2.40"
	4.1	400	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.6	240	0.0050	6.67	47.16	Pipe Channel,
						36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
						n= 0.013 Corrugated PE, smooth interior
	8.0	740	Total			

Subcatchment DR-4: Storage



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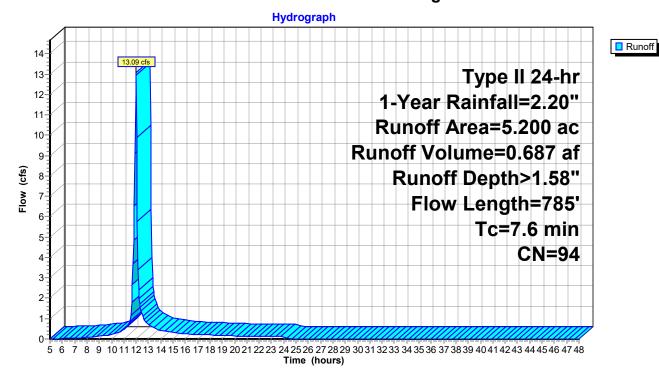
Summary for Subcatchment DR-5: Storage

Runoff = 13.09 cfs @ 11.99 hrs, Volume= 0.687 af, Depth> 1.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac) C	N Desc	cription		
*	4.	900	95 Dens	se Graded	Aggregate	
	0.	300 8	30 >759	% Grass c	over, Good	, HSG D
	5.200 94 Weighted Average				age	
	5.200			00% Pervi		
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	100	0.0100	0.50		Sheet Flow,
						n= 0.023 P2= 2.40"
	3.0	285	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	1.3	400	0.0050	5.09	16.00	Pipe Channel,
						24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
_						n= 0.013
	7.6	785	Total			

Subcatchment DR-5: Storage



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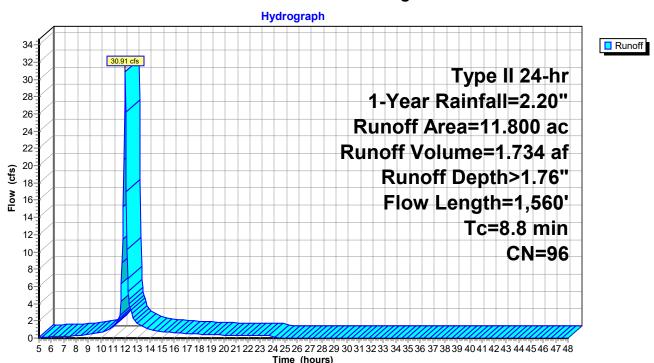
Summary for Subcatchment DR-6: Buldings B & D

Runoff = 30.91 cfs @ 12.00 hrs, Volume= 1.734 af, Depth> 1.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac)	CN	Desc	cription		
*	2.	549	98	Build	ling B		
*	1.	413	98	Build	ling D		
	0.	200	80	>75%	% Ğrass co	over, Good,	, HSG D
*	7.	638	95	Dens	se Graded	Aggregate	
	11.	800	96	Weid	hted Aver	age	
	7.	838		_	2% Pervio	•	
	3.	962		33.58	8% Imperv	ious Area	
					•		
	Тс	Length	S	lope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
	3.3	100	0.0	100	0.50		Sheet Flow,
							n= 0.023 P2= 2.40"
	1.0	100	0.0	100	1.61		Shallow Concentrated Flow,
							Unpaved Kv= 16.1 fps
	4.5	1,360	0.0	050	5.09	16.00	Pipe Channel,
		·					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
							n= 0.013
· <u></u>	8.8	1,560	То	tal	•		

Subcatchment DR-6: Buldings B & D



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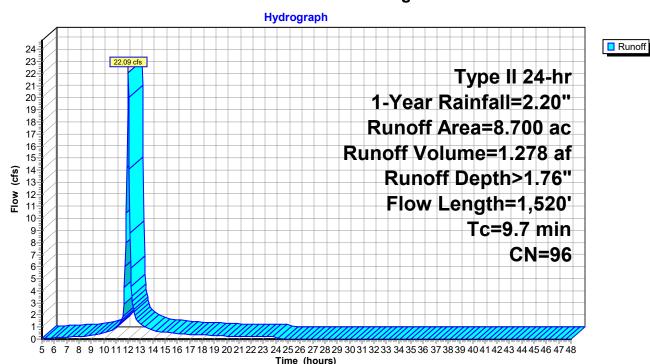
Summary for Subcatchment DR-7: Building C & Rail

Runoff = 22.09 cfs @ 12.01 hrs, Volume= 1.278 af, Depth> 1.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac)	CN	Desc	cription		
*	3.	030	0 98 Building C				
*	0.	970	98	Rail	· ·		
*	4.	400	95	Dens	se Graded	Aggregate	
	0.	300	80	>75%	√ Grass co	over, Good,	HSG D
	8.	700	96	Weig	hted Aver	age	
	4.	700			2% Pervio		
	4.	000		45.98	8% Imperv	ious Area	
					•		
	Tc	Lengtl	า ร	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	10	0.	0100	0.50		Sheet Flow,
							n= 0.023 P2= 2.40"
	2.6	25	0.	0100	1.61		Shallow Concentrated Flow,
							Unpaved Kv= 16.1 fps
	3.8	1,17	0.	0050	5.09	16.00	Pipe Channel,
							24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
							n= 0.013
-	9.7	1,52) T	otal			

Subcatchment DR-7: Building C & Rail



18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

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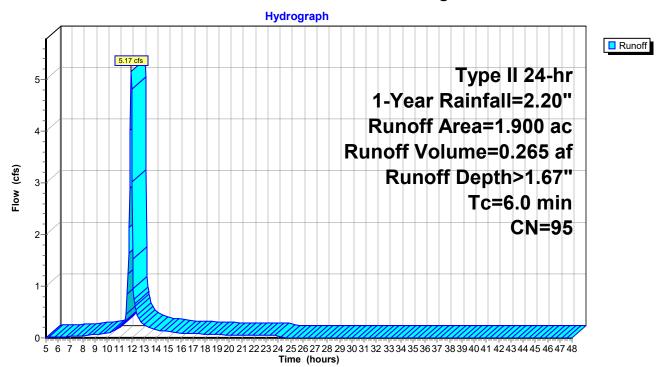
Summary for Subcatchment DR-8A: Parking

Runoff = 5.17 cfs @ 11.96 hrs, Volume= 0.265 af, Depth> 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

_	Area	(ac)	CN	Desc	cription					
*	1.	600	98	Park	Parking					
	0.	300	80	>75%	% Grass co	over, Good	, HSG D			
	1.	900	95	Weig	ghted Aver	age				
	0.300 15.79% Pervious Area					us Area				
	1.600			84.21% Impervious Area						
	Тс	Leng	th	Slope	Velocity	Capacity	Description			
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	6.0						Direct Entry, Minimum			

Subcatchment DR-8A: Parking



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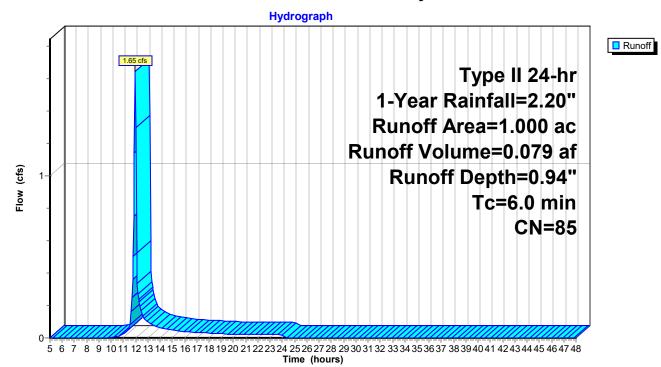
Summary for Subcatchment DR-8B: Roadway & Pond

Runoff = 1.65 cfs @ 11.98 hrs, Volume= 0.079 af, Depth= 0.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

_	Area	(ac)	CN	Desc	cription					
*	0.	300	98	Road	Roadway					
	0.	700	80	>759	√ Grass co	over, Good	, HSG D			
	1.	000	85	Weig	ghted Aver	age				
	0.700 70.00% Pervious Area					us Area				
	0.300			30.00% Impervious Area						
	Tc	Leng		Slope	Velocity	Capacity	Description			
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	6.0						Direct Entry, Minimum			

Subcatchment DR-8B: Roadway & Pond



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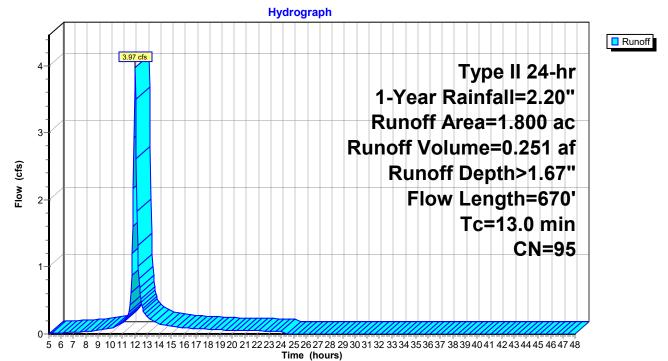
Summary for Subcatchment DR-9A: Parking & Substation

Runoff = 3.97 cfs @ 12.04 hrs, Volume= 0.251 af, Depth> 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac)	CN	Desc	cription		
	0.	230	80	>75%	√ Grass co	over, Good	, HSG D
*	0.	200	92	Com	pacted Gr	avel	
*	1.	200	98	Park	ing and Ro	oad	
*	0.	170	98	Subs	station		
	1.	800	95	Weig	ghted Aver	age	
	0.	430		23.8	9% Pervio	us Area	
	1.	370		76.1	1% Imperv	∕ious Area	
	Tc (min)	Lengtl (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.4	100	0.	0200	1.19		Sheet Flow, Parking Lot Runoff
_	11.6	570	0.0.	0030	0.82		Smooth surfaces n= 0.011 P2= 2.40" Shallow Concentrated Flow, Grass Lined Ditch to Pond Grassed Waterway Kv= 15.0 fps
	13.0	670) To	otal			

Subcatchment DR-9A: Parking & Substation



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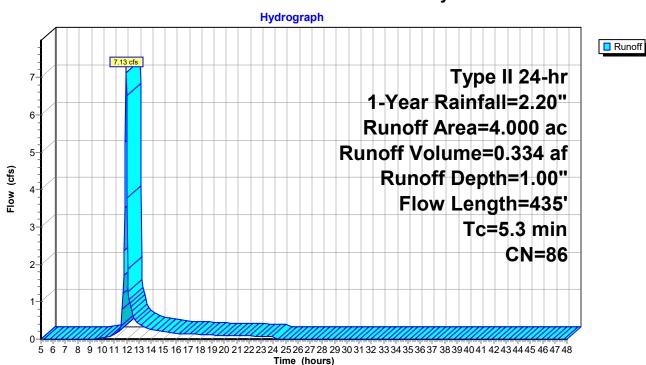
Summary for Subcatchment DR-9B: Roadway

Runoff = 7.13 cfs @ 11.96 hrs, Volume= 0.334 af, Depth= 1.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 1-Year Rainfall=2.20"

	Area	(ac)	CN	Desc	ription		
*	1.	050	95	Dens	se Graded	Aggregate	
*	0.	480	98	Road		00 0	
	2.	470	80	>75%	√6 Grass co	over, Good,	HSG D
	4	000	86	Weig	hted Aver	age	
		520		_)% Pervio	•	
		480			0% Imperv		
	0.	100		12.00	o iniport	100071100	
	Tc	Length	n SI	lope	Velocity	Capacity	Description
	(min)	(feet		ft/ft)	(ft/sec)	(cfs)	2
	3.6	100		250	0.46	()	Sheet Flow, Dense Graded Aggregate Yard
	0.0	100	0.0	200	0.40		n= 0.040 P2= 2.40"
	1.3	230	0 0	100	3.07	9.20	0.0.0
	1.0	200	0.0	100	0.01	3.20	Area= 3.0 sf Perim= 4.0' r= 0.75'
							n= 0.040 Earth, cobble bottom, clean sides
	0.4	105	5 00	050	4.20	7.43	Pipe Channel, driveway culvert
	0.4	100	0.0	000	7.20	7.40	18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
							n= 0.013 Corrugated PE, smooth interior
_	5.3	121	5 Tot	tal			11- 0.010 Corrugated 1 E, Shiboth Interior
	5.5	435	וטו כ	lai			

Subcatchment DR-9B: Roadway



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Summary for Reach 1R: Swale

Inflow Area = 1.900 ac, 84.21% Impervious, Inflow Depth > 1.67" for 1-Year event

Inflow = 5.17 cfs @ 11.96 hrs, Volume= 0.265 af

Outflow = 4.10 cfs @ 12.13 hrs, Volume= 0.265 af, Atten= 21%, Lag= 9.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.75 fps, Min. Travel Time= 6.6 min Avg. Velocity = 0.50 fps, Avg. Travel Time= 22.9 min

Peak Storage= 1,638 cf @ 12.02 hrs

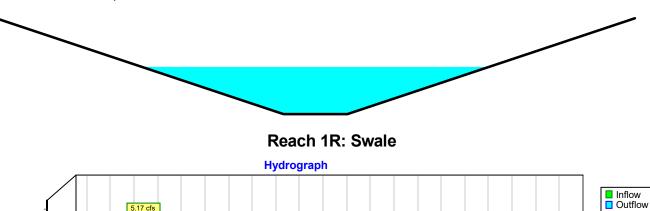
Average Depth at Peak Storage= 0.74', Surface Width= 5.43' Bank-Full Depth= 1.50' Flow Area= 8.3 sf, Capacity= 22.13 cfs

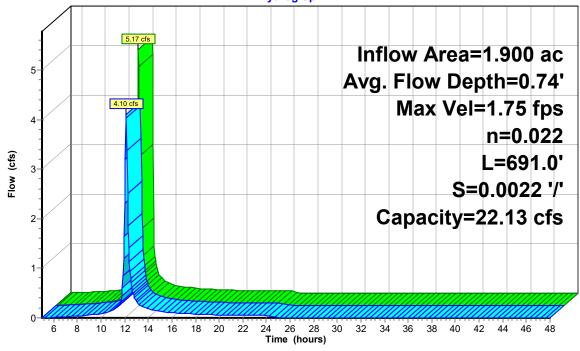
1.00' x 1.50' deep channel, n= 0.022 Earth, clean & straight

Side Slope Z-value= 3.0 '/' Top Width= 10.00'

Length= 691.0' Slope= 0.0022 '/'

Inlet Invert= 15.50', Outlet Invert= 14.00'





18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

Prepared by McFarland Johnson

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Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 0.83" for 1-Year event

Inflow = 4.77 cfs @ 13.30 hrs, Volume= 1.982 af

Outflow = 1.61 cfs @ 21.37 hrs, Volume= 1.851 af, Atten= 66%, Lag= 484.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.05 fps, Min. Travel Time= 305.5 min Avg. Velocity = 0.03 fps, Avg. Travel Time= 568.8 min

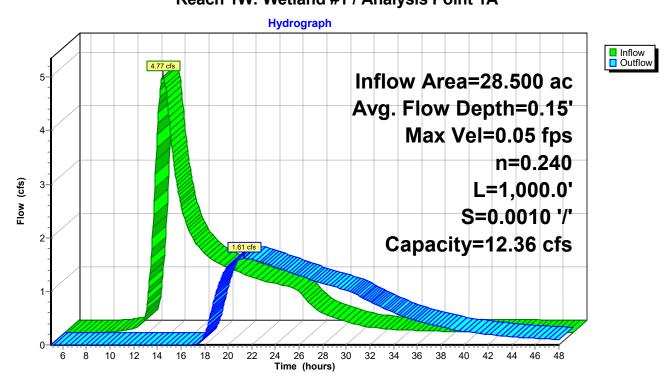
Peak Storage= 29,542 cf @ 16.28 hrs

Average Depth at Peak Storage= 0.15', Surface Width= 200.88' Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240 Side Slope Z-value= 3.0 '/' Top Width= 203.00'

Length= 1,000.0' Slope= 0.0010 '/' Inlet Invert= 6.00', Outlet Invert= 5.00'

Reach 1W: Wetland #1 / Analysis Point 1A



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Summary for Reach 2R: Overflow

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 1.20" for 1-Year event

Inflow = 0.48 cfs @ 13.64 hrs, Volume= 0.581 af

Outflow = 0.48 cfs @ 13.65 hrs, Volume= 0.581 af, Atten= 0%, Lag= 0.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.78 fps, Min. Travel Time= 0.5 min Avg. Velocity = 1.38 fps, Avg. Travel Time= 0.6 min

Peak Storage= 13 cf @ 13.64 hrs

Average Depth at Peak Storage= 0.03', Surface Width= 8.20' Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 569.91 cfs

8.00' x 2.00' deep channel, n= 0.020 Corrugated PE, corrugated interior

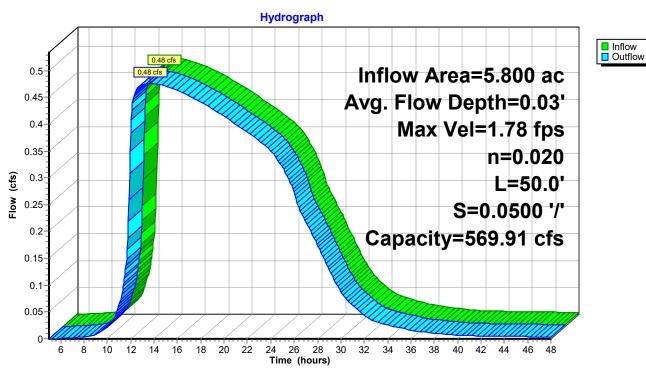
Side Slope Z-value= 3.0 '/' Top Width= 20.00'

Length= 50.0' Slope= 0.0500 '/'

Inlet Invert= 16.50', Outlet Invert= 14.00'



Reach 2R: Overflow



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Summary for Reach 3R: Outlet Pipe

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 0.78" for 1-Year event

Inflow = 1.61 cfs @ 21.37 hrs, Volume= 1.851 af

Outflow = 1.61 cfs @ 21.38 hrs, Volume= 1.851 af, Atten= 0%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.34 fps, Min. Travel Time= 0.3 min Avg. Velocity = 2.22 fps, Avg. Travel Time= 0.5 min

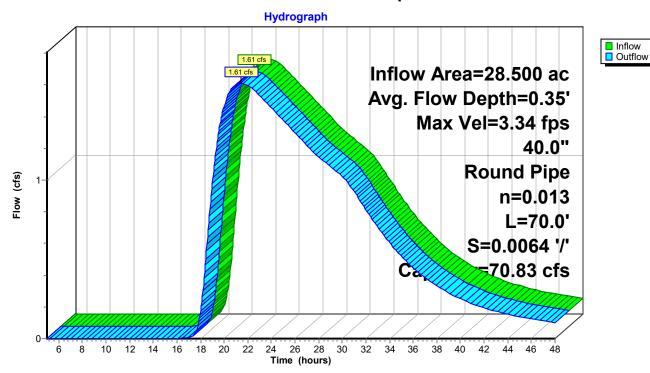
Peak Storage= 34 cf @ 21.38 hrs

Average Depth at Peak Storage= 0.35', Surface Width= 2.04' Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe n= 0.013 Corrugated PE, smooth interior Length= 70.0' Slope= 0.0064 '/' Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 3R: Outlet Pipe



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Inflow
Outflow

Summary for Reach 4R: Overflow

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 1.67" for 1-Year event

Inflow = 2.65 cfs @ 11.99 hrs, Volume= 0.139 af

Outflow = 2.56 cfs @ 12.00 hrs, Volume= 0.139 af, Atten= 3%, Lag= 1.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.29 fps, Min. Travel Time= 0.7 min Avg. Velocity = 0.58 fps, Avg. Travel Time= 2.9 min

Peak Storage= 115 cf @ 11.99 hrs

Average Depth at Peak Storage= 0.30', Surface Width= 4.77' Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 118.65 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch

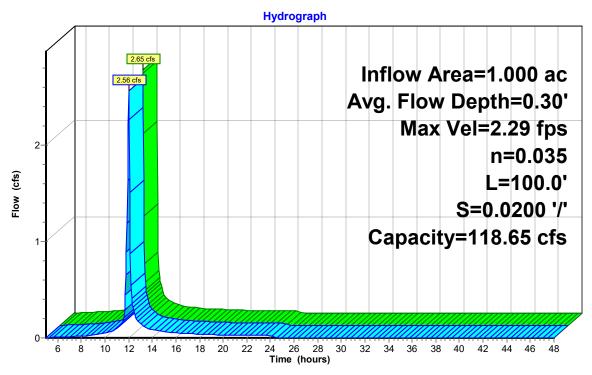
Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 100.0' Slope= 0.0200 '/'

Inlet Invert= 12.00', Outlet Invert= 10.00'



Reach 4R: Overflow



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Outflow

Summary for Reach 5R: Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.00" for 1-Year event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = $0.00 \text{ cfs } \bigcirc 0.00 \text{ sfs } \bigcirc 0.000 \text{ af, Atten= } 0\%$, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 5.00 hrs

Average Depth at Peak Storage= 0.00'

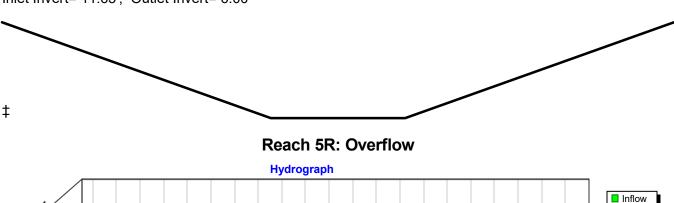
Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 90.48 cfs

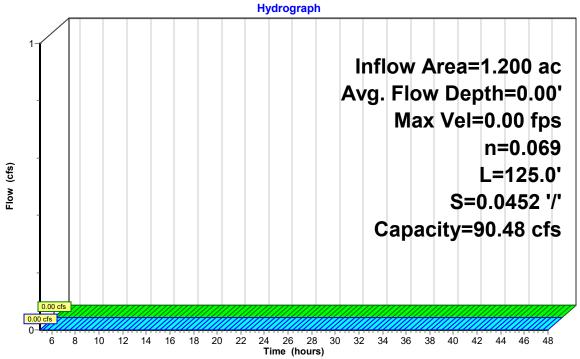
3.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch

Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 125.0' Slope= 0.0452 '/'

Inlet Invert= 11.65', Outlet Invert= 6.00'





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InflowOutflow

Summary for Reach 6R: Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.00" for 1-Year event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = $0.00 \text{ cfs } \bigcirc 0.00 \text{ sfs } \bigcirc 0.000 \text{ af, Atten= } 0\%$, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 5.00 hrs

Average Depth at Peak Storage= 0.00'

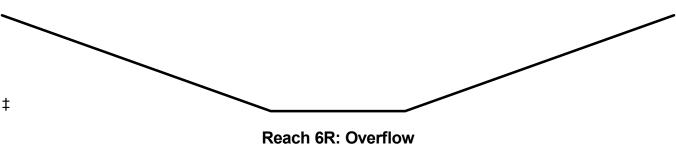
Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 116.91 cfs

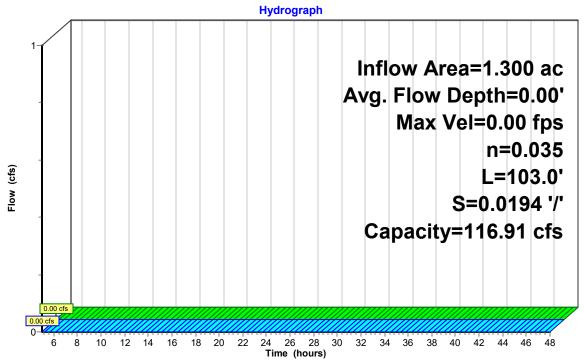
3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch

Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 103.0' Slope= 0.0194 '/'

Inlet Invert= 8.50', Outlet Invert= 6.50'





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Inflow
Outflow

Summary for Reach 7R: Overflow

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth > 1.40" for 1-Year event

Inflow = 0.30 cfs @ 13.53 hrs, Volume= 0.339 af

Outflow = 0.30 cfs @ 13.61 hrs, Volume= 0.339 af, Atten= 0%, Lag= 4.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.55 fps, Min. Travel Time= 3.0 min Avg. Velocity = 0.34 fps, Avg. Travel Time= 4.8 min

Peak Storage= 54 cf @ 13.56 hrs

Average Depth at Peak Storage= 0.07', Surface Width= 8.40' Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 116.81 cfs

8.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch

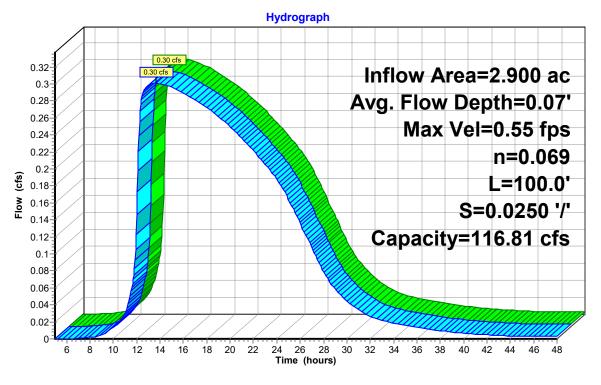
Side Slope Z-value = 3.0 '/' Top Width = 20.00'

Length= 100.0' Slope= 0.0250 '/'

Inlet Invert= 14.50', Outlet Invert= 12.00'



Reach 7R: Overflow



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Inflow
Outflow

Summary for Reach 8R: Dry Swale #1

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 1.67" for 1-Year event

Inflow = 2.72 cfs @ 11.96 hrs, Volume= 0.139 af

Outflow = 2.65 cfs @ 11.99 hrs, Volume= 0.139 af, Atten= 3%, Lag= 1.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.47 fps, Min. Travel Time= 0.7 min Avg. Velocity = 0.61 fps, Avg. Travel Time= 2.9 min

Peak Storage= 114 cf @ 11.98 hrs

Average Depth at Peak Storage= 0.39', Surface Width= 3.57' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 16.53 cfs

2.00' x 1.00' deep channel, n= 0.018 Earth, clean & straight

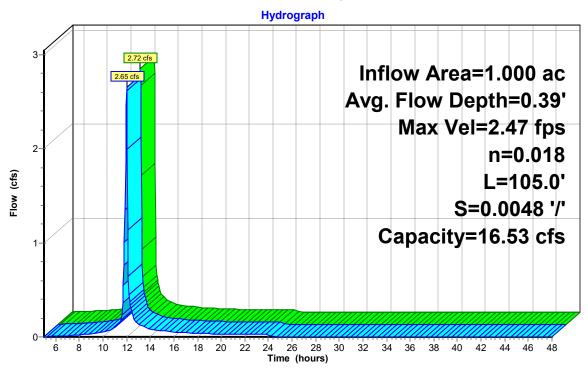
Side Slope Z-value= 2.0 '/' Top Width= 6.00'

Length= 105.0' Slope= 0.0048 '/'

Inlet Invert= 10.00', Outlet Invert= 9.50'



Reach 8R: Dry Swale #1



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Inflow
Outflow

Summary for Reach 10R: Dry Swale #2

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 1.00" for 1-Year event

Inflow = 1.22 cfs @ 12.03 hrs, Volume= 0.064 af

Outflow = 1.20 cfs @ 12.04 hrs, Volume= 0.064 af, Atten= 2%, Lag= 0.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.19 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.01 fps, Avg. Travel Time= 1.9 min

Peak Storage= 44 cf @ 12.03 hrs

Average Depth at Peak Storage= 0.15', Surface Width= 2.93' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 213.76 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight

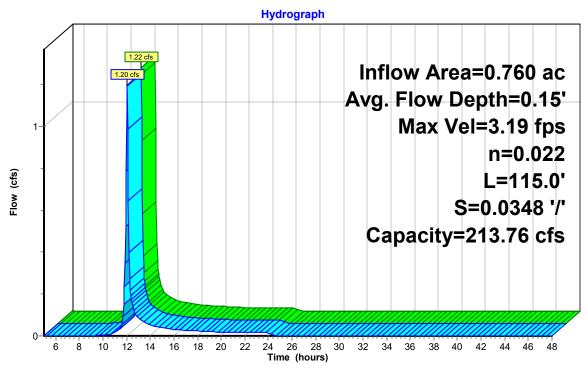
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 115.0' Slope= 0.0348 '/'

Inlet Invert= 37.00', Outlet Invert= 33.00'



Reach 10R: Dry Swale #2



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Summary for Reach 12R: Sediment Basin Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.00" for 1-Year event

Inflow 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 5.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 0.50' Flow Area= 6.0 sf, Capacity= 9.43 cfs

10.00' x 0.50' deep channel, n= 0.069 Riprap, 6-inch

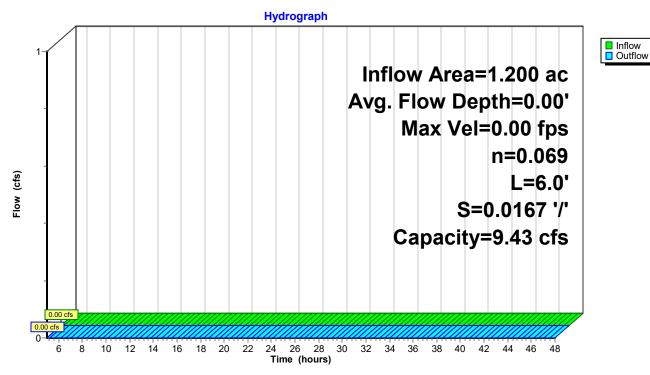
Side Slope Z-value= 4.0 '/' Top Width= 14.00'

Length= 6.0' Slope= 0.0167 '/'

Inlet Invert= 12.00', Outlet Invert= 11.90'



Reach 12R: Sediment Basin Overflow



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Inflow
Outflow

Summary for Reach 13R: Roadside Swale

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.12" for 1-Year event

Inflow = 0.05 cfs @ 12.05 hrs, Volume= 0.012 af

Outflow = 0.04 cfs @ 12.26 hrs, Volume= 0.012 af, Atten= 34%, Lag= 12.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.76 fps, Min. Travel Time= 6.4 min Avg. Velocity = 0.48 fps, Avg. Travel Time= 10.0 min

Peak Storage= 13 cf @ 12.15 hrs

Average Depth at Peak Storage= 0.04', Surface Width= 1.25' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.36 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight

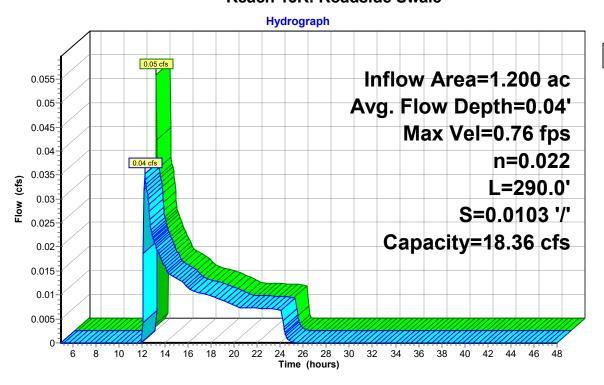
Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 290.0' Slope= 0.0103 '/'

Inlet Invert= 15.00', Outlet Invert= 12.00'



Reach 13R: Roadside Swale



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Inflow
Outflow

Summary for Reach 14R: Roadside Swale

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 1.00" for 1-Year event

Inflow = 1.32 cfs @ 11.97 hrs, Volume= 0.064 af

Outflow = 1.22 cfs @ 12.03 hrs, Volume= 0.064 af, Atten= 7%, Lag= 3.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.99 fps, Min. Travel Time= 1.9 min Avg. Velocity = 1.33 fps, Avg. Travel Time= 5.7 min

Peak Storage= 146 cf @ 11.99 hrs

Average Depth at Peak Storage= 0.13', Surface Width= 2.80' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 289.37 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight

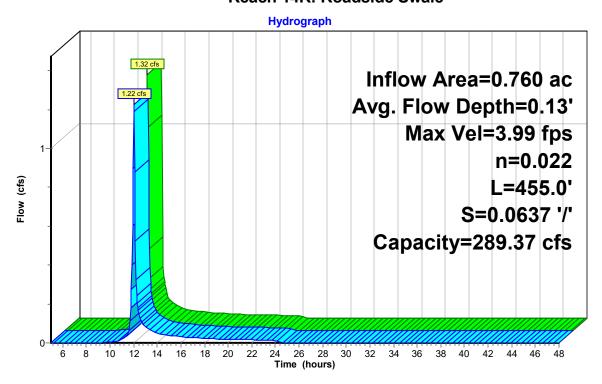
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 455.0' Slope= 0.0637 '/'

Inlet Invert= 66.00', Outlet Invert= 37.00'



Reach 14R: Roadside Swale



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Summary for Reach 15R: Roadside Swale

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.41" for 1-Year event

Inflow = 0.84 cfs @ 11.99 hrs, Volume= 0.045 af

Outflow = 0.46 cfs @ 12.27 hrs, Volume= 0.045 af, Atten= 46%, Lag= 16.5 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity = 0.64 fps, Min. Travel Time = 11.2 min Avg. Velocity = 0.21 fps, Avg. Travel Time = 34.0 min

Peak Storage= 310 cf @ 12.07 hrs

Average Depth at Peak Storage= 0.35', Surface Width= 3.11' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 4.69 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight

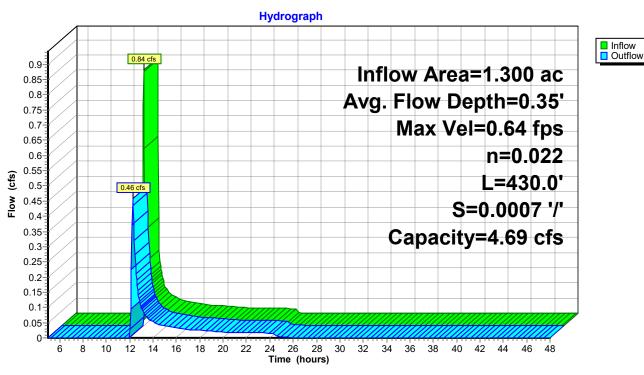
Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 430.0' Slope= 0.0007 '/'

Inlet Invert= 10.00', Outlet Invert= 9.71'



Reach 15R: Roadside Swale



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Summary for Reach 17R: Sediment Basin Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.05" for 1-Year event

Inflow = 0.02 cfs @ 20.86 hrs, Volume= 0.006 af

Outflow = 0.02 cfs @ 20.88 hrs, Volume= 0.006 af, Atten= 0%, Lag= 1.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.13 fps, Min. Travel Time= 0.8 min Avg. Velocity = 0.11 fps, Avg. Travel Time= 0.9 min

Peak Storage= 1 cf @ 20.86 hrs

Average Depth at Peak Storage= 0.01', Surface Width= 15.07' Bank-Full Depth= 0.70' Flow Area= 12.5 sf, Capacity= 24.64 cfs

15.00' x 0.70' deep channel, n= 0.069 Riprap, 6-inch

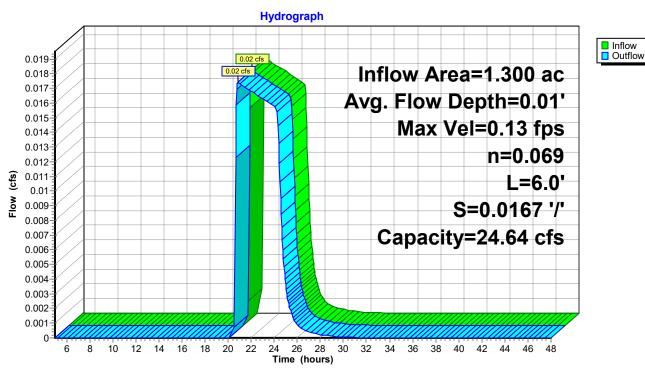
Side Slope Z-value= 4.0 '/' Top Width= 20.60'

Length= 6.0' Slope= 0.0167 '/'

Inlet Invert= 9.00', Outlet Invert= 8.90'

‡

Reach 17R: Sediment Basin Overflow



18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Pond 1P: WQv Pond #1

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth = 1.42" for 1-Year event

Inflow = 4.50 cfs @ 12.11 hrs, Volume= 0.344 af

Outflow = 0.30 cfs @ 13.53 hrs, Volume= 0.339 af, Atten= 93%, Lag= 85.1 min

Primary = 0.30 cfs @ 13.53 hrs, Volume= 0.339 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Starting Elev= 14.00' Surf.Area= 9,229 sf Storage= 19,003 cf

Peak Elev= 14.99' @ 13.53 hrs Surf.Area= 17,494 sf Storage= 27,569 cf (8,566 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= 363.1 min (1,180.3 - 817.1)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,795 cf	Forebay (Prismatic) Listed below (Recalc)
#2	9.00'	57,882 cf	Permanent Pool (Prismatic) Listed below (Recalc)

		·	
	62	2,677 cf Total Av	ailable Storage
E	0 ()	. 01	0 01
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	232	0	0
11.00	569	401	401
12.00	1,018	794	1,194
13.00	1,467	1,243	2,437
14.00	3,249	2,358	4,795
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
9.00	1,145	0	0
10.00	1,751	1,448	1,448
11.00	2,339	2,045	3,493
12.00	2,959	2,649	6,142
13.00	3,597	3,278	9,420
14.00	5,980	4,789	14,209
14.50	7,240	3,305	17,514
15.00	14,392	5,408	22,922
16.00	17,455	15,924	38,845
17.00	20,619	19,037	57,882
Davice Poutin	a Invo	rt Outlet Device	0

Device	Routing	Invert	Outlet Devices
#1	Primary	13.50'	12.0" Round Culvert
	•		L= 50.0' Box, headwall w/3 square edges, Ke= 0.500
			Inlet / Outlet Invert= 13.50' / 13.23' S= 0.0054 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	16.00'	24.0" x 24.0" Horiz. Outlet Structure Top Grate
			C= 0.600 in 24.0" x 24.0" Grate (100% open area)
			Limited to weir flow at low heads
#3	Device 1	14.00'	4.0" Round Reverse Slope Pipe
			L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 9.00' / 14.00' S= -0.1250 '/' Cc= 0.900

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#4 Primary 16.25'

n= 0.010 PVC, smooth interior, Flow Area= 0.09 sf **6.0' long x 1.0' breadth Broad-Crested Rectangular Weir** Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31

Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Primary OutFlow Max=0.30 cfs @ 13.53 hrs HW=14.99' (Free Discharge)

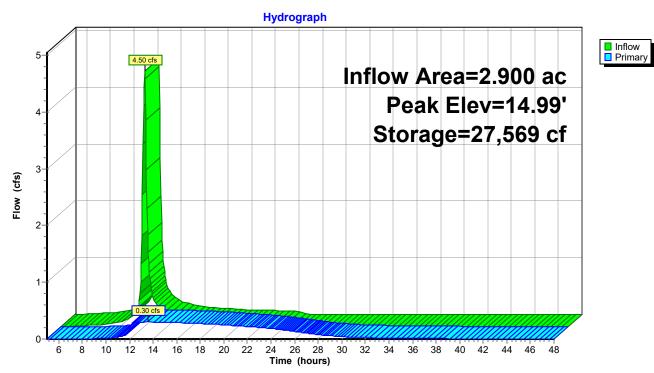
-1=Culvert (Passes 0.30 cfs of 3.14 cfs potential flow)

-2=Outlet Structure Top Grate (Controls 0.00 cfs)

-3=Reverse Slope Pipe (Inlet Controls 0.30 cfs @ 3.45 fps)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: WQv Pond #1



18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Pond 2P: WQv Pond #2

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 1.21" for 1-Year event

Inflow = 10.43 cfs @ 11.98 hrs, Volume= 0.585 af

Outflow = 0.48 cfs @ 13.64 hrs, Volume= 0.581 af, Atten= 95%, Lag= 99.4 min

Primary = 0.48 cfs @ 13.64 hrs, Volume= 0.581 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Starting Elev= 14.00' Surf.Area= 5,917 sf Storage= 9,000 cf

Peak Elev= 15.45' @ 13.64 hrs Surf.Area= 20,156 sf Storage= 23,392 cf (14,393 cf above start)

Plug-Flow detention time= 671.8 min calculated for 0.374 af (64% of inflow)

Center-of-Mass det. time= 373.8 min (1,193.1 - 819.3)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,020 cf	Forebay #1 (Prismatic) Listed below (Recalc)
#2	10.00'	2,575 cf	Forebay #2 (Prismatic) Listed below (Recalc)
#3	10.00'	58,093 cf	Permanent Pool (Prismatic) Listed below (Recalc)

64,688 cf Total Available Storage

	.	,000 01 10101711	anabio Giorago
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	141	0	0
11.00	330	236	236
12.00	562	446	682
13.00	866	714	1,396
14.00	2,023	1,445	2,840
14.50	2,696	1,180	4,020
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	82	Ó	0
11.00	202	142	142
12.00	351	277	419
13.00	535	443	862
14.00	1,323	929	1,791
14.50	1,815	785	2,575
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	375	0	0
11.00	653	514	514
12.00	957	805	1,319
13.00	1,286	1,122	2,441
14.00	2,571	1,929	4,369
14.50	3,307	1,470	5,839
15.00	13,814	4,280	10,119
16.00	17,852	15,833	25,952
17.00	22,659	20,256	46,207
17.50	24,884	11,886	58,093

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Device	Routing	Invert	Outlet Devices
#1	Device 3	16.50'	24.0" x 24.0" Horiz. Orifice/Grate
			C= 0.600 in 24.0" x 24.0" Grate (100% open area)
			Limited to weir flow at low heads
#2	Device 3	14.00'	4.0" Vert. Reverse Slope Pipe C= 0.600
			Limited to weir flow at low heads
#3	Primary	14.00'	12.0" Round Outlet Structure Discard Pipe
			L= 46.0' Box, headwall w/3 square edges, Ke= 0.500
			Inlet / Outlet Invert= 14.00' / 13.77' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#4	Primary	16.60'	10.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.48 cfs @ 13.64 hrs HW=15.45' (Free Discharge)

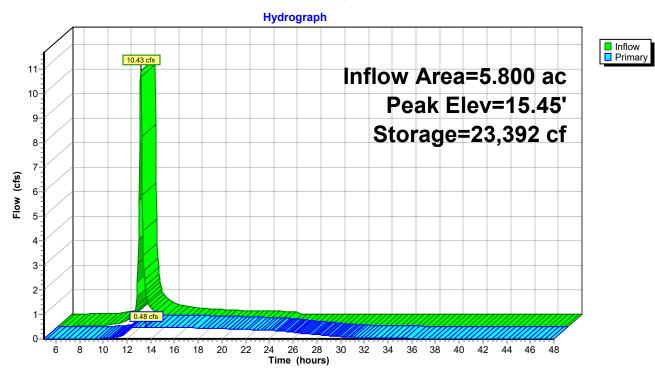
-3=Outlet Structure Discard Pipe (Passes 0.48 cfs of 3.04 cfs potential flow)

-1=Orifice/Grate (Controls 0.00 cfs)

-2=Reverse Slope Pipe (Orifice Controls 0.48 cfs @ 5.46 fps)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 2P: WQv Pond #2



18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Pond 3P: Infiltration Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.00" for 1-Year event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Discarded = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 8.10' @ 5.00 hrs Surf.Area= 109 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no inflow)

Volume	Invert	Avail.	Storage	Storage Description	n		
#1	8.10'	2	2,492 cf	Custom Stage Da	ta (Irregular) Liste	d below (Recalc)	
Elevatio (fee		rf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft <u>)</u>	
8.1	0	109	56.0	0	0	109	
12.0	0	1,415	149.0	2,492	2,492	1,678	
Device	Routing	Inve	ert Outle	et Devices			
#1	Primary	11.6	55' Cha	nnel/Reach using	Reach 5R: Overflo	DW .	
#2	#2 Discarded 8.10' (.500 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 4.00'			

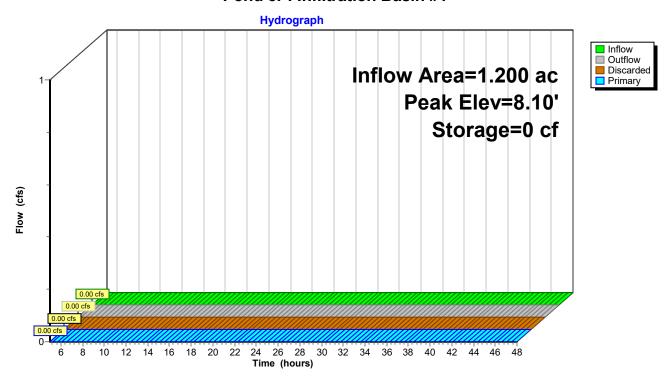
Discarded OutFlow Max=0.00 cfs @ 5.00 hrs HW=8.10' (Free Discharge) **2=Exfiltration** (Passes 0.00 cfs of 0.00 cfs potential flow)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=8.10' (Free Discharge) **1=Channel/Reach** (Controls 0.00 cfs)

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Pond 3P: Infiltration Basin #1



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Summary for Pond 4P: Infiltration Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.05" for 1-Year event

Inflow = 0.02 cfs @ 20.88 hrs, Volume= 0.006 af

Outflow = 0.02 cfs @ 20.97 hrs, Volume= 0.006 af, Atten= 0%, Lag= 5.4 min

Discarded = 0.02 cfs @ 20.97 hrs, Volume= 0.006 af Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 5.82' @ 20.97 hrs Surf.Area= 114 sf Storage= 3 cf

Plug-Flow detention time= 2.7 min calculated for 0.006 af (100% of inflow)

Center-of-Mass det. time= 2.7 min (1,369.3 - 1,366.6)

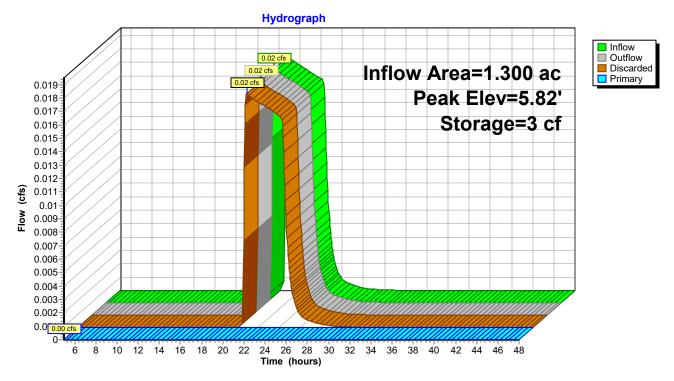
Volume	Inver	t Avail	l.Storage	Storage Description	on		
#1	5.80)'	2,495 cf	Custom Stage Da	ta (Irregular) Liste	ed below (Recalc)	
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
5.8	30	110	56.0	0	0	110	
9.7	70	1,415	150.0	2,495	2,495	1,702	
Device	Routing	Inv	vert Outle	et Devices			
#1	Primary	8	.50' Cha	nnel/Reach using	Reach 6R: Overfl	OW	
#2	#2 Discarded 5.80' 12		.80' 12.0	2.000 in/hr Exfiltration over Surface area			
			Cond	ductivity to Ground	water Elevation = 3	3.00'	

Discarded OutFlow Max=0.03 cfs @ 20.97 hrs HW=5.82' (Free Discharge) **2=Exfiltration** (Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=5.80' (Free Discharge)
—1=Channel/Reach (Controls 0.00 cfs)

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Pond 4P: Infiltration Basin #2



18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Pond 5P: Sedimentation Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.12" for 1-Year event

Inflow = 0.04 cfs @ 12.26 hrs, Volume= 0.012 af

Outflow = 0.00 cfs (a) 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 11.50' @ 31.80 hrs Surf.Area= 427 sf Storage= 505 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

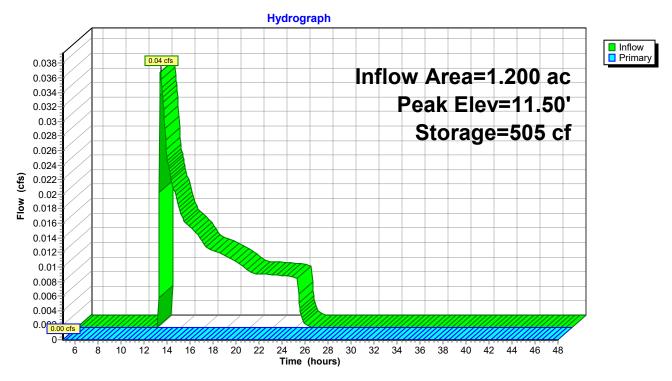
Center-of-Mass det. time= (not calculated: no outflow)

Volume	Inv	ert Ava	il.Storage	Storage Desc	ription			
#1	9.0	00'	1,058 cf	Custom Stag	e Data (I	rregular) List	ed below (Re	ecalc)
Elevatio	• • •	Surf.Area (sq-ft)	Perim. (feet)	Inc.Sto (cubic-fe		Cum.Store (cubic-feet)	Wet. <i>A</i> (se	Area q-ft <u>)</u>
9.0	00	41	25.8		0	0		41
10.0	00	150	46.7		90	90		167
11.0	00	320	66.6	2	230	320		355
12.0	00	550	86.4	4	-30	749		608
12.5	50	687	96.2	3	809	1,058		758
Device	Routing	In	vert Outle	et Devices				
#1	Primary	12	2.00' Cha	nnel/Reach ປ	ising Rea	ch 12R: Sedi	ment Basin (Overflow

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=9.00' (Free Discharge)
1=Channel/Reach (Controls 0.00 cfs)

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Pond 5P: Sedimentation Basin #1



18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Pond 16P: Sedimentation Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.41" for 1-Year event

Inflow = 0.46 cfs @ 12.27 hrs, Volume= 0.045 af

Outflow = 0.02 cfs @ 20.86 hrs, Volume= 0.006 af, Atten= 96%, Lag= 515.7 min

Primary = 0.02 cfs @ 20.86 hrs, Volume= 0.006 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 9.00' @ 20.86 hrs Surf.Area= 893 sf Storage= 1,703 cf

Plug-Flow detention time= 632.6 min calculated for 0.006 af (13% of inflow)

Center-of-Mass det. time= 440.5 min (1,365.0 - 924.5)

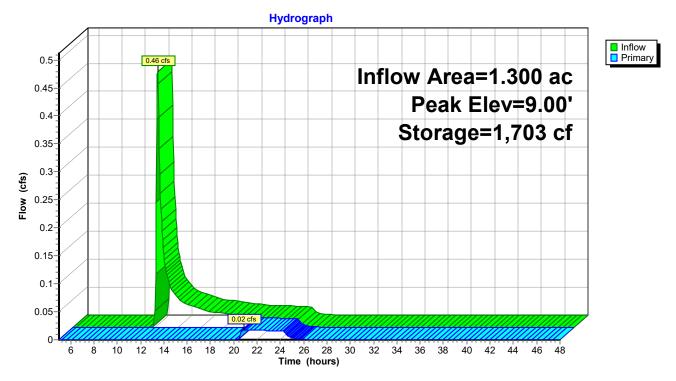
Volume	Inv	ert Ava	il.Storage	Storage Desc	ription			
#1	5.8	30'	2,389 cf	Custom Stag	e Data (Irre	egular) Liste	d below (Recalc)	
Elevation (fee		Surf.Area (sq-ft)	Perim. (feet)	Inc.Sto (cubic-fe		um.Store ubic-feet)	Wet.Area (sq-ft)	
5.8	30	224	80.0		0	0	224	
6.0	00	257	83.0		48	48	266	
7.0	00	438	98.0	3	44	392	500	
8.0	00	650	113.0	5	41	932	773	
9.0	00	892	128.0	7	68	1,700	1,085	
9.7	70	1,079	139.0	6	89	2,389	1,337	
Device	Routing	In	vert Outle	et Devices				
#1	Primary	g	0.00' Cha	nnel/Reach u	sing Reach	17R: Sedin	nent Basin Overflow	

Primary OutFlow Max=0.00 cfs @ 20.86 hrs HW=9.00' (Free Discharge)

1=Channel/Reach (Channel Controls 0.00 cfs @ 0.07 fps)

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Pond 16P: Sedimentation Basin #2



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Summary for Pond AP-1: Analysis Point #1

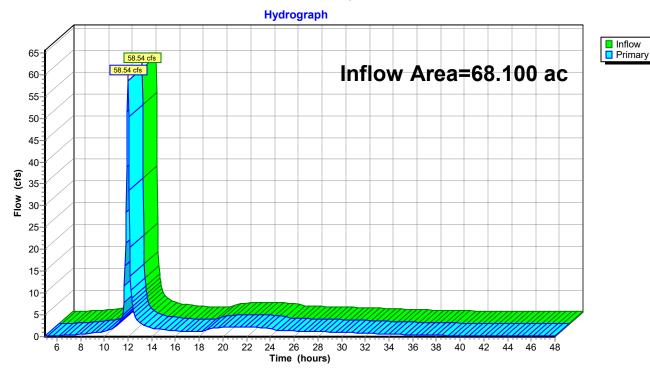
Inflow Area = 68.100 ac, 20.36% Impervious, Inflow Depth > 0.92" for 1-Year event

Inflow = 58.54 cfs @ 12.00 hrs, Volume= 5.220 af

Primary = 58.54 cfs @ 12.00 hrs, Volume= 5.220 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1



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Summary for Pond AP-2: Analysis Point #2

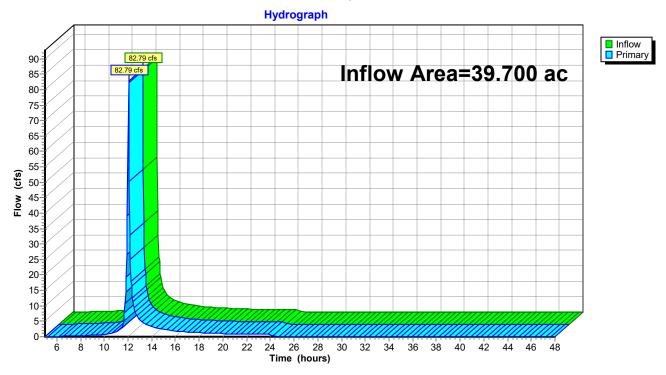
Inflow Area = 39.700 ac, 23.10% Impervious, Inflow Depth > 1.20" for 1-Year event

Inflow = 82.79 cfs @ 12.04 hrs, Volume= 3.954 af

Primary = 82.79 cfs @ 12.04 hrs, Volume= 3.954 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2



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Summary for Pond AP-3: Analysis Point #3

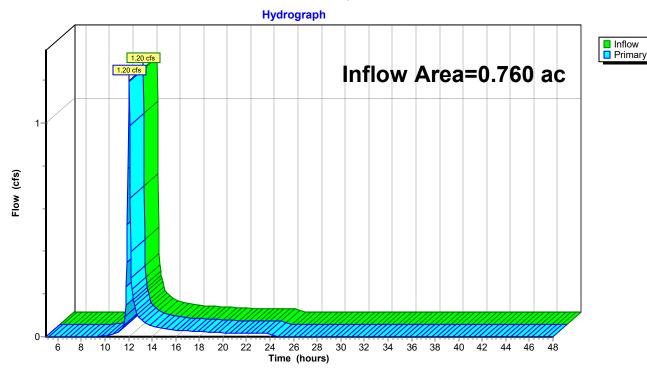
Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 1.00" for 1-Year event

Inflow = 1.20 cfs @ 12.04 hrs, Volume= 0.064 af

Primary = 1.20 cfs @ 12.04 hrs, Volume= 0.064 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3



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Summary for Pond C-1: Chamber Series 1

Inflow Area = 10.300 ac, 66.70% Impervious, Inflow Depth > 1.85" for 1-Year event Inflow 29.34 cfs @ 11.98 hrs, Volume= 1.592 af 27.91 cfs @ 12.04 hrs, Volume= Outflow 1.233 af, Atten= 5%, Lag= 3.7 min 0.10 cfs @ 5.80 hrs, Volume= Discarded = 0.345 af Primary 27.81 cfs @ 12.04 hrs, Volume= 0.888 af Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 12.19' @ 12.04 hrs Surf.Area= 8,454 sf Storage= 28,913 cf

Plug-Flow detention time= 361.5 min calculated for 1.232 af (77% of inflow) Center-of-Mass det. time= 279.3 min (1,056.9 - 777.6)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	11,722 cf	37.08'W x 227.97'L x 5.50'H Field B
			46,496 cf Overall - 17,192 cf Embedded = 29,305 cf x 40.0% Voids
#2B	6.75'	17,192 cf	ADS_StormTech MC-3500 d +Cap x 155 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			155 Chambers in 5 Rows
			Cap Storage= +14.9 cf x 2 x 5 rows = 149.0 cf
#3	13.25'	6,100 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		35,013 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
13.25	600	0	0
13.75	4,900	1,375	1,375
14.00	8,200	1,638	3,013
14.25	16,500	3,088	6,100

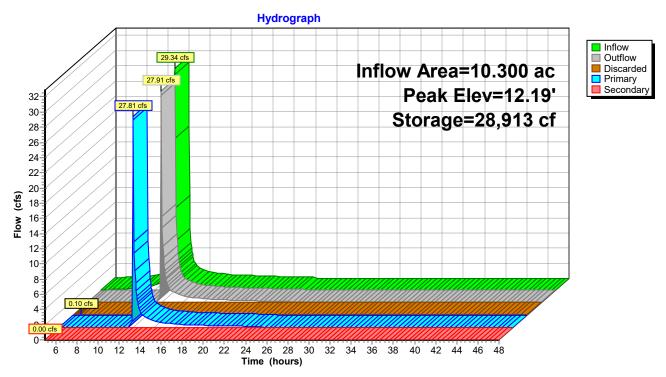
Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	10.00'	36.0" Round Culvert
	•		L= 55.9' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 10.00' / 7.59' S= 0.0431 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	14.24'	50.0' long x 0.7' breadth Concrete Curb
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50
			Coef. (English) 2.76 2.82 2.93 3.09 3.18 3.22 3.27 3.30 3.32
			3 31 3 32

Discarded OutFlow Max=0.10 cfs @ 5.80 hrs HW=6.08' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.10 cfs)

Primary OutFlow Max=25.90 cfs @ 12.04 hrs HW=12.09' (Free Discharge) 2=Culvert (Inlet Controls 25.90 cfs @ 4.92 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge) 3=Concrete Curb (Controls 0.00 cfs)

Pond C-1: Chamber Series 1



18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Pond C-4: Chamber Series 4

Inflow Area =	8.900 ac,	0.00% Impervious, Inflow	Depth > 1.58" for 1-Year event	
Inflow =	22.13 cfs @	11.99 hrs, Volume=	1.175 af	
Outflow =	17.34 cfs @	12.06 hrs, Volume=	0.845 af, Atten= 22%, Lag= 4.4	min
Discarded =	0.07 cfs @	7.60 hrs, Volume=	0.254 af	
Primary =	17.27 cfs @	12.06 hrs, Volume=	0.592 af	
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 12.75' @ 12.07 hrs Surf.Area= 6,391 sf Storage= 21,785 cf

Plug-Flow detention time= 397.3 min calculated for 0.844 af (72% of inflow) Center-of-Mass det. time= 304.6 min (1,103.4 - 798.9)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	8,911 cf	29.92'W x 213.63'L x 5.50'H Field B
			35,151 cf Overall - 12,874 cf Embedded = 22,277 cf x 40.0% Voids
#2B	6.75'	12,874 cf	ADS_StormTech MC-3500 d +Cap x 116 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			116 Chambers in 4 Rows
			Cap Storage= +14.9 cf x 2 x 4 rows = 119.2 cf
#3	14.10'	8,015 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		29,800 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
14.10	400	0	0
14.60	2,400	700	700
14.80	6,300	870	1,570
15.10	10,000	2,445	4,015
15.50	10,000	4,000	8,015

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	11.00'	36.0" Round Culvert
			L= 24.3' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 11.00' / 9.42' S= 0.0650 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

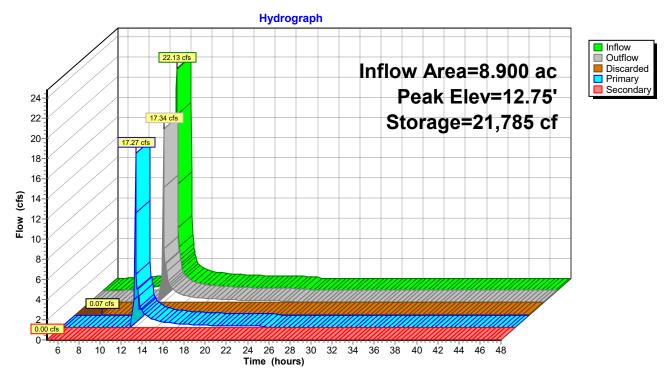
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Discarded OutFlow Max=0.07 cfs @ 7.60 hrs HW=6.10' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=15.10 cfs @ 12.06 hrs HW=12.52' (Free Discharge) 2=Culvert (Inlet Controls 15.10 cfs @ 4.20 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge) 3=Wharf (Controls 0.00 cfs)

Pond C-4: Chamber Series 4



18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Pond C-5: Chamber Series 5

Inflow Area =	5.200 ac,	0.00% Impervious, Inflo	w Depth > 1.58" for 1-Year event
Inflow =	13.09 cfs @	11.99 hrs, Volume=	0.687 af
Outflow =	0.43 cfs @	14.80 hrs, Volume=	0.434 af, Atten= 97%, Lag= 168.8 min
Discarded =	0.11 cfs @	9.00 hrs, Volume=	0.373 af
Primary =	0.32 cfs @	14.80 hrs, Volume=	0.062 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 12.84' @ 14.80 hrs Surf.Area= 4,801 sf Storage= 20,773 cf

Plug-Flow detention time= 879.5 min calculated for 0.434 af (63% of inflow) Center-of-Mass det. time= 777.3 min (1,575.8 - 798.5)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	7,757 cf	28.50'W x 168.47'L x 6.75'H Field B
			32,409 cf Overall - 13,016 cf Embedded = 19,393 cf x 40.0% Voids
#2B	6.75'	13,016 cf	ADS_StormTech MC-4500 b +Cap x 120 Inside #1
			Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf
			Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap
			120 Chambers in 3 Rows
			Cap Storage= +39.5 cf x 2 x 3 rows = 237.0 cf
#3	14.60'	7,420 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		28,193 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
14.60	200	0	0
14.80	1,000	120	120
15.00	10,000	1,100	1,220
15.50	14,800	6,200	7,420

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	1.000 in/hr Exfiltration over Surface area
#2	Primary	12.60'	36.0" Round Culvert
	•		L= 62.8' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 12.60' / 12.29' S= 0.0049 '/' Cc= 0.900
			n= 0.013 Cast iron, coated, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

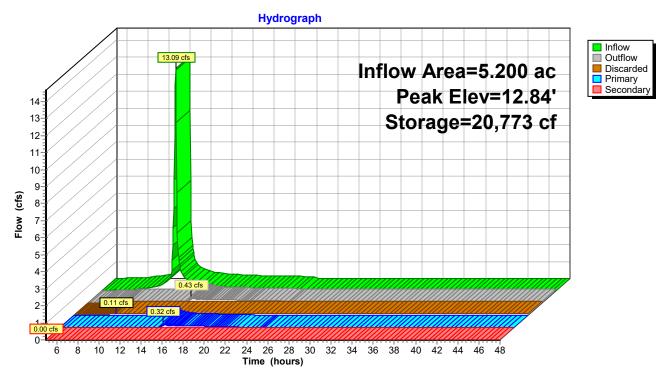
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Discarded OutFlow Max=0.11 cfs @ 9.00 hrs HW=6.10' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.11 cfs)

Primary OutFlow Max=0.31 cfs @ 14.80 hrs HW=12.84' (Free Discharge) 2=Culvert (Barrel Controls 0.31 cfs @ 1.84 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge) 3=Wharf (Controls 0.00 cfs)

Pond C-5: Chamber Series 5



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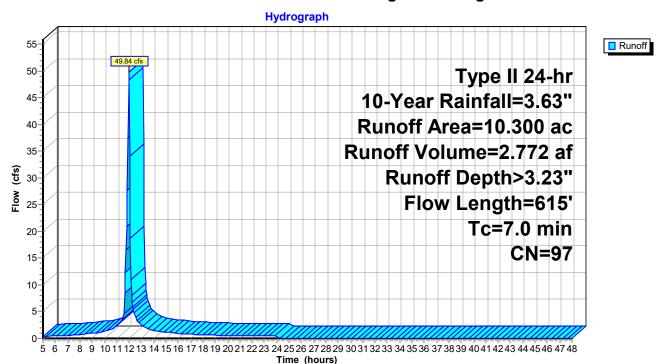
Summary for Subcatchment DR-1: Building A & Storage

Runoff = 49.84 cfs @ 11.98 hrs, Volume= 2.772 af, Depth> 3.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	cription						
*	6.	6.870 98		Build	Building A						
	0.	100	80	>75%	% Grass co	over, Good,	, HSG D				
*	3.	330	95	Dens	Dense Graded Aggregate						
	10.	300	97	Weig	ghted Aver	age					
	3.	430		33.3	0% Pervio	us Area					
	6.	870		66.7	0% Imperv	ious Area					
	Тс	Length	n S	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.3	100	0.0	0100	0.50		Sheet Flow,				
							n= 0.023 P2= 2.40"				
	3.1	300	0.0	0100	1.61		Shallow Concentrated Flow,				
							Unpaved Kv= 16.1 fps				
	0.6	215	0.0	0050	5.91	29.00	Pipe Channel,				
							30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'				
							n= 0.013				
	7.0	615	5 To	otal							

Subcatchment DR-1: Building A & Storage



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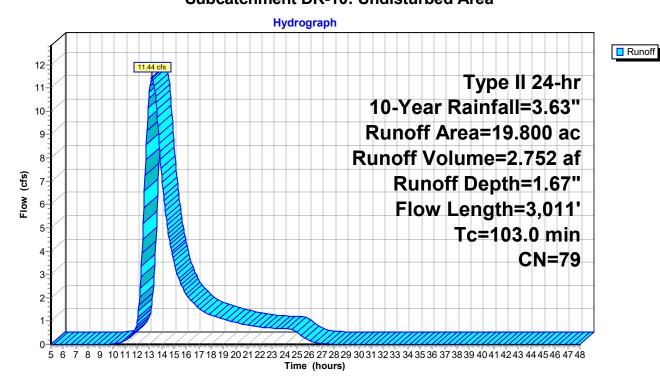
Summary for Subcatchment DR-10: Undisturbed Area

Runoff = 11.44 cfs @ 13.19 hrs, Volume= 2.752 af, Depth= 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

Area	(ac) C	N Desc	cription		
19.	800 7	'9 Woo	ds, Fair, F	ISG D	
19.	800	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
19.7	150	0.0800	0.13		Sheet Flow,
3.0	200	0.0500	1.12		Woods: Light underbrush n= 0.400 P2= 2.40" Shallow Concentrated Flow,
0.0	200	0.0000	1.12		Woodland Kv= 5.0 fps
1.6	250	0.2600	2.55		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
78.7	2,361	0.0100	0.50		Shallow Concentrated Flow, Wetland Flow
0.0	50	0.0500	22.86	161.57	Woodland Kv= 5.0 fps Pipe Channel,
0.0	30	0.0300	22.00	101.57	36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
					n= 0.012 Corrugated PP, smooth interior
103.0	3,011	Total			

Subcatchment DR-10: Undisturbed Area



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Summary for Subcatchment DR-11: Hudson River Bank

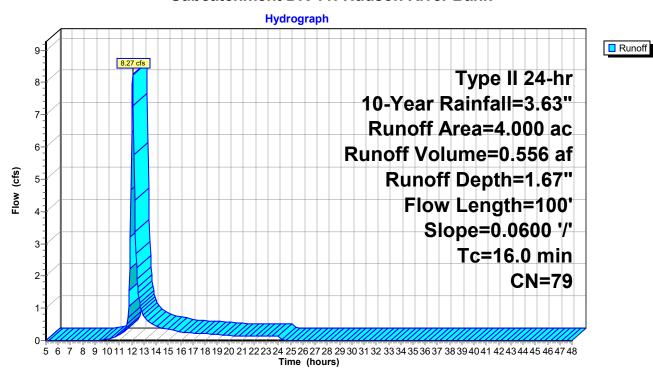
Runoff = 8.27 cfs @ 12.09 hrs, Volume= 0.556 af, Depth= 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

 Area	(ac) C	N Des	cription					
4.	.000	79 Woo	ods, Fair, F	ISG D				
4.000 100.00% Pervious Area								
 Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
16.0	100	0.0600	0.10		Sheet Flow,			

Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-11: Hudson River Bank



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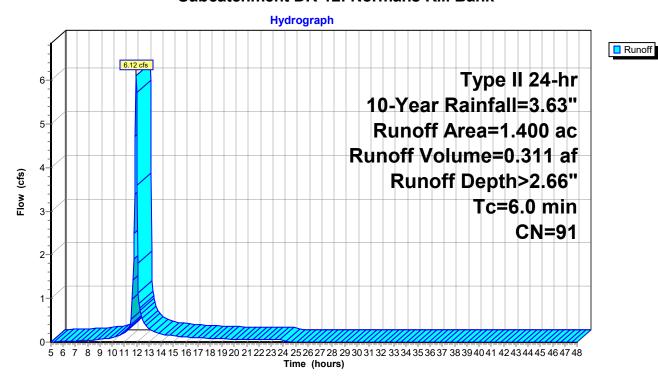
Summary for Subcatchment DR-12: Normans Kill Bank

Runoff = 6.12 cfs @ 11.97 hrs, Volume= 0.311 af, Depth> 2.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

Area	a (ac)	CN	Desc	ription		
	0.430	79	Woo	ds, Fair, H	ISG D	
	0.970	96	Grav	el surface	, HSG D	
	1.400	91	Weig	hted Aver	age	
	1.400		100.0	00% Pervi	ous Area	
To	: Leng	jth :	Slope	Velocity	Capacity	Description
(min)	(fe	et)	(ft/ft)	(ft/sec)	(cfs)	
6.0						Direct Entry, Minimum

Subcatchment DR-12: Normans Kill Bank



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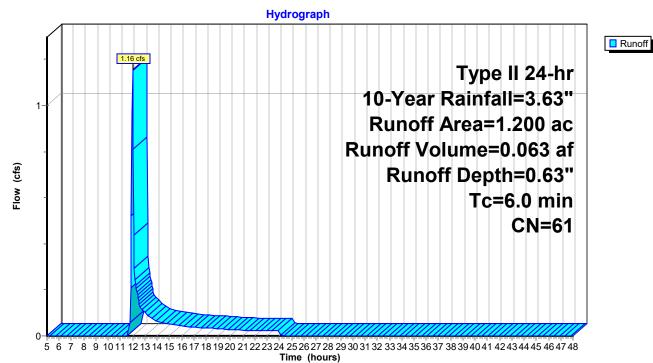
Summary for Subcatchment DR-13: Roadway

Runoff = 1.16 cfs @ 11.99 hrs, Volume= 0.063 af, Depth= 0.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	ription						
*	0.	450	98	Pave	Pavement						
	0.	750	39	>75%	√ Grass co	over, Good	I, HSG A				
	1.200 61 Weighted Average										
	0.750 62.50% Pervious Area										
	0.450 37.50% lm			0% Imperv	ious Area						
	Тс	Leng	th	Slope	Velocity	Capacity	Description				
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)					
	6.0						Direct Entry, Min				

Subcatchment DR-13: Roadway



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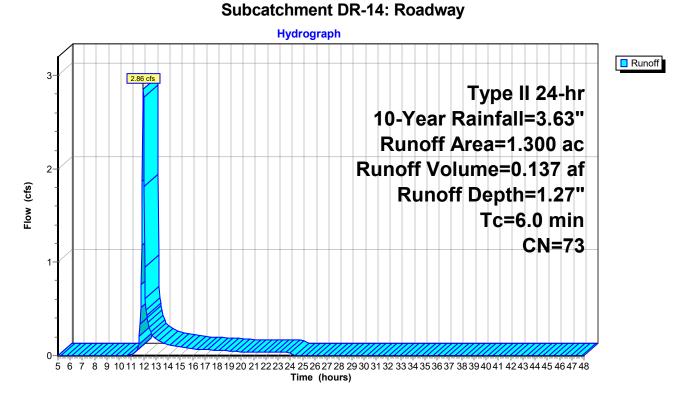
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Summary for Subcatchment DR-14: Roadway

Runoff = 2.86 cfs @ 11.98 hrs, Volume= 0.137 af, Depth= 1.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area	(ac)	CN	Desc	cription						
*	0.	550	98	New	New Pavement						
	0.	550	39	>75%	√ Grass co	over, Good	I, HSG A				
*	0.	200	98	Mill 8	R Fill of Ol	d Pavemen	nt				
	1.300 73 Weighted Average										
	0.	550		42.3	1% Pervio	us Area					
	0.	750		57.6	9% Imperv	∕ious Area					
	Тс	Long	ıth	Slone	Velocity	Canacity	Description				
		Leng	•	Slope	,	Capacity	Description				
_	(min)	(fee	2 ()	(ft/ft)	(ft/sec)	(cfs)					
	6.0						Direct Entry, Min				



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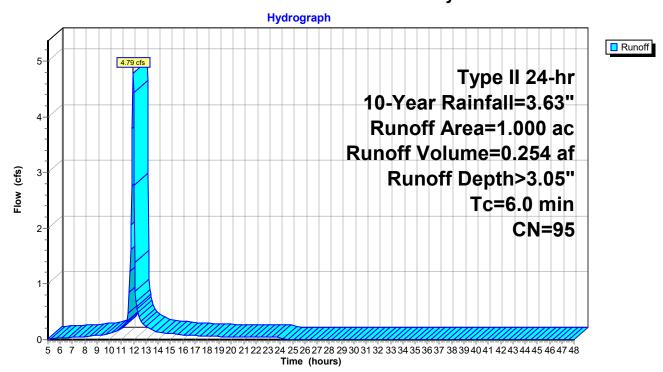
Summary for Subcatchment DR-15: Roadway

Runoff = 4.79 cfs @ 11.96 hrs, Volume= 0.254 af, Depth> 3.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	cription						
*	0.	050	98	New	New Pavement						
	0.	050	39	>75%	√ Grass co	over, Good	I, HSG A				
*	0.	900	98	Mill 8	R Fill of Ol	d Pavemen	nt				
	1.000 95 Weighted Average										
	0.	050		5.00	% Perviou	s Area					
	0.	950		95.0	0% Imperv	∕ious Area					
	т.		41.	01	V/-1!6	0	D				
	Tc	Leng		Slope	Velocity	Capacity	Description				
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)					
	6.0						Direct Entry, Min				

Subcatchment DR-15: Roadway



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Summary for Subcatchment DR-16: Undisturbed Area

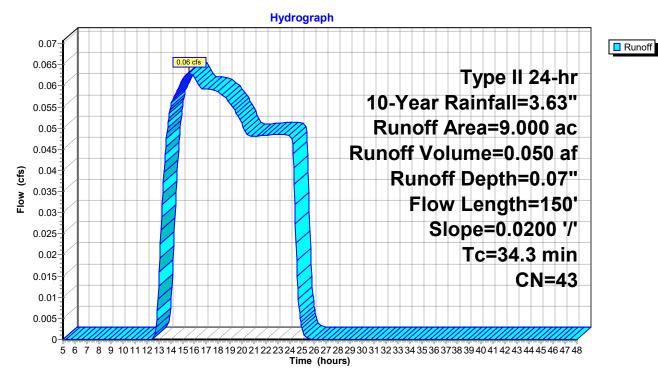
Runoff = 0.06 cfs @ 15.50 hrs, Volume= 0.050 af, Depth= 0.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

 Area	(ac) C	N Des	cription						
9.	000 4	13 Woo	ds/grass o	comb., Fair	, HSG A				
9.000 100.00% Pervious Area									
 Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
34.3	150	0.0200	0.07		Sheet Flow,				

Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-16: Undisturbed Area



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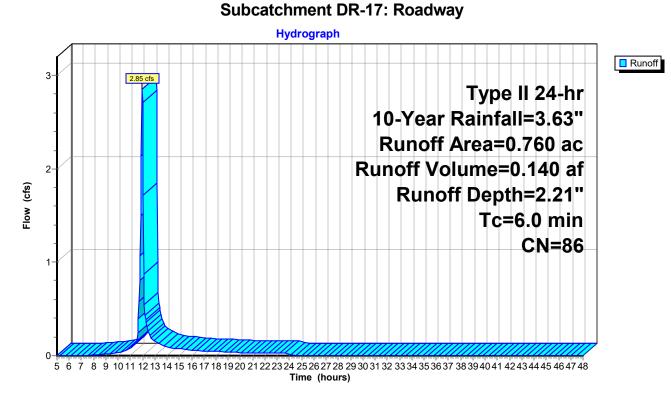
Summary for Subcatchment DR-17: Roadway

Runoff = 2.85 cfs @ 11.97 hrs, Volume= 0.140 af, Depth= 2.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area	(ac)	CN	Desc	cription			
*	0.	140	98	Road	d Widening	9		
*	0.	460	98	Road	dway			
	0.	160	39	>75%	% Grass co	over, Good	, HSG A	
	0.760 86 Weighted Average							
	0.	160		21.0	5% Pervio	us Area		
	0.	600		78.9	5% Imperv	ious Area		
	_	_						
	Тс	Leng		Slope	Velocity	Capacity	Description	
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)		
	6.0						Direct Entry, Minimum	

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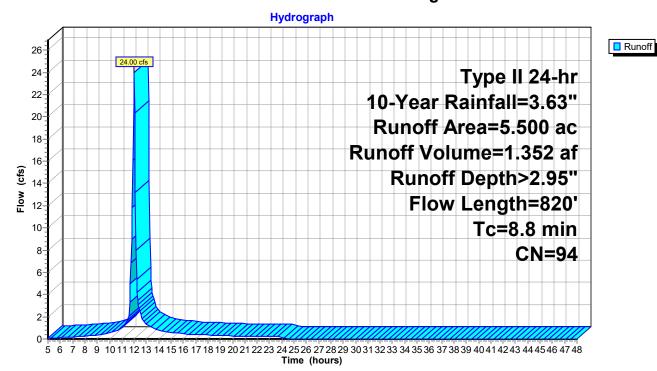
Summary for Subcatchment DR-2: Storage

Runoff = 24.00 cfs @ 12.00 hrs, Volume= 1.352 af, Depth> 2.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area	(ac) C	N Desc	cription		
*	5.	300 9	5 Dens	se Graded	Aggregate	
	0.	200 8	30 >759	% Grass co	over, Good	, HSG D
	5.	500 9	4 Weig	ghted Aver	age	
	5.	500	100.	00% Pervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	100	0.0100	0.50		Sheet Flow,
						n= 0.023 P2= 2.40"
	4.9	470	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.6	250	0.0050	6.67	47.16	Pipe Channel,
						36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
_						n= 0.013
	8.8	820	Total			

Subcatchment DR-2: Storage



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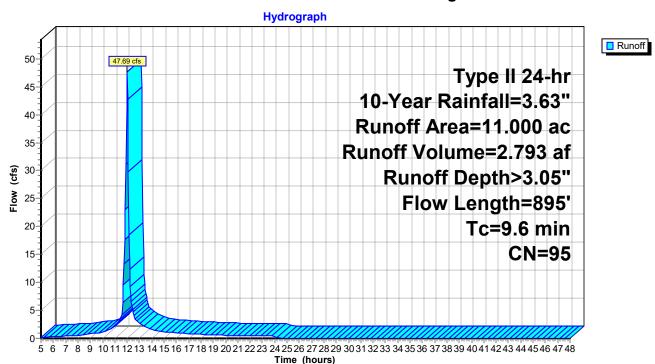
Summary for Subcatchment DR-3: Rail & Storage

Runoff = 47.69 cfs @ 12.00 hrs, Volume= 2.793 af, Depth> 3.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	ription						
*	* 8.300 95			Compacted Gravel							
	0.	400	80	>75%	% Grass co	ss cover, Good, HSG D					
*	2.	300	98	Rail							
	11.	000	95	Weig	hted Aver	age					
	8.	700			9% Pervio						
	2.300			20.9	1% Imperv	rious Area					
					•						
	Тс	Length	n S	lope	Velocity	Capacity	Description				
_	(min)	(feet) (ft/ft)	(ft/sec)	(cfs)					
	3.3	100	0.0	100	0.50		Sheet Flow,				
							n= 0.023 P2= 2.40"				
	5.4	525	0.0	100	1.61		Shallow Concentrated Flow,				
							Unpaved Kv= 16.1 fps				
	0.9	270	0.0	050	5.09	16.00	Pipe Channel,				
							24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'				
							n= 0.013				
	9.6	895	To	tal							

Subcatchment DR-3: Rail & Storage



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Runoff

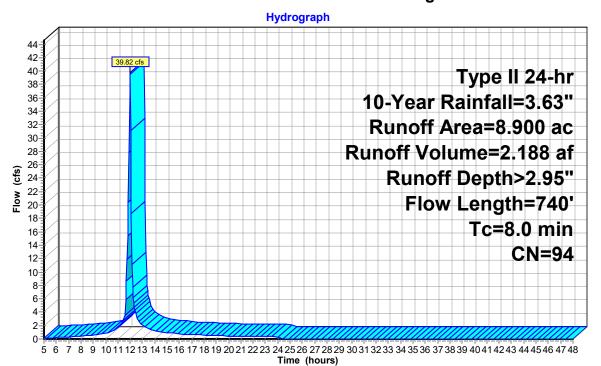
Summary for Subcatchment DR-4: Storage

Runoff = 39.82 cfs @ 11.99 hrs, Volume= 2.188 af, Depth> 2.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area	(ac) C	N Desc	cription		
*	8.	600 9	5 Com	mpacted Gravel		
	0.	300 8	30 >759	∕⁄ Grass co	over, Good	, HSG D
	8.	900 9	94 Weig	ghted Aver	age	
	8.900		100.00%		ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	100	0.0100	0.50		Sheet Flow,
						n= 0.023 P2= 2.40"
	4.1	400	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.6	240	0.0050	6.67	47.16	Pipe Channel,
						36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
						n= 0.013 Corrugated PE, smooth interior
	8.0	740	Total			

Subcatchment DR-4: Storage



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Runoff

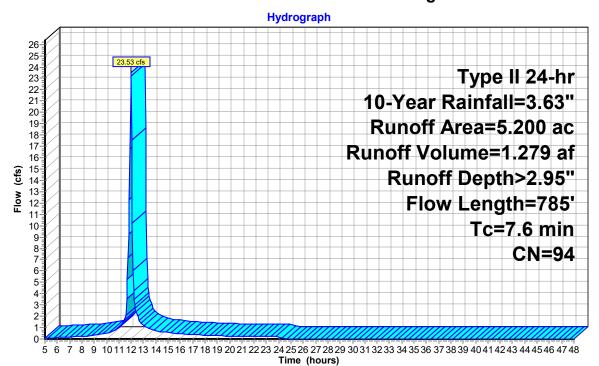
Summary for Subcatchment DR-5: Storage

Runoff = 23.53 cfs @ 11.98 hrs, Volume= 1.279 af, Depth> 2.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac) C	N Desc	cription		
*	4.	900	95 Dense Grade		Aggregate	
	0.	300 8	30 >759	% Grass co	over, Good	, HSG D
	5.200 94 Weighted Average				age	
	5.200			00% Pervi		
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	100	0.0100	0.50		Sheet Flow,
						n= 0.023 P2= 2.40"
	3.0	285	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	1.3	400	0.0050	5.09	16.00	Pipe Channel,
						24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
_						n= 0.013
	7.6	785	Total			

Subcatchment DR-5: Storage



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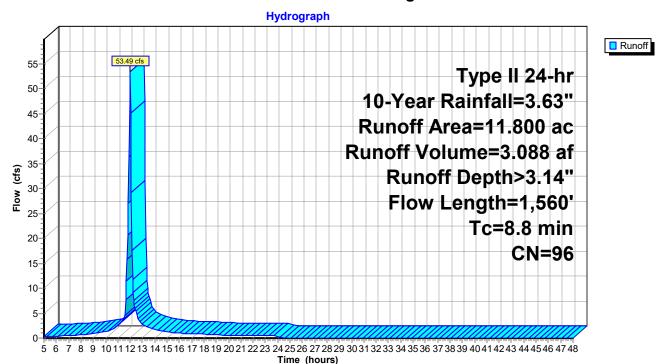
Summary for Subcatchment DR-6: Buldings B & D

Runoff = 53.49 cfs @ 12.00 hrs, Volume= 3.088 af, Depth> 3.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	cription						
*	2.	549	98	Build	ling B						
*	1.	413	98	Build	Building D						
	0.	200	80	>75%	√ Grass co	over, Good,	, HSG D				
*	7.	638	95	Dens	se Graded	Aggregate					
	11.	800	96	Weig	hted Aver	age					
	7.	838		•	2% Pervio	•					
	3.	962		33.5	8% Imperv	ious Area					
					•						
	Tc	Length	1 5	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·				
	3.3	100	0.	0100	0.50		Sheet Flow,				
							n= 0.023 P2= 2.40"				
	1.0	100	0.	0100	1.61		Shallow Concentrated Flow,				
							Unpaved Kv= 16.1 fps				
	4.5	1,360	0.	0050	5.09	16.00	Pipe Channel,				
							24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'				
							n= 0.013				
	8.8	1,560) To	otal							

Subcatchment DR-6: Buldings B & D



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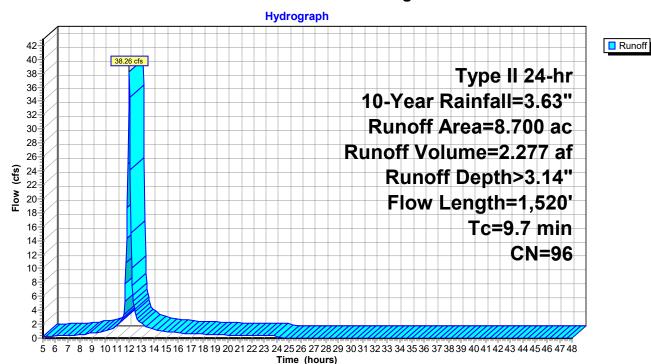
Summary for Subcatchment DR-7: Building C & Rail

Runoff = 38.26 cfs @ 12.00 hrs, Volume= 2.277 af, Depth> 3.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	ription						
*	3.030 98			Build	Building C						
*	0.	970	98	Rail							
*	4.	400	95	Dens	se Graded	Aggregate					
	0.	300	80	>75%	>75% Grass cover, Good, HSG D						
	8.	700	96	Weig	hted Aver	age					
	4.	700		54.0	2% Pervio	us Area					
	4.	000		45.9	8% Imperv	ious Area					
	Тс	Lengtl	າ ເ	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.3	100	0.	0100	0.50		Sheet Flow,				
							n= 0.023 P2= 2.40"				
	2.6	250	0.	0100	1.61		Shallow Concentrated Flow,				
							Unpaved Kv= 16.1 fps				
	3.8	1,170	0.	0050	5.09	16.00	Pipe Channel,				
							24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'				
							n= 0.013				
	9.7	1,520) T	otal							

Subcatchment DR-7: Building C & Rail



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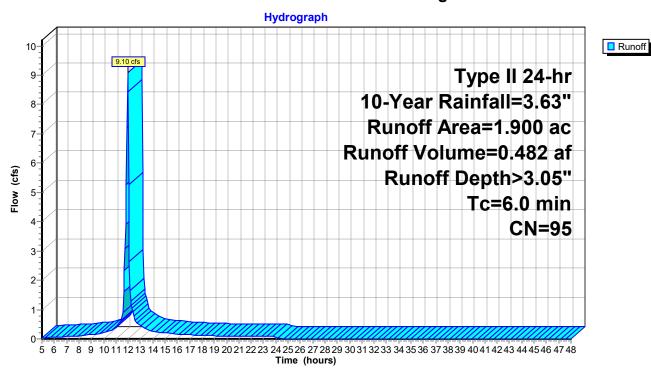
Summary for Subcatchment DR-8A: Parking

Runoff = 9.10 cfs @ 11.96 hrs, Volume= 0.482 af, Depth> 3.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	cription						
*	1.	.600	98	Park	Parking						
	0.	.300	80	>759	% Grass co	over, Good	, HSG D				
	1.900 95 Weighted Average										
	0.300 15.79% Pervious Area										
	1.600 84.21% Impervious Area					rious Area					
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	6.0	(100	<u>., </u>	(14,14)	(.2300)	(0.0)	Direct Entry, Minimum				

Subcatchment DR-8A: Parking



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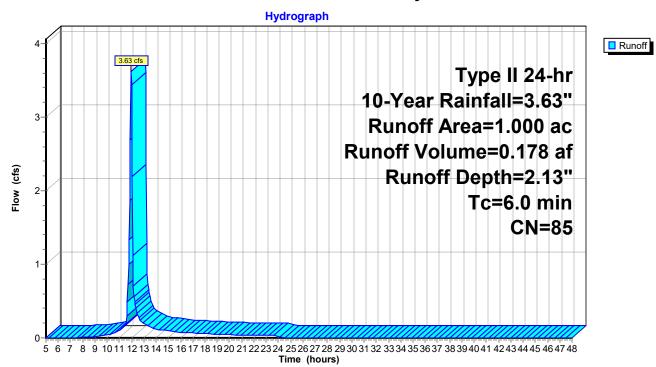
Summary for Subcatchment DR-8B: Roadway & Pond

Runoff = 3.63 cfs @ 11.97 hrs, Volume= 0.178 af, Depth= 2.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area	(ac)	CN	Desc	cription						
*	0.	300	98	Road	Roadway						
_	0.	700	80	>759	√ Grass co	over, Good	, HSG D				
	1.000 85 Weighted Average										
	0.	700		70.0	0% Pervio	us Area					
	0.300 30.00% Impervious Area					ious Area					
	J			Slope	Velocity	Capacity	Description				
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)					
	6.0						Direct Entry, Minimum				

Subcatchment DR-8B: Roadway & Pond



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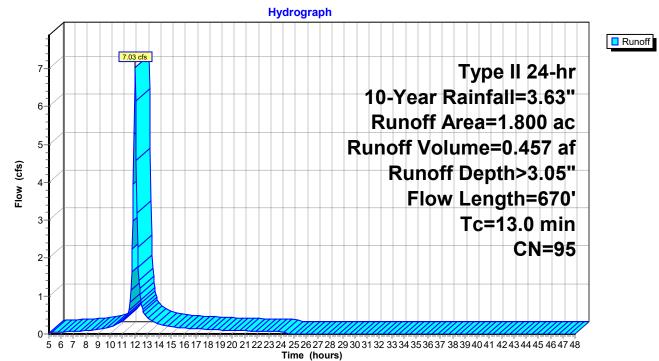
Summary for Subcatchment DR-9A: Parking & Substation

Runoff = 7.03 cfs @ 12.04 hrs, Volume= 0.457 af, Depth> 3.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	cription		
	0.	230	80	>75%	√ Grass co	over, Good	, HSG D
*	0.	200	92	Com	pacted Gr	avel	,
*	1.	200	98	Park	ing and Ro	oad	
*	0.	170	98	Subs	station		
	1.	.800	95	Weig	hted Aver	age	
	0.	430			9% Pervio		
	1.370 76.11% Impervious Area					ious Area	
	Тс	Lengt	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	1.4 100 0.		0.0200	1.19		Sheet Flow, Parking Lot Runoff	
							Smooth surfaces n= 0.011 P2= 2.40"
	11.6	57	0 (0.0030	0.82		Shallow Concentrated Flow, Grass Lined Ditch to Pond
							Grassed Waterway Kv= 15.0 fps
	13.0	67	0	Total	·		

Subcatchment DR-9A: Parking & Substation



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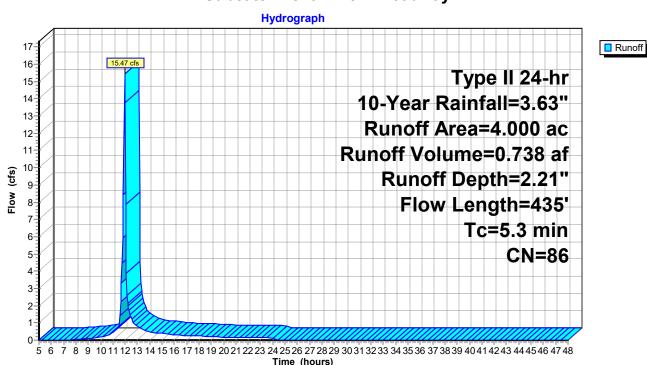
Summary for Subcatchment DR-9B: Roadway

Runoff = 15.47 cfs @ 11.96 hrs, Volume= 0.738 af, Depth= 2.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

	Area	(ac)	CN	Desc	ription		
*	1.	050	95	Dens	se Graded	Aggregate	
*	0.	480	98	Road	dway		
	2.	470			•	over, Good,	HSG D
_	4.	000	86 Wei		Weighted Average		
		520		_	0% Pervio	•	
		480			0% Imperv		
	٠.						
	Tc	Length	n S	lope	Velocity	Capacity	Description
	(min)	(feet		ft/ft)	(ft/sec)	(cfs)	· · · · · · · · · · · · · · · ·
_	3.6	100)250	0.46	, ,	Sheet Flow, Dense Graded Aggregate Yard
	0.0		0.0	,200	0.10		n= 0.040 P2= 2.40"
	1.3	230	0.0	100	3.07	9.20	
	1.0	200	0.0	, 100	0.01	0.20	Area= 3.0 sf Perim= 4.0' r= 0.75'
							n= 0.040 Earth, cobble bottom, clean sides
	0.4	105	5 0 0	050	4.20	7.43	Pipe Channel, driveway culvert
	0		0.0	,000	1.20	7.10	18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
							n= 0.013 Corrugated PE, smooth interior
_	5.3	435	5 To	tal			c.c.c cogatea, clooti interior

Subcatchment DR-9B: Roadway



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 10-Year Rainfall=3.63" Prepared by McFarland Johnson Printed 6/8/2022

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Inflow
Outflow

Summary for Reach 1R: Swale

Inflow Area = 1.900 ac, 84.21% Impervious, Inflow Depth > 3.05" for 10-Year event

Inflow = 9.10 cfs @ 11.96 hrs, Volume= 0.482 af

Outflow = 7.58 cfs @ 12.11 hrs, Volume= 0.482 af, Atten= 17%, Lag= 8.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.05 fps, Min. Travel Time= 5.6 min Avg. Velocity = 0.60 fps, Avg. Travel Time= 19.1 min

Peak Storage= 2,580 cf @ 12.01 hrs

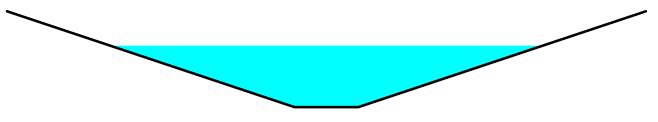
Average Depth at Peak Storage= 0.96', Surface Width= 6.77' Bank-Full Depth= 1.50' Flow Area= 8.3 sf, Capacity= 22.13 cfs

1.00' x 1.50' deep channel, n= 0.022 Earth, clean & straight

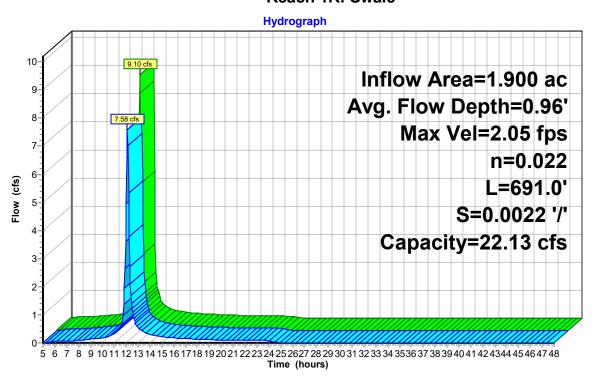
Side Slope Z-value= 3.0 '/' Top Width= 10.00'

Length= 691.0' Slope= 0.0022 '/'

Inlet Invert= 15.50', Outlet Invert= 14.00'



Reach 1R: Swale



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Inflow

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Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 1.93" for 10-Year event

Inflow 12.46 cfs @ 13.19 hrs, Volume= 4.590 af

Outflow 5.17 cfs @ 17.95 hrs, Volume= 4.381 af, Atten= 58%, Lag= 285.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.09 fps, Min. Travel Time= 192.0 min Avg. Velocity = 0.04 fps, Avg. Travel Time= 405.5 min

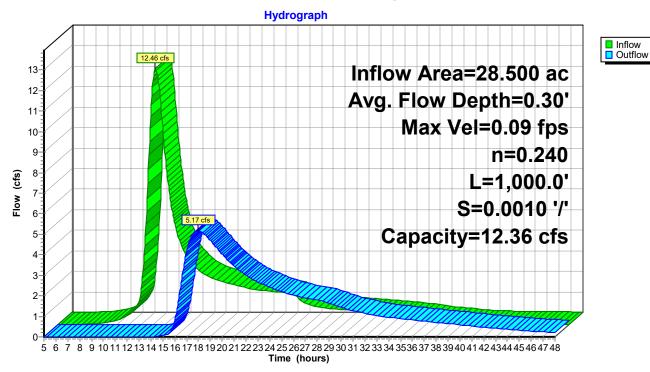
Peak Storage= 59,576 cf @ 14.75 hrs

Average Depth at Peak Storage= 0.30', Surface Width= 201.78' Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240 Side Slope Z-value= 3.0 '/' Top Width= 203.00' Length= 1,000.0' Slope= 0.0010 '/'

Inlet Invert= 6.00', Outlet Invert= 5.00'

Reach 1W: Wetland #1 / Analysis Point 1A



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Summary for Reach 2R: Overflow

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 2.45" for 10-Year event

Inflow = 0.64 cfs @ 14.62 hrs, Volume= 1.187 af

Outflow = 0.64 cfs @ 14.63 hrs, Volume= 1.186 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.94 fps, Min. Travel Time= 0.4 min Avg. Velocity = 1.56 fps, Avg. Travel Time= 0.5 min

Peak Storage= 16 cf @ 14.62 hrs

Average Depth at Peak Storage= 0.04', Surface Width= 8.24' Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 569.91 cfs

8.00' x 2.00' deep channel, n= 0.020 Corrugated PE, corrugated interior

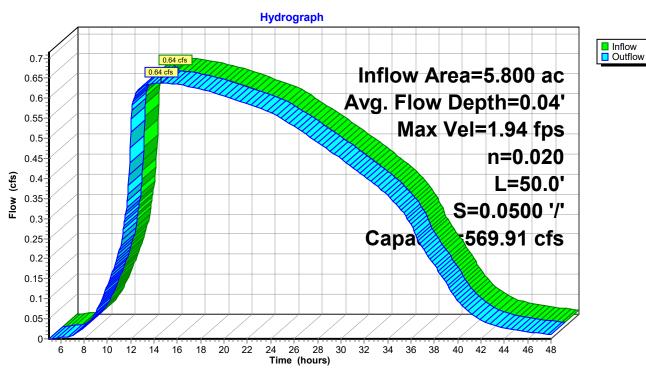
Side Slope Z-value= 3.0 '/' Top Width= 20.00'

Length= 50.0' Slope= 0.0500 '/'

Inlet Invert= 16.50', Outlet Invert= 14.00'



Reach 2R: Overflow



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Summary for Reach 3R: Outlet Pipe

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 1.84" for 10-Year event

Inflow = 5.17 cfs @ 17.95 hrs, Volume= 4.381 af

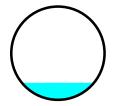
Outflow = 5.17 cfs @ 17.95 hrs, Volume= 4.381 af, Atten= 0%, Lag= 0.4 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

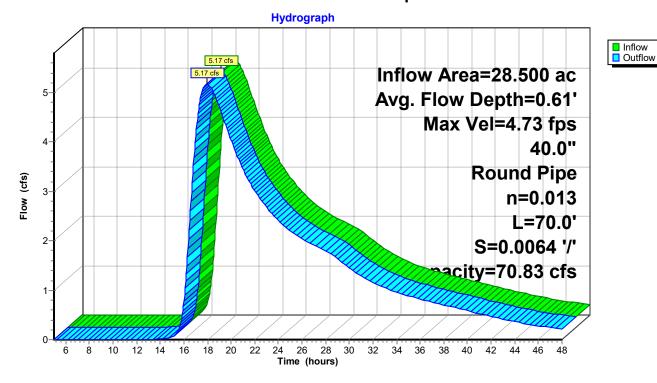
Max. Velocity= 4.73 fps, Min. Travel Time= 0.2 min Avg. Velocity = 2.76 fps, Avg. Travel Time= 0.4 min

Peak Storage= 76 cf @ 17.95 hrs Average Depth at Peak Storage= 0.61', Surface Width= 2.58' Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe n= 0.013 Corrugated PE, smooth interior Length= 70.0' Slope= 0.0064 '/' Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 3R: Outlet Pipe



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Inflow
Outflow

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Summary for Reach 4R: Overflow

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 3.05" for 10-Year event

Inflow = 4.69 cfs @ 11.98 hrs, Volume= 0.254 af

Outflow = 4.56 cfs @ 12.00 hrs, Volume= 0.254 af, Atten= 3%, Lag= 0.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.73 fps, Min. Travel Time= 0.6 min Avg. Velocity = 0.70 fps, Avg. Travel Time= 2.4 min

Peak Storage= 171 cf @ 11.99 hrs

Average Depth at Peak Storage= 0.41', Surface Width= 5.43' Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 118.65 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch

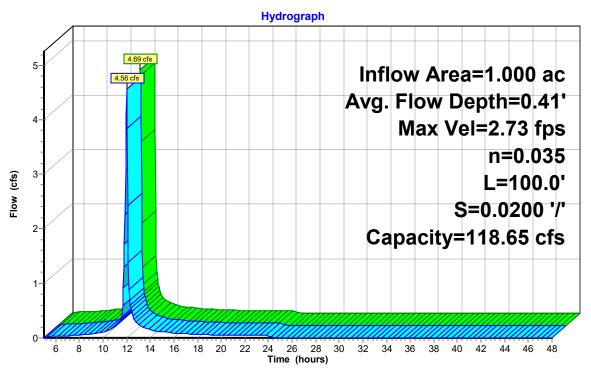
Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 100.0' Slope= 0.0200 '/'

Inlet Invert= 12.00', Outlet Invert= 10.00'



Reach 4R: Overflow



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Summary for Reach 5R: Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.00" for 10-Year event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 5.00 hrs

Average Depth at Peak Storage= 0.00'

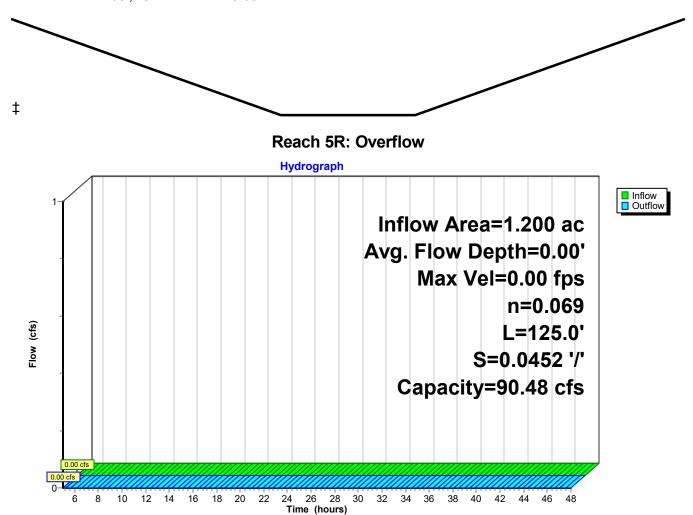
Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 90.48 cfs

3.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch

Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 125.0' Slope= 0.0452 '/'

Inlet Invert= 11.65', Outlet Invert= 6.00'



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InflowOutflow

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Summary for Reach 6R: Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.00" for 10-Year event

Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Outflow = $0.00 \text{ cfs } \bigcirc 0.00 \text{ sfs}$ Solution = 0.000 afs Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 5.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 116.91 cfs

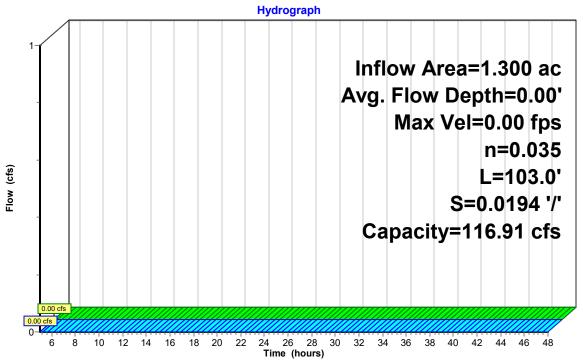
3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch

Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 103.0' Slope= 0.0194 '/'

Inlet Invert= 8.50', Outlet Invert= 6.50'





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Summary for Reach 7R: Overflow

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth > 2.70" for 10-Year event

Inflow = 0.39 cfs @ 14.15 hrs, Volume= 0.652 af

Outflow = 0.39 cfs @ 14.22 hrs, Volume= 0.652 af, Atten= 0%, Lag= 4.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.61 fps, Min. Travel Time= 2.7 min Avg. Velocity = 0.43 fps, Avg. Travel Time= 3.9 min

Peak Storage= 64 cf @ 14.18 hrs

Average Depth at Peak Storage= 0.08', Surface Width= 8.47' Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 116.81 cfs

8.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch

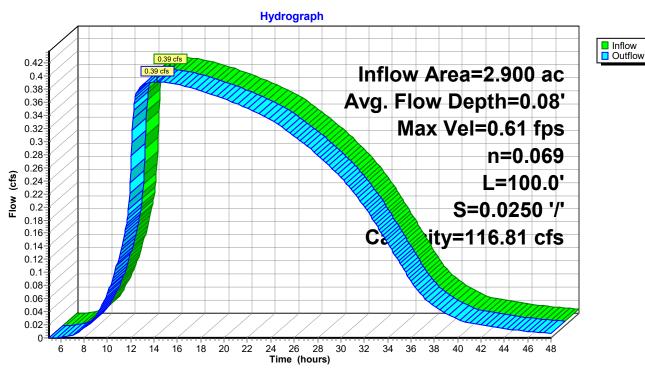
Side Slope Z-value= 3.0 '/' Top Width= 20.00'

Length= 100.0' Slope= 0.0250 '/'

Inlet Invert= 14.50', Outlet Invert= 12.00'



Reach 7R: Overflow



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Inflow
Outflow

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Summary for Reach 8R: Dry Swale #1

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 3.05" for 10-Year event

Inflow = 4.79 cfs @ 11.96 hrs, Volume= 0.254 af

Outflow = 4.69 cfs @ 11.98 hrs, Volume= 0.254 af, Atten= 2%, Lag= 1.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.92 fps, Min. Travel Time= 0.6 min Avg. Velocity = 0.77 fps, Avg. Travel Time= 2.3 min

Peak Storage= 169 cf @ 11.97 hrs

Average Depth at Peak Storage= 0.53', Surface Width= 4.11' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 16.53 cfs

2.00' x 1.00' deep channel, n= 0.018 Earth, clean & straight

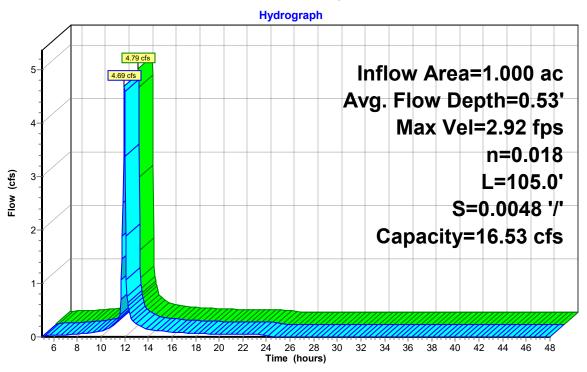
Side Slope Z-value= 2.0 '/' Top Width= 6.00'

Length= 105.0' Slope= 0.0048 '/'

Inlet Invert= 10.00', Outlet Invert= 9.50'



Reach 8R: Dry Swale #1



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Inflow
Outflow

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Summary for Reach 10R: Dry Swale #2

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 2.21" for 10-Year event

Inflow = 2.69 cfs @ 12.01 hrs, Volume= 0.140 af

Outflow = 2.62 cfs @ 12.02 hrs, Volume= 0.140 af, Atten= 3%, Lag= 0.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.08 fps, Min. Travel Time= 0.5 min Avg. Velocity = 1.13 fps, Avg. Travel Time= 1.7 min

Peak Storage= 75 cf @ 12.01 hrs

Average Depth at Peak Storage= 0.24', Surface Width= 3.44' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 213.76 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight

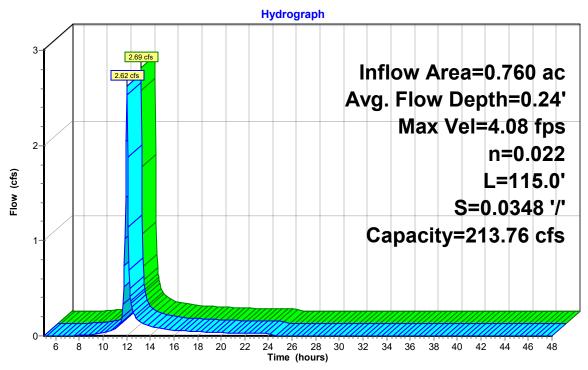
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 115.0' Slope= 0.0348 '/'

Inlet Invert= 37.00', Outlet Invert= 33.00'



Reach 10R: Dry Swale #2



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Outflow

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Summary for Reach 12R: Sediment Basin Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.46" for 10-Year event

Inflow = 0.26 cfs @ 12.31 hrs, Volume= 0.046 af

Outflow = 0.26 cfs @ 12.32 hrs, Volume= 0.046 af, Atten= 1%, Lag= 0.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.42 fps, Min. Travel Time= 0.2 min Avg. Velocity = 0.19 fps, Avg. Travel Time= 0.5 min

Peak Storage= 4 cf @ 12.32 hrs

Average Depth at Peak Storage= 0.06', Surface Width= 10.50' Bank-Full Depth= 0.50' Flow Area= 6.0 sf, Capacity= 9.43 cfs

10.00' x 0.50' deep channel, n= 0.069 Riprap, 6-inch

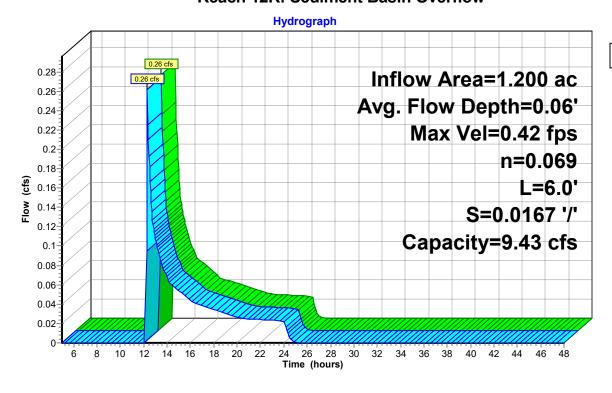
Side Slope Z-value= 4.0 '/' Top Width= 14.00'

Length= 6.0' Slope= 0.0167 '/'

Inlet Invert= 12.00', Outlet Invert= 11.90'



Reach 12R: Sediment Basin Overflow



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Summary for Reach 13R: Roadside Swale

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.63" for 10-Year event

Inflow = 1.16 cfs @ 11.99 hrs, Volume= 0.063 af

Outflow = 1.03 cfs @ 12.06 hrs, Volume= 0.063 af, Atten= 11%, Lag= 3.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.18 fps, Min. Travel Time= 2.2 min Avg. Velocity = 0.77 fps, Avg. Travel Time= 6.3 min

Peak Storage= 141 cf @ 12.02 hrs

Average Depth at Peak Storage= 0.27', Surface Width= 2.62' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.36 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight

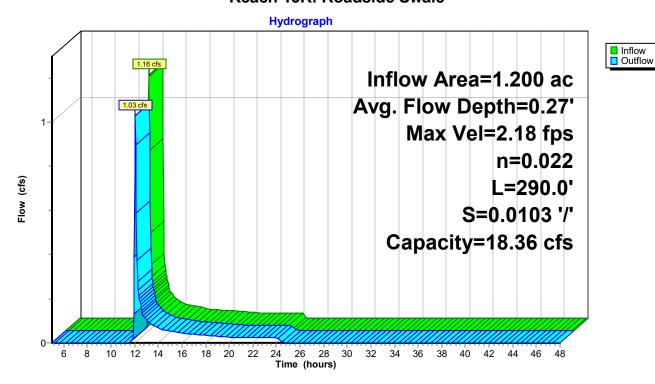
Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 290.0' Slope= 0.0103 '/'

Inlet Invert= 15.00', Outlet Invert= 12.00'



Reach 13R: Roadside Swale



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Inflow
Outflow

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Summary for Reach 14R: Roadside Swale

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 2.21" for 10-Year event

Inflow = 2.85 cfs @ 11.97 hrs, Volume= 0.140 af

Outflow = 2.69 cfs @ 12.01 hrs, Volume= 0.140 af, Atten= 6%, Lag= 2.4 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 5.12 fps, Min. Travel Time= 1.5 min Avg. Velocity = 1.44 fps, Avg. Travel Time= 5.3 min

Peak Storage= 250 cf @ 11.99 hrs

Average Depth at Peak Storage= 0.21', Surface Width= 3.25' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 289.37 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight

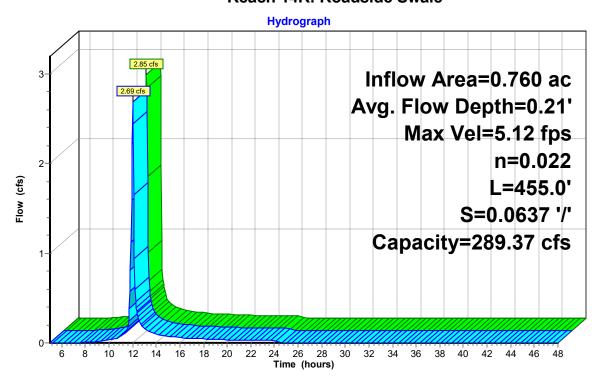
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 455.0' Slope= 0.0637 '/'

Inlet Invert= 66.00', Outlet Invert= 37.00'



Reach 14R: Roadside Swale



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Inflow
Outflow

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Summary for Reach 15R: Roadside Swale

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 1.27" for 10-Year event

Inflow = 2.86 cfs @ 11.98 hrs, Volume= 0.137 af

Outflow = 2.02 cfs @ 12.17 hrs, Volume= 0.137 af, Atten= 29%, Lag= 11.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.95 fps, Min. Travel Time= 7.5 min Avg. Velocity = 0.27 fps, Avg. Travel Time= 26.8 min

Peak Storage= 939 cf @ 12.04 hrs

Average Depth at Peak Storage= 0.70', Surface Width= 5.22' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 4.69 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight

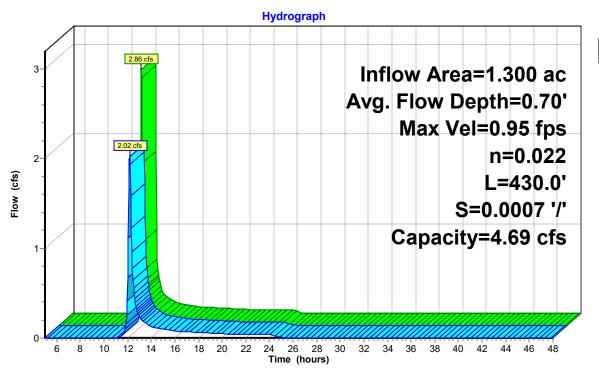
Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 430.0' Slope= 0.0007 '/'

Inlet Invert= 10.00', Outlet Invert= 9.71'



Reach 15R: Roadside Swale



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Summary for Reach 17R: Sediment Basin Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.91" for 10-Year event

Inflow = 1.45 cfs @ 12.31 hrs, Volume= 0.098 af

Outflow = 1.33 cfs @ 12.32 hrs, Volume= 0.098 af, Atten= 9%, Lag= 0.5 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 0.67 fps, Min. Travel Time= 0.1 min Avg. Velocity = 0.17 fps, Avg. Travel Time= 0.6 min

Peak Storage= 12 cf @ 12.32 hrs

Average Depth at Peak Storage= 0.13', Surface Width= 16.07' Bank-Full Depth= 0.70' Flow Area= 12.5 sf, Capacity= 24.64 cfs

15.00' x 0.70' deep channel, n= 0.069 Riprap, 6-inch

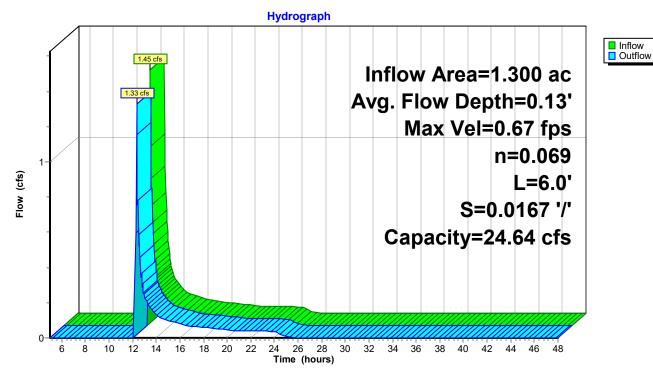
Side Slope Z-value= 4.0 '/' Top Width= 20.60'

Length= 6.0' Slope= 0.0167 '/'

Inlet Invert= 9.00', Outlet Invert= 8.90'



Reach 17R: Sediment Basin Overflow



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Summary for Pond 1P: WQv Pond #1

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth = 2.73" for 10-Year event

Inflow = 8.78 cfs @ 12.07 hrs, Volume= 0.660 af

Outflow = 0.39 cfs @ 14.15 hrs, Volume= 0.652 af, Atten= 96%, Lag= 125.0 min

Primary = 0.39 cfs @ 14.15 hrs, Volume= 0.652 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Starting Elev= 14.00' Surf.Area= 9,229 sf Storage= 19,003 cf

Peak Elev= 15.59' @ 14.15 hrs Surf.Area= 19,456 sf Storage= 36,781 cf (17,778 cf above start)

Plug-Flow detention time= 1,195.5 min calculated for 0.216 af (33% of inflow)

Center-of-Mass det. time= 536.4 min (1,336.8 - 800.3)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,795 cf	Forebay (Prismatic) Listed below (Recalc)
#2	9.00'	57,882 cf	Permanent Pool (Prismatic) Listed below (Recalc)

	62	,677 cf Total Av	ailable Storage				
Elevation	Surf.Area	Inc.Store	Cum.Store				
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)				
10.00	232	0	0				
11.00	569	401	401				
12.00	1,018	794	1,194				
13.00	1,467	1,243	2,437				
14.00	3,249	2,358	4,795				
	,	,	,				
Elevation	Surf.Area	Inc.Store	Cum.Store				
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)				
9.00	1,145	0	0				
10.00	1,751	1,448	1,448				
11.00	2,339	2,045	3,493				
12.00	2,959	2,649	6,142				
13.00	3,597	3,278	9,420				
14.00	5,980	4,789	14,209				
14.50	7,240	3,305	17,514				
15.00	14,392	5,408	22,922				
16.00	17,455	15,924	38,845				
17.00	20,619	19,037	57,882				

Device	Routing	Invert	Outlet Devices
#1	Primary	13.50'	12.0" Round Culvert
	•		L= 50.0' Box, headwall w/3 square edges, Ke= 0.500
			Inlet / Outlet Invert= 13.50' / 13.23' S= 0.0054 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	16.00'	24.0" x 24.0" Horiz. Outlet Structure Top Grate
			C= 0.600 in 24.0" x 24.0" Grate (100% open area)
			Limited to weir flow at low heads
#3	Device 1	14.00'	4.0" Round Reverse Slope Pipe
			L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 9.00' / 14.00' S= -0.1250 '/' Cc= 0.900

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n= 0.010 PVC, smooth interior, Flow Area= 0.09 sf

6.0' long x 1.0' breadth Broad-Crested Rectangular Weir

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00

2.50 3.00

Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31

3.30 3.31 3.32

Primary OutFlow Max=0.39 cfs @ 14.15 hrs HW=15.59' (Free Discharge)

-1=Culvert (Passes 0.39 cfs of 4.20 cfs potential flow)

16.25'

#4

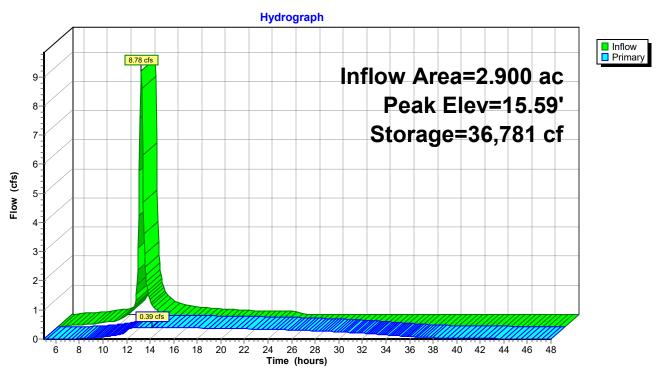
Primary

2=Outlet Structure Top Grate (Controls 0.00 cfs)

-3=Reverse Slope Pipe (Outlet Controls 0.39 cfs @ 4.48 fps)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: WQv Pond #1



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Summary for Pond 2P: WQv Pond #2

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 2.47" for 10-Year event

Inflow = 21.14 cfs @ 11.97 hrs, Volume= 1.195 af

Outflow = 0.64 cfs @ 14.62 hrs, Volume= 1.187 af, Atten= 97%, Lag= 158.7 min

Primary = 0.64 cfs @ 14.62 hrs, Volume= 1.187 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Starting Elev= 14.00' Surf.Area= 5,917 sf Storage= 9,000 cf

Peak Elev= 16.47' @ 14.62 hrs Surf.Area= 24,629 sf Storage= 41,496 cf (32,496 cf above start)

Plug-Flow detention time= 808.8 min calculated for 0.980 af (82% of inflow)

Center-of-Mass det. time= 597.8 min (1,399.8 - 802.0)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,020 cf	Forebay #1 (Prismatic) Listed below (Recalc)
#2	10.00'	2,575 cf	Forebay #2 (Prismatic) Listed below (Recalc)
#3	10.00'	58,093 cf	Permanent Pool (Prismatic) Listed below (Recalc)

64,688 cf Total Available Storage

		•	J
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	141	0	0
11.00	330	236	236
12.00	562	446	682
13.00	866	714	1,396
14.00	2,023	1,445	2,840
14.50	2,696	1,180	4,020
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
			<u>, </u>
10.00	82	0	0
11.00	202	142	142
12.00	351	277	419
13.00	535	443	862
14.00	1,323	929 705	1,791
14.50	1,815	785	2,575
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	375	0	0
11.00	653	514	514
12.00	957	805	1,319
13.00	1,286	1,122	2,441
14.00	2,571	1,929	4,369
14.50	3,307	1,470	5,839
15.00	13,814	4,280	10,119
16.00	17,852	15,833	25,952
17.00	22,659	20,256	46,207
17.50	24,884	11,886	58,093

18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 10-Year Rainfall=3.63"

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Device	Routing	Invert	Outlet Devices
#1	Device 3	16.50'	24.0" x 24.0" Horiz. Orifice/Grate
			C= 0.600 in 24.0" x 24.0" Grate (100% open area)
			Limited to weir flow at low heads
#2	Device 3	14.00'	4.0" Vert. Reverse Slope Pipe C= 0.600
			Limited to weir flow at low heads
#3	Primary	14.00'	12.0" Round Outlet Structure Discard Pipe
			L= 46.0' Box, headwall w/3 square edges, Ke= 0.500
			Inlet / Outlet Invert= 14.00' / 13.77' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#4	Primary	16.60'	10.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.64 cfs @ 14.62 hrs HW=16.47' (Free Discharge)

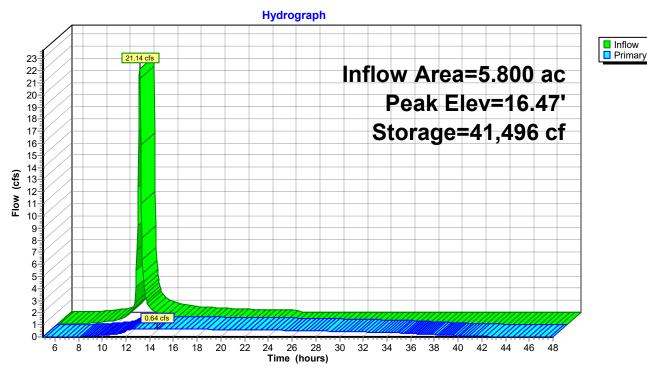
—3=Outlet Structure Discard Pipe (Passes 0.64 cfs of 4.79 cfs potential flow)

1=Orifice/Grate (Controls 0.00 cfs)

—2=Reverse Slope Pipe (Orifice Controls 0.64 cfs @ 7.31 fps)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 2P: WQv Pond #2



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Summary for Pond 3P: Infiltration Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.46" for 10-Year event

Inflow = 0.26 cfs @ 12.32 hrs, Volume= 0.046 af

Outflow = 0.02 cfs @ 24.21 hrs, Volume= 0.034 af, Atten= 94%, Lag= 713.8 min

Discarded = 0.02 cfs @ 24.21 hrs, Volume = 0.034 afPrimary = 0.00 cfs @ 5.00 hrs, Volume = 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 11.15' @ 24.21 hrs Surf.Area= 1,004 sf Storage= 1,468 cf

Plug-Flow detention time= 879.4 min calculated for 0.034 af (73% of inflow)

Center-of-Mass det. time= 771.6 min (1,748.3 - 976.8)

Volume	Inver	t Avai	l.Storage	Storage Descriptio	n		
#1	8.10)'	2,492 cf	Custom Stage Date	ta (Irregular) Listed	d below (Recalc)	
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
8.1	-	109	56.0	0	0	109	
12.0	00	1,415	149.0	2,492	2,492	1,678	
Device	Routing	In	vert Outle	et Devices			
#1	Primary	11	.65' Cha	nnel/Reach using	Reach 5R: Overflo	W	
#2	Discarded	l 8	.10' 0.50	0 in/hr Exfiltration	over Surface area		
			Con	ductivity to Groundy	vater Elevation = 4.	00'	

Discarded OutFlow Max=0.02 cfs @ 24.21 hrs HW=11.15' (Free Discharge) **2=Exfiltration** (Controls 0.02 cfs)

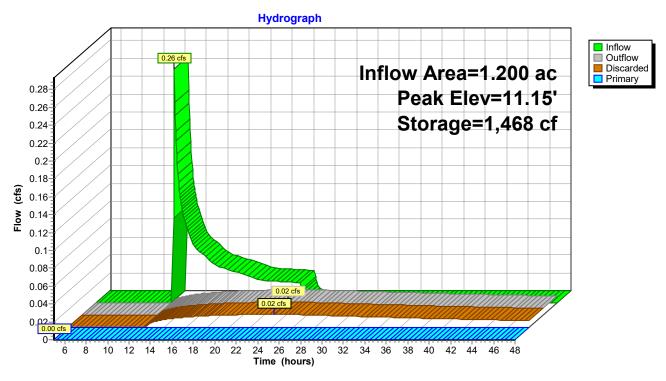
Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=8.10' (Free Discharge)
—1=Channel/Reach (Controls 0.00 cfs)

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Pond 3P: Infiltration Basin #1



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Summary for Pond 4P: Infiltration Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.91" for 10-Year event

Inflow = 1.33 cfs @ 12.32 hrs, Volume= 0.098 af

Outflow = 0.26 cfs @ 12.92 hrs, Volume= 0.098 af, Atten= 80%, Lag= 35.5 min

Discarded = 0.26 cfs @ 12.92 hrs, Volume= 0.098 afPrimary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 8.10' @ 12.92 hrs Surf.Area= 701 sf Storage= 834 cf

Plug-Flow detention time= 35.0 min calculated for 0.098 af (100% of inflow)

Center-of-Mass det. time= 35.0 min (973.5 - 938.5)

Volume	Invert	: Avail	.Storage	Storage Description	n		
#1	5.80	1	2,495 cf	Custom Stage Dat	a (Irregular) Listed	below (Recalc)	
Elevation (fee		urf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
5.8 9.7		110 1,415	56.0 150.0	0 2,495	0 2,495	110 1,702	
Device	Routing	ln۱	ert Outle	et Devices			
#2 Discarded 5.80' 12.0		annel/Reach using Reach 6R: Overflow 000 in/hr Exfiltration over Surface area nductivity to Groundwater Elevation = 3.00'					

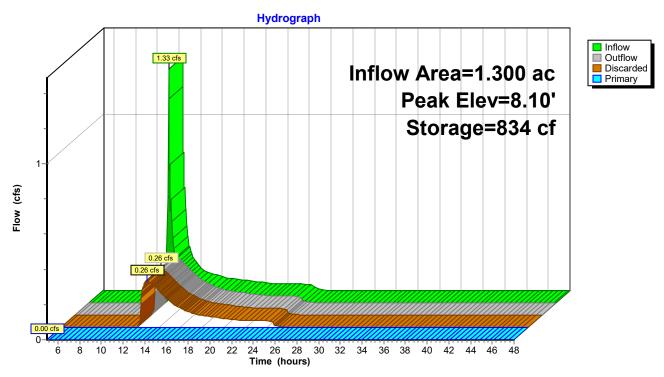
Discarded OutFlow Max=0.26 cfs @ 12.92 hrs HW=8.10' (Free Discharge) **2=Exfiltration** (Controls 0.26 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=5.80' (Free Discharge)
—1=Channel/Reach (Controls 0.00 cfs)

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Pond 4P: Infiltration Basin #2



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Summary for Pond 5P: Sedimentation Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.63" for 10-Year event

Inflow = 1.03 cfs @ 12.06 hrs, Volume= 0.063 af

Outflow = 0.26 cfs @ 12.31 hrs, Volume= 0.046 af, Atten= 74%, Lag= 15.4 min

Primary = 0.26 cfs @ 12.31 hrs, Volume= 0.046 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 12.06' @ 12.32 hrs Surf.Area= 566 sf Storage= 783 cf

Plug-Flow detention time= 185.4 min calculated for 0.046 af (73% of inflow)

Center-of-Mass det. time= 71.3 min (976.1 - 904.8)

Volume	Inv	ert Avai	I.Storage	Storage Descrip	otion		
#1	9.0	00'	1,058 cf	Custom Stage	Data (Irregular) Lis	sted below (Recalc	:)
Elevation (fee		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet	• • • • • • • • • • • • • • • • • • • •	Wet.Area (sq-ft)	
9.0	00	41	25.8	(0	41	
10.0	00	150	46.7	90	90	167	
11.0	00	320	66.6	230	320	355	
12.0		550	86.4	430	749	608	
12.5	50	687	96.2	309	1,058	758	
Device	Routing	In	vert Outle	et Devices			
#1	Primary	12	2.00' Cha	nnel/Reach usi	ng Reach 12R: Sed	diment Basin Over	flow

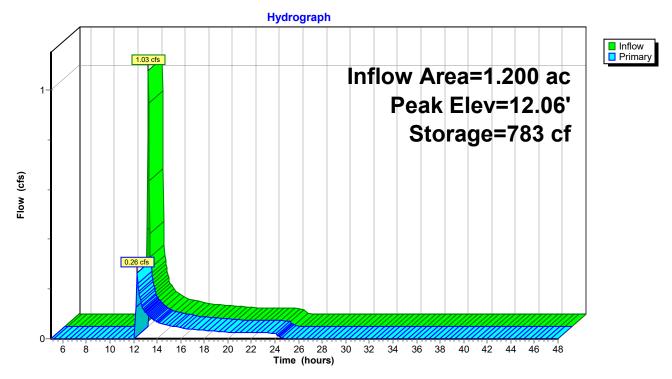
Primary OutFlow Max=0.24 cfs @ 12.31 hrs HW=12.06' (Free Discharge)

1=Channel/Reach (Channel Controls 0.24 cfs @ 0.41 fps)

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Pond 5P: Sedimentation Basin #1



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Summary for Pond 16P: Sedimentation Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 1.27" for 10-Year event

Inflow = 2.02 cfs @ 12.17 hrs, Volume= 0.137 af

Outflow = 1.45 cfs @ 12.31 hrs, Volume= 0.098 af, Atten= 28%, Lag= 8.9 min

Primary = 1.45 cfs @ 12.31 hrs, Volume= 0.098 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 9.14' @ 12.32 hrs Surf.Area= 928 sf Storage= 1,826 cf

Plug-Flow detention time= 174.4 min calculated for 0.098 af (72% of inflow)

Center-of-Mass det. time= 62.3 min (938.0 - 875.7)

Volume	Inv	ert Ava	il.Storage	Storage Desc	ription			
#1	5.8	30'	2,389 cf	Custom Stag	e Data (Irre	egular) Liste	d below (Recalc)	
Elevation (fee		Surf.Area (sq-ft)	Perim. (feet)	Inc.Sto (cubic-fe		um.Store ubic-feet)	Wet.Area (sq-ft)	
5.8	30	224	80.0		0	0	224	
6.0	00	257	83.0		48	48	266	
7.0	00	438	98.0	3	44	392	500	
8.0	00	650	113.0	5	41	932	773	
9.0	00	892	128.0	7	68	1,700	1,085	
9.7	70	1,079	139.0	6	89	2,389	1,337	
Device	Routing	In	vert Outle	et Devices				
#1	Primary	g	0.00' Cha	nnel/Reach u	sing Reach	17R: Sedin	nent Basin Overflow	

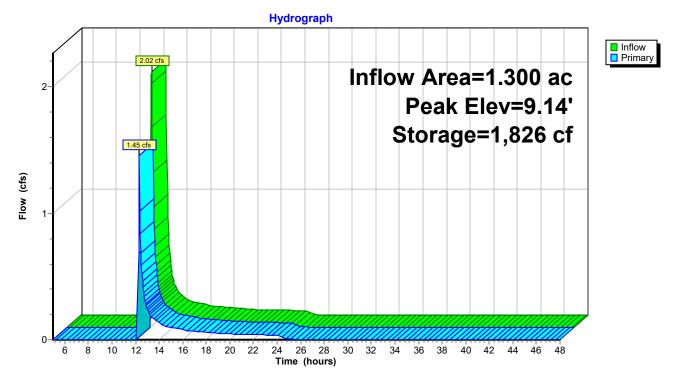
Primary OutFlow Max=1.25 cfs @ 12.31 hrs HW=9.12' (Free Discharge)

1=Channel/Reach (Channel Controls 1.25 cfs @ 0.67 fps)

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Pond 16P: Sedimentation Basin #2



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Summary for Pond AP-1: Analysis Point #1

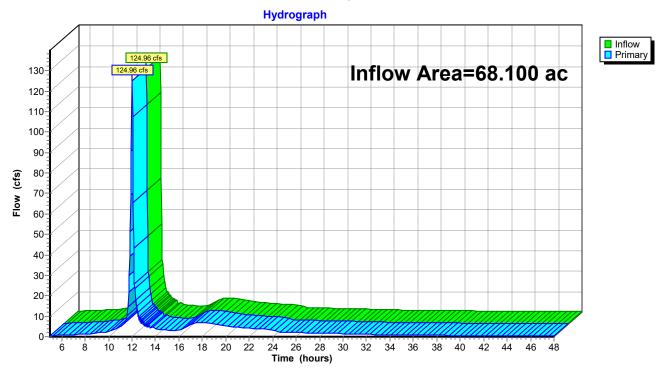
Inflow Area = 68.100 ac, 20.36% Impervious, Inflow Depth > 1.94" for 10-Year event

Inflow = 124.96 cfs @ 12.01 hrs, Volume= 10.994 af

Primary = 124.96 cfs @ 12.01 hrs, Volume= 10.994 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1



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Summary for Pond AP-2: Analysis Point #2

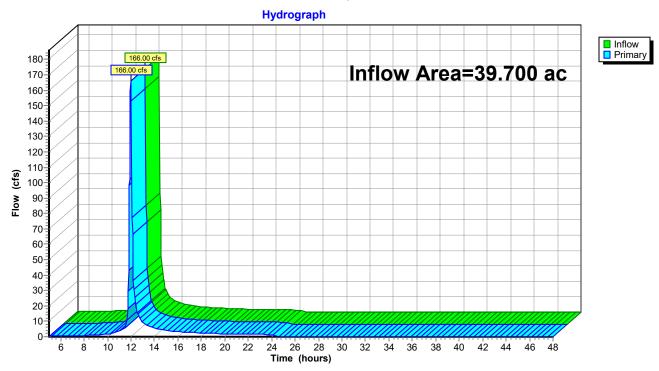
Inflow Area = 39.700 ac, 23.10% Impervious, Inflow Depth > 2.53" for 10-Year event

Inflow = 166.00 cfs @ 11.97 hrs, Volume= 8.362 af

Primary = 166.00 cfs @ 11.97 hrs, Volume= 8.362 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2



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Summary for Pond AP-3: Analysis Point #3

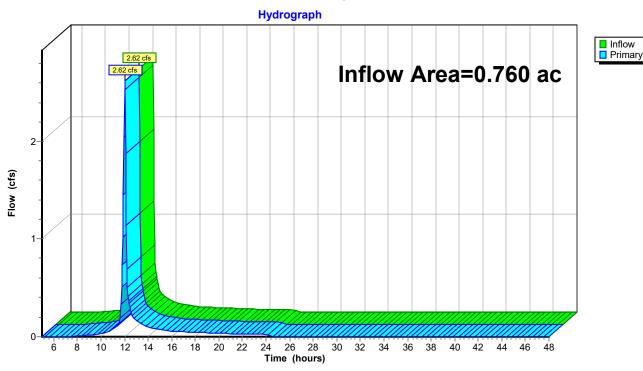
Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 2.21" for 10-Year event

Inflow = 2.62 cfs @ 12.02 hrs, Volume= 0.140 af

Primary = 2.62 cfs @ 12.02 hrs, Volume= 0.140 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3



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Summary for Pond C-1: Chamber Series 1

Inflow Area = 10.300 ac, 66.70% Impervious, Inflow Depth > 3.23" for 10-Year event Inflow 49.84 cfs @ 11.98 hrs, Volume= 2.772 af 50.37 cfs @ 11.97 hrs, Volume= Outflow 2.412 af, Atten= 0%, Lag= 0.0 min 0.13 cfs @ 11.97 hrs, Volume= Discarded = 0.347 af Primary 50.24 cfs @ 11.97 hrs, Volume= 2.065 af Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 13.64' @ 11.97 hrs Surf.Area= 12,440 sf Storage= 29,816 cf

Plug-Flow detention time= 222.6 min calculated for 2.411 af (87% of inflow) Center-of-Mass det. time= 160.8 min (929.8 - 769.0)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	11,722 cf	37.08'W x 227.97'L x 5.50'H Field B
			46,496 cf Overall - 17,192 cf Embedded = 29,305 cf x 40.0% Voids
#2B	6.75'	17,192 cf	ADS_StormTech MC-3500 d +Cap x 155 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			155 Chambers in 5 Rows
			Cap Storage= +14.9 cf x 2 x 5 rows = 149.0 cf
#3	13.25'	6,100 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		35,013 cf	Total Available Storage

Storage Group B created with Chamber Wizard

	Elevation	Surf.Area	Inc.Store	Cum.Store
_	(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
	13.25	600	0	0
	13.75	4,900	1,375	1,375
	14.00	8,200	1,638	3,013
	14.25	16,500	3,088	6,100

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	10.00'	36.0" Round Culvert
	-		L= 55.9' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 10.00' / 7.59' S= 0.0431 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	14.24'	50.0' long x 0.7' breadth Concrete Curb
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50
			Coef. (English) 2.76 2.82 2.93 3.09 3.18 3.22 3.27 3.30 3.32
			3.31 3.32

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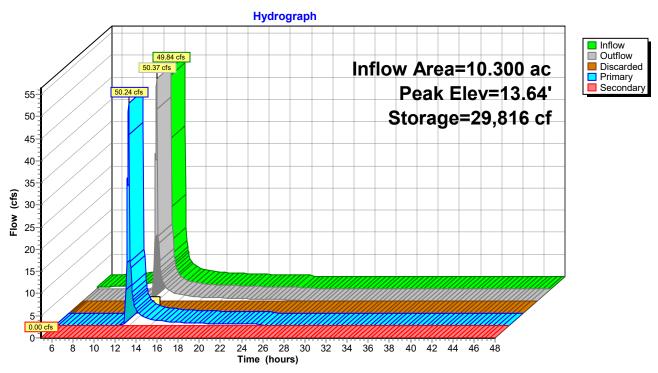
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Discarded OutFlow Max=0.13 cfs @ 11.97 hrs HW=13.50' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.13 cfs)

Primary OutFlow Max=48.14 cfs @ 11.97 hrs HW=13.50' (Free Discharge) 2=Culvert (Inlet Controls 48.14 cfs @ 6.81 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.01' (Free Discharge) 3=Concrete Curb (Controls 0.00 cfs)

Pond C-1: Chamber Series 1



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Summary for Pond C-4: Chamber Series 4

Inflow Area =	8.900 ac,	0.00% Impervious, Inflo	w Depth > 2.95"	for 10-Year event
Inflow =	39.82 cfs @	11.99 hrs, Volume=	2.188 af	
Outflow =	44.40 cfs @	11.96 hrs, Volume=	1.858 af, Atte	en= 0%, Lag= 0.0 min
Discarded =	0.08 cfs @	11.95 hrs, Volume=	0.261 af	
Primary =	44.32 cfs @	11.96 hrs, Volume=	1.597 af	
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 14.18' @ 11.96 hrs Surf.Area= 7,104 sf Storage= 21,828 cf

Plug-Flow detention time= 221.0 min calculated for 1.858 af (85% of inflow) Center-of-Mass det. time= 153.0 min (936.6 - 783.6)

Invert	Avail.Storage	Storage Description
6.00'	8,911 cf	29.92'W x 213.63'L x 5.50'H Field B
		35,151 cf Overall - 12,874 cf Embedded = 22,277 cf x 40.0% Voids
6.75'	12,874 cf	ADS_StormTech MC-3500 d +Cap x 116 Inside #1
		Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
		Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
		116 Chambers in 4 Rows
		Cap Storage= +14.9 cf x 2 x 4 rows = 119.2 cf
14.10'	8,015 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
	29,800 cf	Total Available Storage
	6.00' 6.75'	6.00' 8,911 cf 6.75' 12,874 cf 14.10' 8,015 cf

Storage Group B created with Chamber Wizard

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
14.10	400	0	0
14.60	2,400	700	700
14.80	6,300	870	1,570
15.10	10,000	2,445	4,015
15.50	10,000	4,000	8,015

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	11.00'	36.0" Round Culvert
	-		L= 24.3' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 11.00' / 9.42' S= 0.0650 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

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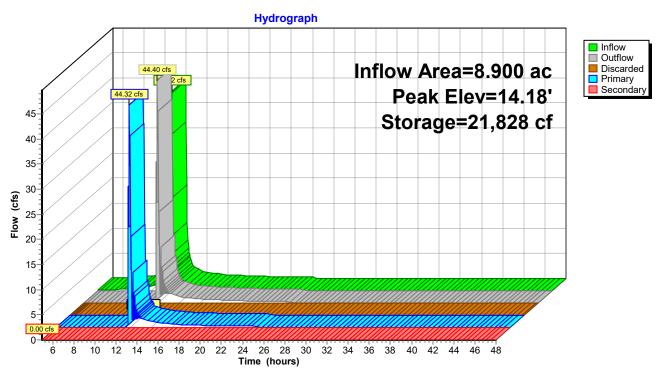
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Discarded OutFlow Max=0.08 cfs @ 11.95 hrs HW=14.15' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.08 cfs)

Primary OutFlow Max=42.04 cfs @ 11.96 hrs HW=14.03' (Free Discharge) 2=Culvert (Inlet Controls 42.04 cfs @ 5.95 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge) 3=Wharf (Controls 0.00 cfs)

Pond C-4: Chamber Series 4



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Summary for Pond C-5: Chamber Series 5

Inflow Area =	5.200 ac,	0.00% Impervious, Inflo	w Depth > 2.95"	for 10-Year event
Inflow =	23.53 cfs @	11.98 hrs, Volume=	1.279 af	
Outflow =	24.69 cfs @	12.02 hrs, Volume=	1.023 af, Atte	en= 0%, Lag= 2.2 min
Discarded =	0.19 cfs @	12.00 hrs, Volume=	0.391 af	
Primary =	24.51 cfs @	12.02 hrs, Volume=	0.633 af	
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 15.19' @ 12.02 hrs Surf.Area= 16,669 sf Storage= 24,121 cf

Plug-Flow detention time= 425.0 min calculated for 1.022 af (80% of inflow) Center-of-Mass det. time= 347.1 min (1,130.4 - 783.3)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	7,757 cf	28.50'W x 168.47'L x 6.75'H Field B
			32,409 cf Overall - 13,016 cf Embedded = 19,393 cf x 40.0% Voids
#2B	6.75'	13,016 cf	ADS_StormTech MC-4500 b +Cap x 120 Inside #1
			Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf
			Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap
			120 Chambers in 3 Rows
			Cap Storage= +39.5 cf x 2 x 3 rows = 237.0 cf
#3	14.60'	7,420 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		28,193 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sg-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
14.60	200	Ó	0
14.80	1,000	120	120
15.00	10,000	1,100	1,220
15.50	14,800	6,200	7,420

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	1.000 in/hr Exfiltration over Surface area
#2	Primary	12.60'	36.0" Round Culvert
			L= 62.8' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 12.60' / 12.29' S= 0.0049 '/' Cc= 0.900
			n= 0.013 Cast iron, coated, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

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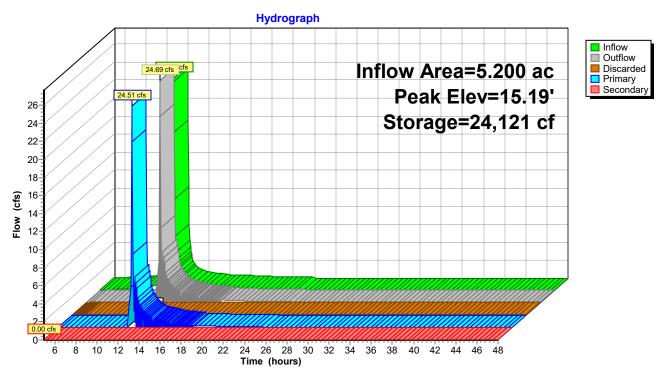
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Discarded OutFlow Max=0.19 cfs @ 12.00 hrs HW=14.85' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.19 cfs)

Primary OutFlow Max=21.56 cfs @ 12.02 hrs HW=14.81' (Free Discharge) 2=Culvert (Barrel Controls 21.56 cfs @ 5.38 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge) 3=Wharf (Controls 0.00 cfs)

Pond C-5: Chamber Series 5



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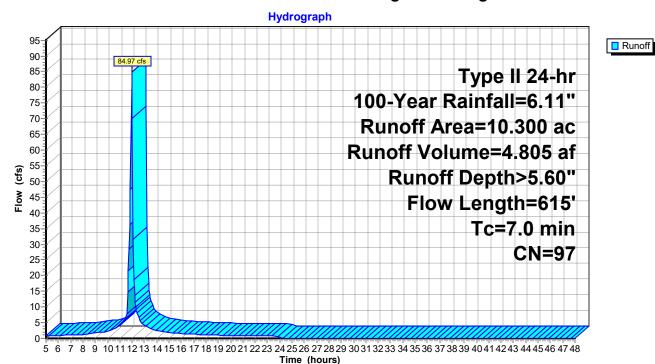
Summary for Subcatchment DR-1: Building A & Storage

Runoff = 84.97 cfs @ 11.98 hrs, Volume= 4.805 af, Depth> 5.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	cription						
*	6.	870	98	Building A							
	0.100 80			>75%	>75% Grass cover, Good, HSG D						
*	3.	330	95	Dens	Dense Graded Aggregate						
	10.	300	97	Weig	Weighted Average						
	3.	430		33.3	0% Pervio	us Area					
	6.870				0% Imperv	ious Area					
	Тс	Length	n S	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.3	100	0.0	0100	0.50		Sheet Flow,				
							n= 0.023 P2= 2.40"				
	3.1	300	0.0	0100	1.61		Shallow Concentrated Flow,				
							Unpaved Kv= 16.1 fps				
	0.6	215	0.0	0050	5.91	29.00	Pipe Channel,				
							30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'				
							n= 0.013				
	7.0	615	5 To	otal							

Subcatchment DR-1: Building A & Storage



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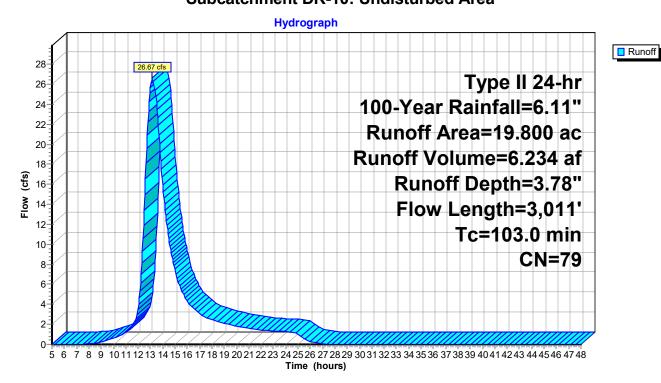
Summary for Subcatchment DR-10: Undisturbed Area

Runoff = 26.67 cfs @ 13.16 hrs, Volume= 6.234 af, Depth= 3.78"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

Area (ac) CN Description									
19.	800 7	'9 Woo	ds, Fair, F	ISG D					
19.	800	100.	00% Pervi	ous Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
19.7	150	0.0800	0.13		Sheet Flow,				
3.0	200	0.0500	1.12		Woods: Light underbrush n= 0.400 P2= 2.40" Shallow Concentrated Flow,				
0.0	200	0.0000	1.12		Woodland Kv= 5.0 fps				
1.6	250	0.2600	2.55		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
78.7	2,361	0.0100	0.50		Shallow Concentrated Flow, Wetland Flow				
0.0	50	0.0500	22.86	161.57	Woodland Kv= 5.0 fps Pipe Channel,				
0.0	30	0.0300	22.00	101.51	36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'				
					n= 0.012 Corrugated PP, smooth interior				
103.0	3,011	Total							

Subcatchment DR-10: Undisturbed Area



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Summary for Subcatchment DR-11: Hudson River Bank

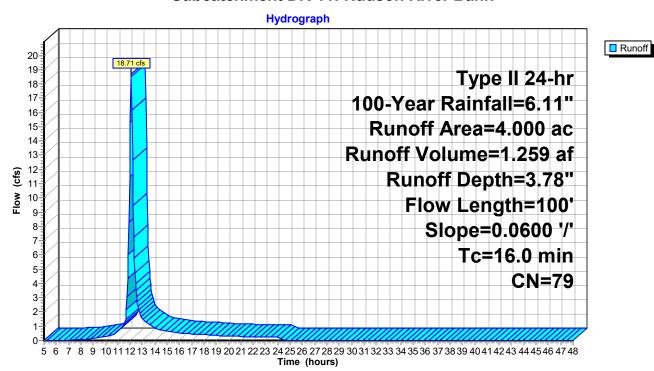
Runoff = 18.71 cfs @ 12.08 hrs, Volume= 1.259 af, Depth= 3.78"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

Area (ac) CN Description							
	4.	.000	79 Woo	ods, Fair, F	ISG D		
	4.	.000	100.	00% Pervi	ous Area		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	16.0	100	0.0600	0.10		Sheet Flow,	

Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-11: Hudson River Bank



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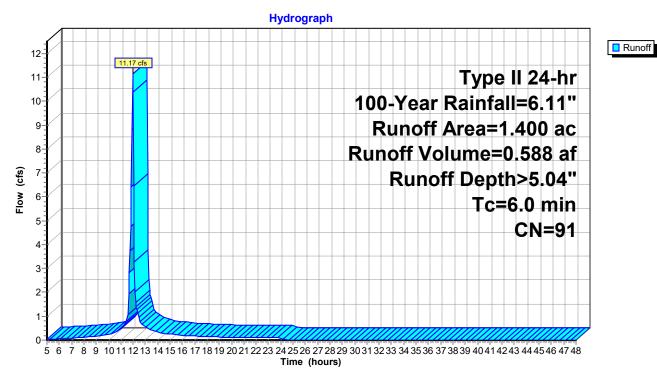
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Summary for Subcatchment DR-12: Normans Kill Bank

Runoff = 11.17 cfs @ 11.96 hrs, Volume= 0.588 af, Depth> 5.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

Subcatchment DR-12: Normans Kill Bank



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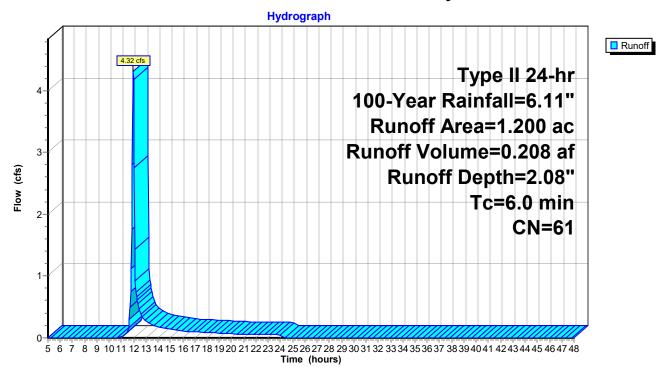
Summary for Subcatchment DR-13: Roadway

Runoff = 4.32 cfs @ 11.98 hrs, Volume= 0.208 af, Depth= 2.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

Area (ac) CN Description										
*	0.	450	98	Pave	Pavement					
	0.	750	39	>75%	√ Grass co	over, Good	I, HSG A			
1.200 61 Weighted Average						age				
0.750 62.50% Pervious Area						us Area				
	0.450			37.5	0% Imperv	ious Area				
	Тс	Leng	th	Slope	Velocity	Capacity	Description			
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	6.0						Direct Entry, Min			

Subcatchment DR-13: Roadway



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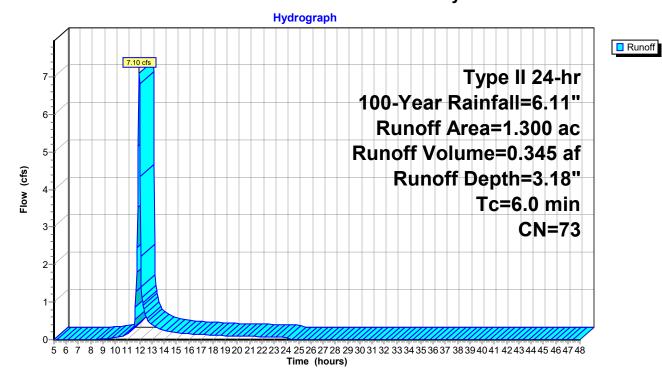
Summary for Subcatchment DR-14: Roadway

Runoff = 7.10 cfs @ 11.97 hrs, Volume= 0.345 af, Depth= 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	cription						
*	0.	550	98	New	New Pavement						
	0.	550	39	>75%	>75% Grass cover, Good, HSG A						
*	0.	200	98	98 Mill & Fill of Old Pavement							
	1.	300	73	Weig	ghted Aver	age					
	0.	550		42.3	1% Pervio	us Area					
	0.	750		57.69	9% Imperv	ious Area					
	т.		41.	01	V/-126	0	D				
	Tc	Leng		Slope	Velocity	Capacity	Description				
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)					
	6.0						Direct Entry, Min				

Subcatchment DR-14: Roadway



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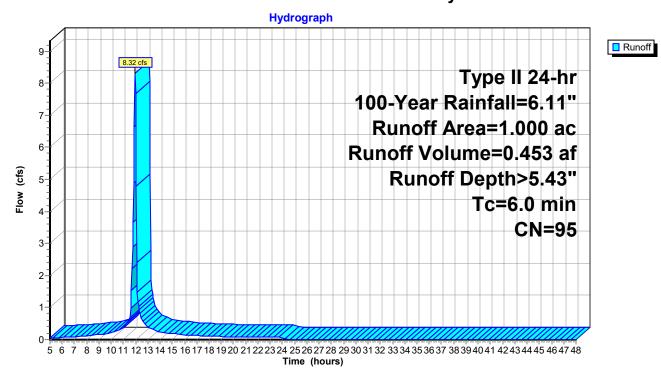
Summary for Subcatchment DR-15: Roadway

Runoff = 8.32 cfs @ 11.96 hrs, Volume= 0.453 af, Depth> 5.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	cription						
*	0.	050	98	New	New Pavement						
	0.	050	39	>75%	>75% Grass cover, Good, HSG A						
*	0.	900	0 98 Mill & Fill of Old Pavement								
	1.	000	95	Weig	ghted Aver						
	0.	050		5.00	% Perviou	s Area					
	0.	950		95.0	0% Imperv	ious Area					
	_										
	Tc	Leng	ıth	Slope	Velocity	Capacity	Description				
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)					
	6.0						Direct Entry, Min				

Subcatchment DR-15: Roadway



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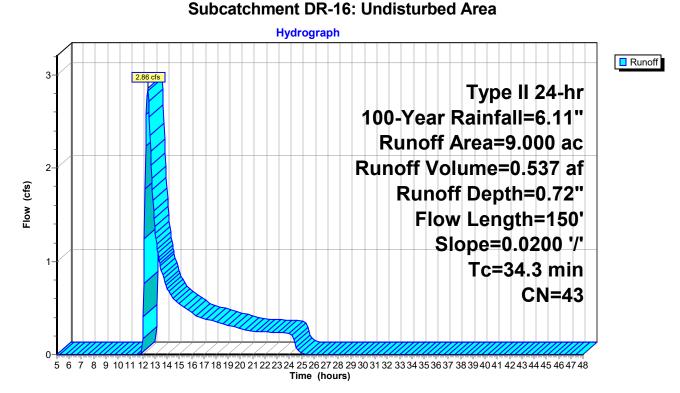
Summary for Subcatchment DR-16: Undisturbed Area

Runoff = 2.86 cfs @ 12.41 hrs, Volume= 0.537 af, Depth= 0.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

 Area (ac) CN Description									
9.	000 4	3 Woo	ds/grass d	omb., Fair,	, HSG A				
9.	000	100.	00% Pervi	ous Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
34.3	150	0.0200	0.07		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"				

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Summary for Subcatchment DR-17: Roadway

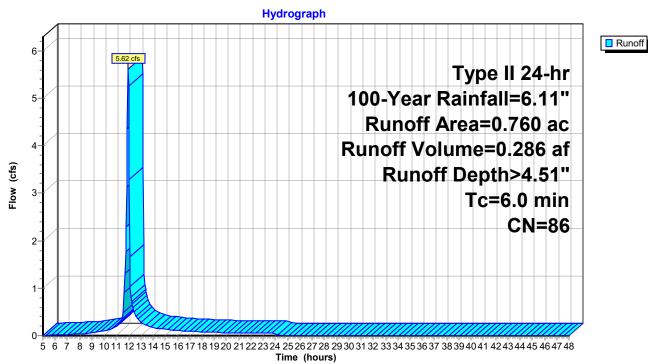
Runoff = 5.62 cfs @ 11.97 hrs, Volume= 0.286 af, Depth> 4.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

_	Area	(ac)	CN	Desc	Description						
*	0.	140	98	Road	Road Widening						
*	0.	460	98	Road	dway						
	0.	160	39	>75%	% Grass co	over, Good	, HSG A				
	0.	760	86	Weig	ghted Aver	age					
	0.	160		21.0	5% Pervio	us Area					
	0.	600		78.9	5% Imperv	ious Area					
	_					_					
	Тс	Leng		Slope	Velocity	Capacity	Description				
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)					
	6.0						Direct Entry, Minimum				

-

Subcatchment DR-17: Roadway



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Runoff

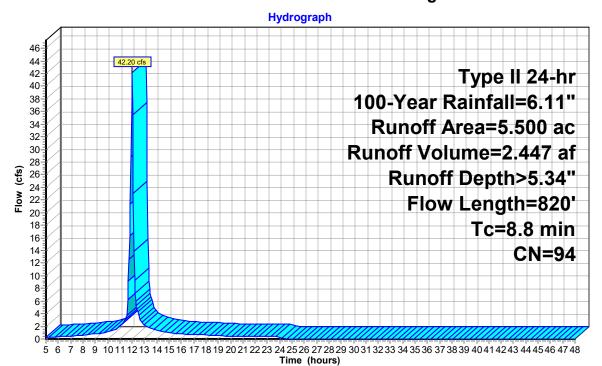
Summary for Subcatchment DR-2: Storage

Runoff = 42.20 cfs @ 12.00 hrs, Volume= 2.447 af, Depth> 5.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area (ac)		CN Description						
*	_			55 5					
_	0.	200 8	30 >75°	<u>% Grass co</u>	over, Good	, HSG D			
	5.	500	4 Weig	ghted Aver	age				
	5.	500	100.	00% Pervi	ous Area				
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	3.3	100	0.0100	0.50		Sheet Flow,			
						n= 0.023 P2= 2.40"			
	4.9	470	0.0100	1.61		Shallow Concentrated Flow,			
						Unpaved Kv= 16.1 fps			
	0.6	250	0.0050	6.67	47.16	Pipe Channel,			
						36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'			
_						n= 0.013			
	8.8	820	Total						

Subcatchment DR-2: Storage



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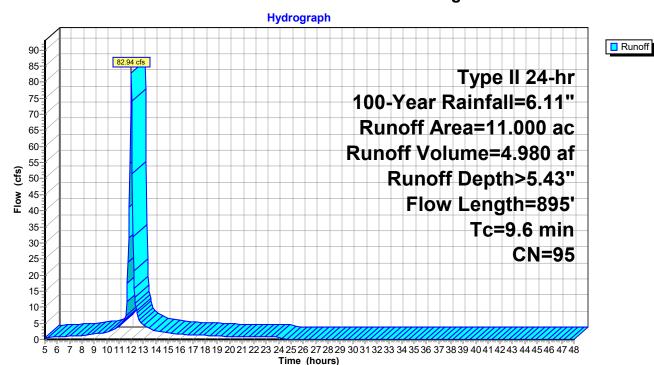
Summary for Subcatchment DR-3: Rail & Storage

Runoff = 82.94 cfs @ 12.00 hrs, Volume= 4.980 af, Depth> 5.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	cription						
*	* 8.300 95 Compacted Grave										
	0.	400	80	>759	>75% Grass cover, Good, HSG D						
*	2.	300	98	Rail	Rail						
	11.	000	95	Weig	Weighted Average						
	8.	700		79.0	9% Pervio	us Area					
	2.	300		20.9	1% Imperv	ious Area					
					-						
	Тс	Length	า S	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.3	100	0.	0100	0.50		Sheet Flow,				
							n= 0.023 P2= 2.40"				
	5.4	52	5 0.	0100	1.61		Shallow Concentrated Flow,				
							Unpaved Kv= 16.1 fps				
	0.9	270	0.	0050	5.09	16.00	Pipe Channel,				
							24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'				
_							n= 0.013				
	9.6	898	5 To	otal							

Subcatchment DR-3: Rail & Storage



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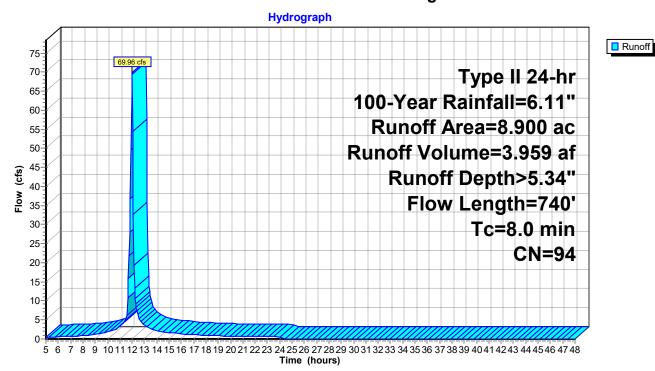
Summary for Subcatchment DR-4: Storage

Runoff = 69.96 cfs @ 11.99 hrs, Volume= 3.959 af, Depth> 5.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

_	Area (ac)		CN Description			
*	8.	600 9	5 Com	pacted Gr	avel	
	0.	300 8	30 >759	∕⁄ Grass co	, HSG D	
	8.	900 9	4 Weig	ghted Aver	age	
	8.	900	100.	00% Pervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	100	0.0100	0.50		Sheet Flow,
						n= 0.023 P2= 2.40"
	4.1	400	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.6	240	0.0050	6.67	47.16	Pipe Channel,
						36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
						n= 0.013 Corrugated PE, smooth interior
	8.0	740	Total			

Subcatchment DR-4: Storage



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Runoff

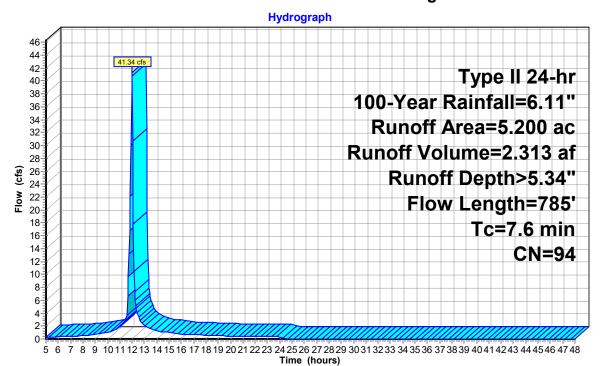
Summary for Subcatchment DR-5: Storage

Runoff = 41.34 cfs @ 11.98 hrs, Volume= 2.313 af, Depth> 5.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac) C	N Desc	cription		
*	4.	900	95 Dens	se Graded	Aggregate	
	0.	300 8	30 >759	% Grass co	over, Good	, HSG D
	5.	200 9	94 Weig	hted Aver	age	
	5.	200		00% Pervi		
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	100	0.0100	0.50		Sheet Flow,
						n= 0.023 P2= 2.40"
	3.0	285	0.0100	1.61		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	1.3	400	0.0050	5.09	16.00	Pipe Channel,
						24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
_						n= 0.013
	7.6	785	Total			

Subcatchment DR-5: Storage



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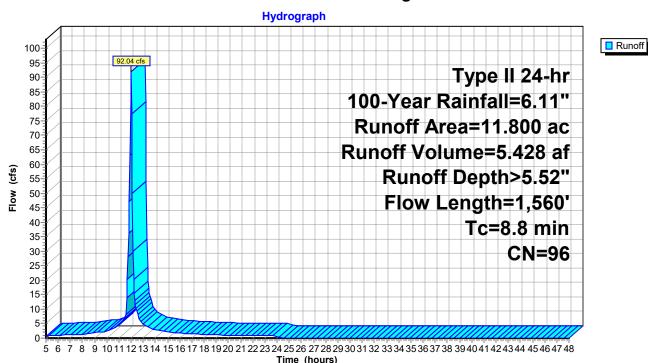
Summary for Subcatchment DR-6: Buldings B & D

Runoff = 92.04 cfs @ 11.99 hrs, Volume= 5.428 af, Depth> 5.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	cription		
*	2.	549	98	Build	ling B		
*	1.	413	98	Build	ling D		
	0.	200	80	>75%	% Ğrass co	over, Good,	, HSG D
*	7.	638	95	Dens	se Graded	Aggregate	
	11.	800	96	Weig	hted Aver	age	
	7.	838			2% Pervio		
	3.	962		33.5	8% Imperv	ious Area	
					•		
	Tc	Length	1 5	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
	3.3	100	0.	0100	0.50		Sheet Flow,
							n= 0.023 P2= 2.40"
	1.0	100	0.	0100	1.61		Shallow Concentrated Flow,
							Unpaved Kv= 16.1 fps
	4.5	1,360	0.	0050	5.09	16.00	Pipe Channel,
							24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
							n= 0.013
	8.8	1,560) To	otal			

Subcatchment DR-6: Buldings B & D



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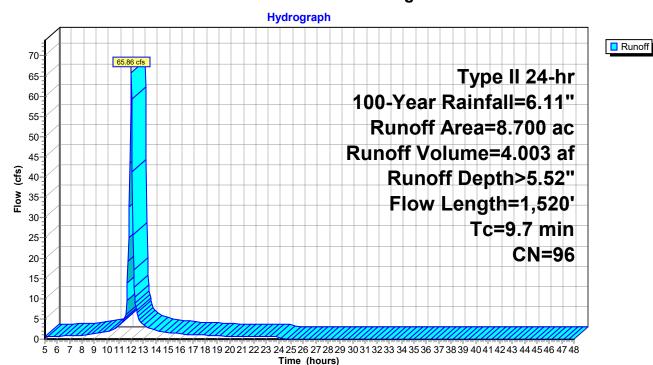
Summary for Subcatchment DR-7: Building C & Rail

Runoff = 65.86 cfs @ 12.00 hrs, Volume= 4.003 af, Depth> 5.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	cription				
*	3.	3.030 98		Build	Building C				
*	0.	970	98	Rail	J				
*	4.	400	95	Dens	se Graded	Aggregate			
	0.	300	80			over, Good,			
	8.	700	96	Weig	hted Aver	age			
	4.	700		54.0	2% Pervio	us Area			
	4.	000		45.9	8% Imperv	ious Area			
					-				
	Tc	Length	າ S	Slope	Velocity	Capacity	Description		
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	3.3	100	0.	0100	0.50		Sheet Flow,		
							n= 0.023 P2= 2.40"		
	2.6	250	0.	0100	1.61		Shallow Concentrated Flow,		
							Unpaved Kv= 16.1 fps		
	3.8	1,170	0.	0050	5.09	16.00	Pipe Channel,		
							24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'		
							n= 0.013		
	9.7	1,520) To	otal					

Subcatchment DR-7: Building C & Rail



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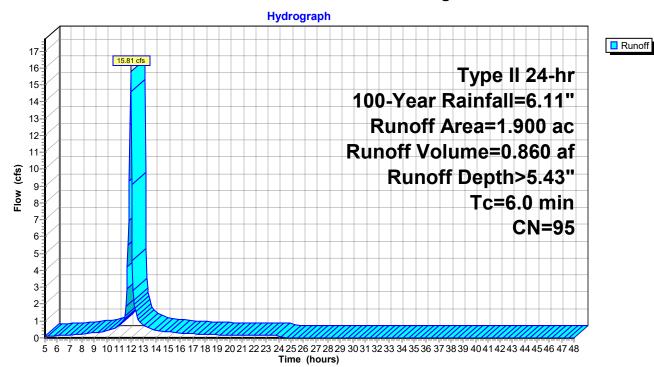
Summary for Subcatchment DR-8A: Parking

Runoff = 15.81 cfs @ 11.96 hrs, Volume= 0.860 af, Depth> 5.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
*	1.	600	98	Park	ing		
	0.	300	80	>75%	% Grass co	over, Good	, HSG D
	1.900 95 Weighted Average						
	0.300 15.79% Pervious Area					us Area	
	1.600			84.21% Impervious Area			
	Тс	Leng	th	Slope	Velocity	Capacity	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	6.0						Direct Entry, Minimum

Subcatchment DR-8A: Parking



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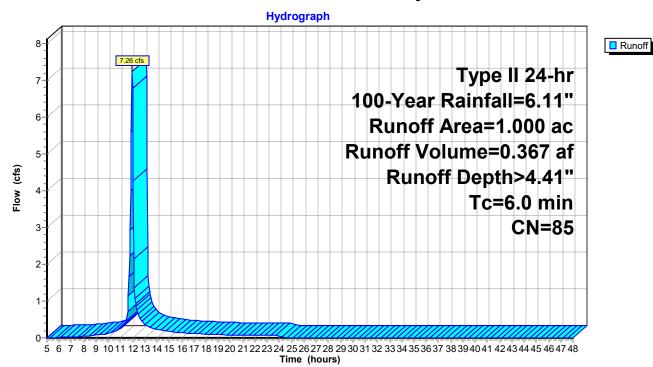
Summary for Subcatchment DR-8B: Roadway & Pond

Runoff = 7.26 cfs @ 11.97 hrs, Volume= 0.367 af, Depth> 4.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	cription		
*	0.	300	98	Road	dway		
	0.	700	80	>75%	√ Grass co	over, Good	, HSG D
	1.	000	85	Weig	ghted Aver	age	
	0.700 70.00% Pervious Area						
	0.300			30.0	0% Imperv	ious Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_		(166	, ()	(11/11)	(10360)	(015)	
	6.0						Direct Entry, Minimum

Subcatchment DR-8B: Roadway & Pond



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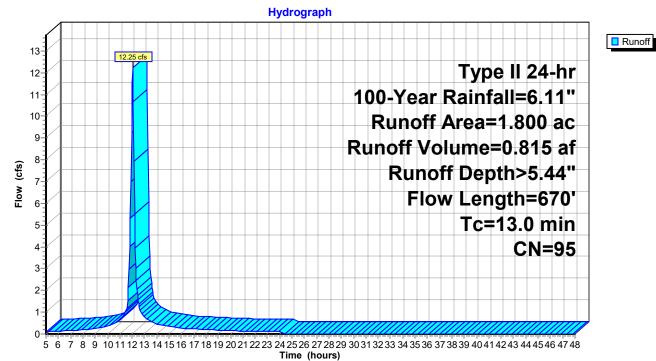
Summary for Subcatchment DR-9A: Parking & Substation

Runoff = 12.25 cfs @ 12.04 hrs, Volume= 0.815 af, Depth> 5.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	cription		
	0.	230	80	>75%	√ Grass co	over, Good	, HSG D
*	0.	200	92	Com	pacted Gr	avel	
*	1.	200	98	Park	ing and Ro	oad	
*	0.	170	98	Subs	station		
	1.800 95 Weighted Average				ghted Aver	age	
	0.	430		23.8	9% Pervio	us Area	
	1.	370		76.1	1% Imperv	∕ious Area	
	Tc (min)	Lengtl (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.4	100	0.	0200	1.19		Sheet Flow, Parking Lot Runoff
_	11.6	570	0 0.	0030	0.82		Smooth surfaces n= 0.011 P2= 2.40" Shallow Concentrated Flow, Grass Lined Ditch to Pond Grassed Waterway Kv= 15.0 fps
	13.0	670) To	otal			

Subcatchment DR-9A: Parking & Substation



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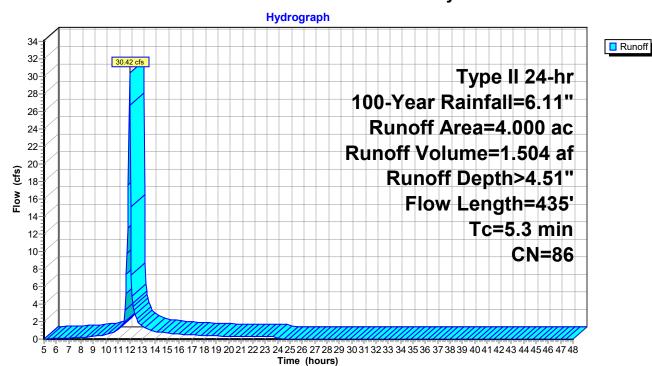
Summary for Subcatchment DR-9B: Roadway

Runoff = 30.42 cfs @ 11.96 hrs, Volume= 1.504 af, Depth> 4.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Type II 24-hr 100-Year Rainfall=6.11"

	Area	(ac)	CN	Desc	ription		
*	1.	050	95	Dens	se Graded	Aggregate	
*	0.	480	98	Road	dway		
	2.	470	80		•	over, Good,	HSG D
_	4.	000	86	Weig	hted Aver	age	
		520		_	0% Pervio	•	
		480			0% Imperv		
	٠.						
	Tc	Length	n S	lope	Velocity	Capacity	Description
	(min)	(feet		ft/ft)	(ft/sec)	(cfs)	· · · · · · · · · · · · · · · ·
_	3.6	100)250	0.46	, ,	Sheet Flow, Dense Graded Aggregate Yard
	0.0		0.0	,_00	0.10		n= 0.040 P2= 2.40"
	1.3	230	0.0	100	3.07	9.20	
	1.0	200	0.0	, 100	0.01	0.20	Area= 3.0 sf Perim= 4.0' r= 0.75'
							n= 0.040 Earth, cobble bottom, clean sides
	0.4	105	5 0 0	050	4.20	7.43	Pipe Channel, driveway culvert
	0		0.0	,000	1.20	7.10	18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
							n= 0.013 Corrugated PE, smooth interior
_	5.3	435	5 To	tal			c.c.c cogatea, clooti interior

Subcatchment DR-9B: Roadway



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InflowOutflow

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Summary for Reach 1R: Swale

Inflow Area = 1.900 ac, 84.21% Impervious, Inflow Depth > 5.43" for 100-Year event

Inflow = 15.81 cfs @ 11.96 hrs, Volume= 0.860 af

Outflow = 13.37 cfs @ 12.09 hrs, Volume= 0.860 af, Atten= 15%, Lag= 7.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.38 fps, Min. Travel Time= 4.8 min Avg. Velocity = 0.71 fps, Avg. Travel Time= 16.3 min

Peak Storage= 3,995 cf @ 12.01 hrs

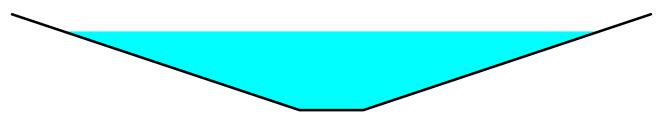
Average Depth at Peak Storage= 1.23', Surface Width= 8.39' Bank-Full Depth= 1.50' Flow Area= 8.3 sf, Capacity= 22.13 cfs

1.00' x 1.50' deep channel, n= 0.022 Earth, clean & straight

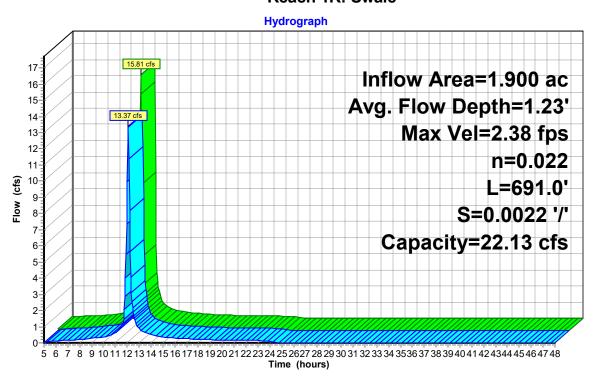
Side Slope Z-value= 3.0 '/' Top Width= 10.00'

Length= 691.0' Slope= 0.0022 '/'

Inlet Invert= 15.50', Outlet Invert= 14.00'



Reach 1R: Swale



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Inflow
Outflow

Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 4.11" for 100-Year event

Inflow = 30.97 cfs @ 13.14 hrs, Volume= 9.753 af

Outflow = 18.15 cfs @ 16.00 hrs, Volume= 9.491 af, Atten= 41%, Lag= 172.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

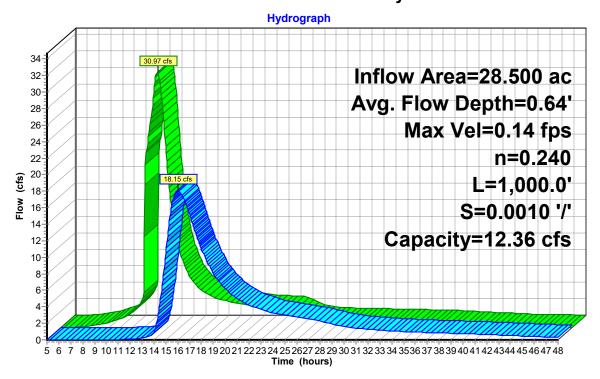
Max. Velocity= 0.14 fps, Min. Travel Time= 118.8 min Avg. Velocity = 0.05 fps, Avg. Travel Time= 314.3 min

Peak Storage= 129,381 cf @ 14.02 hrs

Average Depth at Peak Storage= 0.64', Surface Width= 203.85' Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240 Side Slope Z-value= 3.0 '/' Top Width= 203.00' Length= 1,000.0' Slope= 0.0010 '/' Inlet Invert= 6.00', Outlet Invert= 5.00'

Reach 1W: Wetland #1 / Analysis Point 1A



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Inflow
Outflow

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Summary for Reach 2R: Overflow

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 4.77" for 100-Year event

Inflow = 15.27 cfs @ 12.13 hrs, Volume= 2.307 af

Outflow = 15.48 cfs @ 12.14 hrs, Volume= 2.307 af, Atten= 0%, Lag= 0.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.51 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.77 fps, Avg. Travel Time= 0.5 min

Peak Storage= 119 cf @ 12.14 hrs

Average Depth at Peak Storage= 0.27', Surface Width= 9.62' Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 569.91 cfs

8.00' x 2.00' deep channel, n= 0.020 Corrugated PE, corrugated interior

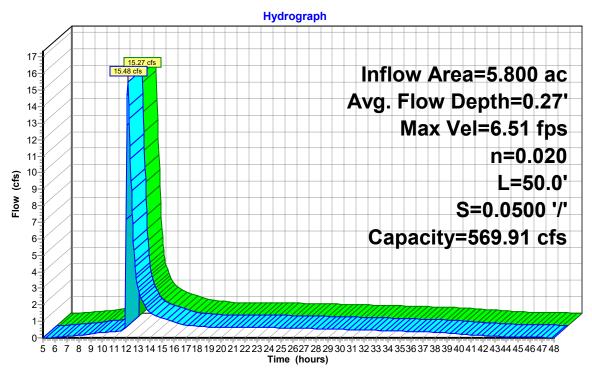
Side Slope Z-value= 3.0 '/' Top Width= 20.00'

Length= 50.0' Slope= 0.0500 '/'

Inlet Invert= 16.50', Outlet Invert= 14.00'



Reach 2R: Overflow



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Inflow
Outflow

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Summary for Reach 3R: Outlet Pipe

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 4.00" for 100-Year event

Inflow = 18.15 cfs @ 16.00 hrs, Volume= 9.491 af

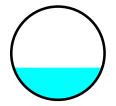
Outflow = 18.15 cfs @ 16.01 hrs, Volume= 9.490 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

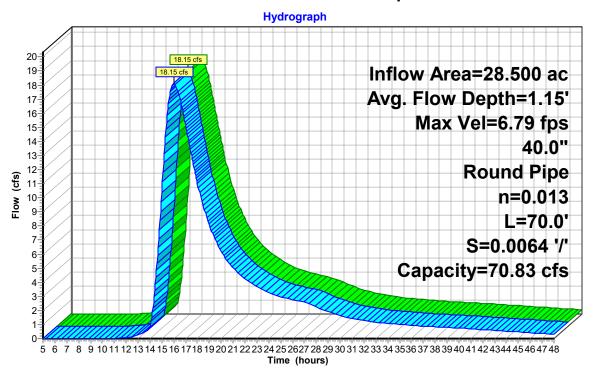
Max. Velocity= 6.79 fps, Min. Travel Time= 0.2 min Avg. Velocity = 3.26 fps, Avg. Travel Time= 0.4 min

Peak Storage= 187 cf @ 16.00 hrs Average Depth at Peak Storage= 1.15', Surface Width= 3.17' Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe n= 0.013 Corrugated PE, smooth interior Length= 70.0' Slope= 0.0064 '/' Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 3R: Outlet Pipe



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Inflow
Outflow

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Summary for Reach 4R: Overflow

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 5.43" for 100-Year event

Inflow = 8.17 cfs @ 11.98 hrs, Volume= 0.452 af

Outflow = 8.00 cfs @ 11.99 hrs, Volume= 0.452 af, Atten= 2%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.21 fps, Min. Travel Time= 0.5 min Avg. Velocity = 0.87 fps, Avg. Travel Time= 1.9 min

Peak Storage= 253 cf @ 11.98 hrs

Average Depth at Peak Storage= 0.55', Surface Width= 6.28' Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 118.65 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch

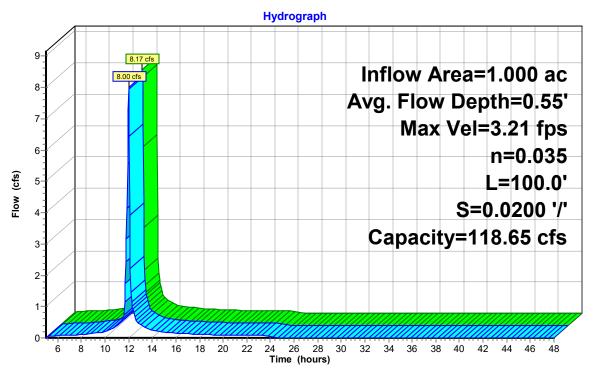
Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 100.0' Slope= 0.0200 '/'

Inlet Invert= 12.00', Outlet Invert= 10.00'



Reach 4R: Overflow



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Inflow
Outflow

Summary for Reach 5R: Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 1.24" for 100-Year event

Inflow = 1.86 cfs @ 12.17 hrs, Volume= 0.124 af

Outflow = 1.56 cfs @ 12.22 hrs, Volume= 0.124 af, Atten= 16%, Lag= 3.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.68 fps, Min. Travel Time= 1.2 min Avg. Velocity = 0.58 fps, Avg. Travel Time= 3.6 min

Peak Storage= 132 cf @ 12.20 hrs

Average Depth at Peak Storage= 0.28', Surface Width= 4.65' Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 90.48 cfs

3.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch

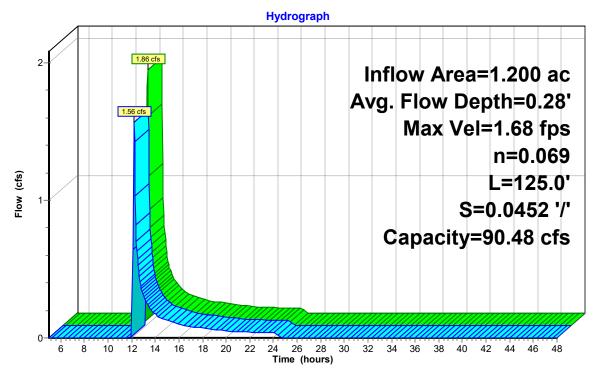
Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 125.0' Slope= 0.0452 '/'

Inlet Invert= 11.65', Outlet Invert= 6.00'



Reach 5R: Overflow



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Inflow
Outflow

Summary for Reach 6R: Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 1.08" for 100-Year event

Inflow = 6.03 cfs @ 12.16 hrs, Volume= 0.117 af

Outflow = 5.16 cfs @ 12.19 hrs, Volume= 0.117 af, Atten= 14%, Lag= 1.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.82 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.06 fps, Avg. Travel Time= 1.6 min

Peak Storage= 209 cf @ 12.17 hrs

Average Depth at Peak Storage= 0.47', Surface Width= 5.80' Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 116.91 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch

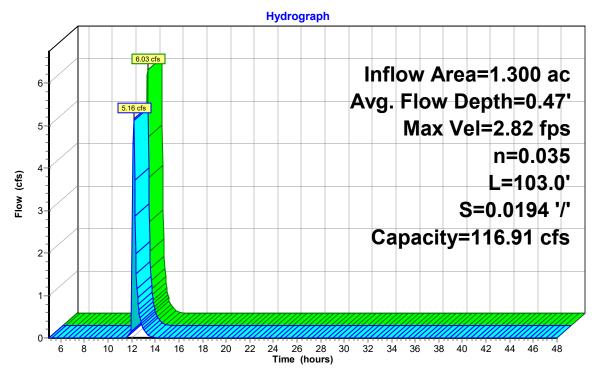
Side Slope Z-value= 3.0 '/' Top Width= 15.00'

Length= 103.0' Slope= 0.0194 '/'

Inlet Invert= 8.50', Outlet Invert= 6.50'



Reach 6R: Overflow



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Inflow
Outflow

Summary for Reach 7R: Overflow

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth > 5.02" for 100-Year event

Inflow = 3.28 cfs @ 12.41 hrs, Volume= 1.212 af

Outflow = 3.26 cfs @ 12.44 hrs, Volume= 1.212 af, Atten= 0%, Lag= 2.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.35 fps, Min. Travel Time= 1.2 min Avg. Velocity = 0.53 fps, Avg. Travel Time= 3.2 min

Peak Storage= 243 cf @ 12.42 hrs

Average Depth at Peak Storage= 0.28', Surface Width= 9.65' Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 116.81 cfs

8.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch

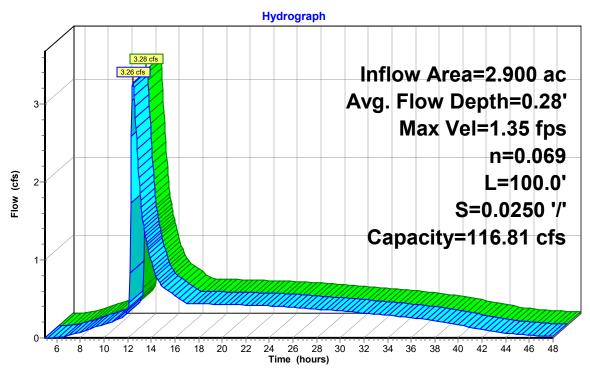
Side Slope Z-value= 3.0 '/' Top Width= 20.00'

Length= 100.0' Slope= 0.0250 '/'

Inlet Invert= 14.50', Outlet Invert= 12.00'



Reach 7R: Overflow



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Inflow
Outflow

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Summary for Reach 8R: Dry Swale #1

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 5.43" for 100-Year event

Inflow = 8.32 cfs @ 11.96 hrs, Volume= 0.453 af

Outflow = 8.17 cfs @ 11.98 hrs, Volume= 0.452 af, Atten= 2%, Lag= 1.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.41 fps, Min. Travel Time= 0.5 min Avg. Velocity = 0.96 fps, Avg. Travel Time= 1.8 min

Peak Storage= 252 cf @ 11.97 hrs

Average Depth at Peak Storage= 0.71', Surface Width= 4.82' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 16.53 cfs

2.00' x 1.00' deep channel, n= 0.018 Earth, clean & straight

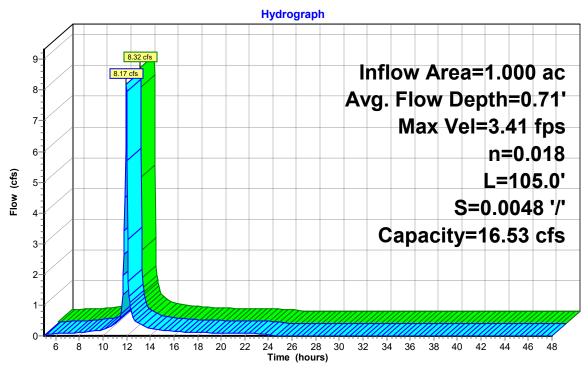
Side Slope Z-value= 2.0 '/' Top Width= 6.00'

Length= 105.0' Slope= 0.0048 '/'

Inlet Invert= 10.00', Outlet Invert= 9.50'



Reach 8R: Dry Swale #1



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Inflow
Outflow

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Summary for Reach 10R: Dry Swale #2

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth > 4.51" for 100-Year event

Inflow = 5.36 cfs @ 12.00 hrs, Volume= 0.286 af

Outflow = 5.25 cfs @ 12.01 hrs, Volume= 0.286 af, Atten= 2%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 5.03 fps, Min. Travel Time= 0.4 min Avg. Velocity = 1.34 fps, Avg. Travel Time= 1.4 min

Peak Storage= 122 cf @ 12.00 hrs

Average Depth at Peak Storage= 0.35', Surface Width= 4.09' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 213.76 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight

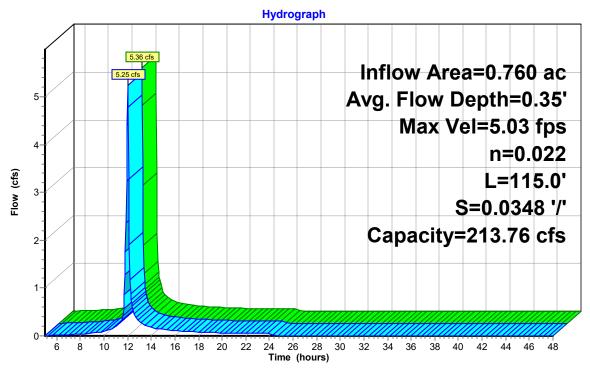
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 115.0' Slope= 0.0348 '/'

Inlet Invert= 37.00', Outlet Invert= 33.00'



Reach 10R: Dry Swale #2



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Summary for Reach 12R: Sediment Basin Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 1.91" for 100-Year event

Inflow = 4.02 cfs @ 12.04 hrs, Volume= 0.191 af

Outflow = 3.89 cfs @ 12.04 hrs, Volume= 0.191 af, Atten= 3%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.16 fps, Min. Travel Time= 0.1 min Avg. Velocity = 0.28 fps, Avg. Travel Time= 0.4 min

Peak Storage= 20 cf @ 12.04 hrs

Average Depth at Peak Storage= 0.30', Surface Width= 12.40' Bank-Full Depth= 0.50' Flow Area= 6.0 sf, Capacity= 9.43 cfs

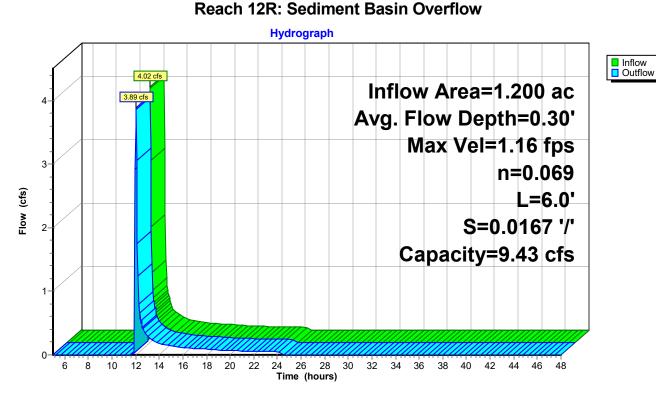
10.00' x 0.50' deep channel, n= 0.069 Riprap, 6-inch

Side Slope Z-value= 4.0 '/' Top Width= 14.00'

Length= 6.0' Slope= 0.0167 '/'

Inlet Invert= 12.00', Outlet Invert= 11.90'

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Inflow
Outflow

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Summary for Reach 13R: Roadside Swale

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 2.08" for 100-Year event

Inflow = 4.32 cfs @ 11.98 hrs, Volume= 0.208 af

Outflow = 3.95 cfs @ 12.02 hrs, Volume= 0.208 af, Atten= 9%, Lag= 2.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.15 fps, Min. Travel Time= 1.5 min Avg. Velocity = 1.04 fps, Avg. Travel Time= 4.6 min

Peak Storage= 386 cf @ 12.00 hrs

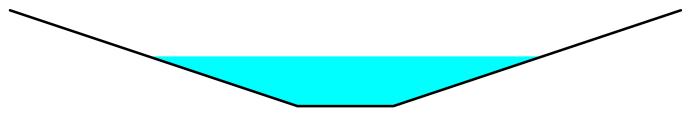
Average Depth at Peak Storage= 0.52', Surface Width= 4.12' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.36 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight

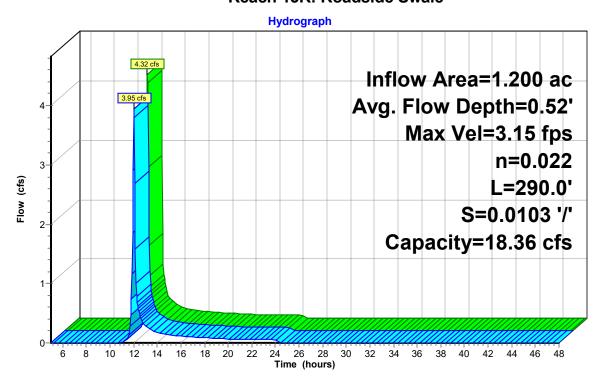
Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 290.0' Slope= 0.0103 '/'

Inlet Invert= 15.00', Outlet Invert= 12.00'



Reach 13R: Roadside Swale



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Inflow
Outflow

Summary for Reach 14R: Roadside Swale

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth > 4.51" for 100-Year event

Inflow = 5.62 cfs @ 11.97 hrs, Volume= 0.286 af

Outflow = 5.36 cfs @ 12.00 hrs, Volume= 0.286 af, Atten= 5%, Lag= 2.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.27 fps, Min. Travel Time= 1.2 min Avg. Velocity = 1.65 fps, Avg. Travel Time= 4.6 min

Peak Storage= 402 cf @ 11.98 hrs

Average Depth at Peak Storage= 0.30', Surface Width= 3.82' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 289.37 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight

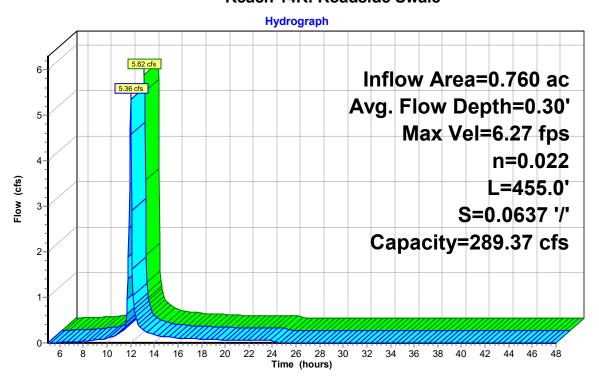
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 455.0' Slope= 0.0637 '/'

Inlet Invert= 66.00', Outlet Invert= 37.00'



Reach 14R: Roadside Swale



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Summary for Reach 15R: Roadside Swale

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 3.18" for 100-Year event

Inflow = 7.10 cfs @ 11.97 hrs, Volume= 0.345 af

Outflow = 5.76 cfs @ 12.12 hrs, Volume= 0.345 af, Atten= 19%, Lag= 9.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.22 fps, Min. Travel Time= 5.9 min Avg. Velocity = 0.33 fps, Avg. Travel Time= 22.0 min

Peak Storage= 2,022 cf @ 12.02 hrs

Average Depth at Peak Storage= 1.10', Surface Width= 7.60' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 4.69 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight

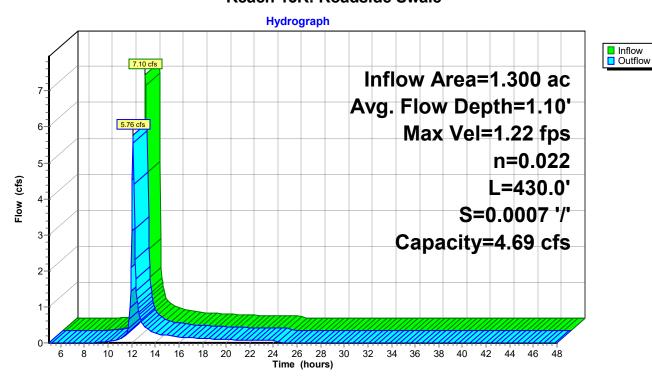
Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 430.0' Slope= 0.0007 '/'

Inlet Invert= 10.00', Outlet Invert= 9.71'



Reach 15R: Roadside Swale



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Summary for Reach 17R: Sediment Basin Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 2.82" for 100-Year event

Inflow = 5.75 cfs @ 12.13 hrs, Volume= 0.305 af

Outflow = 5.82 cfs @ 12.14 hrs, Volume= 0.305 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.19 fps, Min. Travel Time= 0.1 min Avg. Velocity = 0.23 fps, Avg. Travel Time= 0.4 min

Peak Storage= 29 cf @ 12.14 hrs

Average Depth at Peak Storage= 0.30', Surface Width= 17.42' Bank-Full Depth= 0.70' Flow Area= 12.5 sf, Capacity= 24.64 cfs

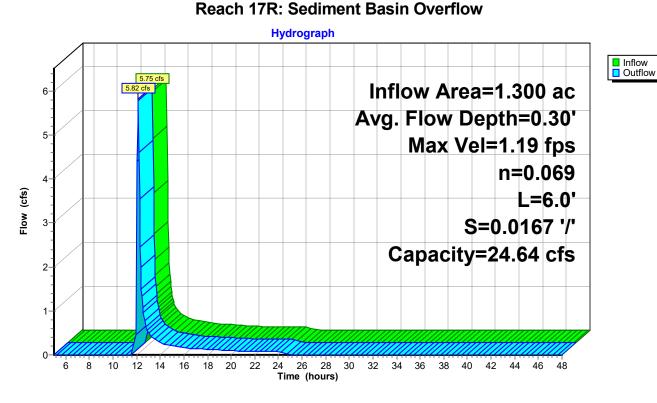
15.00' x 0.70' deep channel, n= 0.069 Riprap, 6-inch

Side Slope Z-value= 4.0 '/' Top Width= 20.60'

Length= 6.0' Slope= 0.0167 '/'

Inlet Invert= 9.00', Outlet Invert= 8.90'

‡



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Summary for Pond 1P: WQv Pond #1

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth > 5.08" for 100-Year event

Inflow = 16.96 cfs @ 12.03 hrs, Volume= 1.227 af

Outflow = 3.28 cfs @ 12.41 hrs, Volume= 1.212 af, Atten= 81%, Lag= 22.8 min

Primary = 3.28 cfs @ 12.41 hrs, Volume= 1.212 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Starting Elev= 14.00' Surf.Area= 9,229 sf Storage= 19,003 cf

Peak Elev= 16.23' @ 12.41 hrs Surf.Area= 21,418 sf Storage= 47,659 cf (28,656 cf above start)

Plug-Flow detention time= 930.0 min calculated for 0.775 af (63% of inflow)

Center-of-Mass det. time= 522.7 min (1,309.6 - 786.9)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,795 cf	Forebay (Prismatic) Listed below (Recalc)
#2	9.00'	57,882 cf	Permanent Pool (Prismatic) Listed below (Recalc)

		·	
	62	2,677 cf Total Av	ailable Storage
E	0 ()	. 01	0 01
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	232	0	0
11.00	569	401	401
12.00	1,018	794	1,194
13.00	1,467	1,243	2,437
14.00	3,249	2,358	4,795
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
9.00	1,145	0	0
10.00	1,751	1,448	1,448
11.00	2,339	2,045	3,493
12.00	2,959	2,649	6,142
13.00	3,597	3,278	9,420
14.00	5,980	4,789	14,209
14.50	7,240	3,305	17,514
15.00	14,392	5,408	22,922
16.00	17,455	15,924	38,845
17.00	20,619	19,037	57,882
Davice Poutin	a Invo	rt Outlet Device	0

Device	Routing	Invert	Outlet Devices
#1	Primary	13.50'	12.0" Round Culvert
	•		L= 50.0' Box, headwall w/3 square edges, Ke= 0.500
			Inlet / Outlet Invert= 13.50' / 13.23' S= 0.0054 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	16.00'	24.0" x 24.0" Horiz. Outlet Structure Top Grate
			C= 0.600 in 24.0" x 24.0" Grate (100% open area)
			Limited to weir flow at low heads
#3	Device 1	14.00'	4.0" Round Reverse Slope Pipe
			L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 9.00' / 14.00' S= -0.1250 '/' Cc= 0.900

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n= 0.010 PVC, smooth interior, Flow Area= 0.09 sf #4 Primary

6.0' long x 1.0' breadth Broad-Crested Rectangular Weir 16.25'

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00

2.50 3.00

Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31

3.30 3.31 3.32

Primary OutFlow Max=3.26 cfs @ 12.41 hrs HW=16.23' (Free Discharge)

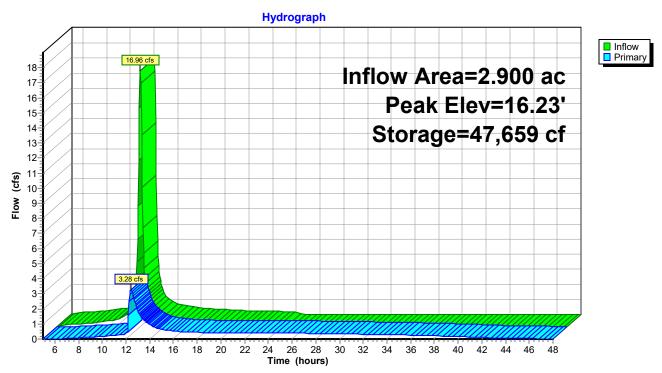
1=Culvert (Passes 3.26 cfs of 5.08 cfs potential flow)

-2=Outlet Structure Top Grate (Weir Controls 2.80 cfs @ 1.55 fps)

-3=Reverse Slope Pipe (Outlet Controls 0.46 cfs @ 5.29 fps)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: WQv Pond #1



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Summary for Pond 2P: WQv Pond #2

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 4.80" for 100-Year event

Inflow = 40.22 cfs @ 11.97 hrs, Volume= 2.320 af

Outflow = 15.27 cfs @ 12.13 hrs, Volume= 2.307 af, Atten= 62%, Lag= 9.6 min

Primary = 15.27 cfs @ 12.13 hrs, Volume= 2.307 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Starting Elev= 14.00' Surf.Area= 5,917 sf Storage= 9,000 cf

Peak Elev= 17.07' @ 12.13 hrs Surf.Area= 27,493 sf Storage= 54,456 cf (45,456 cf above start)

Plug-Flow detention time= 493.6 min calculated for 2.098 af (90% of inflow)

Center-of-Mass det. time= 393.8 min (1,180.5 - 786.7)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,020 cf	Forebay #1 (Prismatic) Listed below (Recalc)
#2	10.00'	2,575 cf	Forebay #2 (Prismatic) Listed below (Recalc)
#3	10.00'	58,093 cf	Permanent Pool (Prismatic) Listed below (Recalc)

64,688 cf Total Available Storage

□[O A	l Ota	O Ot
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	141	0	0
11.00	330	236	236
12.00	562	446	682
13.00	866	714	1,396
14.00	2,023	1,445	2,840
14.50	2,696	1,180	4,020
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	82	0	0
11.00	202	142	142
12.00	351	277	419
13.00	535	443	862
14.00	1,323	929	1,791
14.50	1,815	785	2,575
	•		,
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
10.00	375	0	0
11.00	653	514	514
12.00	957	805	1,319
13.00	1,286	1,122	2,441
14.00	2,571	1,929	4,369
14.50	3,307	1,470	5,839
15.00	13,814	4,280	10,119
16.00	17,852	15,833	25,952
17.00	22,659	20,256	46,207
17.50	24,884	11,886	58,093
17.00	24,004	11,000	00,000

18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 100-Year Rainfall=6.11"

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Device	Routing	Invert	Outlet Devices
#1	Device 3	16.50'	24.0" x 24.0" Horiz. Orifice/Grate
			C= 0.600 in 24.0" x 24.0" Grate (100% open area)
			Limited to weir flow at low heads
#2	Device 3	14.00'	4.0" Vert. Reverse Slope Pipe C= 0.600
			Limited to weir flow at low heads
#3	Primary	14.00'	12.0" Round Outlet Structure Discard Pipe
			L= 46.0' Box, headwall w/3 square edges, Ke= 0.500
			Inlet / Outlet Invert= 14.00' / 13.77' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#4	Primary	16.60'	10.0' long x 0.5' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=15.12 cfs @ 12.13 hrs HW=17.07' (Free Discharge)

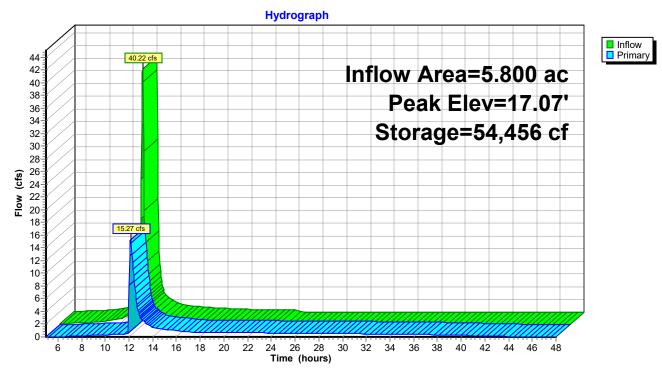
-3=Outlet Structure Discard Pipe (Barrel Controls 5.57 cfs @ 7.09 fps)

-1=Orifice/Grate (Passes < 11.22 cfs potential flow)

-2=Reverse Slope Pipe (Passes < 0.72 cfs potential flow)

-4=Broad-Crested Rectangular Weir (Weir Controls 9.55 cfs @ 2.04 fps)

Pond 2P: WQv Pond #2



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Summary for Pond 3P: Infiltration Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 1.91" for 100-Year event

Inflow = 3.89 cfs @ 12.04 hrs, Volume= 0.191 af

Outflow = 1.88 cfs @ 12.17 hrs, Volume= 0.172 af, Atten= 52%, Lag= 7.9 min

Discarded = 0.02 cfs @ 12.17 hrs, Volume= 0.048 af Primary = 1.86 cfs @ 12.17 hrs, Volume= 0.124 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 11.94' @ 12.17 hrs Surf.Area= 1,383 sf Storage= 2,406 cf

Plug-Flow detention time= 296.0 min calculated for 0.172 af (90% of inflow)

Center-of-Mass det. time= 245.1 min (1,121.7 - 876.7)

Volume	Inver	t Avai	I.Storage	Storage Description	on		
#1	8.10)'	2,492 cf	Custom Stage Da	ta (Irregular) Liste	ed below (Recalc)	
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft <u>)</u>	
8.1 12.0	-	109 1,415	56.0 149.0	0 2,492	0 2,492	109 1,678	
Device Routing Invert Outlet Devices							
#1	Primary	11	.65' Cha	nnel/Reach using	Reach 5R: Overflo	OW	
#2	Discarded	8	.10' 0.50	0 in/hr Exfiltration	over Surface area	3	
			Con	ductivity to Groundy	vater Elevation = 4	1.00'	

Discarded OutFlow Max=0.02 cfs @ 12.17 hrs HW=11.91' (Free Discharge) **2=Exfiltration** (Controls 0.02 cfs)

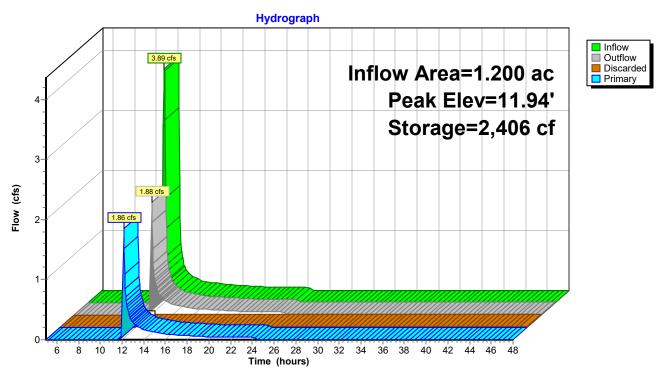
Primary OutFlow Max=1.65 cfs @ 12.17 hrs HW=11.91' (Free Discharge)
—1=Channel/Reach (Channel Controls 1.65 cfs @ 1.64 fps)

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Pond 3P: Infiltration Basin #1



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Summary for Pond 4P: Infiltration Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 2.82" for 100-Year event

Inflow = 5.82 cfs @ 12.14 hrs, Volume= 0.305 af

Outflow = 6.44 cfs @ 12.16 hrs, Volume= 0.305 af, Atten= 0%, Lag= 1.3 min

Discarded = 0.42 cfs @ 12.16 hrs, Volume= 0.189 af Primary = 6.03 cfs @ 12.16 hrs, Volume= 0.117 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 8.97' @ 12.16 hrs Surf.Area= 1,059 sf Storage= 1,597 cf

Plug-Flow detention time= 29.1 min calculated for 0.305 af (100% of inflow)

Center-of-Mass det. time= 29.1 min (895.2 - 866.1)

Volume	Invert	Avail.	Storage	Storage Descriptio	n		
#1	5.80'		2,495 cf	Custom Stage Dat	t a (Irregular) Listed	below (Recalc)	
Elevatio		rf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
5.8	30	110	56.0	0	0	110	
9.7	' 0	1,415	150.0	2,495	2,495	1,702	
Device Routing Invert Outlet Devices							
#1	Primary	8.9	50' Cha	nnel/Reach using	Reach 6R: Overflow	V	
#2	Discarded	5.8	80' 12.0	00 in/hr Exfiltration	over Surface area		
			Cond	ductivity to Groundw	ater Elevation = 3.0	00'	

Discarded OutFlow Max=0.41 cfs @ 12.16 hrs HW=8.95' (Free Discharge) **2=Exfiltration** (Controls 0.41 cfs)

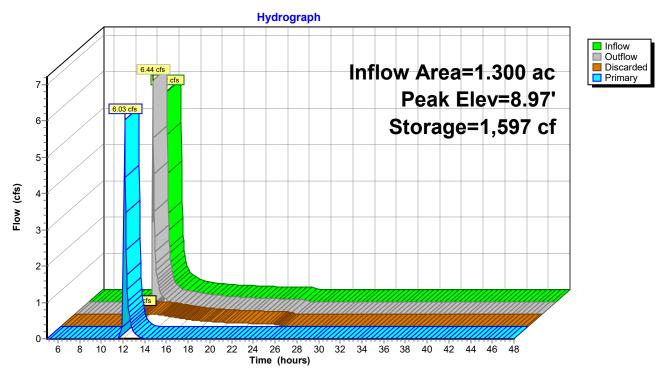
Primary OutFlow Max=5.55 cfs @ 12.16 hrs HW=8.95' (Free Discharge)
1=Channel/Reach (Channel Controls 5.55 cfs @ 2.85 fps)

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Pond 4P: Infiltration Basin #2



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 100-Year Rainfall=6.11"

Prepared by McFarland Johnson

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Summary for Pond 5P: Sedimentation Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 2.08" for 100-Year event

Inflow = 3.95 cfs @ 12.02 hrs, Volume= 0.208 af

Outflow = 4.02 cfs @ 12.04 hrs, Volume= 0.191 af, Atten= 0%, Lag= 1.1 min

Primary = 4.02 cfs @ 12.04 hrs, Volume= 0.191 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 12.31' @ 12.04 hrs Surf.Area= 632 sf Storage= 930 cf

Plug-Flow detention time= 59.3 min calculated for 0.191 af (92% of inflow)

Center-of-Mass det. time= 15.9 min (876.3 - 860.4)

Volume	Inve	ert Avai	I.Storage	Storage Descri	otion		
#1	9.0	00'	1,058 cf	Custom Stage	Data (Irregular) Lis	sted below (Recalc))
Elevation (fee		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet			
9.0	00	41	25.8	(0	41	
10.0	00	150	46.7	90	90	167	
11.0	00	320	66.6	230	320	355	
12.0	00	550	86.4	430	749	608	
12.5	50	687	96.2	309	9 1,058	758	
Device	Routing	In	vert Outle	et Devices			
#1	Primary	12	2.00' Cha	nnel/Reach usi	ng Reach 12R: Sed	diment Basin Overf	low

Primary OutFlow Max=3.89 cfs @ 12.04 hrs HW=12.30' (Free Discharge)

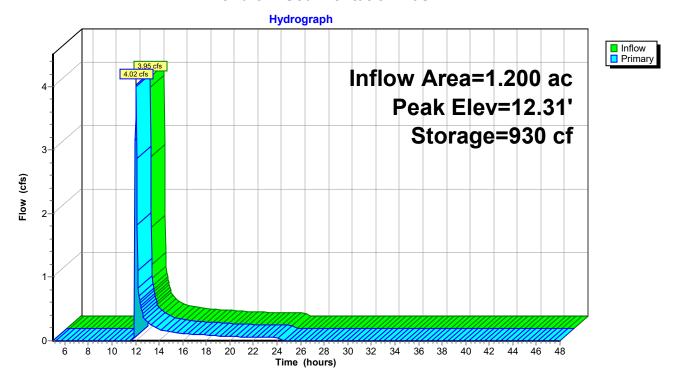
1=Channel/Reach (Channel Controls 3.89 cfs @ 1.16 fps)

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Pond 5P: Sedimentation Basin #1



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Summary for Pond 16P: Sedimentation Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 3.18" for 100-Year event

Inflow = 5.76 cfs @ 12.12 hrs, Volume= 0.345 af

Outflow = 5.75 cfs @ 12.13 hrs, Volume= 0.305 af, Atten= 0%, Lag= 0.8 min

Primary = 5.75 cfs @ 12.13 hrs, Volume= 0.305 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 9.30' @ 12.13 hrs Surf.Area= 970 sf Storage= 1,979 cf

Plug-Flow detention time= 79.9 min calculated for 0.305 af (89% of inflow)

Center-of-Mass det. time= 21.8 min (865.8 - 843.9)

Volume	Inve	ert Ava	il.Storage	Storage Des	scription	า		
#1	5.8	30'	2,389 cf	Custom Sta	age Dat	a (Irregular) Lis	ted below (Reca	ılc)
Elevatio	on	Surf.Area	Perim.	Inc.S	Store	Cum.Store	Wet.Are	а
(fee		(sq-ft)	(feet)	(cubic-	feet)	(cubic-feet)	(sq-f	
5.8	30	224	80.0	-	0	0	22	4
6.0	0	257	83.0		48	48	26	6
7.0	0	438	98.0		344	392	50	0
8.0	0	650	113.0		541	932	77	3
9.0	0	892	128.0		768	1,700	1,08	5
9.7	0	1,079	139.0		689	2,389	1,33	7
Device	Routing	In	vert Outle	et Devices				
#1	Primary	Ç	0.00' Cha	nnel/Reach	usina F	Reach 17R: Sed	iment Basin Ove	erflow

Primary OutFlow Max=5.60 cfs @ 12.13 hrs HW=9.30' (Free Discharge)

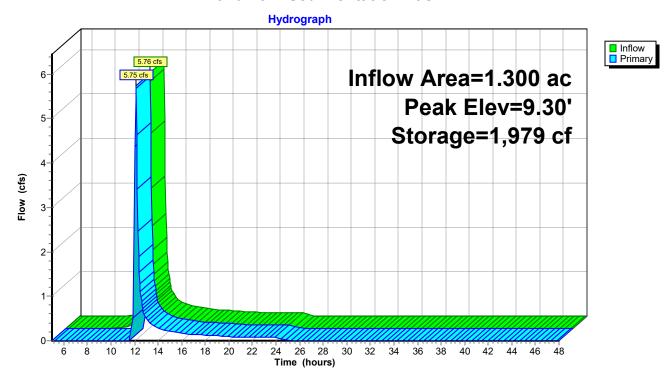
1=Channel/Reach (Channel Controls 5.60 cfs @ 1.17 fps)

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Pond 16P: Sedimentation Basin #2



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Summary for Pond AP-1: Analysis Point #1

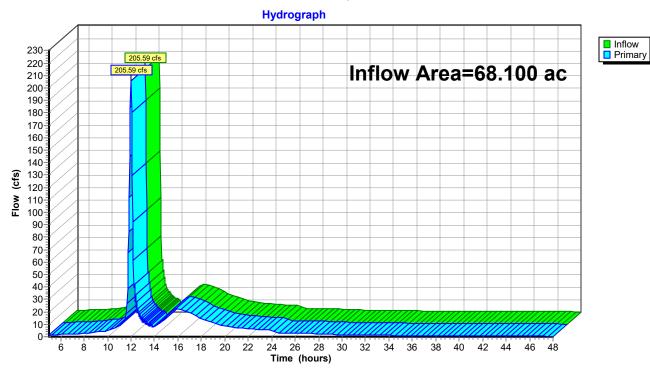
Inflow Area = 68.100 ac, 20.36% Impervious, Inflow Depth > 3.95" for 100-Year event

Inflow = 205.59 cfs @ 12.00 hrs, Volume= 22.396 af

Primary = 205.59 cfs @ 12.00 hrs, Volume= 22.396 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1



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Summary for Pond AP-2: Analysis Point #2

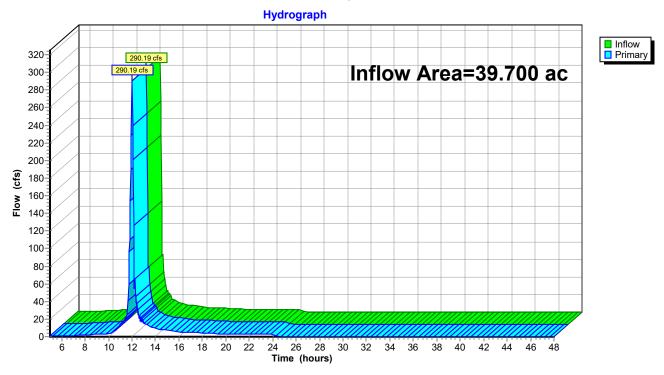
Inflow Area = 39.700 ac, 23.10% Impervious, Inflow Depth > 4.88" for 100-Year event

Inflow = 290.19 cfs @ 12.00 hrs, Volume= 16.144 af

Primary = 290.19 cfs @ 12.00 hrs, Volume= 16.144 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2



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Summary for Pond AP-3: Analysis Point #3

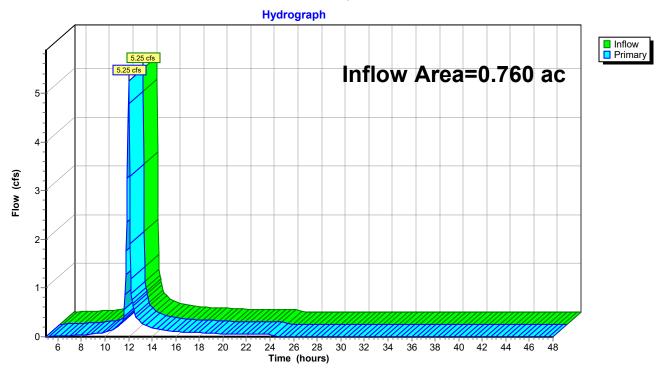
Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth > 4.51" for 100-Year event

Inflow = 5.25 cfs @ 12.01 hrs, Volume= 0.286 af

Primary = 5.25 cfs @ 12.01 hrs, Volume= 0.286 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3



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Summary for Pond C-1: Chamber Series 1

Inflow Area =	10.300 ac, 66.70% Impervious, Inflow	Depth > 5.60" for 100-Year event
Inflow =	84.97 cfs @ 11.98 hrs, Volume=	4.805 af
Outflow =	95.05 cfs @ 12.00 hrs, Volume=	4.444 af, Atten= 0%, Lag= 1.4 min
Discarded =	0.29 cfs @ 12.00 hrs, Volume=	0.351 af
Primary =	60.22 cfs @ 12.00 hrs, Volume=	3.951 af
Secondary =	34.55 cfs @ 12.00 hrs, Volume=	0.143 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 14.63' @ 12.00 hrs Surf.Area= 24,954 sf Storage= 35,013 cf

Plug-Flow detention time= 141.1 min calculated for 4.438 af (92% of inflow) Center-of-Mass det. time= 101.1 min (864.7 - 763.5)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	11,722 cf	37.08'W x 227.97'L x 5.50'H Field B
			46,496 cf Overall - 17,192 cf Embedded = 29,305 cf x 40.0% Voids
#2B	6.75'	17,192 cf	ADS_StormTech MC-3500 d +Cap x 155 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			155 Chambers in 5 Rows
			Cap Storage= +14.9 cf x 2 x 5 rows = 149.0 cf
#3	13.25'	6,100 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		35,013 cf	Total Available Storage

Storage Group B created with Chamber Wizard

	Elevation	Surf.Area	Inc.Store	Cum.Store
_	(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
	13.25	600	0	0
	13.75	4,900	1,375	1,375
	14.00	8,200	1,638	3,013
	14.25	16,500	3,088	6,100

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	10.00'	36.0" Round Culvert
	•		L= 55.9' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 10.00' / 7.59' S= 0.0431 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	14.24'	50.0' long x 0.7' breadth Concrete Curb
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50
			Coef. (English) 2.76 2.82 2.93 3.09 3.18 3.22 3.27 3.30 3.32
			3 31 3 32

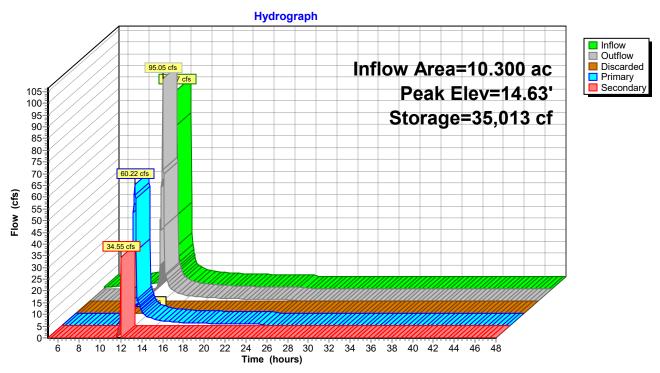
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Discarded OutFlow Max=0.29 cfs @ 12.00 hrs HW=14.61' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.29 cfs)

Primary OutFlow Max=60.19 cfs @ 12.00 hrs HW=14.63' (Free Discharge) 2=Culvert (Inlet Controls 60.19 cfs @ 8.52 fps)

Secondary OutFlow Max=34.34 cfs @ 12.00 hrs HW=14.63' (Free Discharge) —3=Concrete Curb (Weir Controls 34.34 cfs @ 1.76 fps)

Pond C-1: Chamber Series 1



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Summary for Pond C-4: Chamber Series 4

Inflow Area =	8.900 ac,	0.00% Impervious, Inflow	Depth > 5.34"	for 100-Year event
Inflow =	69.96 cfs @	11.99 hrs, Volume=	3.959 af	
Outflow =	56.32 cfs @	12.04 hrs, Volume=	3.628 af, Atte	en= 20%, Lag= 3.3 min
Discarded =	0.19 cfs @	12.03 hrs, Volume=	0.264 af	
Primary =	56.13 cfs @	12.04 hrs, Volume=	3.364 af	
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 15.22' @ 12.04 hrs Surf.Area= 16,391 sf Storage= 26,993 cf

Plug-Flow detention time= 137.4 min calculated for 3.627 af (92% of inflow) Center-of-Mass det. time= 92.3 min (865.1 - 772.9)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	8,911 cf	29.92'W x 213.63'L x 5.50'H Field B
			35,151 cf Overall - 12,874 cf Embedded = 22,277 cf x 40.0% Voids
#2B	6.75'	12,874 cf	ADS_StormTech MC-3500 d +Cap x 116 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			116 Chambers in 4 Rows
			Cap Storage= +14.9 cf x 2 x 4 rows = 119.2 cf
#3	14.10'	8,015 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		29,800 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
14.10	400	0	0
14.60	2,400	700	700
14.80	6,300	870	1,570
15.10	10,000	2,445	4,015
15.50	10,000	4,000	8,015

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	11.00'	36.0" Round Culvert
	•		L= 24.3' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 11.00' / 9.42' S= 0.0650 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

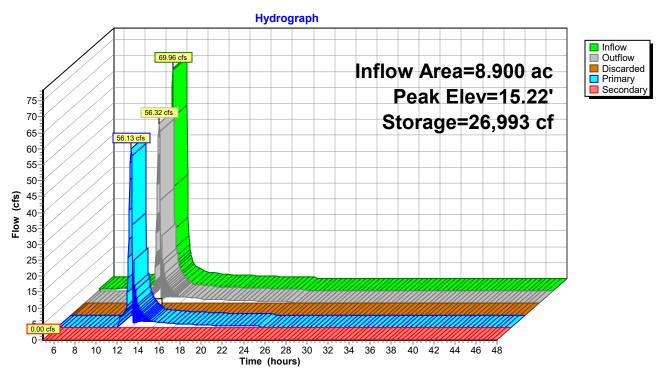
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Discarded OutFlow Max=0.19 cfs @ 12.03 hrs HW=15.16' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.19 cfs)

Primary OutFlow Max=55.90 cfs @ 12.04 hrs HW=15.20' (Free Discharge) 2=Culvert (Inlet Controls 55.90 cfs @ 7.91 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.01' (Free Discharge) 3=Wharf (Controls 0.00 cfs)

Pond C-4: Chamber Series 4



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Summary for Pond C-5: Chamber Series 5

Inflow Area =	5.200 ac,	0.00% Impervious, Inflow	Depth > 5.34" 1	for 100-Year event
Inflow =	41.34 cfs @	11.98 hrs, Volume=	2.313 af	
Outflow =	30.89 cfs @	12.05 hrs, Volume=	2.057 af, Atten	= 25%, Lag= 3.9 min
Discarded =	0.42 cfs @	12.05 hrs, Volume=	0.401 af	
Primary =	30.47 cfs @	12.05 hrs, Volume=	1.656 af	
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 15.35' @ 12.05 hrs Surf.Area= 18,202 sf Storage= 26,138 cf

Plug-Flow detention time= 242.1 min calculated for 2.054 af (89% of inflow) Center-of-Mass det. time= 188.6 min (961.1 - 772.5)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	7,757 cf	28.50'W x 168.47'L x 6.75'H Field B
			32,409 cf Overall - 13,016 cf Embedded = 19,393 cf x 40.0% Voids
#2B	6.75'	13,016 cf	ADS_StormTech MC-4500 b +Cap x 120 Inside #1
			Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf
			Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap
			120 Chambers in 3 Rows
			Cap Storage= +39.5 cf x 2 x 3 rows = 237.0 cf
#3	14.60'	7,420 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		28,193 cf	Total Available Storage

Storage Group B created with Chamber Wizard

	Elevation	Surf.Area	Inc.Store	Cum.Store
_	(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
	14.60	200	0	0
	14.80	1,000	120	120
	15.00	10,000	1,100	1,220
	15.50	14,800	6,200	7,420

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	1.000 in/hr Exfiltration over Surface area
#2	Primary	12.60'	36.0" Round Culvert
	•		L= 62.8' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 12.60' / 12.29' S= 0.0049 '/' Cc= 0.900
			n= 0.013 Cast iron, coated, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

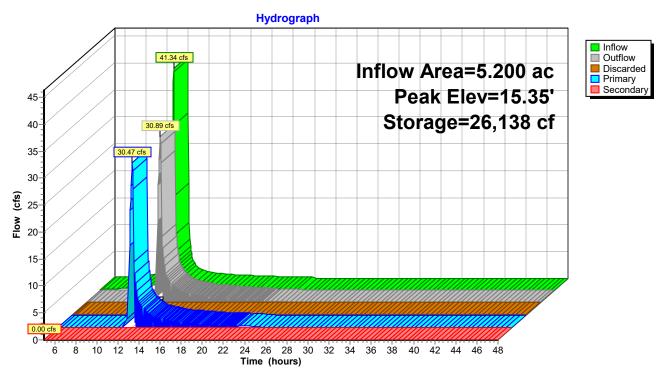
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Discarded OutFlow Max=0.42 cfs @ 12.05 hrs HW=15.35' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.42 cfs)

Primary OutFlow Max=30.43 cfs @ 12.05 hrs HW=15.35' (Free Discharge) 2=Culvert (Barrel Controls 30.43 cfs @ 5.87 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.01' (Free Discharge) 3=Wharf (Controls 0.00 cfs)

Pond C-5: Chamber Series 5



Appendix C

Water Quality and Runoff Reduction Volume Calculations

Version 1.8 Total Water Quality Volume Calculation
Last Updated: 11/09/2015 WQv(acre-feet) = [(P)(Rv)(A)] /12

Is this project subject to Chapter 10 of the NYS Design Manual (i.e. WQv is equal to post-	
development 1 year runoff volume)?	No

Design Point:

P= 1.20 inch

Manually enter P, Total Area and Impervious Cover.

Breakdown of Subcatchments							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft³)	Description	
1	10.30	10.20	99%	0.94	42,055		
2	5.50	5.30	96%	0.92	21,884		
3	11.00	10.60	96%	0.92	43,769		
4	8.90	8.60	97%	0.92	35,505		
5	5.20	4.90	94%	0.90	20,258		
6	11.80	11.60	98%	0.93	47,846		
7	8.70	8.40	97%	0.92	34,681		
8	2.90	2.00	69%	0.67	8,437		
9	5.80	3.10	53%	0.53	13,361		
10	0.00	0.00					
Subtotal (1-30)	76.70	65.89	86%	0.82	273,874	Subtotal 1	
Total	76.70	65.89	86%	0.82	273,874	Initial WQv	

Identify Runoff Reduction Techniques By Area							
Technique	Total Contributing Area	Contributing Impervious Area	Notes				
	(Acre)	(Acre)					
Conservation of Natural Areas	4.00	0.00	minimum 10,000 sf				
Riparian Buffers	0.00	0.00	maximum contributing length 75 feet to 150 feet				
Filter Strips	0.00	0.00					
Tree Planting	0.00	0.00	Up to 100 sf directly connected impervious area may be subtracted per tree				
Total	4.00	0.00					

Recalculate WQv after application of Area Reduction Techniques							
	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Runoff Coefficient Rv	WQv (ft³)		
"< <initial td="" wqv"<=""><td>76.70</td><td>65.89</td><td>86%</td><td>0.82</td><td>273,874</td></initial>	76.70	65.89	86%	0.82	273,874		
Subtract Area	-4.00	0.00					
WQv adjusted after Area Reductions	72.70	65.89	91%	0.87	273,007		
Disconnection of Rooftops		0.00					
Adjusted WQv after Area Reduction and Rooftop Disconnect	72.70	65.89	91%	0.87	273,007		
WQv reduced by Area Reduction techniques					868		

Total Water Quality Volume Calculation WQv(acre-feet) = [(P)(Rv)(A)] /12

	Additional Subcatchments								
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Description			
11	4.00	0.00	0%	0.05	868	Conservation of Natural Areas			
12	0.00	0.00							
13	1.10	0.45	41%	0.42	1,995	Infiltration Basin			
14	1.10	0.55	50%	0.50	2,386	Infiltration Basin			
15	0.10	0.05	50%	0.50	217	Dry Swale			
16	0.00	0.00							
17	0.30	0.14	47%	0.47	612	Dry Swale			
18									
19									
20									
21									
22									
23									
24									
25									
26									
27									
28									
29									
30									
Subtotal	6.60	1.19	18%	0.21	6,077	Subtotal			

Total Water Quality Volume Calculation WQv(acre-feet) = [(P)(Rv)(A)] /12

			Subcatchments			
Catchment	Total Area	Impervious	Percent	Runoff	WQv	Description
Catchinent	TOTAL ALEA	Cover	Impervious	Coefficient		Description
	(Acres)	(Acres)	%	Rv	(ft ³)	
1	10.30	10.20	0.99	0.94	42055.46	
2	5.50	5.30	0.96	0.92	21,884	
3	11.00	10.60	0.96	0.92	43768.91	
4	8.90	8.60	0.97	0.92	35505.30	
5	5.20	4.90	0.94	0.90	20257.76	
6	11.80	11.60	0.98	0.93	47846.49	
7	8.70	8.40	0.97	0.92	34681.11	
8	2.90	2.00	0.69	0.67	8437.12	
9	5.80	3.10	0.53	0.53	13360.58	
10	0.00	0.00				
11	4.00	0.00	0.00	0.05	867.57	Conservation of Natural Areas
12	0.00	0.00				
13	1.10	0.45	0.41	0.42	1995.41	Infiltration Basin
14	1.10	0.55	0.50	0.50	2385.82	Infiltration Basin
15	0.10	0.05	0.50	0.50	216.89	Dry Swale
16	0.00	0.00				
17	0.30	0.14	0.47	0.47	611.64	Dry Swale
18						
19						
20						
21						
22						
23						
24						
25						
26						
27						
28						
29						
30						

	Runoff Reduction Volume and Treated volumes									
	Runoff Reduction Techiques/Standard SMPs		Total Contributing Area	Total Contributing Impervious Area	WQv Reduced (RRv)	WQv Treated				
			(acres)	(acres)	cf	cf				
	Conservation of Natural Areas	RR-1	4.00	0.00						
Area/Volume Reduction	Sheetflow to Riparian Buffers/Filter Strips	RR-2	0.00	0.00						
nc	Tree Planting/Tree Pit	RR-3	0.00	0.00						
Rec	Disconnection of Rooftop Runoff	RR-4		0.00						
шe	Vegetated Swale	RR-5	0.00	0.00	0					
ınıc	Rain Garden	RR-6	0.00	0.00	0					
χ	Stormwater Planter	RR-7	0.00	0.00	0					
Area	Rain Barrel/Cistern	RR-8	0.00	0.00	0					
1	Porous Pavement	RR-9	0.00	0.00	0					
	Green Roof (Intensive & Extensive)	RR-10	0.00	0.00	0					
	Infiltration Trench	I-1	0.00	0.00	0	0				
IPs city	Infiltration Basin	I-2	26.60	24.70	62378	7042				
SN	Dry Well	I-3	0.00	0.00	0	0				
ard / Ca	Underground Infiltration System	I-4								
Standard SMPs w/RRv Capacity	Bioretention & Infiltration Bioretention	F-5	0.00	0.00	0	0				
	Dry swale	0-1	0.40	0.19	87	766				
	Micropool Extended Detention (P-1)	P-1				21798.000				
	Wet Pond (P-2)	P-2								
	Wet Extended Detention (P-3)	P-3								
	Multiple Pond system (P-4)	P-4								
S	Pocket Pond (p-5)	P-5								
Α̈́	Surface Sand filter (F-1)	F-1								
rd S	Underground Sand filter (F-2)	F-2								
ıdaı	Perimeter Sand Filter (F-3)	F-3								
Standard SMPs	Organic Filter (F-4)	F-4				181790.000				
,	Shallow Wetland (W-1)	W-1								
	Extended Detention Wetland (W-2	W-2								
	Pond/Wetland System (W-3)	W-3								
	Pocket Wetland (W-4)	W-4								
	Wet Swale (O-2)	0-2								
	Totals by Area Reduction	\rightarrow	4.00	0.00	868					
	Totals by Volume Reduction	\rightarrow	0.00	0.00	0					
	Totals by Standard SMP w/RRV	\rightarrow	27.00	24.89	62466	7808				
	Totals by Standard SMP	\rightarrow	0.00	0.00		203588				
T	otals (Area + Volume + all SMPs)	\rightarrow	31.00	24.89	63,333	211,396				
	Impervious Cover √	error								

Minimum RRv

Enter the Soils Da	ta for the site	
Soil Group	Acres	S
A	2.30	55%
В		40%
С		30%
D	70.40	20%
Total Area	72.7	
Calculate the Mini	imum RRv	
S =	0.21	
Impervious =	65.89	acre
Precipitation	1.195	in
Rv	0.95	
Minimum RRv	57,313	ft3
	1.32	af

Planning

Practice	Description	Application
Preservation of Undisturbed Areas	Delineate and place into permanent conservation undisturbed forests, native vegetated areas, riparian corridors, wetlands, and natural terrain.	Considered & Applied
Preservation of Buffers	Define, delineate and preserve naturally vegetated buffers along perennial streams, rivers, shorelines and wetlands.	Considered & Not Applied
Reduction of Clearing and Grading	Limit clearing and grading to the minimum amount needed for roads, driveways, foundations, utilities and stormwater management facilities.	Considered & Applied
Locating Development in Less Sensitive Areas	Avoid sensitive resource areas such as floodplains, steep slopes, erodible soils, wetlands, mature forests and critical habitats by locating development to fit the terrain in areas that will create the least impact.	Considered & Applied
Open Space Design	Use clustering, conservation design or open space design to reduce impervious cover, preserve more open space and protect water resources.	N/A
Soil Restoration	Restore the original properties and porosity of the soil by deep till and amendment with compost to reduce the generation of runoff and enhance the runoff reduction performance of post construction practices.	N/A
Roadway Reduction	Minimize roadway widths and lengths to reduce site impervious area	Considered & Applied
Sidewalk Reduction	Minimize sidewalk lengths and widths to reduce site impervious area	Considered & Applied
Driveway Reduction	Minimize driveway lengths and widths to reduce site impervious area	N/A
Cul-de-sac Reduction	Minimize the number of cul-de-sacs and incorporate landscaped areas to reduce their impervious cover.	N/A
Building Footprint Reduction	Reduce the impervious footprint of residences and commercial buildings by using alternate or taller buildings while maintaining the same floor to area ratio.	Considered & Applied
Parking Reduction	Reduce imperviousness on parking lots by eliminating unneeded spaces, providing compact car spaces and efficient parking lanes, minimizing stall dimensions, using porous pavement surfaces in overflow parking areas, and using multi-storied parking decks where appropriate.	Considered & Applied

NOI QUESTIONS

#	NOI Question	Reported Value		
		cf	af	
28	Total Water Quality Volume (WQv) Required	273874	6.287	
30	Total RRV Provided	63333	1.454	
31	Is RRv Provided ≥WQv Required?	No		
32	Minimum RRv	57313	1.316	
32a	Is RRv Provided ≥ Minimum RRv Required?	Yes		
33a	Total WQv Treated	211396	4.853	
34	Sum of Volume Reduced & Treated	274729	6.307	
34	Sum of Volume Reduced and Treated	274729	6.307	
35	Is Sum RRv Provided and WQv Provided ≥WQv Required?	Yes		

	Apply Peak Flow Attenuation							
36	Channel Protection	Срv						
37	Overbank	Qp						
37	Extreme Flood Control	Qf						
	Are Quantity Control requirements met?	Yes	Plan Completed					

Design Point:]					
	E	Inter Site Data	For Drainage	Area to	be Treated	by Practice	
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
1	10.30	10.20	0.99	0.94	42055.46	1.20	
Reduced by Disconnection of 0.00		99%	0.94	42,055	< <wqv adj<="" after="" td=""><td>_</td></wqv>	_	
Pnœt της portion or the wαν that is not rec reased to this practice.			ticeu ioi ali pir	actices	0	ft ³	
		Pretrea	tment Technic	gues to Pi	revent Clog	ging	
Infiltration Rate	<u> </u>		1.50	in/hour	Okay		
Pretreatment Sizing			25	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour		
Pretreatment R	eguired Volu	ıme	10,514	ft ³			
Pretreatment P			11,000	ft ³			
Pretreatment T	echniques ut	ilized	Other	<i>p</i> -			
			Size An Inf	iltration E	Basin		
Design Volume	42,055	ft ³	WQv				
Basal Area Required	42,055	ft ²	Infiltration pi through the f		_	ned to exfiltrate	the entire WQv
Basal Area Provided	23,609	ft ²					
Design Depth	1.00	ft					
Volume Provided	23,609	ft ³	Storage Volume provided in infiltration basin area (not including pretreatment.				
			Determine R	unoff Red	duction		
RRv	21,248	ft ³	90% of the storage provided in the basin or WQv whichever is smaller				
Volume Treated	20,807	ft ³	This is the portion of the WQv that is not reduced/infiltrated				
Sizing √			The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.				

WQv of the contributing area.

Enter Site Data For Drainage Area to be Treated by Practice									
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description		
4	8.90	8.60	0.97	0.92	35505.30	1.20			
Reduced by Disc	connection of		97%	0.92	35,505	< <wqv adjusting="" after="" disconnected="" for="" p="" rooftops<=""></wqv>			
Pnot to this pr		that is not red	0	ft ³					

		Pretrea	tment Technic	ques to P	revent Clogging				
Infiltration Rate			0.80	in/hour	Okay				
Pretreatment Si	zing		25	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour				
Pretreatment R	ume	8,876	ft ³						
Pretreatment P	rovided		10,000	ft ³					
Pretreatment T	echniques u	tilized	Other						
Size An Infiltration Basin									
Design Volume	35,505	ft ³	WQv						
Basal Area Required	35,505	ft ²	Infiltration practices shall be designed to exfiltrate the entire WQv through the floor of each practice.						
Basal Area Provided	20,516	ft ²							
Design Depth	1.00	ft							
Volume Provided	20,516	ft ³	Storage Volu pretreatment	•	led in infiltration basin ared	(not including			
			Determine R	unoff Red	luction				
RRv	18,464	ft ³	90% of the storage provided in the basin or WQv whichever is smaller						
Volume Treated	17,041	ft ³	This is the portion of the WQv that is not reduced/infiltrated						
Sizing V			The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.						

Enter Site Data For Drainage Area to be Treated by Practice									
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description		
5	5.20	4.90	0.94	0.90	20257.76	1.20			
Reduced by Disc	connection of		94%	0.90	20,258	< <wqv adjusting="" after="" for<br="">Disconnected Rooftops</wqv>			
Pnoft the portion routed to this pr		that is not red		ft ³					

		Pretrea	tment Technic	ques to P	revent Clogging				
Infiltration Rate			0.50	in/hour	Okay				
Pretreatment Si		25	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour					
Pretreatment Required Volume			5,064	ft ³					
Pretreatment P	rovided		5,100	ft ³					
Pretreatment Techniques utilized			Other						
Size An Infiltration Basin									
Design Volume	20,258	ft ³	WQv						
Basal Area Required	20,258	ft ²	Infiltration practices shall be designed to exfiltrate the entire WQv through the floor of each practice.						
Basal Area Provided	20,473	ft ²							
Design Depth	1.00	ft							
Volume Provided	20,473	ft ³	Storage Volu pretreatment	•	led in infiltration basin area	(not including			
			Determine R	unoff Red	luction				
RRv	18,426	ft ³	90% of the st	torage pro	ovided in the basin or WQv	whichever is smaller			
Volume Treated	1,832	ft ³	This is the portion of the WQv that is not reduced/infiltrated						
Sizing V	ОК		_	The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.					

Enter Site Data For Drainage Area to be Treated by Practice									
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description		
13	1.10	0.45	0.41	0.42	1995.41	1.20	Infiltration Basin		
Reduced by Disconnection of 41% 0.42 Proof the portion of the way that is not reduced for all practices					1,995	< <wqv adjusting="" after="" for<br="">Disconnected Rooftops</wqv>			
routed to this pr		that is not red		ft ³					

		Pretrea	tment Technic	ques to Pi	revent Clogging				
Infiltration Rate			4.50	in/hour	Okay				
Pretreatment Si		50	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour					
Pretreatment Required Volume			998	ft ³					
Pretreatment P	rovided		1,058	ft ³					
Pretreatment T	tilized	Sedimentatio	n Basin						
Size An Infiltration Basin									
Design Volume	1,995	ft ³	WQv						
Basal Area Required	512	ft ²	Infiltration practices shall be designed to exfiltrate the entire WQv through the floor of each practice.						
Basal Area Provided	639	ft ²							
Design Depth	3.90	ft							
Volume Provided	2,492	ft ³	pretreatment	t.	led in infiltration basin area (no	ot including			
			Determine R	unoff Rec	luction				
RRv	1,995	ft ³	90% of the st	torage pro	ovided in the basin or WQv whi	ichever is smaller			
Volume Treated	0	ft ³	This is the po	rtion of th	ne WQv that is not reduced/infi	ltrated			
Sizing V	ОК		The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.						

Design Point:								
3	E	nter Site Data	For Drainage	Area to	be Treated	by Practice		
Catchment Number	Area		Percent Impervious %	Rv	WQv (ft³)	Precipitation (in)	Description	
14	1.10	0.55	0.50	0.50	2385.82	1.20	Infiltration Basin	
Enter Imperviou Reduced by Disc Rooftons	50%	0.50	2,386	< <wqv adj<="" after="" td=""><td>_</td></wqv>	_			
<u>Pਨਿਦੀ ਵਿਸ਼ਦ ਸ਼ਹਾ ਸ਼ਹਾ</u> routed to this pr		that is not red	uceu ioi ali pia	actices	0	ft ³		
		Pretrea	tment Technic	gues to P	revent Clog	ging		
Infiltration Rate			12.00	in/hour	Okay			
Pretreatment Sizing			100	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour			
Pretreatment R	2,386	ft ³						
Pretreatment P	2,389	ft ³						
Pretreatment T	Sedimentation Basin							
			Size An Inf	iltration E	Basin			
Design Volume	2,386	ft ³	WQv					
Basal Area Required	612	ft ²	Infiltration pi through the f		_	gned to exfiltrate	the entire WQv	
Basal Area Provided	640	ft²						
Design Depth	3.90	ft						
Volume Provided	2,494	ft ³	Storage Volu pretreatment	•	led in infiltr	ation basin area	(not including	
			Determine R	unoff Red	duction			
RRv	2,245	ft ³	90% of the st	torage pro	ovided in th	e basin or WQv	whichever is smalle	
Volume Treated	141	ft ³	This is the po	rtion of th	ne WQv tha	t is not reduced/	infiltrated	
Sizing √	OK		The infiltration		•	e storage equal t	o or greater than th	

WQv of the contributing area.

Dry Swale Worksheet

Design Point:									
Catchment	Enter Total Area	Site Data For Impervious	Percent		reated by WQv	Practice Precipitation			
Number	(Acres)	Area (Acres)	Impervious %	Rv	(ft ³)	(in)	Description		
15	0.10	0.05	0.50	0.50	216.89	1.20	Dry Swale		
Enter Impervious Area Reduced by Disconnection of Rooftops 0.00			50%	0.50	217	< <wqv ac<br="" after="">Disconnected R</wqv>			
	Pretreatn	nent Provided			I	Pretreatment T	echnique		
Pretrea	atment (10% of	WQv)	22	ft ³					
Calculate Available Storage Capacity									
Bottom Width	1	ft			-	ht feet to avoid less than two feet			
Side Slope (X:1)	2	Okay	Channels shall be designed with moderate side slopes (flatter than 3:1) for most conditions. 2:1 is the absolute maximum side slope						
Longitudinal Slope	0%	Okay	Maximum longitudinal slope shall be 4%						
Flow Depth	0.75	ft	Maximum ponding depth of one foot at the mid-point of the channel, and a maximum depth of 18" at the end point of the channel (for storage of the WQv)						
Top Width	4	ft			•	Γ _W			
Area	1.88	sf	1		:				
Minimum Length	104	ft				d			
Actual Length	105	ft]			B_{W}			
End Point Depth check	1.00	Okay	A maximum of storage of the			end point of the	channel (for		
Storage Capacity	219	ft ³							
Soil Group (HSG	i)		Α						
			Runoff Redu	ıction					
Is the Dry Swale practice?	contributing flo	ow to another	No	Select	Practice				
RRv	87	ft ³	Runnoff Red		-	in HSG A and B	and 20% in HSG C		
Volume Treated	129	ft ³	This is the dif			*	ted and the runoff		
Volume Directed	0	ft ³	This volume i	s directe	ed another	practice			
Volume √	Okay		Check to be s	ure that	channel is	long enough to	store WQv		

Dry Swale Worksheet

Design Point:]						
	Enter	Site Data For	Drainage Area	to be T	reated by	Practice		
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description	
17	0.30	0.14	0.47	0.47	611.64	1.20	Dry Swale	
Enter Impervious Area Reduced by Disconnection of Rooftops 0.00			47%	0.47	47 612 < <wqv adjusting="" after="" disconnected="" for="" rooftops<="" td=""></wqv>			
		nent Provided	I	. 2		Pretreatment T	echnique	
Pretrea	atment (10% of '	<u> </u>	61	ft ³				
		Calculat	e Available St	orage C	apacity			
Bottom Width	2	ft	_			-	ht feet to avoid less than two feet	
Side Slope (X:1)	3	Okay	Channels shall be designed with moderate side slopes (flatter than 3:1) for most conditions. 2:1 is the absolute maximum side slope					
Longitudinal Slope	3%	Okay	Maximum longitudinal slope shall be 4%					
Flow Depth	1	ft	Maximum ponding depth of one foot at the mid-point of the channel, and a maximum depth of 18" at the end point of the channel (for storage of the WQv)					
Top Width	8	ft			-	Γ _w		
Area	5.00	sf	1		:	.1	/	
Minimum Length	110	ft				d		
Actual Length	115	ft			ŀ	B _W		
End Point Depth check	1.50	Okay	A maximum of the		18" at the	end point of the	e channel (for	
Storage Capacity	636	ft ³						
Soil Group (HSG	i)		D					
			Runoff Redu	ıction				
Is the Dry Swale practice?	contributing flo	ow to another	No Select Practice					
RRv	127	ft ³	Runnoff Redu and D up to t			in HSG A and B	and 20% in HSG C	
Volume Treated	484	ft ³	This is the dif reduction ach				ted and the runoff	
Volume Directed	0	ft ³	This volume i	s directe	ed another	practice		
Volume √	Okay		Check to be s	ure that	channel is	long enough to	store WQv	
				_				

Conservation of Natural Areas

Design Point:											
Enter Site Data For Drainage Area to be Treated by Practice											
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	WOV		Precipitation (in)	Description				
11	4.00	0.00	0.00	0.05	867.57	1.20	Conservation of Natural Areas				
			Design E	lements							
Is Contiguous A	rea ≥ 10,000 t	ft2?				Yes					
Will limits of dis		•			_	Yes					
Is the Conserva					asement	Yes					
Does the easem managed and b		e	Yes								
Does the conse	rvation area r	eceive runoff	from other co	ntributin	g areas?	No					
Does Conservat	ion Area draii	Yes									
Is Sheet Flow to being Used for t	•	ready	No								
Are All Criteria in Section 5.3.1 Met? Area Reduction Adjustments											
		, , , , , , , , , , , , , , , , , , ,	Tea Reductio	n Aujustr	nents						
	Subtract	4.00	Acres from To	otal Area							
	Subtract	0.00	Acres from To	otal Impe	rvious Ar	ea					



Date:1/18/2022Project:Port of AlbanyLocation:Albany, NYPrepared For:Natalie Olivieri

Purpose: To calculate the water quality flow rate (Qwq) over a given site area. In this situation the WQv

to be analyzed is the runoff produced by the first 1.2 inch(es) of rainfall, per Fig 4.1 of the New

York State Stormwater Management Design Manual

Reference: United States Department of Agriculture Natural Resources Conservation Service TR-55

Manual, New York State Stormwater Management Design Manual - 2015

Formulas: $WQv = \frac{(P)(R_v)(A)}{12}$

 $R_v = (0.05 + 0.009(I)$

 $CN = 1000/[10+5P+10Qa-10(Qa^2+1.25QaP)^{1/2}]$

 $Qwq = (q_u)^*(A)^*(Qa)$

Structure:	WQU 1		Structure:	WQU 2		Structure:	WQU 3	
Р	1.20	in.	Р	1.20	in.	Р	1.20	in.
Α	10.300	ac	Α	5.500	ac	Α	11.000	ac
I	99.03	%	I	96.36	%	I	96.36	%
t_c	10.0	min.	t _c	10.0	min.	t _c	10.4	min.
t_{c}	0.167	hr.	t_c	0.167	hr.	t_c	0.173	hr.
R_{v}	0.941		R_v	0.917]	R_v	0.917]
43% WQv	0.413	ac-ft	90% WQv	0.504	ac-ft	90% WQv	1.009	ac-ft
43% WQv	18003.65	ft ³	90% WQv	21971.66	ft ³	90% WQv	43938.97	ft ³
Qa	1.129	in.	Qa	1.101	in.	Qa	1.100	in.
CN	97.00		CN	94.00]	CN	95.00	
I_a	0.062		I_a	0.128]	I_a	0.105	
I _a /P	0.052		I _a /P	0.107		I _a /P	0.088	
qu	1000	(csm/in)	qu	1000	(csm/in)	qu	1000	(csm/in)
Α	0.01609	miles ²	Α	0.00859	miles ²	Α	0.01719	miles ²
Qwq	7.81	cfs	Qwq	9.46	cfs	Qwq	18.91	cfs



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Formulas: $WQv = \frac{(P)(R_v)(A)}{12}$

 $R_v = (0.05 + 0.009(I)$

 $CN = 1000/[10+5P+10Qa-10(Qa^2+1.25QaP)^{1/2}]$

 $Qwq = (q_u)^*(A)^*(Qa)$

Structure:	WQU 4		Structure:	WQU 6	
Р	1.20	in.	Р	1.20	in.
Α	8.900	ac	Α	11.800	ac
1	96.63	%	I	98.31	%
t_c	10.0	min.	$t_{\mathtt{c}}$	10.0	min.
t_c	0.167	hr.	t_c	0.167	hr.
R_v	0.92		R_{v}	0.935	
42% WQv	0.342	ac-ft	90% WQv	1.103	ac-ft
42% WQv	14912.10	ft ³	90% WQv	48059.75	ft ³
Qa	1.104	in.	Qa	1.122	in.
CN	94.00		CN	96.00	
I_a	0.128		l _a	0.083	
I _a /P	0.107		I _a /P	0.069	
qu	1000	(csm/in)	qu	1000	(csm/in)
Α	0.01391	miles ²	Α	0.01844	miles ²
Qwq	6.44	cfs	Qwq	20.69	cfs



Date:1/18/2022Project:Port of AlbanyLocation:Albany, NYPrepared For:Natalie Olivieri

Purpose: To calculate the water quality flow rate (Qwq) over a given site area. In this situation

the WQv to be analyzed is the runoff produced by the first 1.2 inch(es) of rainfall, per

Fig 4.1 of the New York State Stormwater Management Design Manual

Reference: United States Department of Agriculture Natural Resources Conservation Service TR-

55 Manual, New York State Stormwater Management Design Manual - 2015

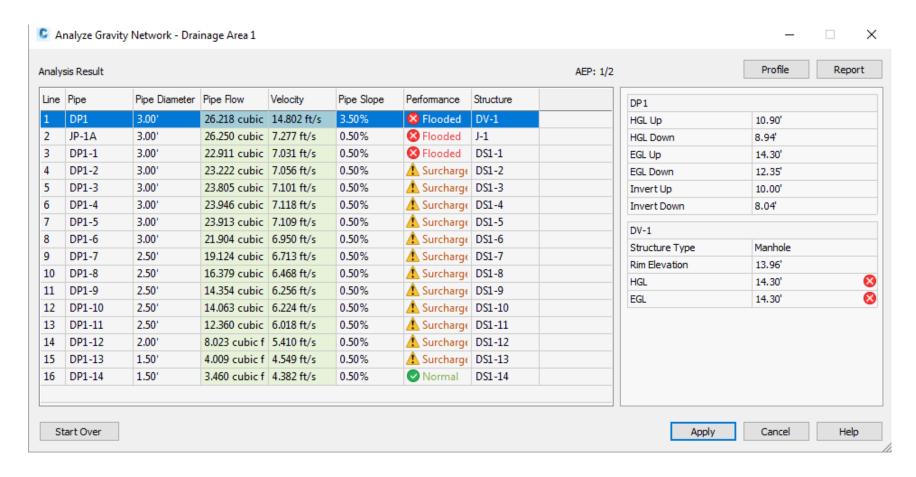
Formulas: $WQv = \frac{(P)(R_v)(A)}{12}$

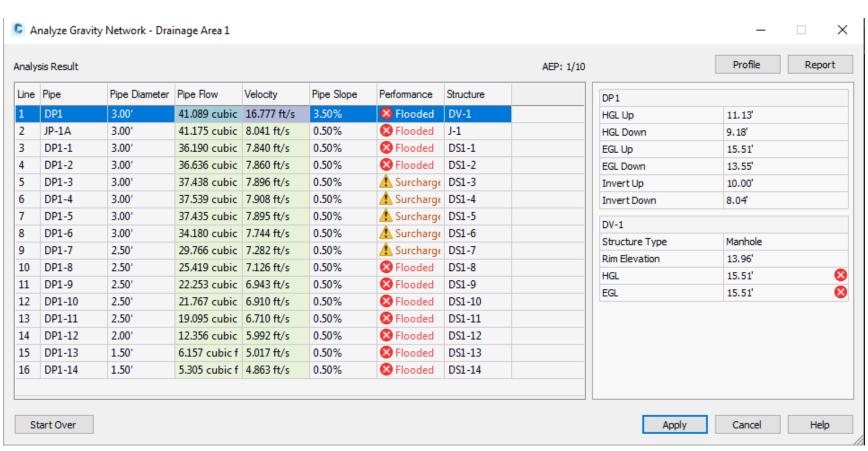
 $R_v = (0.05 + 0.009(I))$

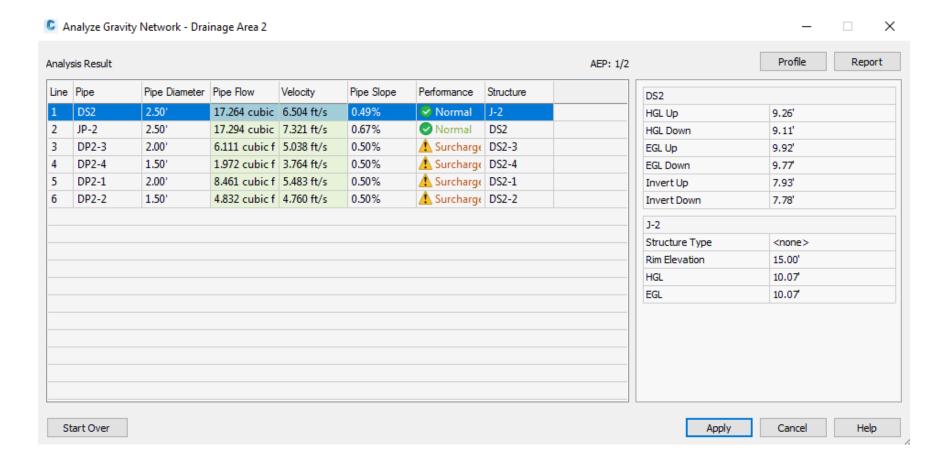
 $CN = 1000/[10+5P+10Qa-10(Qa^2+1.25QaP)^{1/2}]$

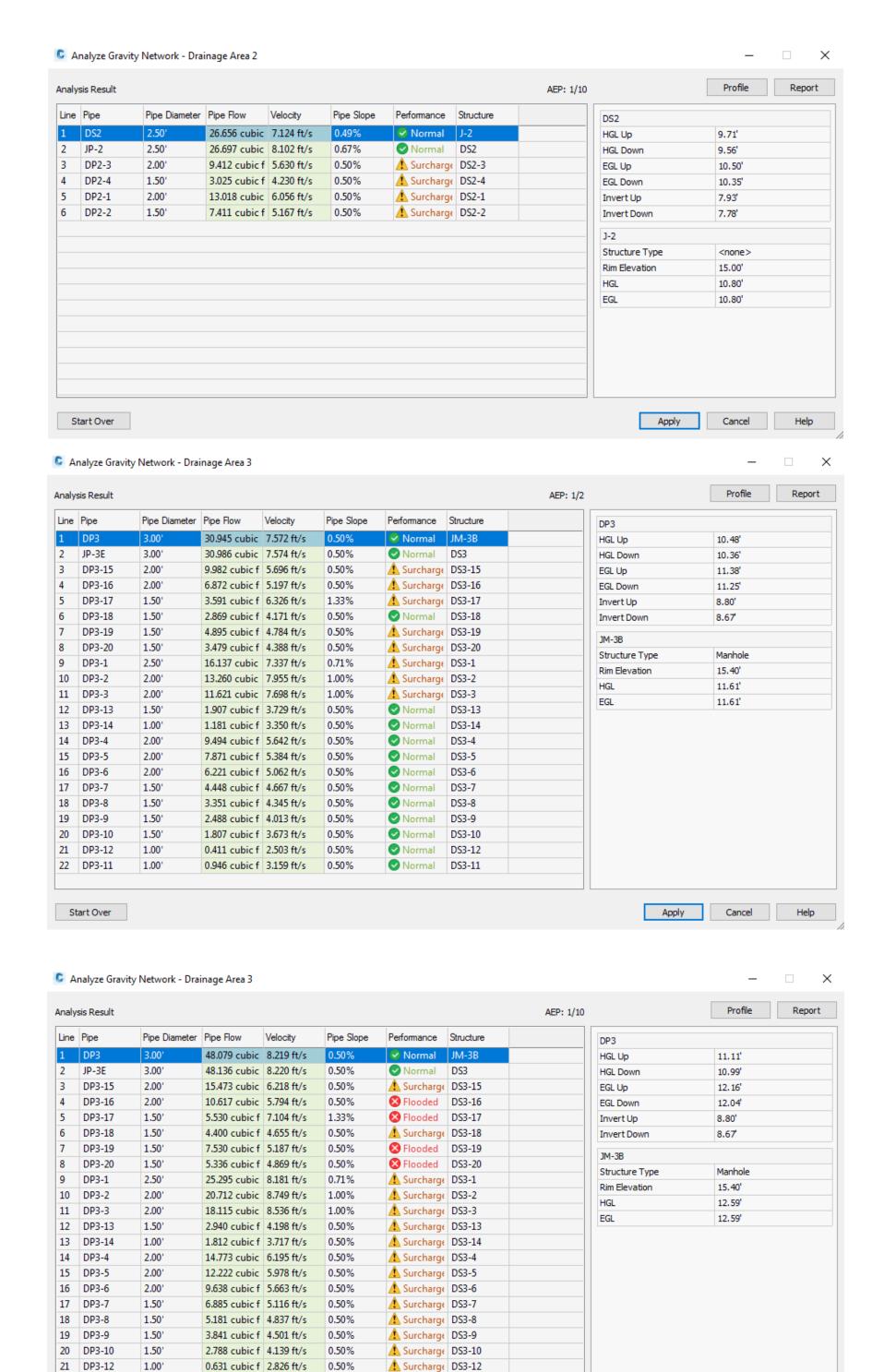
 $Qwq = (q_u)^*(A)^*(Qa)$

WQU7 Structure: Ρ 1.20 in. Α 8.700 ac 96.55 % I t_{c} 10.5 min. 0.175 hr. t_{c} 0.919 R_v 90% WQv 0.800 ac-ft 90% WQv 34826.22 ft³ Qa 1.103 in. CN 96.00 I_a 0.083 I_a/P 0.069 1000 qu (csm/in) Α 0.01359 miles² 14.99 cfs Qwq









22 DP3-11

Start Over

1.00

1.451 cubic f 3.528 ft/s

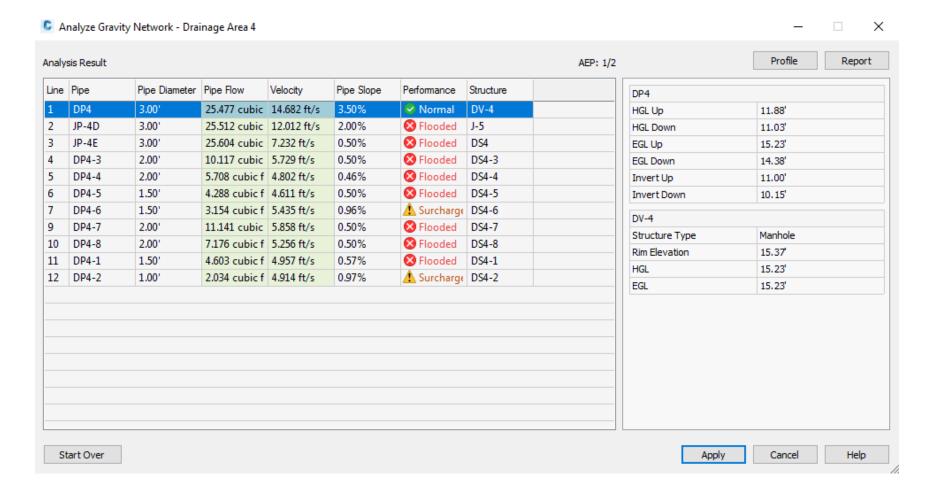
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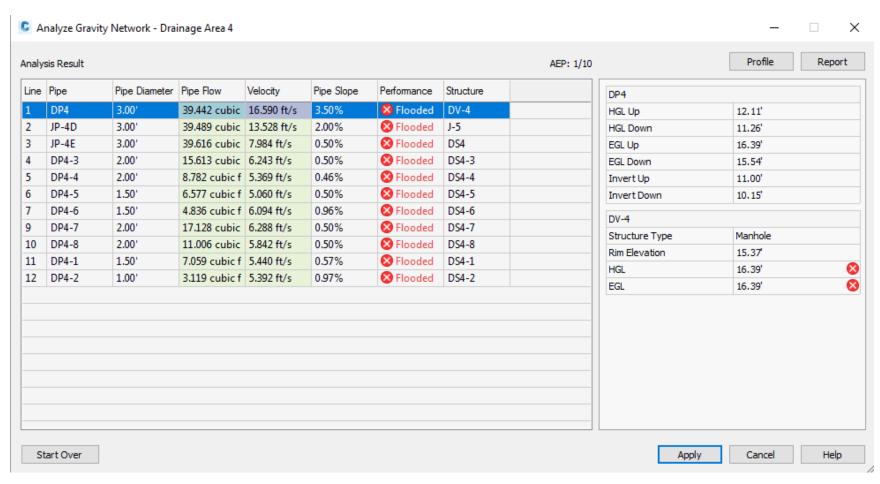
▲ Surcharge DS3-11

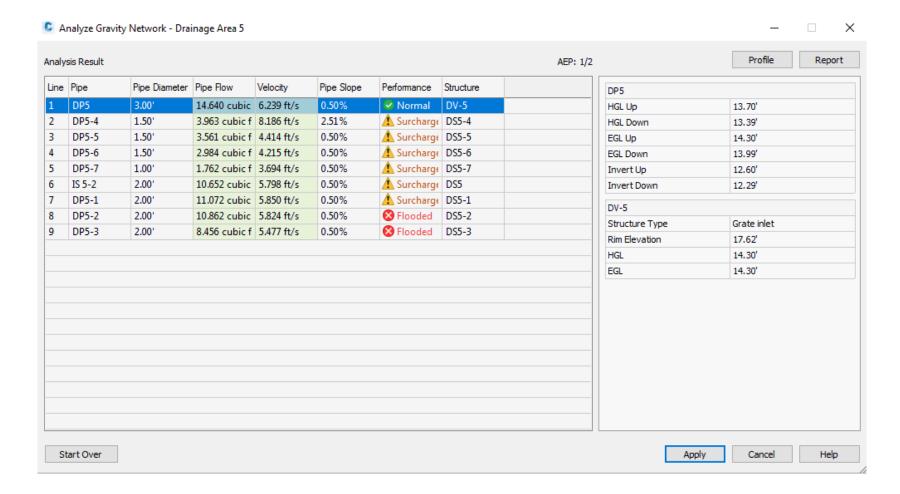
Apply

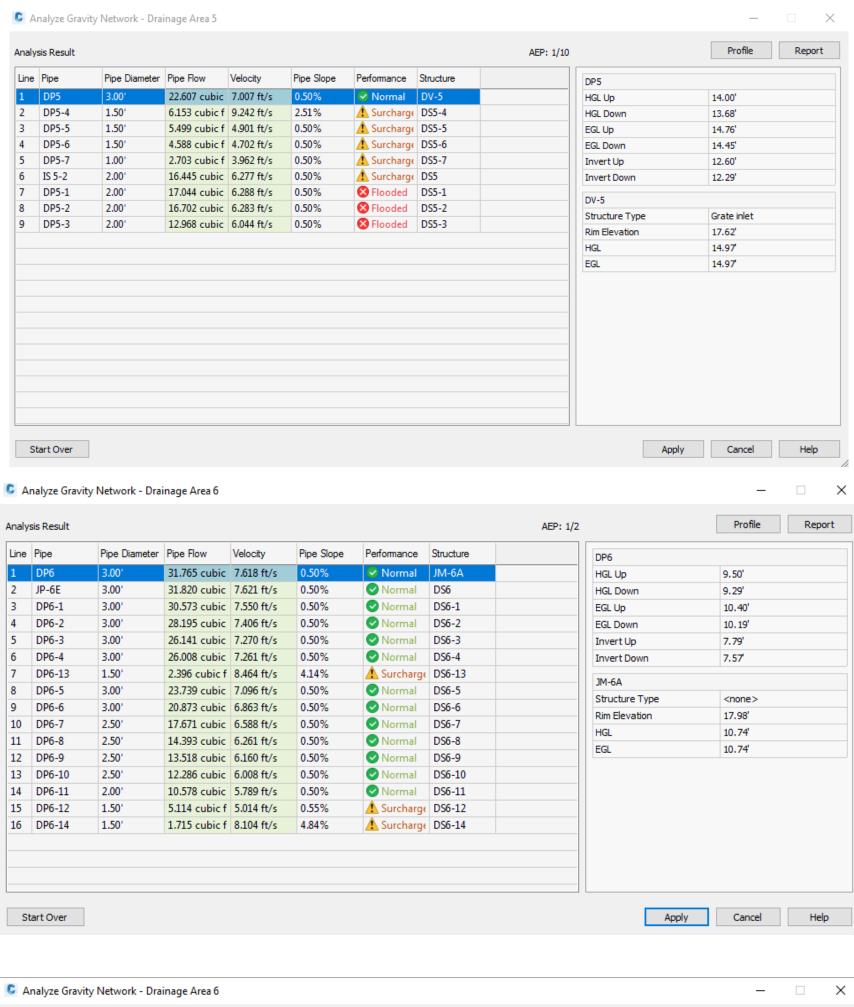
Cancel

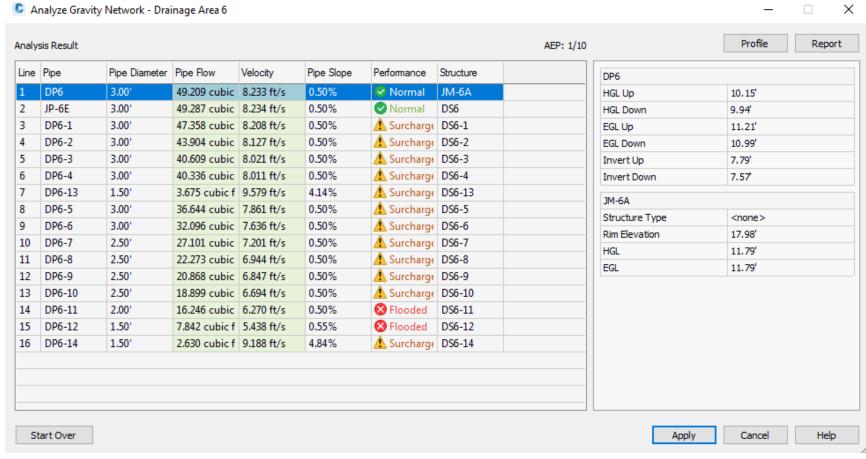
Help

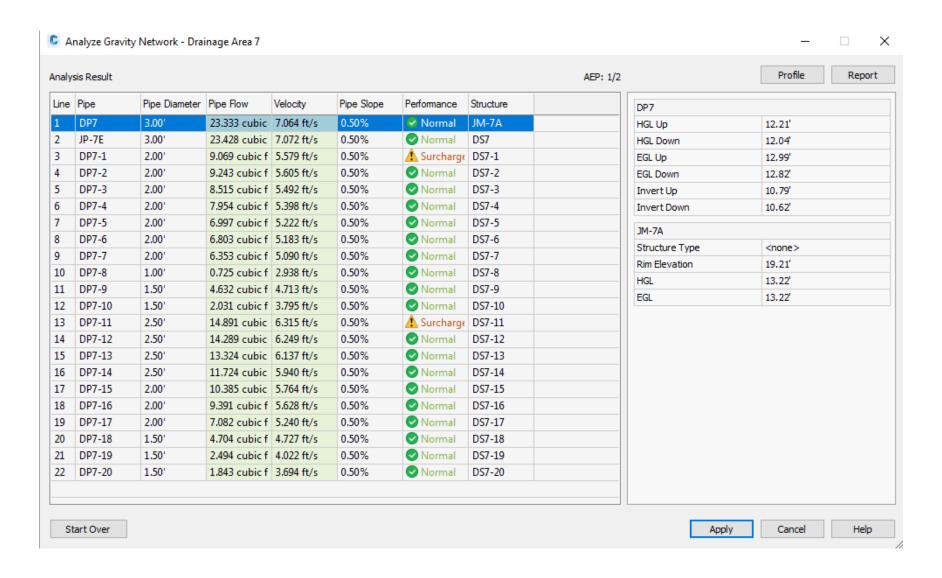


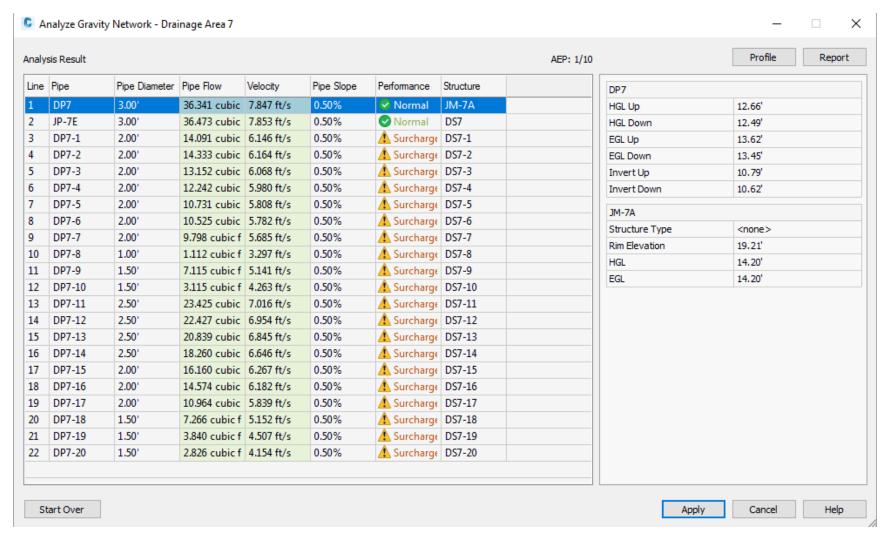












Appendix D

Stormwater Practice Specifications

StormTech® MC-3500

Chamber

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots, thus maximizing land usage for private (commercial) and public applications. StormTech chambers can also be used in conjunction with Green Infrastructure, thus enhancing the performance and extending the service life of these practices.



(not to scale)

Size (L x W x H)

90" x 77" x 45" 2286 mm x 1956 mm x 1143 mm

Chamber Storage 109.9 ft³ (3.11 m³)

Min. Installed Storage* 175.0 ft³ (4.96 m³)

Weight 134 lbs (60.8 kg)

Shipping

15 chambers/pallet 7 end caps/pallet 7 pallets/truck

*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below chambers, 6" (150 mm) of stone between chambers/end caps and 40% stone porosity.

Nominal End Cap Specifications (not to scale)

Size (L x W x H)26.5" x 71" x 45.1"
673 mm x 1803 mm x 1145 mm

End Cap Storage 14.9 ft³ (0.42 m³)

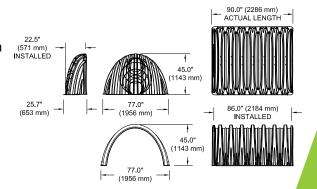
Min. Installed Storage* 45.1 ft³ (1.28 m³)

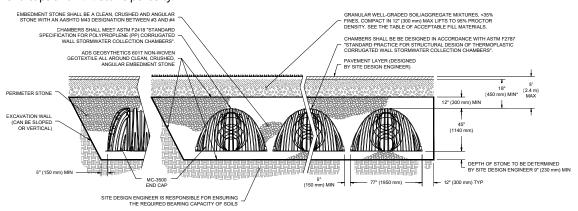
Weight

49 lbs (22.2 kg)

*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below, 6" (150 mm) of stone perimeter, 6" (150 mm) of stone between chambers/end caps and 40% stone porosity.







*MINIMUM COVER TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY OCCUR, INCREASE COVER TO 24" (600 mm



StormTech MC-3500 Specifications

Storage Volume Per Chamber

Bare Chamber		Chamber and Stone Foundation Depth in. (mm)					
	Storage ft³ (m³)	9 in (230 mm)	12 in (300 mm)	15 in (375 mm)	18 in (450 mm)		
Chamber	109.9 (3.11)	175.0 (4.96)	179.9 (5.09)	184.9 (5.24)	189.9 (5.38)		
End Cap	14.9 (0.42)	45.1 (1.28)	46.6 (1.32)	48.3 (1.37)	49.9 (1.41)		

Note: Assumes 6" (150 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume.

Amount of Stone Per Chamber

English	Stone Foundation Depth					
English Tons (yds³)	9 in	12 in	15 in	18 in		
Chamber	8.5 (6.0)	9.1 (6.5)	9.7 (6.9)	10.4 (7.4)		
End Cap	3.9 (2.8) 4.1 (2.9)		4.3 (3.1)	4.5 (3.2)		
Metric Kilograms (m³)	230 mm	300 mm	375 mm	450 mm		
Chamber	7711 (4.6)	8255 (5.0)	8800 (5.3)	9435 (5.7)		
End Cap	3538 (2.1)	3719 (2.2)	3901 (2.4)	4082 (2.5)		

Note: Assumes 12" (300 mm) of stone above and 6" (150 mm) row spacing and 6" (150 mm) of perimeter stone in front of end caps.

Volume Excavation Per Chamber yd³ (m³)

		Stone Foundation Depth					
	9 in (230 mm)	12 in (300 mm)	15 in (375mm)	18 in (450 mm)			
Chamber	11.9 (9.1)	12.4 (9.5)	12.8 (9.8)	13.3 (10.2)			
End Cap	4.0 (3.1)	4.1 (3.3)	4.3 (3.3)	4.4 (3.4)			

Note: Assumes 6" (150 mm) of separation between chamber rows and 24" (600 mm) of cover. The volume of excavation will vary as depth of cover increases.

Working on a project?

Visit us at www.stormtech.com and utilize the Design Tool

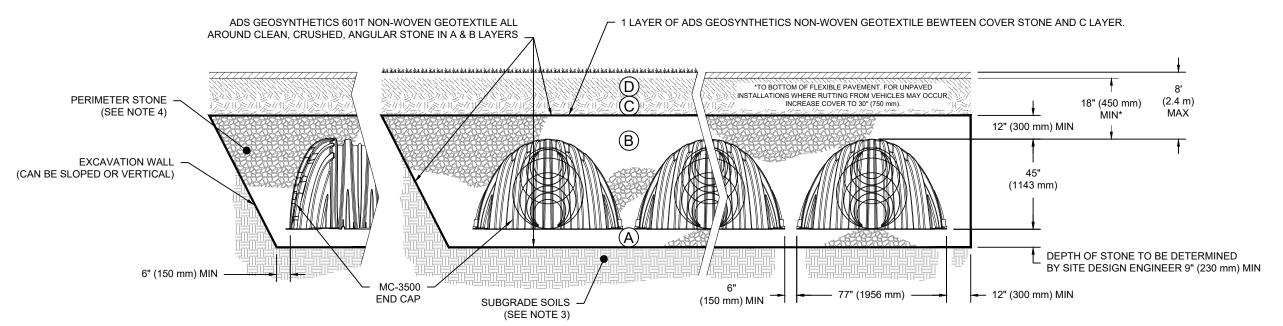


ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 24" (600 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 12" (300 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 ¹ 3, 4	NO COMPACTION REQUIRED.
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43¹ 3, 4	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. ^{2,3}

PLEASE NOTE:

- 1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
- 2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
- 3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.
- 4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.



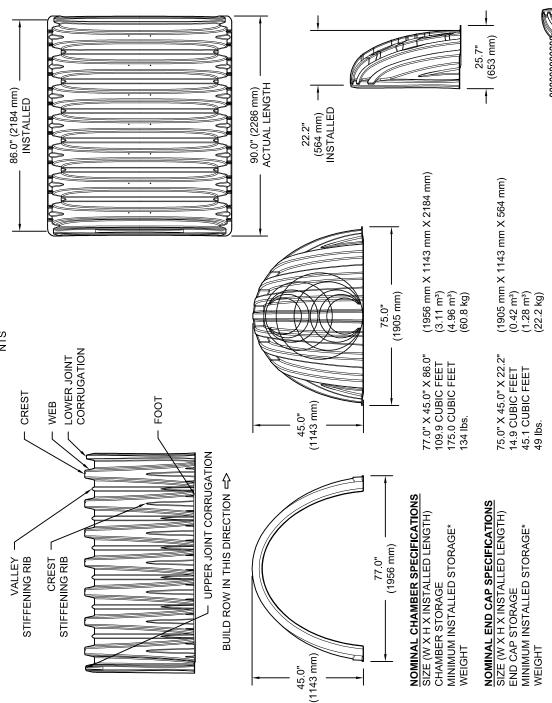
*FOR COVER DEPTHS GREATER THAN 8.0' (2.4 m) PLEASE CONTACT STORMTECH

NOTES:

- 1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418-16a, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 45x76 DESIGNATION SS.
- 2. MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 500 LBS/IN/IN. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

AC-3500	STANDARD CROSS SECTION	05-10-19 DRAWN: KR		CHECKED: NR	O CONSTRUCTION. IT IS THE ULTIMA
DM	STANDARD (DATE: 05-10-19	:	PROJECT #:	ALL REVIEW THIS DRAWING PRIOR 1
				DESCRIPTION	RESENTATIVE. THE SITE DESIGN ENGINEER SH. JATIONS, AND PROJECT REQUIREMENTS.
				DATE DRWN CHKD	HER PROJECT REP ABLE LAWS, REGUL
				DATE	EER OR OTH
***	Stormlech	Detention-Retention Water Quality	70 INWOOD ROAD, SUITE 3 ROCKY HILL CT 06067	860-529-8188 888-892-2694 WWW.STORMTECH.COM	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMA RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.
4640 TRUEMAN BLVD					ED BASED ON INFORMATION PROV GN ENGINEER TO ENSURE THAT T
	ADVANCED DRAINAGE SYSTEMS, INC.				THIS DRAWING HAS BEEN PREPARE RESPONSIBILITY OF THE SITE DESIG
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MC-3500 TECHNICAL SPECIFICATION

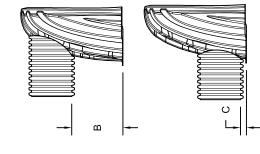


*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION, 6" (152 mm) OF STONE BETWEEN CHAMBERS, 6" (152 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY

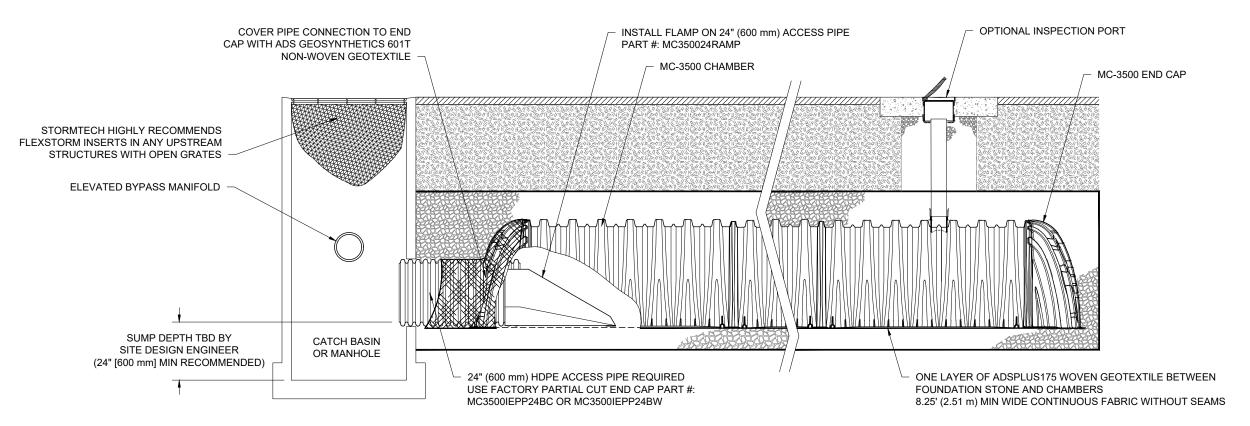
STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B" STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T" END CAPS WITH A WELDED CROWN PLATE END WITH "C" END CAPS WITH A PREFABRICATED WELDED STUB END WITH "W"

PART#	STUB	В	C
MC3500IEPP06T	(8" (15)	33.21" (844 mm)	
MC3500IEPP06B	(0.66" (17 mm)
MC3500IEPP08T	(8, 100)	31.16" (791 mm)	
MC3500IEPP08B	(200	-	0.81" (21 mm)
MC3500IEPP10T	(26) "01	29.04" (738 mm)	-
MC3500IEPP10B	(10 (200 11111)	-	0.93" (24 mm)
MC3500IEPP12T	(300)	26.36" (670 mm)	
MC3500IEPP12B	(300 11111)	ļ	1.35" (34 mm)
MC3500IEPP15T	15" (375 mm)	23.39" (594 mm)	
MC3500IEPP15B	(111111)		1.50" (38 mm)
MC3500IEPP18TC		20.03" (509 mm)	
MC3500IEPP18TW	18" (450 mm)	(203 [[]]])	i.
MC3500IEPP18BC	(111111 00+) 01		1 77" (15 mm)
MC3500IEPP18BW		ļ	(+) (+)
MC3500IEPP24TC		14 48" (368 mm)	
MC3500IEPP24TW	24" (600 mm)	14:40 (300 11111)	
MC3500IEPP24BC	(11111)		2 (16" (52 mm)
MC3500IEPP24BW			2.00 (02 11111)
MC3500IEPP30BC	30" (750 mm)	ļ	2.75" (70 mm)

NOTE: ALL DIMENSIONS ARE NOMINAL



CUSTOM PRECORED INVERTS ARE
AVAILABLE UPON REQUEST.
INVENTORIED MANIFOLDS INCLUDE
12-24" (300-600 mm) SIZE ON SIZE
AND 15-48" (375-1200 mm)
ECCENTRIC MANIFOLDS. CUSTOM
INVERT LOCATIONS ON THE MC-3500
END CAP CUT IN THE FIELD ARE NOT
RECOMMENDED FOR PIPE SIZES
GREATER THAN 10" (250 mm). THE
INVERT LOCATION IN COLUMN 'B'
ARE THE HIGHEST POSSIBLE FOR
THE PIPE SIZE.



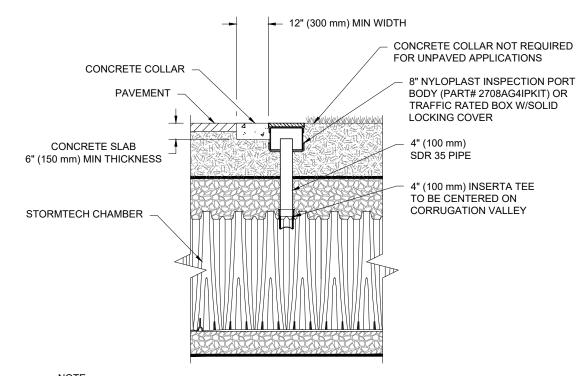
MC-3500 ISOLATOR ROW PLUS DETAIL

INSPECTION & MAINTENANCE

- INSPECT ISOLATOR ROW PLUS FOR SEDIMENT
 - A. INSPECTION PORTS (IF PRESENT)
 - REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
 - REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
 - USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG A.3.
 - LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
 - IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3. A 5
 - B. ALL ISOLATOR PLUS ROWS
 - REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
 - USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



INSPECTION PORTS MAY BE CONNECTED THROUGH ANY CHAMBER CORRUGATION VALLEY.

4" PVC INSPECTION PORT DETAIL (MC SERIES CHAMBER)

Storm

4640 TRUEMAN BLVD HILLIARD, OH 43026

ISOLATOR ROW PLUS DETAILS

08/26/20

MC-3500

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MC-4500 CHAMBER

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots, thus maximizing land usage for private (commercial) and public applications. StormTech chambers can also be used in conjunction with Green Infrastructure, thus enhancing the performance and extending the service life of these practices.

STORMTECH MC-4500 CHAMBER

(not to scale)

Nominal Chamber Specifications

Size (L x W x H) 52" x 100" x 60" 1321 mm x 2540 mm x 1524 mm

Chamber Storage 106.5 ft³ (3.01 m³)

Min. Installed Storage* 162.6 ft³ (4.60 m³)

Weight

Nominal 125 lbs (56.7 kg)

Shipping

7 chambers/pallet 5 end caps/pallet 11 pallets/truck

*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below chambers, 9" (230 mm) of stone between chambers/end caps and 40% stone porosity.

STORMTECH MC-4500 END CAP (not to scale)

Nominal End Cap Specifications

Size (L x W x H)38" x 90" x 61"
965 mm x 2286 mm x 1549 mm

End Cap Storage 39.5 ft³ (1.12 m³)

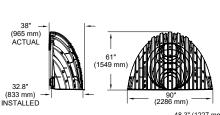
Min. Installed Storage* 115.3 ft³ (3.26 m³)

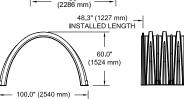
Weight

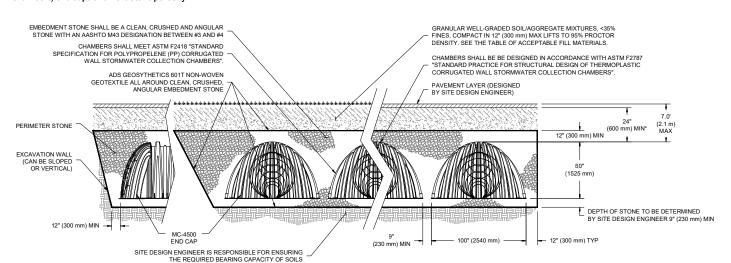
Nominal 90.0 lbs (40.8 kg)

*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below, 12" (300 mm) of stone perimeter, 9" (230 mm) of stone between chambers/end caps and 40% stone porosity.













MC-4500 CHAMBER SPECIFICATIONS

STORAGE VOLUME PER CHAMBER FT3 (M3)

Bare Chamber Storage ft³ (m³)		Chamber and Stone Foundation Depth in. (mm)				
		9" (230 mm)	12" (300 mm)	15" (375 mm)	18" (450 mm)	
MC-4500 Chamber	106.5 (3.01)	162.6 (4.60)	166.3 (4.71)	169.9 (4.81)	173.6 (4.91)	
MC-4500 End Cap	39.5 (1.12)	115.3 (3.26)	118.6 (3.36)	121.9 (3.45)	125.2 (3.54)	

Note: Assumes 9" (230 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume. End cap volume assumes 12" (300 mm) stone perimeter in front of end cap.

AMOUNT OF STONE PER CHAMBER

ENGLICH TONC (v.d-3)	Stone Foundation Depth					
ENGLISH TONS (yds ³)	9"	12"	15"	18"		
MC-4500 Chamber	7.4 (5.2)	7.8 (5.5)	8.3 (5.9)	8.8 (6.2)		
MC-4500 End Cap	9.8 (7.0)	10.2 (7.3)	10.6 (7.6)	11.1 (7.9)		
METRIC KILOGRAMS (m³)	230 mm	300 mm	375 mm	450 mm		
MC-4500 Chamber	6713 (4.0)	7076 (4.2)	7529 (4.5)	7983 (4.7)		
MC-4500 End Cap	8890 (5.3)	9253 (5.5)	9616 (5.8)	10069 (6.0)		

Note: Assumes 12" (300 mm) of stone above and 9" (230 mm) row spacing and 12" (300 mm) of perimeter stone in front of end caps.

VOLUME EXCAVATION PER CHAMBER YD3 (M3)

		Stone Foundation Depth				
	9" (230 mm)	' (230 mm) 12" (300 mm) 15" (375m		18" (450 mm)		
MC-4500 Chamber	10.5 (8.0)	10.8 (8.3)	11.2 (8.5)	11.5 (8.8)		
MC-4500 End Cap	9.7 (7.4)	10.0 (7.6)	10.3 (7.9)	10.6 (8.1)		

Note: Assumes 9" (230 mm) of separation between chamber rows, 12" (300 mm) of perimeter in front of the end caps, and 24" (600 mm) of cover. The volume of excavation will vary as depth of cover increases.



Working on a project? Visit us at www.stormtech.com and utilize the StormTech Design Tool

For more information on the StormTech MC-4500 Chamber and other ADS products, please contact our Customer Service Representatives at 1-800-821-6710

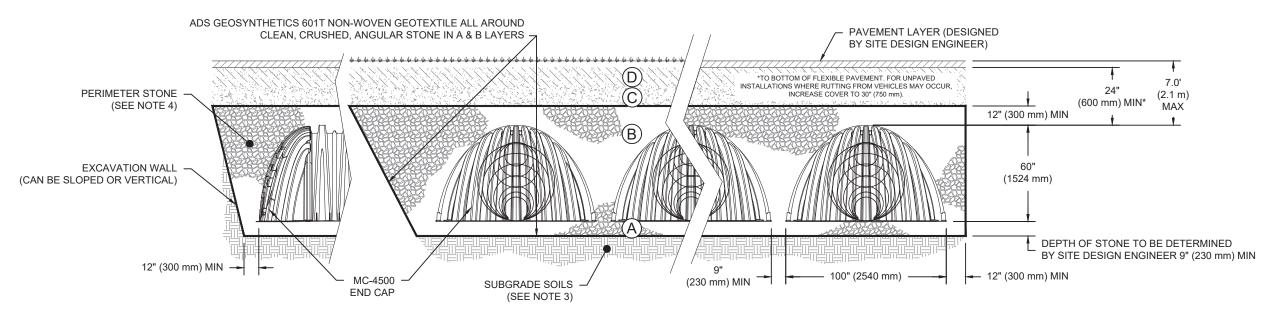
Advanced Drainage Systems, Inc. 4640 Trueman Blvd., Hilliard, OH 43026 1-800-821-6710 www.ads-pipe.com

ACCEPTABLE FILL MATERIALS: STORMTECH MC-4500 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 24" (600 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 12" (300 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 ¹ 3, 4	NO COMPACTION REQUIRED.
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 ¹ 3, 4	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. ^{2,3}

PLEASE NOTE:

- 1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
- 2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
- 3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.
- 4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.



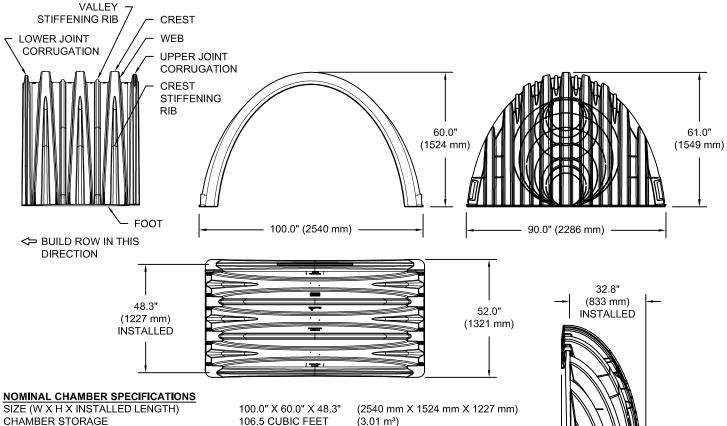
*FOR COVER DEPTHS GREATER THAN 7.0' (2.1 m) PLEASE CONTACT STORMTECH

NOTES:

- 1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418-16a, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 60x101
- 2. MC-4500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 500 LBS/IN/IN. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

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MC-4500 TECHNICAL SPECIFICATION



(4.60 m³)

(56.7 kg)

CHAMBER STORAGE MINIMUM INSTALLED STORAGE* WEIGHT (NOMINAL)

NOMINAL END CAP SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH)

90.0" X 61.0" X 32.8"

162.6 CUBIC FEET

125.0 lbs.

(2286 mm X 1549 mm X 833 mm)

39.5 CUBIC FEET (1.12 m³) 115.3 CUBIC FEET (3.26 m³) 90 lbs. (40.8 kg)

MINIMUM INSTALLED STORAGE*

WEIGHT (NOMINAL)

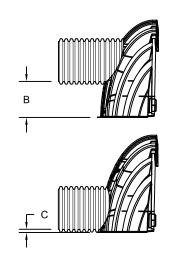
END CAP STORAGE

*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION AND BETWEEN CHAMBERS, 12" (305 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY.

PARTIAL CUT HOLES AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B" PARTIAL CUT HOLES AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T" END CAPS WITH A PREFABRICATED WELDED STUB END WITH "W"

PART#	STUB	В	С
MC4500IEPP06T	6" (150 mm)	42.54" (1081 mm)	
MC4500IEPP06B	6 (150111111)		0.86" (22 mm)
MC4500IEPP08T	8" (200 mm)	40.50" (1029 mm)	
MC4500IEPP08B	6 (200 111111)		1.01" (26 mm)
MC4500IEPP10T	10" (250 mm)	38.37" (975 mm)	
MC4500IEPP10B	10 (230 11111)		1.33" (34 mm)
MC4500IEPP12T	12" (300 mm)	35.69" (907 mm) 	
MC4500IEPP12B	12 (300 11111)		1.55" (39 mm)
MC4500IEPP15T	15" (375 mm)	32.72" (831 mm) 	
MC4500IEPP15B	13 (3/311111)		1.70" (43 mm)
MC4500IEPP18T		29.36" (746 mm)	
MC4500IEPP18TW	18" (450 mm)	23.30 (740 11111)	
MC4500IEPP18B			1.97" (50 mm)
MC4500IEPP18BW			1.97 (50 11111)
MC4500IEPP24T		23.05" (585 mm)	
MC4500IEPP24TW	24" (600 mm)	23.03 (303 11111)	<u></u>
MC4500IEPP24B			2.26" (57 mm)
MC4500IEPP24BW			2.20 (37 111111)
MC4500IEPP30BW	30" (750 mm)		2.95" (75 mm)
MC4500IEPP36BW	36" (900 mm)		3.25" (83 mm)
MC4500IEPP42BW	42" (1050 mm)		3.55" (90 mm)

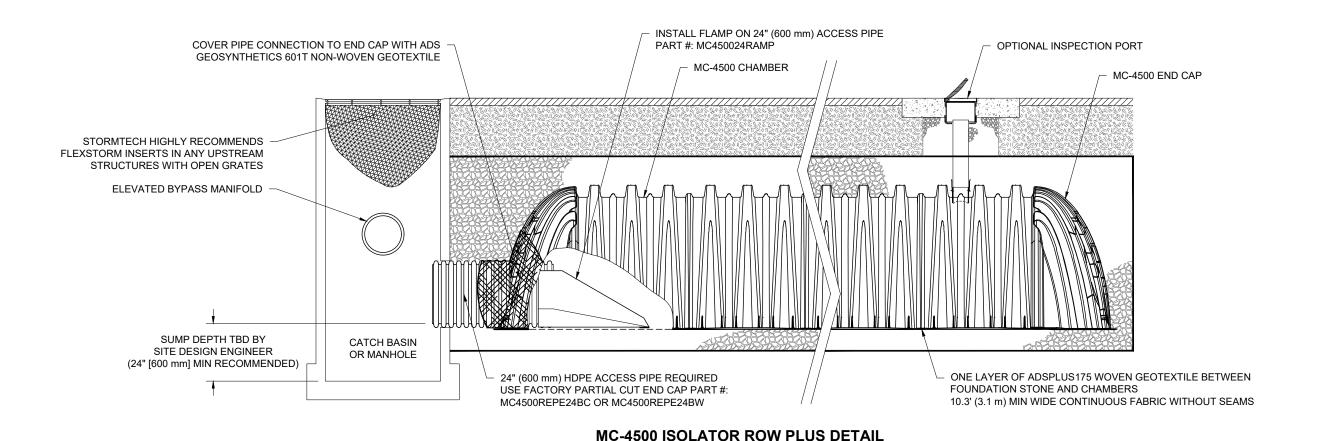
NOTE: ALL DIMENSIONS ARE NOMINAL



38.0

(965 mm)

CUSTOM PRECORED INVERTS ARE AVAILABLE UPON REQUEST. INVENTORIED MANIFOLDS INCLUDE 12-24" (300-600 mm) SIZE ON SIZE AND 15-48" (375-1200 mm) ECCENTRIC MANIFOLDS. CUSTOM INVERT LOCATIONS ON THE MC-4500 END CAP CUT IN THE FIELD ARE NOT RECOMMENDED FOR PIPE SIZES GREATER THAN 10" (250 mm). THE INVERT LOCATION IN COLUMN 'B' ARE THE HIGHEST POSSIBLE FOR THE PIPE SIZE.



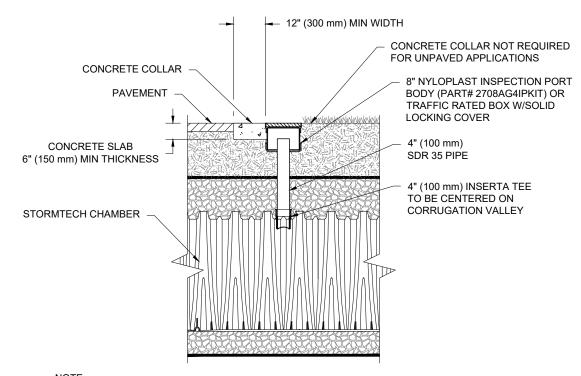
INSPECTION & MAINTENANCE

INSPECT ISOLATOR ROW PLUS FOR SEDIMENT

- A. INSPECTION PORTS (IF PRESENT)
- REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
- REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
- USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG A.3.
- LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3. A 5
- B. ALL ISOLATOR PLUS ROWS
- REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
- USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
- ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



INSPECTION PORTS MAY BE CONNECTED THROUGH ANY CHAMBER CORRUGATION VALLEY.

4" PVC INSPECTION PORT DETAIL (MC SERIES CHAMBER)

SHEET

Storm

4640 TRUEMAN BLVD HILLIARD, OH 43026

ISOLATOR ROW PLUS DETAILS

08/26/20

MC-4500

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CHECKED:

PROJECT

OF





The experts you need to



Contech is the leader in stormwater solutions, helping engineers, contractors and owners with infrastructure and land development projects throughout North America.

With our responsive team of stormwater experts, local regulatory expertise and flexible solutions, Contech is the trusted partner you can count on for stormwater management solutions.

Your Contech Team



STORMWATER CONSULTANT

It's my job to recommend the best solution to meet permitting requirements.



STORMWATER DESIGN ENGINEER

I work with consultants to design the best approved solution to meet your project's needs.



REGULATORY MANAGER

I understand the local stormwater regulations and what solutions will be approved.



SALES ENGINEER

I make sure our solutions meet the needs of the contractor during construction.



Setting new standards in Stormwater Treatment – Jellyfish® Filter

The Jellyfish Filter is a stormwater quality treatment technology featuring high flow pretreatment and membrane filtration in a compact stand-alone system. Jellyfish removes floatables, trash, oil, debris, TSS, fine silt-sized particles, and a high percentage of particulate-bound pollutants; including phosphorus, nitrogen, metals and hydrocarbons. The high surface area membrane cartridges, combined with up-flow hydraulics, frequent, passive backwashing, and rinseable/reusable cartridges ensure long-lasting performance.

The Jellyfish Filter has been tested in the field and laboratory, and has received approval from numerous stormwater regulatory agencies.

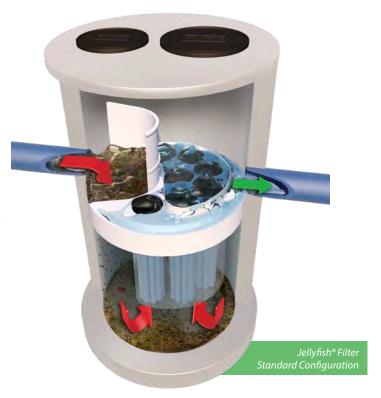
Jellyfish® Filter



How the Jellyfish® Filter Treats Stormwater

Tested in the field and laboratory ...

- Stormwater enters the Jellyfish through the inlet pipe and traps floating pollutants behind the maintenance access wall and below the cartridge deck.
- Water is conveyed below the cartridge deck where a separation skirt around the cartridges isolates oil, trash and debris outside the filtration zone.
- Water is directed to the filtration zone and up through the top of the cartridge where it exits via the outlet pipe.
- The membrane filters provide a very large surface area to effectively remove fine sand and silt-sized particles, and a high percentage of particulate-bound pollutants such as nitrogen, phosphorus, metals, and hydrocarbons while ensuring long-lasting treatment.
- As influent flow subsides, the water in the backwash pool flows back into the lower chamber. This passive backwash extends cartridge life.
- The draindown cartridge(s) located outside the backwash pool enables water levels to balance.



Learn More:

www.ContechES.com/jellyfish









APPLICATION TIPS

- The Peak Diversion Jellyfish provides treatment and highflow bypass in one structure, eliminating the need for a separate bypass structure.
- LID and GI are complemented by filtration solutions, as they help keep sites free from fine sediments that can impede performance, remove unsightly trash, and provide a single point of maintenance.
- Selecting a filter with a long maintenance cycle and low maintenance cost will result in healthy waterways and happy property owners.



The pleated tentacles of the Jellyfish® Filter provide a large surface area for pollutant removal.

POLLUTANT OF CONCERN	% REMOVAL
Total Trash	99%
Total Suspended Solids (TSS)	89%
Total Phosphorus (TP)	59%
Total Nitrogen (TN)	51%
Total Copper (TCu)	> 50%
Total Zinc (TZn)	> 50%



Sources: TARP II Field Study - 2012 JF 4-2-1 Configuration MRDC Floatables Testing – 2008 JF6-6-1 Configuration

Jellyfish® Filter Features and Benefits

FEATURE	BENEFITS
High surface area membrane filtration	Low flux rate promotes cake filtration and slows membrane occlusion
High design treatment flow rate per cartridge (up to 80 gpm (5 L/s))	Compact system with a small footprint, lower construction cost
Low driving head (typically 18 inches or less (457 mm))	Design flexibility, lower construction cost
Lightweight cartridges with passive backwash	Easy maintenance and low life-cycle cost



The Jellyfish Filter can be configured in a manhole, catch basin, or vault.

Select Jellyfish® Filter Certifications and Verifications

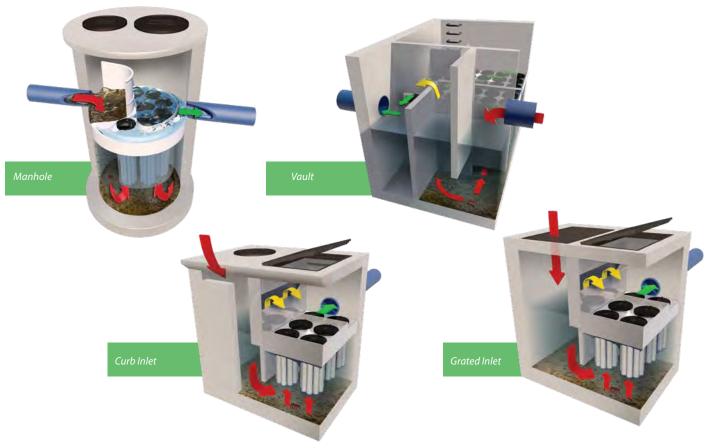
The Jellyfish Filter has been reviewed by numerous state and federal programs, including:

- Washington State Department of Ecology (TAPE) GULD BASIC,
 Phosphorus
- Virginia Department of Environmental Quality (VA DEQ)
- Texas Commission of Environmental Quality (TCEQ)
- Canada ISO 14034 Environmental Management Environmental Technology Verification (ETV)
- Philadelphia Water District (PWD)
- Maryland Department of the Environment (MD DOE)



Multiple system configurations to optimize your site

The Jellyfish Filter can be manufactured in a variety of configurations: manhole, catch basin, vault, fiberglass tank, or custom configurations. Typically, 18 inches (457 mm) of driving head is designed into the system. For low drop sites, the designed driving head can be less.



Jellyfish® Filter Maintenance

- Jellyfish Filter cartridges are light weight and reusable
- Maintenance of the filter cartridges is performed by removing, rinsing and reusing the cartridge tentacles.
- Vacuum extraction of captured pollutants in the sump is recommended at the same time.
- Full cartridge replacement intervals differ by site due to varying pollutant loading and type, and maintenance frequency.

 Replacement is anticipated every 2-5 years.
- Contech® has created a network of Certified Maintenance Providers to provide maintenance on stormwater BMP's.



The Jellyfish® Filter tentacle is light and easy to clean.



A partner









Few companies offer the wide range of highquality stormwater resources you can find with us — state-of-the-art products, decades of expertise, and all the maintenance support you need to operate your system cost-effectively.

THE CONTECH WAY

Contech® Engineered Solutions provides innovative, cost-effective site solutions to engineers, contractors, and developers on projects across North America. Our portfolio includes bridges, drainage, erosion control, retaining wall, sanitary sewer and stormwater management products.

TAKE THE NEXT STEP

For more information: www.ContechES.com

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Appendix E

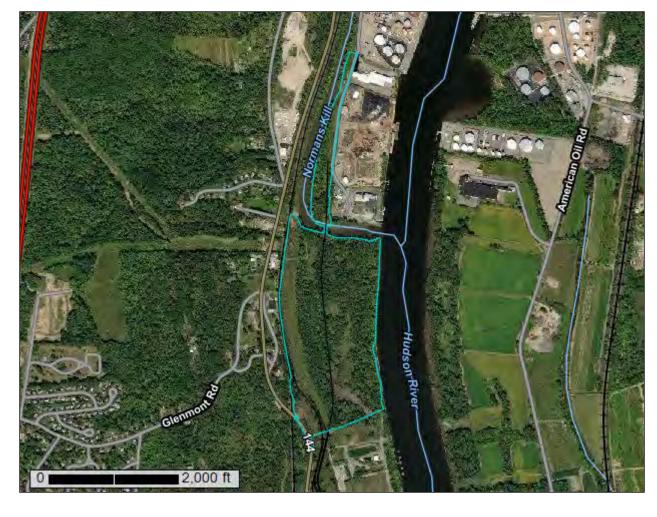
NRCS Soils Report



NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Albany County, New York



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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Albany County, New York	
HuE—Hudson silt loam, 25 to 45 percent slopes	
NrD—Nassau very channery silt loam, hilly, very rocky	
Ug—Udorthents, loamy	15
Ur—Urban land	
W—Water	
Wo—Wayland soils complex, non-calcareous substratum, 0 to 3	
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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

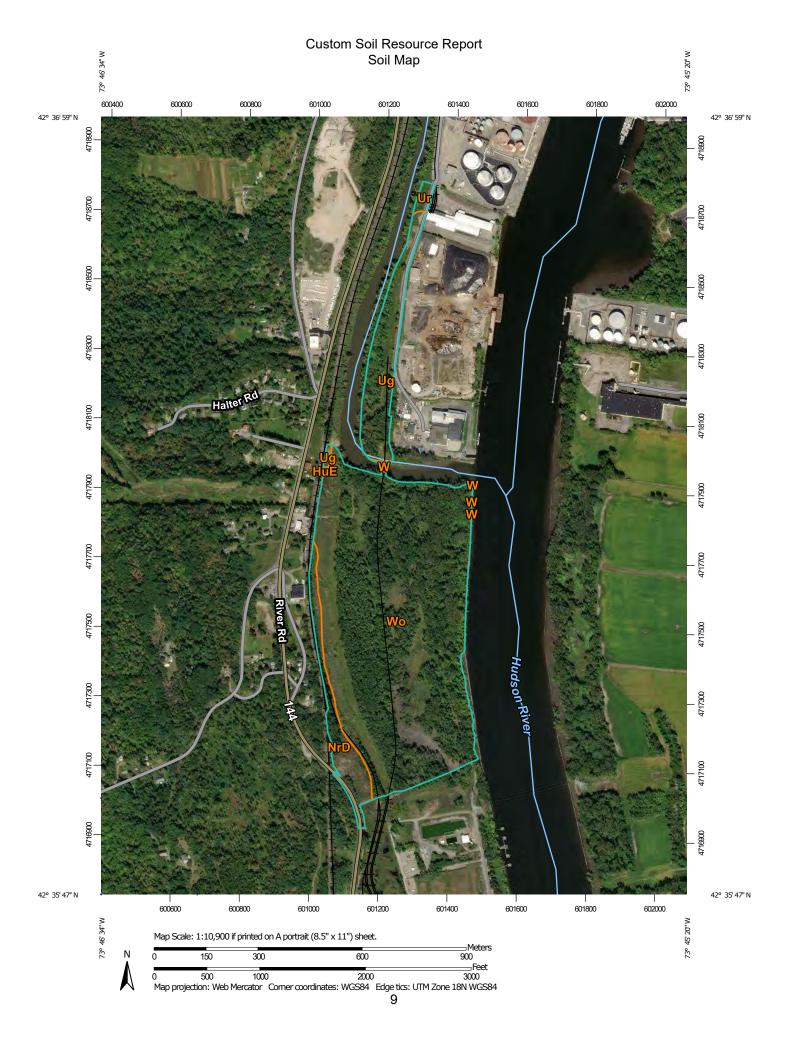
After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

Blowout

_ _

اکا

Borrow Pit

Ж

Clay Spot

 \Diamond

Closed Depression

V

Gravel Pit

...

Gravelly Spot

0

Landfill Lava Flow

٨.

Marsh or swamp

汆

Mine or Quarry

9

Miscellaneous Water
Perennial Water

0

Rock Outcrop

+

Saline Spot

. .

Sandy Spot

Severely Eroded Spot

⇔

Sinkhole

V

Slide or Slip

Ø

Sodic Spot

GEND

8

Spoil Area Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

Water Features

~

Streams and Canals

Transportation

+++

Rails

~

Interstate Highways

US Routes

 \sim

Major Roads

 \sim

Local Roads

Background

100

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15.800.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Albany County, New York Survey Area Data: Version 19, Aug 29, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 1, 2014—Sep 22, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
HuE	Hudson silt loam, 25 to 45 percent slopes	0.1	0.1%
NrD	Nassau very channery silt loam, hilly, very rocky	7.2	6.7%
Ug	Udorthents, loamy	11.6	10.7%
Ur	Urban land	0.8	0.8%
W	Water	0.1	0.1%
Wo	Wayland soils complex, non- calcareous substratum, 0 to 3 percent slopes, frequently flooded	88.7	81.7%
Totals for Area of Interest		108.6	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Albany County, New York

HuE—Hudson silt loam, 25 to 45 percent slopes

Map Unit Setting

National map unit symbol: 9pg8 Elevation: 300 to 1,800 feet

Mean annual precipitation: 36 to 41 inches Mean annual air temperature: 45 to 48 degrees F

Frost-free period: 100 to 170 days

Farmland classification: Not prime farmland

Map Unit Composition

Hudson and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hudson

Setting

Landform: Lake plains

Landform position (two-dimensional): Summit Landform position (three-dimensional): Riser

Down-slope shape: Concave Across-slope shape: Convex

Parent material: Clayey and silty glaciolacustrine deposits

Typical profile

H1 - 0 to 11 inches: silt loam
H2 - 11 to 16 inches: silty clay loam
H3 - 16 to 31 inches: silty clay
H4 - 31 to 60 inches: clay

Properties and qualities

Slope: 25 to 45 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 18 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 15 percent

Available water supply, 0 to 60 inches: High (about 9.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: C/D

Ecological site: F144AY018NY - Moist Lake Plain

Hydric soil rating: No

Minor Components

Unnamed soils

Percent of map unit: 5 percent

Unadilla

Percent of map unit: 5 percent

Hydric soil rating: No

Colonie

Percent of map unit: 3 percent

Hydric soil rating: No

Udifluvents

Percent of map unit: 1 percent

Hydric soil rating: No

Fluvaquents

Percent of map unit: 1 percent Landform: Flood plains

Hydric soil rating: Yes

NrD—Nassau very channery silt loam, hilly, very rocky

Map Unit Setting

National map unit symbol: 9ph1 Elevation: 600 to 1,800 feet

Mean annual precipitation: 36 to 41 inches
Mean annual air temperature: 45 to 48 degrees F

Frost-free period: 100 to 170 days

Farmland classification: Not prime farmland

Map Unit Composition

Nassau, hilly, and similar soils: 70 percent

Minor components: 30 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Nassau, Hilly

Setting

Landform: Benches, ridges, till plains

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Channery loamy till derived mainly from local slate or shale

Typical profile

H1 - 0 to 8 inches: very channery silt loam H2 - 8 to 16 inches: very channery silt loam H3 - 16 to 20 inches: unweathered bedrock

Properties and qualities

Slope: 15 to 25 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

Minor Components

Rock outcrop

Percent of map unit: 9 percent Hydric soil rating: Unranked

Manlius

Percent of map unit: 8 percent

Hydric soil rating: No

Unnamed soils

Percent of map unit: 8 percent

Lordstown

Percent of map unit: 5 percent

Hydric soil rating: No

Ug—Udorthents, loamy

Map Unit Setting

National map unit symbol: 9pj1 Elevation: 0 to 1,640 feet

Mean annual precipitation: 36 to 41 inches
Mean annual air temperature: 45 to 48 degrees F

Frost-free period: 100 to 170 days

Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, loamy, and similar soils: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Loamy

Typical profile

H1 - 0 to 4 inches: loam

H2 - 4 to 70 inches: channery loam

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.06 to 5.95 in/hr)

Depth to water table: About 36 to 72 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 15 percent

Available water supply, 0 to 60 inches: Low (about 5.5 inches)

Minor Components

Unnamed soils

Percent of map unit: 10 percent

Ur-Urban land

Map Unit Setting

National map unit symbol: 9pj8

Mean annual precipitation: 36 to 41 inches Mean annual air temperature: 45 to 48 degrees F

Frost-free period: 100 to 170 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Typical profile

H1 - 0 to 6 inches: variable

Minor Components

Unnamed soils

Percent of map unit: 10 percent

Udorthents

Percent of map unit: 5 percent

Hydric soil rating: No

W-Water

Map Unit Composition

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Wo—Wayland soils complex, non-calcareous substratum, 0 to 3 percent slopes, frequently flooded

Map Unit Setting

National map unit symbol: 2srgt Elevation: 160 to 1,970 feet

Mean annual precipitation: 31 to 70 inches Mean annual air temperature: 43 to 52 degrees F

Frost-free period: 105 to 180 days

Farmland classification: Not prime farmland

Map Unit Composition

Wayland and similar soils: 60 percent

Wayland, very poorly drained, and similar soils: 30 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wayland

Setting

Landform: Flood plains

Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Silty and clayey alluvium derived from interbedded sedimentary

rock

Typical profile

Ap - 0 to 9 inches: silt loam Bg - 9 to 21 inches: silt loam Cg1 - 21 to 28 inches: silt loam Cg2 - 28 to 47 inches: silt loam Cg3 - 47 to 54 inches: silt loam Cg4 - 54 to 60 inches: silt loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: FrequentNone

Frequency of ponding: None

Calcium carbonate, maximum content: 5 percent Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very high (about 13.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D Hydric soil rating: Yes

Description of Wayland, Very Poorly Drained

Setting

Landform: Flood plains

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Silty and clayey alluvium derived from interbedded sedimentary

rock

Typical profile

A - 0 to 9 inches: mucky silt loam Bg - 9 to 21 inches: silt loam Cg1 - 21 to 28 inches: silt loam Cg2 - 28 to 47 inches: silt loam Cg3 - 47 to 54 inches: silt loam Cg4 - 54 to 60 inches: silt loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 inches Frequency of flooding: NoneFrequent Frequency of ponding: Frequent

Calcium carbonate, maximum content: 5 percent Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very high (about 13.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D Hydric soil rating: Yes

Minor Components

Holderton

Percent of map unit: 10 percent

Landform: Flood plains

Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Linear

Hydric soil rating: No

Soil Information for All Uses

Soil Properties and Qualities

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

Hydrologic Soil Group

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

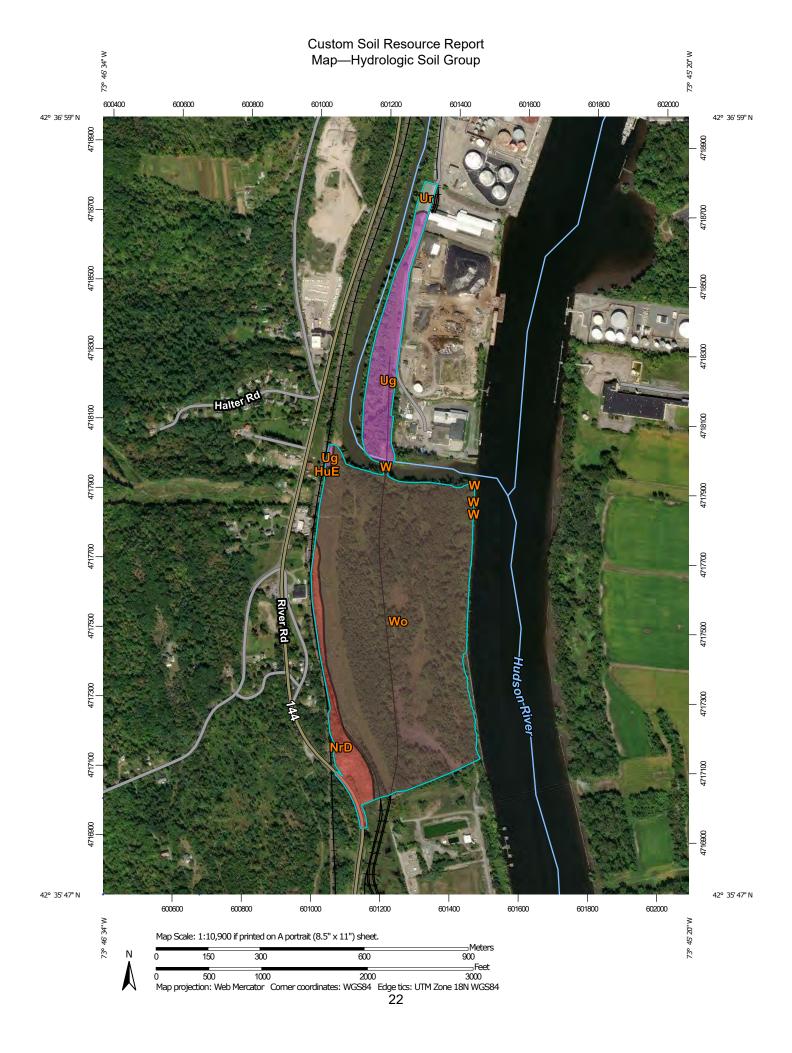
Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



MAP LEGEND MAP INFORMATION Area of Interest (AOI) The soil surveys that comprise your AOI were mapped at С 1:15.800. Area of Interest (AOI) C/D Soils Please rely on the bar scale on each map sheet for map D Soil Rating Polygons measurements. Not rated or not available Α Source of Map: Natural Resources Conservation Service **Water Features** A/D Web Soil Survey URL: Streams and Canals В Coordinate System: Web Mercator (EPSG:3857) Transportation B/D Rails ---Maps from the Web Soil Survey are based on the Web Mercator С projection, which preserves direction and shape but distorts Interstate Highways distance and area. A projection that preserves area, such as the C/D **US Routes** Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. D Major Roads \sim Not rated or not available -Local Roads This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Rating Lines Background Aerial Photography Soil Survey Area: Albany County, New York Survey Area Data: Version 19, Aug 29, 2021 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jul 1, 2014—Sep 22, C/D 2017 The orthophoto or other base map on which the soil lines were Not rated or not available compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor **Soil Rating Points** shifting of map unit boundaries may be evident. Α A/D B/D

Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI	
HuE	Hudson silt loam, 25 to 45 percent slopes	C/D	0.1	0.1%	
NrD	Nassau very channery silt loam, hilly, very rocky	D	7.2	6.7%	
Ug	Udorthents, loamy	A	11.6	10.7%	
Ur	Urban land		0.8	0.8%	
W	Water		0.1	0.1%	
Wo	Wayland soils complex, non-calcareous substratum, 0 to 3 percent slopes, frequently flooded	B/D	88.7	81.7%	
Totals for Area of Interest			108.6	100.0%	

Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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Appendix F

Infiltration Test Results





June 7, 2022

McFarland-Johnson, Inc. 66 Railroad Place – Suite 402 Saratoga Springs, NY 12866

Attn: Mr. Steven Boisvert, P.E.

p: (518) 580-9380 e: sboisvert@mjinc.com

Re: Infiltration Testing

Proposed Marmen Manufacturing Facility

Port of Albany, NY

Terracon Project No. JB215020

Dear Mr. Boisvert:

This report presents the results of the supplemental subsurface investigation and infiltration testing program completed by Terracon at the referenced site.

A total of 21 test borings (IT-1 thru IT-15, along with IT-1A, IT-7A, IT-8A, IT-10A, IT-10B and IT-12A) were completed as part of the investigation, with their locations and depths specified by McFarland-Johnson. Individual subsurface logs for each borehole are attached herewith, along with a subsurface investigation plan(s) indicating their locations.

Infiltration tests were performed adjacent to each of these test borings and were numbered correspondingly. The tests were conducted using 4-inch diameter PVC pipe in general accord with the guidelines in Appendix D of the NYS Stormwater Management Design Manual. Results of this testing are presented for your use on the attached infiltration test data sheets, along with a tabular summary.

We appreciate the opportunity to be of service on this project. Please contact us at your convenience if you have any questions or if anything further is needed.

Respectfully,

Terracon Consultants - NY, Inc.

John S. Hutchison, P.E. Senior Geotechnical Engineer Joseph Robichaud, Jr., P.E. Principal / Office Manager

Attachments: - Subsurface investigation plan(s)

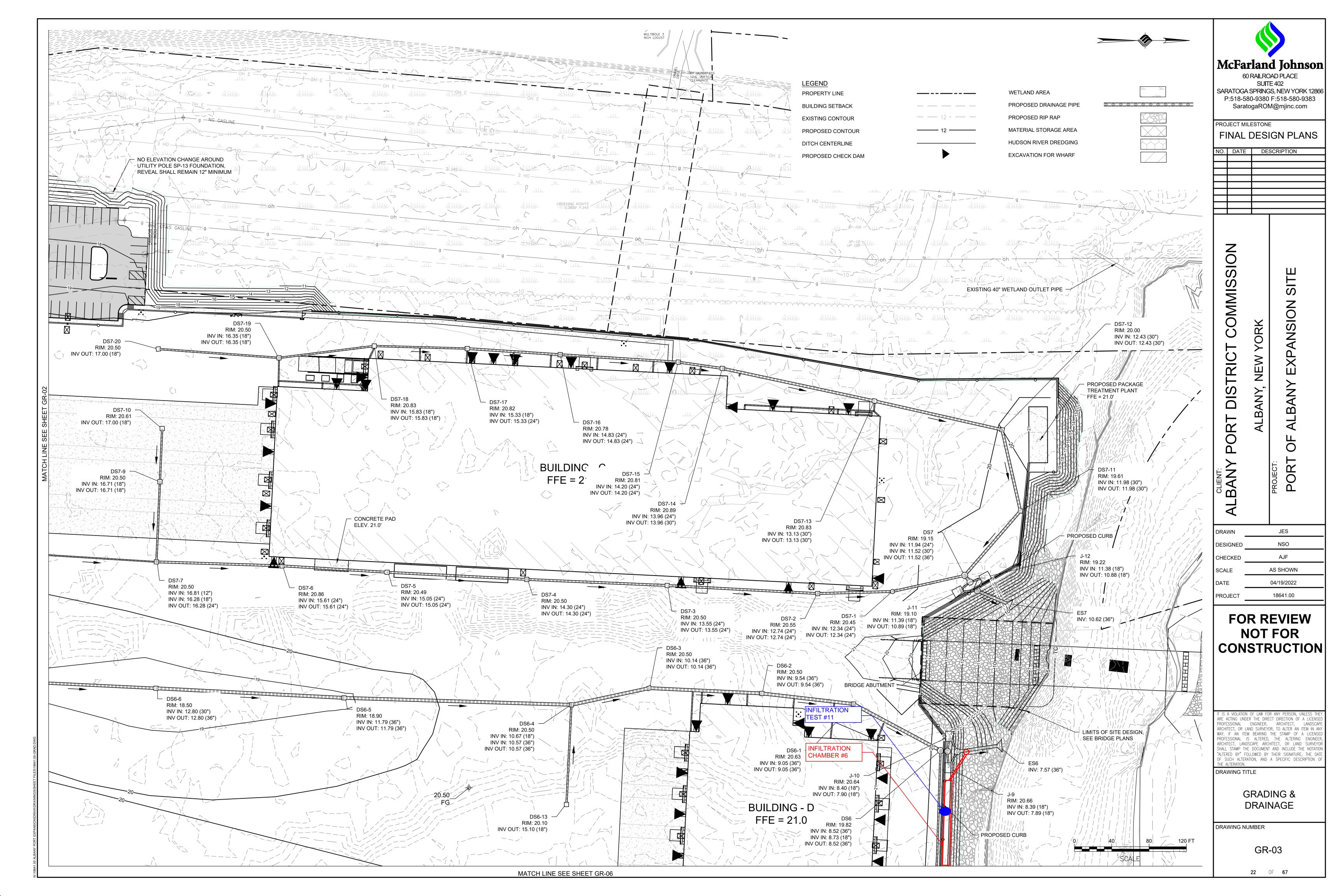
- Test boring logs

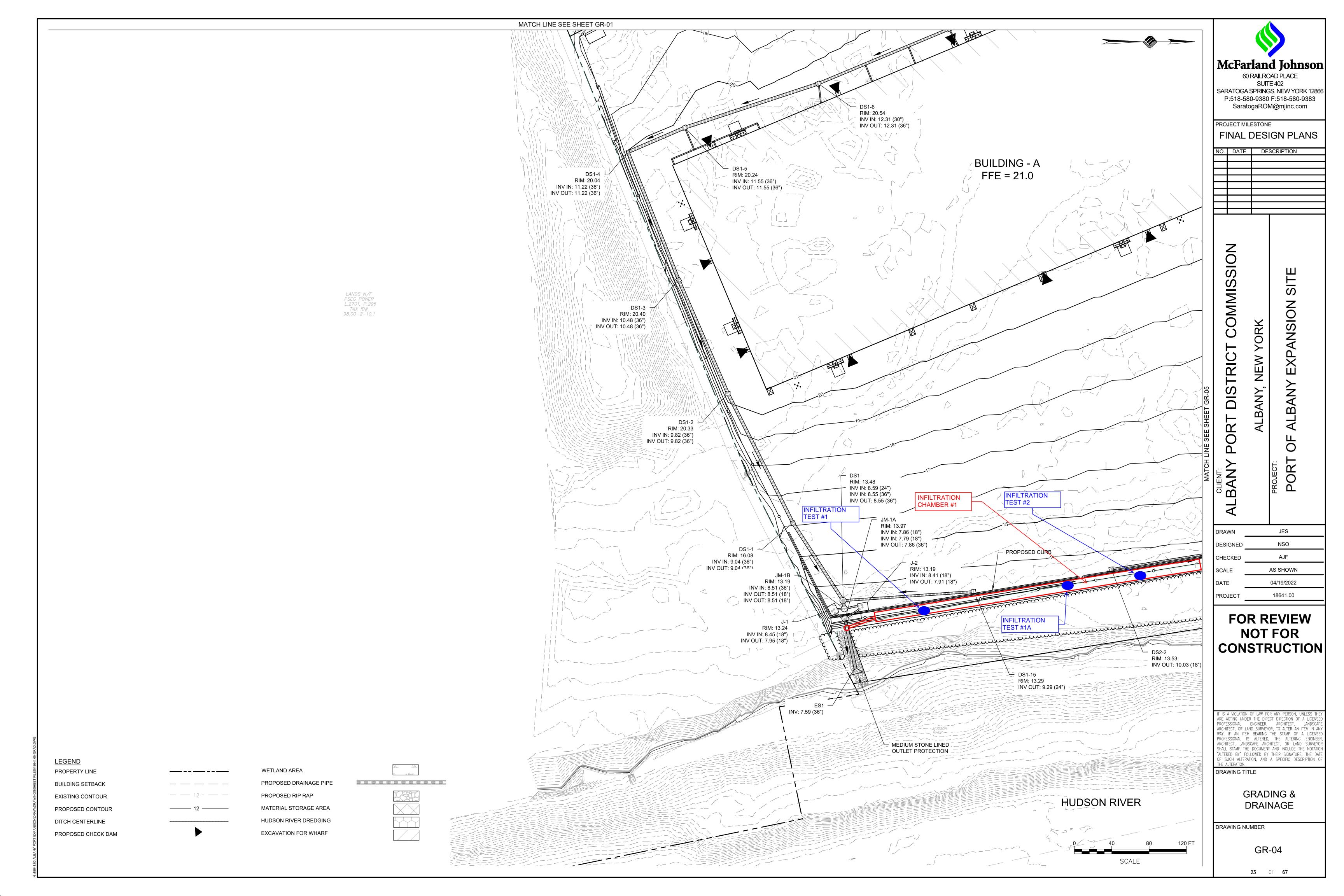
- Infiltration test results summary table

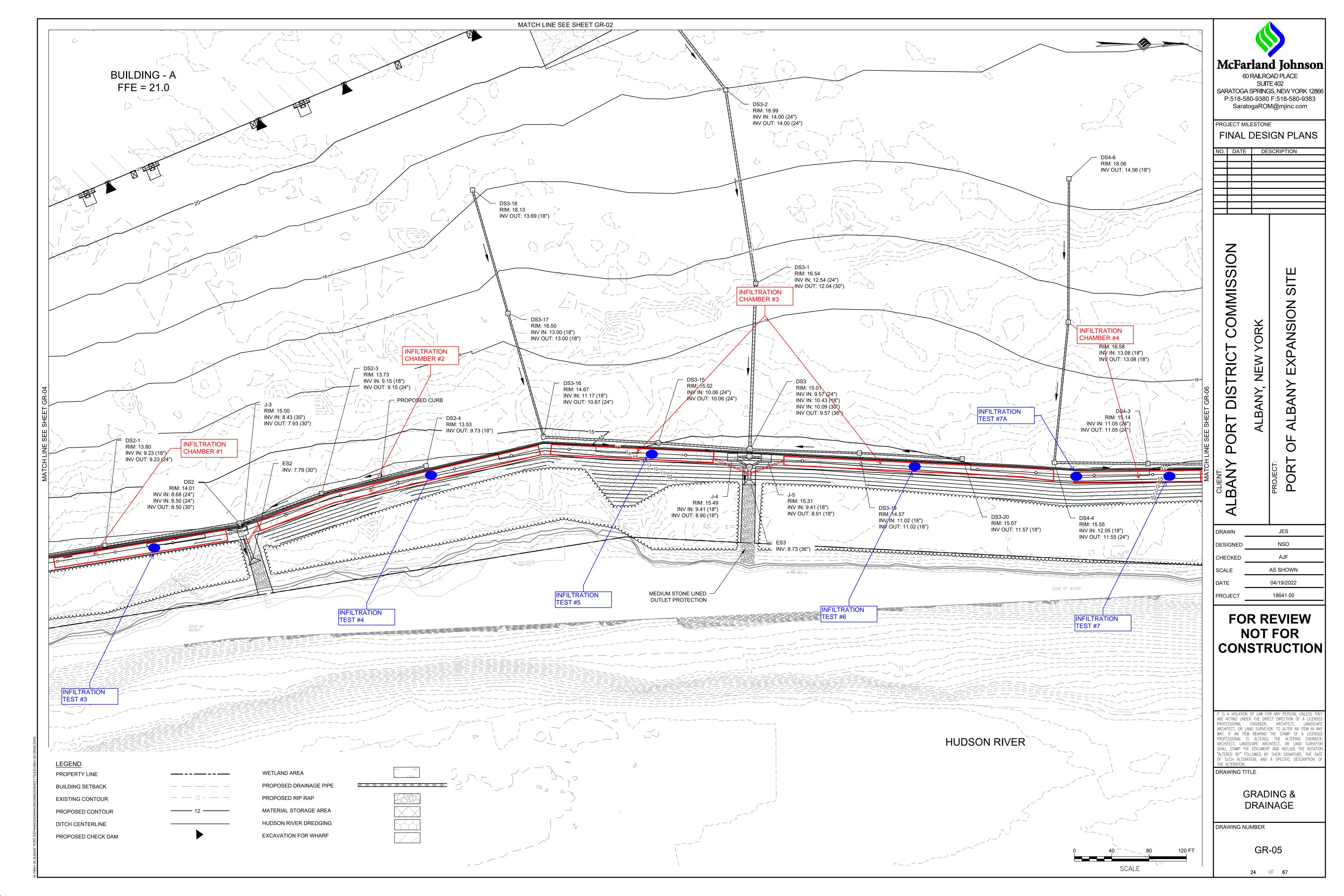
- Infiltration test data sheets

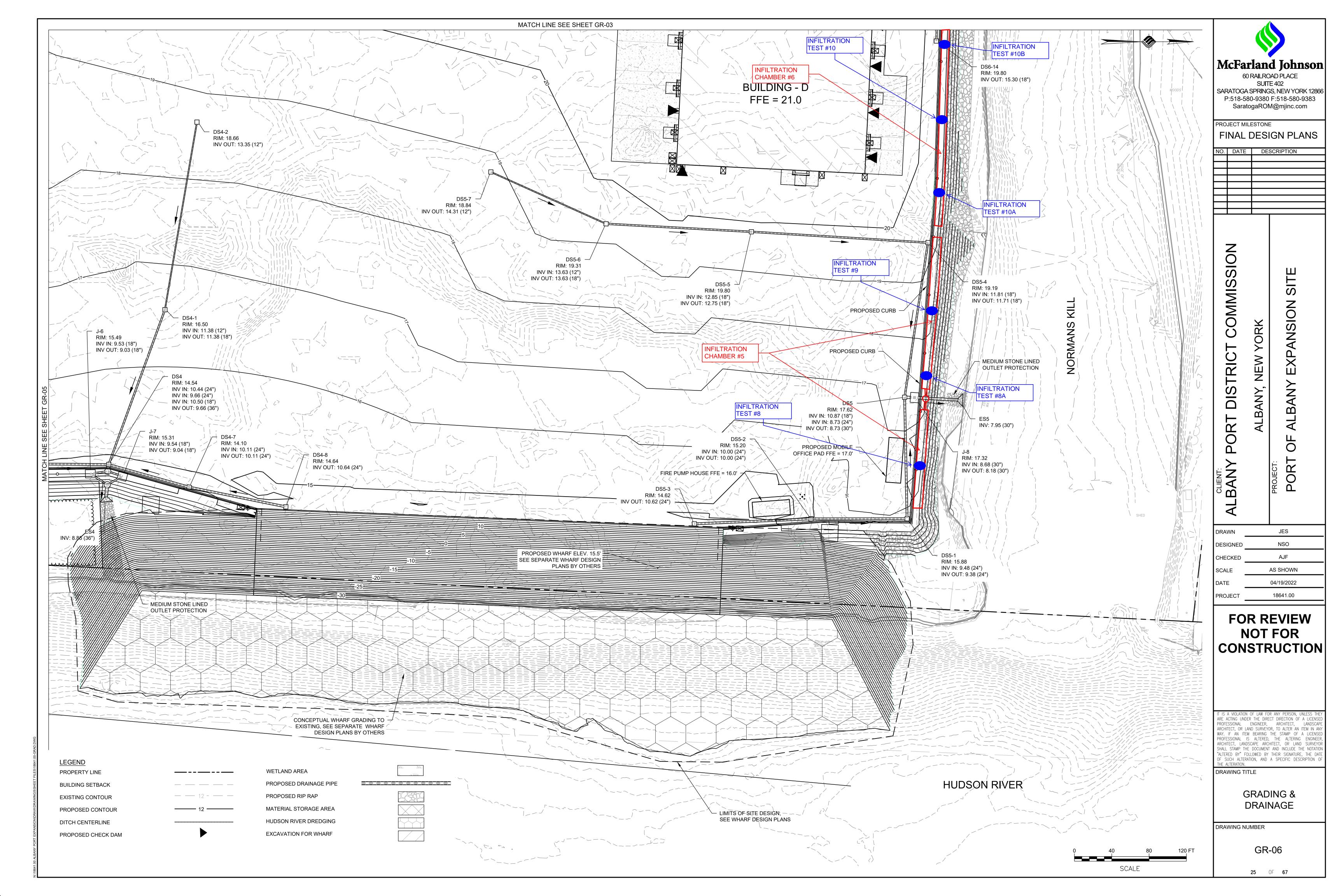
Terracon Consultants – NY, Inc. 30 Corporate Circle, Suite 201 Albany, NY 12203 p (518) 266-0310 f (518) 266-9238 terracon.com

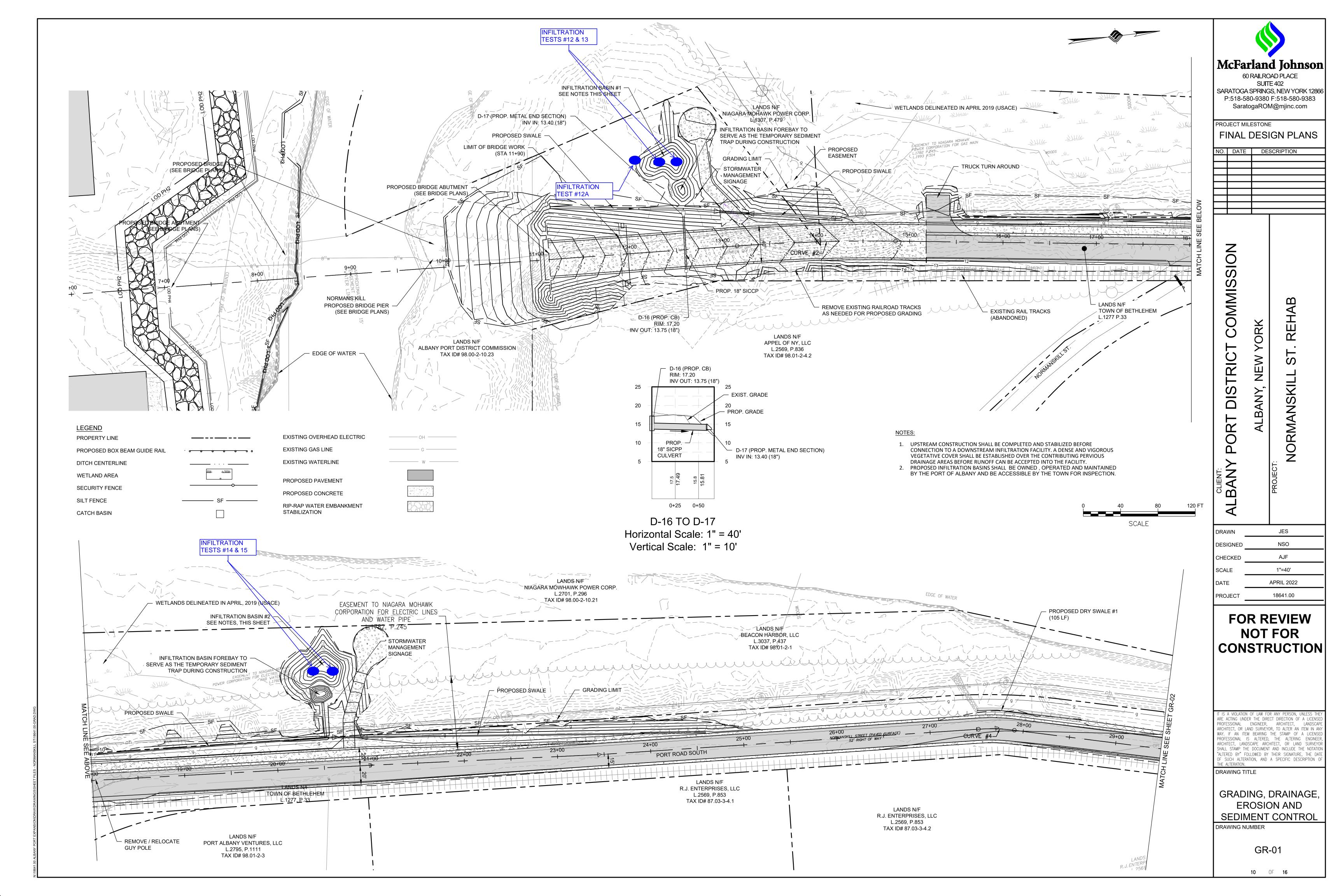
Environmental - Facilities - Geotechnical - Materials











Port of Albany Expansion Site
Infiltration Test Summary Table

			Location	·	EG Elev. *	Test Depth			Results **
Test #	Northing	Easting	Lat	Long	(ft)	(ft)	Test Elev.	Test Date	(in/hr)
IT-1	1373126.03	690476.39	N042° 36' 00.83"	W073° 45' 47.69"	16.6	10.0	6.6	5/12/2022	1.7
IT-1A	1373285.45	690441.73	N042° 36' 02.41"	W073° 45' 48.14"	14.3	8.0	6.3	5/18/2022	1.7
IT-2	1373428.1	690427.42	N042° 36' 03.82"	W073° 45' 48.31"	15.3	9.0	6.3	5/12/2022	0
IT-3	1373669.92	690372.95	N042° 36' 06.21"	W073° 45' 49.01"	10.8	4.5	6.3	5/13/2022	0.2
IT-4	1373828.59	690333.82	N042° 36' 07.78"	W073° 45' 49.51"	12.8	6.5	6.3	5/12/2022	0.2
IT-5	1374016.28	690316.2	N042° 36' 09.64"	W073° 45' 49.73"	9.1	2.5	6.6	5/12/2022	-0.2
IT-6	1374286.56	690329.4	N042° 36' 12.31"	W073° 45' 49.52"	10.7	4.0	6.7	5/13/2022	0
IT-7	1374550.28	690339.68	N042° 36' 14.91"	W073° 45' 49.35"	9.6	3.0	6.6	5/13/2022	1.2
IT-7A	1374449.39	690328.11	N042° 36' 13.92"	W073° 45' 49.52"	11.2	5.0	6.2	5/18/2022	0.5
IT-8	1375558.9	690328.24	N042° 36' 24.88"	W073° 45' 49.39"	12.4	6.0	6.4	5/12/2022	2.6
IT-8A	1375555.8	690230.63	N042° 36' 24.86"	W073° 45' 50.69"	14.8	7.0	7.8	5/18/2022	0.4
IT-9	1375569.02	690181.72	N042° 36' 24.99"	W073° 45' 51.35"	13.6	7.0	6.6	5/13/2022	0.1
IT-10	1375581.89	689989.53	N042° 36' 25.13"	W073° 45' 53.91"	17.3	11.0	6.3	5/13/2022	1.2
IT-10A	1375579.21	690067.6	N042° 36' 25.10"	W073° 45' 52.87"	17.4	11.0	6.4	5/18/2022	0
IT-10B	1375586.34	689908.31	N042° 36' 25.18"	W073° 45' 55.00"	16.7	9.5	7.2	5/18/2022	0
IT-11	1375587.41	689824.53	N042° 36' 25.20"	W073° 45' 56.12"	15.4	9.0	6.4	5/12/2022	0.1
IT-12	1376092.03	689570.93	N042° 36' 30.21"	W073° 45' 59.45"	14.0	6.0	8.0	5/13/2022	0.5
IT-12A	1376065.55	689567.77	N042° 36' 29.95"	W073° 45' 59.50"	12.7	4.0	8.7	5/18/2022	8.6
IT-13	1376115.27	689572.99	N042° 36' 30.44"	W073° 45' 59.42"	14.6	6.5	8.1	5/13/2022	0.1
IT-14	1376905.51	689652.3	N042° 36' 38.24"	W073° 45' 58.27"	5.8	1.0	4.8	5/13/2022	12.4
IT-15	1376922.65	689655.08	N042° 36' 38.41"	W073° 45' 58.23"	5.8	1.0	4.8	5/13/2022	>24

^{*} Note EG elevations may have changed from the tree clearing work.

 $[\]ensuremath{^{**}}$ Represents result of final trial at each location.



INFILTRATION TEST RESULTS							
PROJECT: Proposed Marmen Manufacturing Facility				PROJECT NO.	PROJECT NO. JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: M	lay 12 and 13, 2022			
WEATHER:	M. Sunny 70°-	80° F		TESTER: J. Hu	ıtchison, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)		
		1	0.12	60	1.4		
	10.0	2	0.12	60	1.4		
IT-1		3	0.15	60	1.8		
		4	0.14	60	1.7		
		NOTE: Infiltration rate during final trial run = 1.7 inches per hour					
	9.0	1	0.07	60	0.8		
		2	0.00	60	0.0		
IT-2		3	-	-	-		
		4	-	-	-		
		NOTE: Infiltration rate during final trial run = 0.0 inches per hour					
		1	0.02	60	0.2		
	4.5	2	-	-	-		
IT-3		3	-	-	-		
		4	-	-	-		
Notos		NOTE: Infiltra	tion rate during fir	nal trial run = 0.2 inch	es per hour		

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-1 – Fill (coal ash w/ crushed stone and slag)

Test Location IT-2 – Sandy silt (ML)

Test Location IT-3 - Silt (ML)

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INFILTRATION TEST RESULTS						
PROJECT:	Proposed Marr	PROJECT NO.	PROJECT NO. JB215020			
PROJECT L	PROJECT LOCATION: t/o Bethlehem, NY				lay 12 and 13, 2022	
WEATHER:	M. Sunny 70°-	-80° F		TESTER: J. Hu	ıtchison, et al.	
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)	
		1	0.06	60	0.7	
	6.5	2	0.02	60	0.2	
IT-4		3	-	-	-	
		4	-	-	-	
		NOTE: Infiltration rate during final trial run = 0.2 inches per hour				
	2.5	1	0.02	60	0.8	
		2	-0.02	60	-0.2	
IT-5		3	-	-	-	
		4	-	-	-	
		NOTE: Infiltration rate during final trial run = -0.2 inches per hour				
		1	0.00	60	0.0	
		2	-	-	-	
IT-6	4.0	3	-	-	-	
		4	-	-	-	
Natas		NOTE: Infiltra	tion rate during fir	nal trial run = 0.0 inch	es per hour	

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-4 – Silt and clay (CL-ML)

Test Location IT-5 - Silt (ML)

Test Location IT-6 – Silt w/ sand (ML)

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INFILTRATION TEST RESULTS						
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO. JB215020			
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: M	lay 12 and 13, 2022		
WEATHER:	M. Sunny 70°-	-80° F		TESTER: J. Hu	ıtchison, et al.	
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)	
		1	0.14	60	1.7	
	3.0	2	0.22	60	2.6	
IT-7		3	0.10	60	1.2	
		4	-	-	-	
		NOTE: Infiltration rate during final trial run = 1.2 inches per hour				
	6.0	1	0.29	60	3.5	
		2	0.23	60	2.8	
IT-8		3	0.23	60	2.8	
		4	0.22	60	2.6	
		NOTE: Infiltration rate during final trial run = 2.6 inches per hour				
		1	0.01	60	0.1	
	7.0	2	0.01	60	0.1	
IT-9		3	0.01	60	0.1	
		4	0.01	60	0.1	
Notoo:		NOTE: Infiltra	tion rate during fir	nal trial run = 0.1 inch	es per hour	

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-7 – Silt (ML)

Test Location IT-8 – Silty sand (SM)

Test Location IT-9 – Silt with sand (ML)



INFILTRATION TEST RESULTS						
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO.	PROJECT NO. JB215020		
PROJECT L	OCATION: t/o	Bethlehem, I	NY	TEST DATE: M	lay 12 and 13, 2022	
WEATHER:	M. Sunny 70°-	80° F		TESTER: J. Hu	utchison, et al.	
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)	
		1	0.28	60	3.4	
	11.0	2	0.07	60	0.8	
IT-10		3	0.10	60	1.2	
		4	0.10	60	1.2	
		NOTE: Infiltration rate during final trial run = 1.2 inches per hour				
	9.0	1	0.02	60	0.2	
		2	0.01	60	0.1	
IT-11		3	-	-	-	
		4	-	-	-	
		NOTE: Infiltration rate during final trial run = 0.1 inches per hour				
		1	0.04	60	0.5	
		2	0.02	60	0.2	
IT-12	6.0	3	0.04	60	0.5	
		4	-	-	-	
Notes:		NOTE: Infiltra	tion rate during fir	nal trial run = 0.5 inch	es per hour	

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-10 – Silty clay (CL-ML)

Test Location IT-11 – Silt (ML)

Test Location IT-12 - Fill (sandy silt)



INFILTRATION TEST RESULTS						
PROJECT:	Proposed Marr	PROJECT NO.	JB215020			
PROJECT L	PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: M	lay 12 and 13, 2022	
WEATHER:	M. Sunny 70°-	80° F		TESTER: J. Hu	ıtchison, et al.	
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)	
		1	0.08	60	1.0	
	6.5	2	0.00	60	0.0	
IT-13		3	0.01	60	0.1	
		4	-	-	-	
		NOTE: Infiltration rate during final trial run = 0.1 inches per hour				
	1.0	1	1.93	52	> 24	
		2	1.93	56	> 24	
IT-14		3	1.93	64	21.8	
		4	1.03	60	12.4	
		NOTE: Infiltration rate during final trial run = 12.4 inches per hour				
		1	1.80	4	> 24	
		2	1.80	7	> 24	
IT-15	1.0	3	1.80	7	> 24	
		4	1.80	8	> 24	
Notos:		NOTE: Infiltra	tion rate during fir	nal trial run > 24 inch	es per hour	

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-13 – Sandy silt (ML)

Test Location IT-14 – Sandy silt (ML)

Test Location IT-15 – Silt (ML)

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INFILTRATION TEST RESULTS						
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO.	JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: N	May 18, 2022		
WEATHER:	P. Sunny 68°	F		TESTER: J. La	mm, et al.	
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)	
		1	0.10	60	1.2	
	8.0	2	0.12	60	1.4	
IT-1A		3	0.15	60	1.8	
		4	0.14	60	1.7	
		NOTE: Infiltration rate during final trial run = 1.7 inches per hour				
	5.0	1	0.04	60	0.5	
		2	0.02	60	0.2	
IT-7A		3	0.06	60	0.7	
		4	0.04	60	0.5	
		NOTE: Infiltration rate during final trial run = 0.5 inches per hour				
		1	0.02	60	0.2	
		2	0.02	60	0.2	
IT-8A	7.0	3	0.02	60	0.2	
		4	0.03	60	0.4	
		NOTE: Infiltra	ation rate during fir	nal trial run = 0.4 incl	hes per hour	

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-1A – Fill (coal ash)

Test Location IT-7A – Sandy silt (ML)

Test Location IT-8A – Silty sand (SM)

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	INFILTRATION TEST RESULTS						
PROJECT:	PROJECT: Proposed Marmen Manufacturing Facility				PROJECT NO. JB215020		
PROJECT L	PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: N	lay 18, 2022		
WEATHER:	P. Sunny 68°	F		TESTER: J. La	mm, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)		
		1	0.00	60	0.0		
	11.0	2	0.00	60	0.0		
IT-10A		3	0.00	60	0.0		
		4	-	-	-		
		NOTE: Infiltration rate during final trial run = 0.0 inches per hour					
	9.5	1	0.03	60	0.4		
		2	0.00	60	0.0		
IT-10B		3	0.00	60	0.0		
		4	-	-	-		
		NOTE: Infiltra	tion rate during fir	nal trial run = 0.0 inch	es per hour		
		1	0.52	60	6.2		
		2	0.54	60	6.5		
IT-12A	4.0	3	0.56	60	6.7		
		4	0.72	60	8.6		
		NOTE: Infiltration rate during final trial run = 8.6 inches per hour					

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-10A – Silty clay (CL-ML)

Test Location IT-10B – Sandy silt (ML)

Test Location IT-12A – Silty sand (SM)

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APPENDIX D

MAINTENANCE INSPECTION CHECKLISTS

Stormwater Pond/Wetland Operation, Maintenance and Management Inspection Checklist

Project		
Site Status:	:	
Date:		
Time:		
Inspector:		
1		

Maintenance Item	Satisfactory/ Unsatisfactory	Comments					
Embankment and emergency spillway (Annual, After Major Storms)							
Vegetation and ground cover adequate							
2. Embankment erosion							
3. Animal burrows							
4. Unauthorized planting							
5. Cracking, bulging, or sliding of dam							
a. Upstream face							
b. Downstream face							
c. At or beyond toe							
downstream							
upstream							
d. Emergency spillway							
6.Pond, toe & chimney drains clear and functioning							
7.Seeps/leaks on downstream face							
8. Slope protection or riprap failure							
9. Vertical/horizontal alignment of top of dam "As-Built"							

Maintenance Item	Satisfactory/ Unsatisfactory	Comments
10. Emergency spillway clear of obstructions and debris		
11. Other (specify)		
2. Riser and principal spillway (Annual)		•
Type: Reinforced concrete Corrugated pipe Masonry 1. Low flow orifice obstructed		
Low flow trash rack. a. Debris removal necessary		
b. Corrosion control		
Weir trash rack maintenance a. Debris removal necessary		
b. corrosion control		
4. Excessive sediment accumulation insider riser		
Concrete/masonry condition riser and barrels a. cracks or displacement		
b. Minor spalling (<1")		
c. Major spalling (rebars exposed)		
d. Joint failures		
e. Water tightness		
6. Metal pipe condition		
7. Control valve a. Operational/exercised		
b. Chained and locked		
Pond drain valve a. Operational/exercised		
b. Chained and locked		
9. Outfall channels functioning		
10. Other (specify)		

Maintenance Item	Satisfactory/ Unsatisfactory	Comments
3. Permanent Pool (Wet Ponds) (month	hly)	
Undesirable vegetative growth		
2. Floating or floatable debris removal required		
3. Visible pollution		
4. Shoreline problem		
5. Other (specify)		
4. Sediment Forebays		
1.Sedimentation noted		
2. Sediment cleanout when depth < 50% design depth		
5. Dry Pond Areas		
1. Vegetation adequate		
2. Undesirable vegetative growth		
3. Undesirable woody vegetation		
4. Low flow channels clear of obstructions		
5. Standing water or wet spots		
6. Sediment and / or trash accumulation		
7. Other (specify)		
6. Condition of Outfalls (Annual, After Major Storm	s)	
1. Riprap failures		
2. Slope erosion		
3. Storm drain pipes		
4.Endwalls / Headwalls		
5. Other (specify)		
7. Other (Monthly)		
1. Encroachment on pond, wetland or easement area		

Maintenance Item	Satisfactory/ Unsatisfactory	Comments
2. Complaints from residents		
3.Aesthetics a. Grass growing required		
b. Graffiti removal needed		
c. Other (specify)		
4. Conditions of maintenance access routes.		
5. Signs of hydrocarbon build-up		
6. Any public hazards (specify)		
8. Wetland Vegetation (Annual)		
Vegetation healthy and growing Wetland maintaining 50% surface area coverage of wetland plants after the second growing season. (If unsatisfactory, reinforcement plantings needed)		
Dominant wetland plants: Survival of desired wetland plant species Distribution according to landscaping plan? Evidence of invasive species		
Maintenance of adequate water depths for desired wetland plant species		
5. Harvesting of emergent plantings needed		
Have sediment accumulations reduced pool volume significantly or are plants "choked" with sediment		
7. Eutrophication level of the wetland.		
8. Other (specify)		
Comments:		

Actions to be Taken:			

Project:

Infiltration Trench Operation, Maintenance, and Management Inspection Checklist

Location: Site Status:		
Date:		
Time:		
Inspector:		
Maintenance Item	SATISFACTORY / UNSATISFACTORY	COMMENTS
1. Debris Cleanout (Monthly	<i>y</i>)	
Trench surface clear of debris		
Inflow pipes clear of debris		
Overflow spillway clear of debris		
Inlet area clear of debris		
2. Sediment Traps or Forebays (A	nnual)	
Obviously trapping sediment		
Greater than 50% of storage volume remaining		
3. Dewatering (Monthly)		
Trench dewaters between storms		
4. Sediment Cleanout of Trench	(Annual)	
No evidence of sedimentation in trench		
Sediment accumulation doesn't yet require cleanout		
5. Inlets (Annual)		

Maintenance Item	SATISFACTORY / UNSATISFACTORY	COMMENTS
Good condition		
No evidence of erosion		
6. Outlet/Overflow Spillway (Annua	l)	
Good condition, no need for repair		
No evidence of erosion		
7. Aggregate Repairs (Annual)		
Surface of aggregate clean		
Top layer of stone does not need replacement		
Trench does not need rehabilitation		
Comments:		
Actions to be Taken:		

5. Sediment Deposition

Sand/Organic Filter Operation, Maintenance and Management Inspection Checklist

Project: Location: Site Status:		
Date:		
Time:		
Inspector:		
Maintenance Item	SATISFACTORY / UNSATISFACTORY	COMMENTS
1. Debris Cleanout (Monthly		
Contributing areas clean of debris		
Filtration facility clean of debris		
Inlet and outlets clear of debris		
2. Oil and Grease (Monthly)		
No evidence of filter surface clogging		
Activities in drainage area minimize oil and grease entry		
3. Vegetation (Monthly)		
Contributing drainage area stabilized		
No evidence of erosion		
Area mowed and clipping removed		
4. Water Retention Where Required	(Monthly)	
Water holding chambers at normal pool		
No evidence of leakage		

(Annual)

Maintenance Item	SATISFACTORY / UNSATISFACTORY	COMMENTS
Filter chamber free of sediments		
Sedimentation chamber not more than half full of sediments		
6. Structural Components (Annual)		
No evidence of structural deterioration		
Any grates are in good condition		
No evidence of spalling or cracking of structural parts		
7. Outlet/Overflow Spillway (Annua		
Good condition, no need for repairs		
No evidence of erosion (if draining into a natural channel)		
8. Overall Function of Facility	(Annual)	
Evidence of flow bypassing facility		
No noticeable odors outside of facility		
Comments:		
Actions to be Taken:		

Open Channel Operation, Maintenance, and Management Inspection Checklist

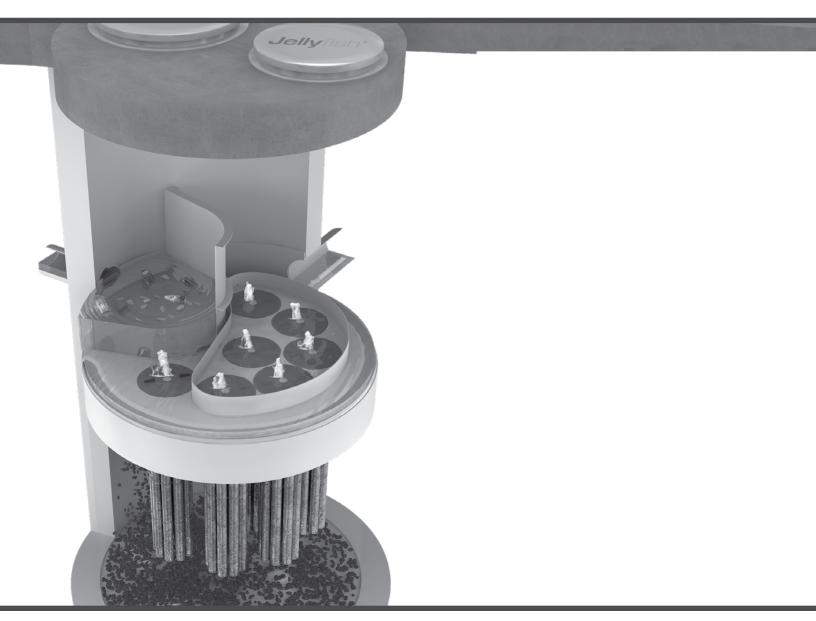
Project: Location: Site Status:			
Date:			
Time:			
Inspector:			

Maintenance Item	SATISFACTORY/ UNSATISFACTORY	COMMENTS
1. Debris Cleanout (Monthly)		
Contributing areas clean of debris		
2. Check Dams or Energy Dissipators	s (Annual, After M	lajor Storms)
No evidence of flow going around structures		
No evidence of erosion at downstream toe		
Soil permeability		
Groundwater / bedrock		
3. Vegetation (Monthly)		
Mowing done when needed		
Minimum mowing depth not exceeded		
No evidence of erosion		
Fertilized per specification		
4. Dewatering (Monthly)		
Dewaters between storms		

	Maintenance Item	SATISFACTORY/ UNSATISFACTORY	COMMENTS
6. Outlet/Overflow Spillway (Annual) Good condition, no need for repairs No evidence of erosion Comments:	5. Sediment deposition (Annual)		
Good condition, no need for repairs No evidence of erosion Comments:	Clean of sediment		
No evidence of erosion Comments:	6. Outlet/Overflow Spillway (Annua	al)	
No evidence of erosion Comments: Actions to be Taken:	Good condition, no need for repairs		
	No evidence of erosion		



Jellyfish® Filter Maintenance Guide





JELLYFISH® FILTER INSPECTION & MAINTENANCE GUIDE

Jellyfish units are often just one of many structures in a more comprehensive stormwater drainage and treatment system.

In order for maintenance of the Jellyfish filter to be successful, it is imperative that all other components be properly maintained. The maintenance and repair of upstream facilities should be carried out prior to Jellyfish maintenance activities.

In addition to considering upstream facilities, it is also important to correct any problems identified in the drainage area. Drainage area concerns may include: erosion problems, heavy oil loading, and discharges of inappropriate materials.

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1.0 Inspection and Maintenance Overview

The primary purpose of the Jellyfish® Filter is to capture and remove pollutants from stormwater runoff. As with any filtration system, these pollutants must be removed to maintain the filter's maximum treatment performance. Regular inspection and maintenance are required to insure proper functioning of the system.

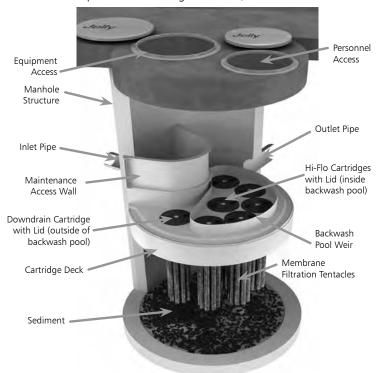
Maintenance frequencies and requirements are site specific and vary depending on pollutant loading. Additional maintenance activities may be required in the event of non-storm event runoff, such as base-flow or seasonal flow, an upstream chemical spill or due to excessive sediment loading from site erosion or extreme runoff events. It is a good practice to inspect the system after major storm events.

Inspection activities are typically conducted from surface observations and include:

- Observe if standing water is present
- Observe if there is any physical damage to the deck or cartridge lids
- Observe the amount of debris in the Maintenance Access Wall (MAW) or inlet bay for vault systems

Maintenance activities include:

- Removal of oil, floatable trash and debris
- Removal of collected sediments
- Rinsing and re-installing the filter cartridges
- Replace filter cartridge tentacles, as needed



Note: Separator Skirt not shown

2.0 Inspection Timing

Inspection of the Jellyfish Filter is key in determining the maintenance requirements for, and to develop a history of, the site's pollutant loading characteristics. In general, inspections should be performed at the times indicated below; or per the approved project stormwater quality documents (if applicable), whichever is more frequent.

- A minimum of quarterly inspections during the first year of operation to assess the sediment and floatable pollutant accumulation, and to ensure proper functioning of the system.
- 2. Inspection frequency in subsequent years is based on the inspection and maintenance plan developed in the first year of operation. Minimum frequency should be once per year.
- 3. Inspection is recommended after each major storm event.
- 4. Inspection is required immediately after an upstream oil, fuel or other chemical spill.

3.0 Inspection Procedure

The following procedure is recommended when performing inspections:

- 1. Provide traffic control measures as necessary.
- 2. Inspect the MAW or inlet bay for floatable pollutants such as trash, debris, and oil sheen.
- Measure oil and sediment depth in several locations, by lowering a sediment probe until contact is made with the floor of the structure. Record sediment depth, and presences of any oil layers.
- 4. Inspect cartridge lids. Missing or damaged cartridge lids to be replaced.
- 5. Inspect the MAW (where appropriate), cartridge deck and receptacles, and backwash pool weir, for damaged or broken components.

3.1 Dry weather inspections

- Inspect the cartridge deck for standing water, and/or sediment on the deck.
- No standing water under normal operating conditions.
- Standing water inside the backwash pool, but not outside the backwash pool indicates, that the filter cartridges need to be rinsed.





Inspection Utilizing Sediment Probe

- Standing water outside the backwash pool is not anticipated and may indicate a backwater condition caused by high water elevation in the receiving water body, or possibly a blockage in downstream infrastructure.
- Any appreciable sediment (≥1/16") accumulated on the deck surface should be removed.

3.2 Wet weather inspections

- Observe the rate and movement of water in the unit.
 Note the depth of water above deck elevation within the MAW or inlet bay.
- Less than 6 inches, flow should be exiting the cartridge lids of each of the draindown cartridges (i.e. cartridges located outside the backwash pool).
- Greater than 6 inches, flow should be exiting the cartridge lids of each of the draindown cartridges and each of the hi-flo cartridges (i.e. cartridges located inside the backwash pool), and water should be overflowing the backwash pool weir.
- 18 inches or greater and relatively little flow is exiting the cartridge lids and outlet pipe, this condition indicates that the filter cartridges need to be rinsed.

4.0 Maintenance Requirements

Required maintenance for the Jellyfish Filter is based upon results of the most recent inspection, historical maintenance records, or the site specific water quality management plan; whichever is more frequent. In general, maintenance requires some combination of the following:

- Sediment removal for depths reaching 12 inches or greater, or within 3 years of the most recent sediment cleaning, whichever occurs sooner.
- 2. Floatable trash, debris, and oil removal.
- 3. Deck cleaned and free from sediment.
- 4. Filter cartridges rinsed and re-installed as required by the most recent inspection results, or within 12 months of the most recent filter rinsing, whichever occurs sooner.
- Replace tentacles if rinsing does not restore adequate hydraulic capacity, remove accumulated sediment, or if damaged or missing. It is recommended that tentacles should remain in service no longer than 5 years before replacement.
- Damaged or missing cartridge deck components must be repaired or replaced as indicated by results of the most recent inspection.
- 7. The unit must be cleaned out and filter cartridges inspected immediately after an upstream oil, fuel, or chemical spill. Filter cartridge tentacles should be replaced if damaged or compromised by the spill.

5.0 Maintenance Procedure

The following procedures are recommended when maintaining the Jellyfish Filter:

- 1. Provide traffic control measures as necessary.
- Open all covers and hatches. Use ventilation equipment as required, according to confined space entry procedures. Caution: Dropping objects onto the cartridge deck may cause damage.

- 3. Perform Inspection Procedure prior to maintenance activity.
- 4. To access the cartridge deck for filter cartridge service, descend into the structure and step directly onto the deck. Caution: Do not step onto the maintenance access wall (MAW) or backwash pool weir, as damage may result. Note that the cartridge deck may be slippery.
- 5. Maximum weight of maintenance crew and equipment on the cartridge deck not to exceed 450 lbs.

5.1 Filter Cartridge Removal

- 1. Remove a cartridge lid.
- Remove cartridges from the deck using the lifting loops in the cartridge head plate. Rope or a lifting device (available from Contech) should be used. Caution: Should a snag occur, do not force the cartridge upward as damage to the tentacles may result. Wet cartridges typically weigh between 100 and 125 lbs.
- 3. Replace and secure the cartridge lid on the exposed empty receptacle as a safety precaution. Contech does not recommend exposing more than one empty cartridge receptacle at a time.

5.2 Filter Cartridge Rinsing

1. Remove all 11 tentacles from the cartridge head plate. Take care not to lose or damage the O-ring seal as well as the plastic threaded nut and connector.



- Position tentacles in a container (or over the MAW), with the threaded connector (open end) facing down, so rinse water is flushed through the membrane and captured in the container.
- 3. Using the Jellyfish rinse tool (available from Contech) or a low-pressure garden hose sprayer, direct water spray onto the tentacle membrane, sweeping from top to bottom along the length of the tentacle. Rinse until all sediment is removed from the membrane. Caution: Do not use a high pressure sprayer or focused stream of water on the membrane. Excessive water pressure may damage the membrane.

- 4. Collected rinse water is typically removed by vacuum hose.
- 5. Reassemble cartridges as detailed later in this document. Reuse O-rings and nuts, ensuring proper placement on each tentacle.

5.3 Sediment and Flotables Extraction

- Perform vacuum cleaning of the Jellyfish Filter only after filter cartridges have been removed from the system. Access the lower chamber for vacuum cleaning only through the maintenance access wall (MAW) opening. Be careful not to damage the flexible plastic separator skirt that is attached to the underside of the deck on manhole systems. Do not lower the vacuum wand through a cartridge receptacle, as damage to the receptacle will result.
- 2. Vacuum floatable trash, debris, and oil, from the MAW opening or inlet bay. Alternatively, floatable solids may be removed by a net or skimmer.



Vacuuming Sump Through MAW

- 3. Pressure wash cartridge deck and receptacles to remove all sediment and debris. Sediment should be rinsed into the sump area. Take care not to flush rinse water into the outlet pipe.
- 4. Remove water from the sump area. Vacuum or pump equipment should only be introduced through the MAW or inlet bay.
- 5. Remove the sediment from the bottom of the unit through the MAW or inlet bay opening.



Vacuuming Sump Through MAW

6. For larger diameter Jellyfish Filter manholes (≥8-ft) and some vaults complete sediment removal may be facilitated by removing a cartridge lid from an empty receptacle and inserting a jetting wand (not a vacuum wand) through the receptacle. Use the sprayer to rinse loosened sediment toward the vacuum hose in the MAW opening, being careful not to damage the receptacle.

5.4 Filter Cartridge Reinstallation and Replacement

- Cartridges should be installed after the deck has been cleaned.
 It is important that the receptacle surfaces be free from grit and debris.
- 2. Remove cartridge lid from deck and carefully lower the filter cartridge into the receptacle until head plate gasket is seated squarely in receptacle. Caution: Do not force the cartridge downward; damage may occur.
- Replace the cartridge lid and check to see that both male threads are properly seated before rotating approximately 1/3 of a full rotation until firmly seated. Use of an approved rim gasket lubricant may facilitate installation. See next page for additional details.
- 4. If rinsing is ineffective in removing sediment from the tentacles, or if tentacles are damaged, provisions must be made to replace the spent or damaged tentacles with new tentacles. Contact Contech to order replacement tentacles.

5.5 Chemical Spills

Caution: If a chemical spill has been captured, do not attempt maintenance. Immediately contact the local hazard response agency and contact Contech.

5.6 Material Disposal

The accumulated sediment found in stormwater treatment and conveyance systems must be handled and disposed of in accordance with regulatory protocols. It is possible for sediments to contain measurable concentrations of heavy metals and organic chemicals (such as pesticides and petroleum products). Areas with the greatest potential for high pollutant loading include industrial areas and heavily traveled roads. Sediments and water must be disposed of in accordance with all applicable waste disposal regulations. When scheduling maintenance, consideration must be made for the disposal of solid and liquid wastes. This typically requires coordination with a local landfill for solid waste disposal. For liquid waste disposal a number of options are available including a municipal vacuum truck decant facility, local waste water treatment plant or on-site treatment and discharge.

Jellyfish Filter Components & Filter Cartridge Assembly and Installation

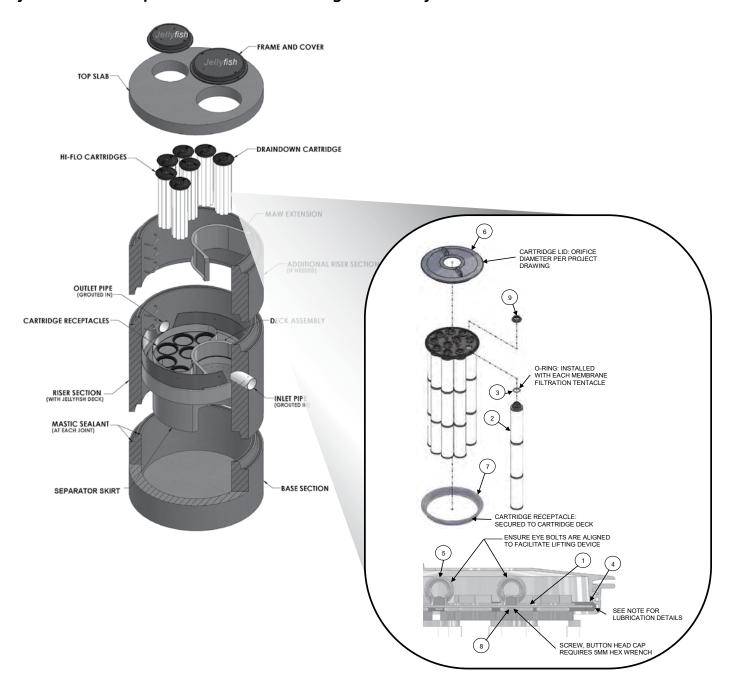


TABLE 1: BOM

-	
ITEM NO.	DESCRIPTION
1	JF HEAD PLATE
2	JF TENTACLE
3	JF O-RING
	JF HEAD PLATE
4	GASKET
5	JF CARTRIDGE EYELET
6	JF 14IN COVER
7	JF RECEPTACLE
	BUTTON HEAD CAP
8	SCREW M6X14MM SS
9	JF CARTRIDGE NUT

TABLE 2: APPROVED GASKET LUBRICANTS

PART NO.	MFR	DESCRIPTION
78713	LA-CO	LUBRI-JOINT
40501	HERCULES	DUCK BUTTER
30600	OATEY	PIPE LUBRICANT
PSLUBXL1Q	PROSELECT	PIPE JOINT LUBRICANT

NOTES:

Head Plate Gasket Installation:

Install Head Plate Gasket (Item 4) onto the Head Plate (Item 1) and liberally apply a lubricant from Table 2: Approved Gasket Lubricants onto the gasket where it contacts the Receptacle (Item 7) and Cartridge Lide (ITem 6). Follow Lubricant manufacturer's instructions.

Lid Assembly:

Rotate Cartridge Lid counter-clockwise until both male threads drop down and properly seat. Then rotate Cartridge Lid clock-wise approximately one-third of a full rotation until Cartridge Lid is firmly secured, creating a watertight seal.

Jellyfish Filter Inspection and Maintenance Log						
Owner:				Jellyfish Model No:		
Location:				GPS Coordinates:		
Land Use:	Commercial:		Industrial:		Service Station:	
Ro	oadway/Highway:		Airport:		Residential:	
Date/Time:						
Inspector:						
Maintenance Contractor:						
Visible Oil Present: (Y/N)						
Oil Quantity Removed:						
Floatable Debris Present: (Y/N)						
Floatable Debris Removed: (Y/N)						
Water Depth in Backwash Pool						
Draindown Cartridges externally rinsed and recommissioned: (Y/N)						
New tentacles put on Draindown Cartridges: (Y/N)						
Hi-Flo Cartridges externally rinsed and recommissioned: (Y/N)						
New tentacles put on Hi-Flo Cartridges: (Y/N)						
Sediment Depth Measured: (Y/N)						
Sediment Depth (inches or mm):						
Sediment Removed: (Y/N)						
Cartridge Lids intact: (Y/N)						
Observed Damage:						
Comments:						
						7





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Support

- Drawings and specifications are available at www.conteches.com/jellyfish.
- Site-specific design support is available from Contech Engineered Solutions.
- Find a Certified Maintenance Provider at www.conteches.com/ccmp

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Isolator® Row Plus

O&M Manual





The Isolator® Row Plus

Introduction

An important component of any Stormwater Pollution Prevention Plan is inspection and maintenance. The StormTech Isolator Row Plus is a technique to inexpensively enhance Total Suspended Solids (TSS) and Total Phosphorus (TP) removal with easy access for inspection and maintenance.

The Isolator Row Plus

The Isolator Row Plus is a row of StormTech chambers, either SC-160, SC-310, SC-310-3, SC-740, DC-780, MC-3500 or MC-7200 models, that is surrounded with filter fabric and connected to a closely located manhole for easy access. The fabric-wrapped chambers provide for sediment settling and filtration as stormwater rises in the Isolator Row Plus and passes through the filter fabric. The open bottom chambers and perforated sidewalls (SC-310, SC- 310-3 and SC-740 models) allow stormwater to flow both vertically and horizontally out of the chambers. Sediments are captured in the Isolator Row Plus protecting the adjacent stone and chambers storage areas from sediment accumulation.

ADS geotextile fabric is placed between the stone and the Isolator Row Plus chambers. The woven geotextile provides a media for stormwater filtration, a durable surface for maintenance, prevents scour of the underlying stone and remains intact during high pressure jetting. A non-woven fabric is placed over the chambers to provide a filter media for flows passing through the chamber's sidewall. The non-woven fabric is not required over the SC-160, DC-780, MC-3500 or MC-7200 models as these chambers do not have perforated side walls.

The Isolator Row Plus is designed to capture the "first flush" runoff and offers the versatility to be sized on a volume basis or a flow-rate basis. An upstream manhole provides access to the Isolator Row Plus and includes a high/low concept such that stormwater flow rates or volumes that exceed the capacity of the Isolator Row Plus bypass through a manifold to the other chambers. This is achieved with an elevated bypass manifold or a high-flow weir. This creates a differential between the Isolator Row Plus row of chambers and the manifold to the rest of the system, thus allowing for settlement time in the Isolator Row Plus. After Stormwater flows through the Isolator Row Plus and into the rest of the chamber system it is either exfiltrated into the soils below or passed at a controlled rate through an outlet manifold and outlet control structure.

The Isolator Row FLAMPTM (patent pending) is a flared end ramp apparatus attached to the inlet pipe on the inside of the chamber end cap. The FLAMP provides a smooth transition from pipe invert to fabric bottom. It is configured to improve chamber function performance by enhancing outflow of solid debris that would otherwise collect at the chamber's end. It also serves to improve the fluid and solid flow into the access pipe during maintenance and cleaning and to guide cleaning and inspection equipment back into the inlet pipe when complete.

The Isolator Row Plus may be part of a treatment train system. The treatment train design and pretreatment device selection by the design engineer is often driven by regulatory requirements. Whether pretreatment is used or not, StormTech recommend using the Isolator Row Plus to minimize maintenance requirements and maintenance costs.

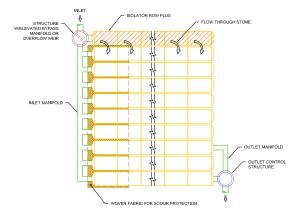
Note: See the StormTech Design Manual for detailed information on designing inlets for a StormTech system, including the Isolator Row Plus.



Looking down the Isolator Row PLUS from the manhole opening, ADS PLUS Fabric is shown between the chamber and stone base.



StormTech Isolator Row PLUS with Overflow Spillway (not to scale)



Isolator Row Plus Inspection/Maintenance

Inspection

The frequency of inspection and maintenance varies by location. A routine inspection schedule needs to be established for each individual location based upon site specific variables. The type of land use (i.e. industrial, commercial, residential), anticipated pollutant load, percent imperviousness, climate, etc. all play a critical role in determining the actual frequency of inspection and maintenance practices.

At a minimum, StormTech recommends annual inspections. Initially, the Isolator Row Plus should be inspected every 6 months for the first year of operation. For subsequent years, the inspection should be adjusted based upon previous observation of sediment deposition.

The Isolator Row Plus incorporates a combination of standard manhole(s) and strategically located inspection ports (as needed). The inspection ports allow for easy access to the system from the surface, eliminating the need to perform a confined space entry for inspection purposes.

If upon visual inspection it is found that sediment has accumulated, a stadia rod should be inserted to determine the depth of sediment. When the average depth of sediment exceeds 3 inches throughout the length of the Isolator Row Plus, clean-out should be performed.

Maintenance

The Isolator Row Plus was designed to reduce the cost of periodic maintenance. By "isolating" sediments to just one row, costs are dramatically reduced by eliminating the need to clean out each row of the entire storage bed. If inspection indicates the potential need for maintenance, access is provided

via a manhole(s) located on the end(s) of the row for cleanout. If entry into the manhole is required, please follow local and OSHA rules for a confined space entries.

Maintenance is accomplished with the JetVac process. The JetVac process utilizes a high pressure water nozzle to propel itself down the Isolator Row Plus while scouring and suspending sediments. As the nozzle is retrieved, the captured pollutants are flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/JetVac combination vehicles. Selection of an appropriate JetVac nozzle will improve maintenance efficiency. Fixed nozzles designed for culverts or large diameter pipe cleaning are preferable. Rear facing jets with an effective spread of at least 45" are best. StormTech recommends a maximum nozzle pressure of 2000 psi be utilized during cleaning. JetVac reels can vary in length. For ease of maintenance, ADS recommends Isolator Row Plus lengths up to 200' (61 m). The JetVac process shall only be performed on StormTech Isolator Row Plus that have ADS Plus Fabric (as specified by StormTech) over their angular base stone.

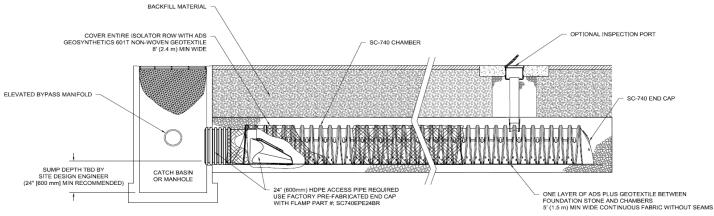






StormTech Isolator Row PLUS (not to scale)

Note: Non-woven fabric is only required over the inlet pipe connection into the end cap for SC-160LP, DC-780, MC-3500 and MC-7200 chamber models and is not required over the entire Isolator Row PLUS.



Isolator Row Plus Step By Step Maintenance Procedures

Step 1

Inspect Isolator Row Plus for sediment.

- A) Inspection ports (if present)
 - i. Remove lid from floor box frame
 - ii. Remove cap from inspection riser
 - iii. Using a flashlight and stadia rod, measure depth of sediment and record results on maintenance log.
 - iv. If sediment is at or above 3 inch depth, proceed to Step 2. If not, proceed to Step 3.
- B) All Isolator Row Plus
 - i. Remove cover from manhole at upstream end of Isolator Row Plus
 - ii. Using a flashlight, inspect down Isolator Row Plus through outlet pipe
 - 1. Mirrors on poles or cameras may be used to avoid a confined space entry
 - 2. Follow OSHA regulations for confined space entry if entering manhole
 - iii. If sediment is at or above the lower row of sidewall holes (approximately 3 inches), proceed to Step 2.

If not, proceed to Step 3.

Step 2

Clean out Isolator Row Plus using the JetVac process.

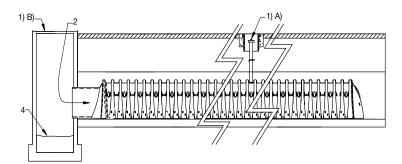
- A) A fixed floor cleaning nozzle with rear facing nozzle spread of 45 inches or more is preferable
- B) Apply multiple passes of JetVac until backflush water is clean
- C) Vacuum manhole sump as required

Step 3

Replace all caps, lids and covers, record observations and actions.

Step 4

Inspect & clean catch basins and manholes upstream of the StormTech system.



Sample Maintenance Log

Date	Stadia Rod Fixed point to chamber bottom (1)	Fixed point to top of sediment (2)	Sedi- ment Depth (1)–(2)	Observations/Actions	Inspector
3/15/11	6.3 ft	none		New installation. Fixed point is CI frame at grade	MCG
9/24/11		6.2	0.1 ft	Some grit felt	SM
6/20/13		5.8	o.s ft	Mucky feel, debris visible in manhole and in Isolator Row PLUS, maintenance due	NV
7/7/13	6.3 ft		0	System jetted and vacuumed	DJM

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Chapter 5: Green Infrastructure Practices

Section 5.1 Planning for Green Infrastructure: Preservation of Natural Features and Conservation Design

5.1.6 Soil Restoration

Description

Soil Restoration is a required practice applied across areas of a development site where soils have been disturbed and will be vegetated in order to recover the original properties and porosity of the soil. Healthy soil is vital to a sustainable environment and landscape. A deep, well drained soil, rich in organic matter, absorbs rainwater, helps prevent flooding and soil erosion, filters out water pollutants, and promotes vigorous plant growth that requires less irrigation, pesticides, and fertilizer.

Soil Restoration is applied in the cleanup, restoration, and landscaping phase of construction followed by the permanent establishment of an appropriate, deep-rooted groundcover to help maintain the restored soil structure. Soil restoration includes mechanical decompaction, compost amendment, or both.

Many runoff reduction practices need Soil Restoration measures applied over and adjacent to the practice to achieve runoff reduction performance. (See typical compacted soil in Figure 5.15). Consult individual profile sheets for specific design criteria.

Key Benefits

- More marketable buildings and landscapes
- Less stormwater runoff, better water quality
- Healthier, aesthetically pleasing landscapes

Figure 5.14 Shows typical compacted soils that nearly reach the bulk density of concrete (Schueler et al 2000)



- Increased porosity on redevelopment sites where impervious cover is converted to pervious
- Achieves performance standards on runoff reduction practices
- Decreases runoff volume generated and lowers the demand on runoff control structures
- Enhances direct groundwater recharge
- Promotes successful long-term revegetation by restoring soil organic matter, permeability, drainage and water holding capacity for healthy root system development of trees, shrubs and deep-rooted ground covers, minimizing lawn chemical requirements, plant drowning during wet periods, and burnout during dry periods

Typical Perceived Obstacles and Realities

Chapter 5: Green Infrastructure Practices

Section 5.1 Planning for Green Infrastructure: Preservation of Natural Features and Conservation Design

- Higher cost due to soil restoration- application of soil de-compaction and enhancement may have additional initial cost; however, they provide benefit in reducing the need for conveyance structures.
- Space constraints and obstruction for use of equipment post construction space may limit the ability of some of the de-compaction equipment, however, alternative equipment and sensible planning help overcome this obstacle.

Discussion

Tilling exposes compacted soil devoid of oxygen to air and recreates temporary air space. In addition, research has shown that the incorporation of organic compost, can greatly improve temporary water storage in the soil and subsequent runoff reduction through infiltration and evapotranspiration.

Soils that have a permanent high water table close to the surface (0-12 inches), either influenced by a clay or other highly impervious layer of material, may have bulk densities so naturally high that compaction has little added impact on infiltration (Lacey 2008). However, these soils will still benefit from the addition of compost. The water holding capacity, penetration, structural stability, and fertility of clay soils were improved with compost mixing (Avnimelech and Cohen 1988).

Table 5.3 describes various soil disturbance activities related to land development, soil types and the requirements for soil restoration for each activity. Soil Restoration or modification of curve numbers is a required practice. Restoration is applied across areas of a development site where soils have been compacted and will be vegetated according to the criteria defined in Table 5.3. If Soil Restoration is not applied according to these criteria, designers are required to:

- a) Increase the calculated WQv by factoring in the compacted areas that have not been kept as impervious cover (including areas of cut or fill, heavy traffic areas on site, or Impervious Cover reduction in redevelopment projects unless aeration or full soil restoration is applied, per Table 5.3).
- b) Change by one level the post-construction hydrologic soil group (HSG) to a less permeable group than the original condition. This is applied to all volumetric and discharge rate control computations.

Chapter 5: Green Infrastructure Practices

Section 5.1 Planning for Green Infrastructure: Preservation of Natural Features and Conservation Design

Table 5.3 Soil Restoration Requirements								
Type of Soil Disturbance	Soil Restora	tion Requirement	Comments/Examples					
No soil disturbance	Restoration not permitted		Preservation of Natural Features					
Minimal soil disturbance	Restoration not required		Clearing and grubbing					
Areas where topsoil is	HSG A &B	HSG C&D	Protect area from any ongoing construction activities.					
stripped only - no change in grade	apply 6 inches of topsoil	Aerate* and apply 6 inches of topsoil						
	HSG A &B	HSG C & D						
Areas of cut or fill	Aerate and apply 6 inches of topsoil	Apply full Soil Restoration **						
Heavy traffic areas on site (especially in a zone 5-25 feet around buildings but not within a 5 foot perimeter around foundation walls)	Apply full Soil Restoration (decompaction and compost enhancement)							
Areas where Runoff Reduction and/or Infiltration practices are applied	Restoration not required, but may be applied to enhance the reduction specified for appropriate practices.		Keep construction equipment from crossing these areas. To protect newly installed practice from any ongoing construction activities construct a single phase operation fence area					
Redevelopment projects	Soil Restoration is required on redevelopment projects in areas where existing impervious area will be converted to pervious area.							

^{*}Aeration includes the use of machines such as tractor-drawn implements with coulters making a narrow slit in the soil, a roller with many spikes making indentations in the soil, or prongs which function like a mini-subsoiler.

Using this Practice

During periods of relatively low to moderate subsoil moisture, the disturbed subsoils are returned to rough grade and the following Soil Restoration steps applied:

1) Apply 3 inches of compost over subsoil

^{**} Per "Deep Ripping and De-compaction, DEC 2008".

Chapter 5: Green Infrastructure Practices

Section 5.1 Planning for Green Infrastructure: Preservation of Natural Features and Conservation Design

- 2) Till compost into subsoil to a depth of at least 12 inches using a cat-mounted ripper, tractor-mounted disc, or tiller, mixing, and circulating air and compost into subsoils
- 3) Rock-pick until uplifted stone/rock materials of four inches and larger size are cleaned off the site
- 4) Apply topsoil to a depth of 6 inches
- 5) Vegetate as required by approved plan.

At the end of the project an inspector should be able to push a 3/8" metal bar 12 inches into the

Figure 5.15 Soil aerator implement

soil just with body weight. Figures 5.16 and 5.17 show two attachments used for soil decompaction. Tilling (step 2 above) should not be performed within the drip line of any existing trees or over utility installations that are within 24 inches of the surface.

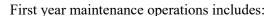
COMPOST SPECIFICATIONS

Compost shall be aged, from plant derived materials, free of viable weed seeds, have no visible free water or dust produced when handling, pass through a half inch screen and have a pH suitable to grow desired plants.

Maintenance

A simple maintenance agreement should identify where Soil Restoration is applied, where newly restored areas are/cannot be cleared, who the responsible parties are to ensure that routine vegetation improvements

are made (i.e., thinning, invasive plant removal, etc.). Soil compost amendments within a filter strip or grass channel should be located in public right of way, or within a dedicated stormwater or drainage easement.



• Initial inspections for the first six months (once after each storm greater than half- inch)



Figure 5.16 Soil aerator implement

- Chapter 5: Green Infrastructure Practices
- Section 5.1 Planning for Green Infrastructure: Preservation of Natural Features and Conservation Design
 - Reseeding to repair bare or eroding areas to assure grass stabilization
 - Water once every three days for first month, and then provide a half inch of water per week during first year. Irrigation plan may be adjusted according to the rain event.
 - Fertilization may be needed in the fall after the first growing season to increase plant vigor
 - Ongoing Maintenance:

Two points help ensure lasting results of decompaction:

- 1) Planting the appropriate ground cover with deep roots to maintain the soil structure
- 2) Keeping the site free of vehicular and foot traffic or other weight loads. Consider pedestrian footpaths. (Sometimes it may be necessary to de-thatch the turf every few years)

References/Further Resources

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APPENDIX E

SPDES PERMIT



NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION

SPDES GENERAL PERMIT FOR STORMWATER DISCHARGES

From

CONSTRUCTION ACTIVITY

Permit No. GP- 0-20-001

Issued Pursuant to Article 17, Titles 7, 8 and Article 70

of the Environmental Conservation Law

Effective Date: January 29, 2020 Expiration Date: January 28, 2025

John J. Ferguson

Chief Permit Administrator

Authorized Signature

Date

Address:

NYS DEC

Division of Environmental Permits

625 Broadway, 4th Floor Albany, N.Y. 12233-1750

PREFACE

Pursuant to Section 402 of the Clean Water Act ("CWA"), stormwater *discharges* from certain *construction activities* are unlawful unless they are authorized by a *National Pollutant Discharge Elimination System* ("NPDES") permit or by a state permit program. New York administers the approved State Pollutant Discharge Elimination System (SPDES) program with permits issued in accordance with the New York State Environmental Conservation Law (ECL) Article 17, Titles 7, 8 and Article 70.

An owner or operator of a construction activity that is eligible for coverage under this permit must obtain coverage prior to the commencement of construction activity. Activities that fit the definition of "construction activity", as defined under 40 CFR 122.26(b)(14)(x), (15)(i), and (15)(ii), constitute construction of a point source and therefore, pursuant to ECL section 17-0505 and 17-0701, the owner or operator must have coverage under a SPDES permit prior to commencing construction activity. The owner or operator cannot wait until there is an actual discharge from the construction site to obtain permit coverage.

*Note: The italicized words/phrases within this permit are defined in Appendix A.

NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION SPDES GENERAL PERMIT FOR STORMWATER DISCHARGES FROM CONSTRUCTION ACTIVITIES

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Part 1. PERMIT COVERAGE AND LIMITATIONS

A. Permit Application

This permit authorizes stormwater *discharges* to *surface waters of the State* from the following *construction activities* identified within 40 CFR Parts 122.26(b)(14)(x), 122.26(b)(15)(i) and 122.26(b)(15)(ii), provided all of the eligibility provisions of this permit are met:

- Construction activities involving soil disturbances of one (1) or more acres; including disturbances of less than one acre that are part of a larger common plan of development or sale that will ultimately disturb one or more acres of land; excluding routine maintenance activity that is performed to maintain the original line and grade, hydraulic capacity or original purpose of a facility;
- Construction activities involving soil disturbances of less than one (1) acre
 where the Department has determined that a SPDES permit is required for
 stormwater discharges based on the potential for contribution to a violation of a
 water quality standard or for significant contribution of pollutants to surface
 waters of the State.
- 3. Construction activities located in the watershed(s) identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.

B. Effluent Limitations Applicable to Discharges from Construction Activities

Discharges authorized by this permit must achieve, at a minimum, the effluent limitations in Part I.B.1. (a) - (f) of this permit. These limitations represent the degree of effluent reduction attainable by the application of best practicable technology currently available.

1. Erosion and Sediment Control Requirements - The *owner or operator* must select, design, install, implement and maintain control measures to *minimize* the *discharge* of *pollutants* and prevent a violation of the *water quality standards*. The selection, design, installation, implementation, and maintenance of these control measures must meet the non-numeric effluent limitations in Part I.B.1.(a) – (f) of this permit and be in accordance with the New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016, using sound engineering judgment. Where control measures are not designed in conformance with the design criteria included in the technical standard, the *owner or operator* must include in the *Stormwater Pollution Prevention Plan* ("SWPPP") the reason(s) for the

deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.

- a. **Erosion and Sediment Controls.** Design, install and maintain effective erosion and sediment controls to *minimize* the *discharge* of *pollutants* and prevent a violation of the *water quality standards*. At a minimum, such controls must be designed, installed and maintained to:
 - (i) *Minimize* soil erosion through application of runoff control and soil stabilization control measure to *minimize pollutant discharges*;
 - (ii) Control stormwater *discharges*, including both peak flowrates and total stormwater volume, to *minimize* channel and *streambank* erosion and scour in the immediate vicinity of the *discharge* points;
 - (iii) Minimize the amount of soil exposed during construction activity;
 - (iv) Minimize the disturbance of steep slopes;
 - (v) Minimize sediment discharges from the site;
 - (vi) Provide and maintain *natural buffer*s around surface waters, direct stormwater to vegetated areas and maximize stormwater infiltration to reduce *pollutant discharges*, unless *infeasible*;
 - (vii) Minimize soil compaction. Minimizing soil compaction is not required where the intended function of a specific area of the site dictates that it be compacted;
 - (viii) Unless *infeasible*, preserve a sufficient amount of topsoil to complete soil restoration and establish a uniform, dense vegetative cover; and
 - (ix) *Minimize* dust. On areas of exposed soil, *minimize* dust through the appropriate application of water or other dust suppression techniques to control the generation of pollutants that could be discharged from the site.
- b. **Soil Stabilization**. In areas where soil disturbance activity has temporarily or permanently ceased, the application of soil stabilization measures must be initiated by the end of the next business day and completed within fourteen (14) days from the date the current soil disturbance activity ceased. For construction sites that *directly discharge* to one of the 303(d) segments

listed in Appendix E or is located in one of the watersheds listed in Appendix C, the application of soil stabilization measures must be initiated by the end of the next business day and completed within seven (7) days from the date the current soil disturbance activity ceased. See Appendix A for definition of *Temporarily Ceased*.

- c. **Dewatering**. *Discharges* from *dewatering* activities, including *discharges* from *dewatering* of trenches and excavations, must be managed by appropriate control measures.
- d. Pollution Prevention Measures. Design, install, implement, and maintain effective pollution prevention measures to *minimize* the *discharge* of pollutants and prevent a violation of the water quality standards. At a minimum, such measures must be designed, installed, implemented and maintained to:
 - (i) Minimize the discharge of pollutants from equipment and vehicle washing, wheel wash water, and other wash waters. This applies to washing operations that use clean water only. Soaps, detergents and solvents cannot be used:
 - (ii) Minimize the exposure of building materials, building products, construction wastes, trash, landscape materials, fertilizers, pesticides, herbicides, detergents, sanitary waste, hazardous and toxic waste, and other materials present on the site to precipitation and to stormwater. Minimization of exposure is not required in cases where the exposure to precipitation and to stormwater will not result in a discharge of pollutants, or where exposure of a specific material or product poses little risk of stormwater contamination (such as final products and materials intended for outdoor use); and
 - (iii) Prevent the *discharge* of *pollutants* from spills and leaks and implement chemical spill and leak prevention and response procedures.
- e. **Prohibited** *Discharges*. The following *discharges* are prohibited:
 - (i) Wastewater from washout of concrete;
 - (ii) Wastewater from washout and cleanout of stucco, paint, form release oils, curing compounds and other construction materials;

- (iii) Fuels, oils, or other *pollutants* used in vehicle and equipment operation and maintenance;
- (iv) Soaps or solvents used in vehicle and equipment washing; and
- (v) Toxic or hazardous substances from a spill or other release.
- f. Surface Outlets. When discharging from basins and impoundments, the outlets shall be designed, constructed and maintained in such a manner that sediment does not leave the basin or impoundment and that erosion at or below the outlet does not occur.

C. Post-construction Stormwater Management Practice Requirements

- 1. The owner or operator of a construction activity that requires post-construction stormwater management practices pursuant to Part III.C. of this permit must select, design, install, and maintain the practices to meet the performance criteria in the New York State Stormwater Management Design Manual ("Design Manual"), dated January 2015, using sound engineering judgment. Where post-construction stormwater management practices ("SMPs") are not designed in conformance with the performance criteria in the Design Manual, the owner or operator must include in the SWPPP the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is equivalent to the technical standard.
- 2. The *owner or operator* of a *construction activity* that requires post-construction stormwater management practices pursuant to Part III.C. of this permit must design the practices to meet the applicable *sizing criteria* in Part I.C.2.a., b., c. or d. of this permit.

a. Sizing Criteria for New Development

- (i) Runoff Reduction Volume ("RRv"): Reduce the total Water Quality Volume ("WQv") by application of RR techniques and standard SMPs with RRv capacity. The total WQv shall be calculated in accordance with the criteria in Section 4.2 of the Design Manual.
- (ii) Minimum RRv and Treatment of Remaining Total WQv: Construction activities that cannot meet the criteria in Part I.C.2.a.(i) of this permit due to site limitations shall direct runoff from all newly constructed impervious areas to a RR technique or standard SMP with RRv capacity unless infeasible. The specific site limitations that prevent the reduction of 100% of the WQv shall be documented in the SWPPP.

For each impervious area that is not directed to a RR technique or standard SMP with RRv capacity, the SWPPP must include documentation which demonstrates that all options were considered and for each option explains why it is considered infeasible.

In no case shall the runoff reduction achieved from the newly constructed impervious areas be less than the Minimum RRv as calculated using the criteria in Section 4.3 of the Design Manual. The remaining portion of the total WQv that cannot be reduced shall be treated by application of standard SMPs.

- (iii) Channel Protection Volume ("Cpv"): Provide 24 hour extended detention of the post-developed 1-year, 24-hour storm event; remaining after runoff reduction. The Cpv requirement does not apply when:
 - (1) Reduction of the entire Cpv is achieved by application of runoff reduction techniques or infiltration systems, or
 - (2) The site discharges directly to tidal waters, or fifth order or larger streams.
- (iv) Overbank Flood Control Criteria ("Qp"): Requires storage to attenuate the post-development 10-year, 24-hour peak discharge rate (Qp) to predevelopment rates. The Qp requirement does not apply when:
 - (1) the site discharges directly to tidal waters or fifth order or larger streams, or
 - (2) A downstream analysis reveals that *overbank* control is not required.
- (v) Extreme Flood Control Criteria ("Qf"): Requires storage to attenuate the post-development 100-year, 24-hour peak discharge rate (Qf) to predevelopment rates. The Qf requirement does not apply when:
 - (1) the site discharges directly to tidal waters or fifth order or larger streams, or
 - (2) A downstream analysis reveals that *overbank* control is not required.

b. Sizing Criteria for New Development in Enhanced Phosphorus Removal Watershed

(i) Runoff Reduction Volume (RRv): Reduce the total Water Quality Volume (WQv) by application of RR techniques and standard SMPs with RRv capacity. The total WQv is the runoff volume from the 1-year, 24 hour design storm over the post-developed watershed and shall be

calculated in accordance with the criteria in Section 10.3 of the Design Manual.

(ii) Minimum RRv and Treatment of Remaining Total WQv: Construction activities that cannot meet the criteria in Part I.C.2.b.(i) of this permit due to site limitations shall direct runoff from all newly constructed impervious areas to a RR technique or standard SMP with RRv capacity unless infeasible. The specific site limitations that prevent the reduction of 100% of the WQv shall be documented in the SWPPP. For each impervious area that is not directed to a RR technique or standard SMP with RRv capacity, the SWPPP must include documentation which demonstrates that all options were considered and for each option explains why it is considered infeasible.

In no case shall the runoff reduction achieved from the newly constructed *impervious areas* be less than the Minimum RRv as calculated using the criteria in Section 10.3 of the Design Manual. The remaining portion of the total WQv that cannot be reduced shall be treated by application of standard SMPs.

- (iii) Channel Protection Volume (Cpv): Provide 24 hour extended detention of the post-developed 1-year, 24-hour storm event; remaining after runoff reduction. The Cpv requirement does not apply when:
 - (1) Reduction of the entire Cpv is achieved by application of runoff reduction techniques or infiltration systems, or
 - (2) The site *discharge*s directly to tidal waters, or fifth order or larger streams.
- (iv) Overbank Flood Control Criteria (Qp): Requires storage to attenuate the post-development 10-year, 24-hour peak discharge rate (Qp) to predevelopment rates. The Qp requirement does not apply when:
 - (1) the site *discharge*s directly to tidal waters or fifth order or larger streams, or
 - (2) A downstream analysis reveals that *overbank* control is not required.
- (v) Extreme Flood Control Criteria (Qf): Requires storage to attenuate the post-development 100-year, 24-hour peak *discharge* rate (Qf) to predevelopment rates. The Qf requirement does not apply when:
 - (1) the site *discharge*s directly to tidal waters or fifth order or larger streams, or
 - (2) A downstream analysis reveals that *overbank* control is not required.

c. Sizing Criteria for Redevelopment Activity

- (i) Water Quality Volume (WQv): The WQv treatment objective for redevelopment activity shall be addressed by one of the following options. Redevelopment activities located in an Enhanced Phosphorus Removal Watershed (see Part III.B.3. and Appendix C of this permit) shall calculate the WQv in accordance with Section 10.3 of the Design Manual. All other redevelopment activities shall calculate the WQv in accordance with Section 4.2 of the Design Manual.
 - (1) Reduce the existing *impervious cover* by a minimum of 25% of the total disturbed, *impervious area*. The Soil Restoration criteria in Section 5.1.6 of the Design Manual must be applied to all newly created pervious areas, or
 - (2) Capture and treat a minimum of 25% of the WQv from the disturbed, *impervious area* by the application of standard SMPs; or reduce 25% of the WQv from the disturbed, *impervious area* by the application of RR techniques or standard SMPs with RRv capacity., or
 - (3) Capture and treat a minimum of 75% of the WQv from the disturbed, *impervious area* as well as any additional runoff from tributary areas by application of the alternative practices discussed in Sections 9.3 and 9.4 of the Design Manual., or
 - (4) Application of a combination of 1, 2 and 3 above that provide a weighted average of at least two of the above methods. Application of this method shall be in accordance with the criteria in Section 9.2.1(B) (IV) of the Design Manual.

If there is an existing post-construction stormwater management practice located on the site that captures and treats runoff from the *impervious area* that is being disturbed, the WQv treatment option selected must, at a minimum, provide treatment equal to the treatment that was being provided by the existing practice(s) if that treatment is greater than the treatment required by options 1-4 above.

- (ii) Channel Protection Volume (Cpv): Not required if there are no changes to hydrology that increase the discharge rate from the project site.
- (iii) Overbank Flood Control Criteria (Qp): Not required if there are no changes to hydrology that increase the discharge rate from the project site.
- (iv) Extreme Flood Control Criteria (Qf): Not required if there are no changes to hydrology that increase the *discharge* rate from the project site

d. Sizing Criteria for Combination of Redevelopment Activity and New Development

Construction projects that include both New Development and Redevelopment Activity shall provide post-construction stormwater management controls that meet the sizing criteria calculated as an aggregate of the Sizing Criteria in Part I.C.2.a. or b. of this permit for the New Development portion of the project and Part I.C.2.c of this permit for Redevelopment Activity portion of the project.

D. Maintaining Water Quality

The Department expects that compliance with the conditions of this permit will control discharges necessary to meet applicable water quality standards. It shall be a violation of the ECL for any discharge to either cause or contribute to a violation of water quality standards as contained in Parts 700 through 705 of Title 6 of the Official Compilation of Codes, Rules and Regulations of the State of New York, such as:

- 1. There shall be no increase in turbidity that will cause a substantial visible contrast to natural conditions:
- 2. There shall be no increase in suspended, colloidal or settleable solids that will cause deposition or impair the waters for their best usages; and
- 3. There shall be no residue from oil and floating substances, nor visible oil film, nor globules of grease.

If there is evidence indicating that the stormwater *discharges* authorized by this permit are causing, have the reasonable potential to cause, or are contributing to a violation of the *water quality standards*; the *owner or operator* must take appropriate corrective action in accordance with Part IV.C.5. of this general permit and document in accordance with Part IV.C.4. of this general permit. To address the *water quality standard* violation the *owner or operator* may need to provide additional information, include and implement appropriate controls in the SWPPP to correct the problem, or obtain an individual SPDES permit.

If there is evidence indicating that despite compliance with the terms and conditions of this general permit it is demonstrated that the stormwater *discharges* authorized by this permit are causing or contributing to a violation of *water quality standards*, or if the Department determines that a modification of the permit is necessary to prevent a violation of *water quality standards*, the authorized *discharges* will no longer be eligible for coverage under this permit. The Department may require the *owner or operator* to obtain an individual SPDES permit to continue discharging.

E. Eligibility Under This General Permit

- 1. This permit may authorize all *discharges* of stormwater from *construction* activity to surface waters of the State and groundwaters except for ineligible discharges identified under subparagraph F. of this Part.
- 2. Except for non-stormwater *discharges* explicitly listed in the next paragraph, this permit only authorizes stormwater *discharges*; including stormwater runoff, snowmelt runoff, and surface runoff and drainage, from *construction activities*.
- 3. Notwithstanding paragraphs E.1 and E.2 above, the following non-stormwater discharges are authorized by this permit: those listed in 6 NYCRR 750-1.2(a)(29)(vi), with the following exception: "Discharges from firefighting activities are authorized only when the firefighting activities are emergencies/unplanned"; waters to which other components have not been added that are used to control dust in accordance with the SWPPP; and uncontaminated discharges from construction site de-watering operations. All non-stormwater discharges must be identified in the SWPPP. Under all circumstances, the owner or operator must still comply with water quality standards in Part I.D of this permit.
- 4. The *owner or operator* must maintain permit eligibility to *discharge* under this permit. Any *discharges* that are not compliant with the eligibility conditions of this permit are not authorized by the permit and the *owner or operator* must either apply for a separate permit to cover those ineligible *discharges* or take steps necessary to make the *discharge* eligible for coverage.

F. Activities Which Are Ineligible for Coverage Under This General Permit

All of the following are **not** authorized by this permit:

- 1. *Discharge*s after *construction activities* have been completed and the site has undergone *final stabilization*;
- 2. *Discharge*s that are mixed with sources of non-stormwater other than those expressly authorized under subsection E.3. of this Part and identified in the SWPPP required by this permit;
- 3. *Discharges* that are required to obtain an individual SPDES permit or another SPDES general permit pursuant to Part VII.K. of this permit;
- 4. Construction activities or discharges from construction activities that may adversely affect an endangered or threatened species unless the owner or

operator has obtained a permit issued pursuant to 6 NYCRR Part 182 for the project or the Department has issued a letter of non-jurisdiction for the project. All documentation necessary to demonstrate eligibility shall be maintained on site in accordance with Part II.D.2 of this permit;

- 5. *Discharges* which either cause or contribute to a violation of *water quality* standards adopted pursuant to the *ECL* and its accompanying regulations;
- 6. Construction activities for residential, commercial and institutional projects:
 - a. Where the *discharges* from the *construction activities* are tributary to waters of the state classified as AA or AA-s; and
 - b. Which are undertaken on land with no existing impervious cover; and
 - c. Which disturb one (1) or more acres of land designated on the current United States Department of Agriculture ("USDA") Soil Survey as Soil Slope Phase "D", (provided the map unit name is inclusive of slopes greater than 25%), or Soil Slope Phase "E" or "F" (regardless of the map unit name), or a combination of the three designations.
- 7. Construction activities for linear transportation projects and linear utility projects:
 - a. Where the *discharges* from the *construction activities* are tributary to waters of the state classified as AA or AA-s: and
 - b. Which are undertaken on land with no existing impervious cover; and
 - c. Which disturb two (2) or more acres of land designated on the current USDA Soil Survey as Soil Slope Phase "D" (provided the map unit name is inclusive of slopes greater than 25%), or Soil Slope Phase "E" or "F" (regardless of the map unit name), or a combination of the three designations.

- 8. Construction activities that have the potential to affect an historic property, unless there is documentation that such impacts have been resolved. The following documentation necessary to demonstrate eligibility with this requirement shall be maintained on site in accordance with Part II.D.2 of this permit and made available to the Department in accordance with Part VII.F of this permit:
 - a. Documentation that the construction activity is not within an archeologically sensitive area indicated on the sensitivity map, and that the construction activity is not located on or immediately adjacent to a property listed or determined to be eligible for listing on the National or State Registers of Historic Places, and that there is no new permanent building on the construction site within the following distances from a building, structure, or object that is more than 50 years old, or if there is such a new permanent building on the construction site within those parameters that NYS Office of Parks, Recreation and Historic Preservation (OPRHP), a Historic Preservation Commission of a Certified Local Government, or a qualified preservation professional has determined that the building, structure, or object more than 50 years old is not historically/archeologically significant.
 - 1-5 acres of disturbance 20 feet
 - 5-20 acres of disturbance 50 feet
 - 20+ acres of disturbance 100 feet, or
 - b. DEC consultation form sent to OPRHP, and copied to the NYS DEC Agency Historic Preservation Officer (APO), and
 - (i) the State Environmental Quality Review (SEQR) Environmental Assessment Form (EAF) with a negative declaration or the Findings Statement, with documentation of OPRHP's agreement with the resolution; or
 - (ii) documentation from OPRHP that the *construction activity* will result in No Impact; or
 - (iii) documentation from OPRHP providing a determination of No Adverse Impact; or
 - (iv) a Letter of Resolution signed by the owner/operator, OPRHP and the DEC APO which allows for this *construction activity* to be eligible for coverage under the general permit in terms of the State Historic Preservation Act (SHPA); or
 - c. Documentation of satisfactory compliance with Section 106 of the National Historic Preservation Act for a coterminous project area:

- (i) No Affect
- (ii) No Adverse Affect
- (iii) Executed Memorandum of Agreement, or

d. Documentation that:

- (i) SHPA Section 14.09 has been completed by NYS DEC or another state agency.
- 9. *Discharges* from *construction activities* that are subject to an existing SPDES individual or general permit where a SPDES permit for *construction activity* has been terminated or denied; or where the *owner or operator* has failed to renew an expired individual permit.

Part II. PERMIT COVERAGE

A. How to Obtain Coverage

- An owner or operator of a construction activity that is not subject to the
 requirements of a regulated, traditional land use control MS4 must first prepare
 a SWPPP in accordance with all applicable requirements of this permit and
 then submit a completed Notice of Intent (NOI) to the Department to be
 authorized to discharge under this permit.
- 2. An owner or operator of a construction activity that is subject to the requirements of a regulated, traditional land use control MS4 must first prepare a SWPPP in accordance with all applicable requirements of this permit and then have the SWPPP reviewed and accepted by the regulated, traditional land use control MS4 prior to submitting the NOI to the Department. The owner or operator shall have the "MS4 SWPPP Acceptance" form signed in accordance with Part VII.H., and then submit that form along with a completed NOI to the Department.
- 3. The requirement for an *owner or operator* to have its SWPPP reviewed and accepted by the *regulated, traditional land use control MS4* prior to submitting the NOI to the Department does not apply to an *owner or operator* that is obtaining permit coverage in accordance with the requirements in Part II.F. (Change of *Owner or Operator*) or where the *owner or operator* of the *construction activity* is the *regulated, traditional land use control MS4*. This exemption does not apply to *construction activities* subject to the New York City Administrative Code.

B. Notice of Intent (NOI) Submittal

 Prior to December 21, 2020, an owner or operator shall use either the electronic (eNOI) or paper version of the NOI that the Department prepared. Both versions of the NOI are located on the Department's website (http://www.dec.ny.gov/). The paper version of the NOI shall be signed in accordance with Part VII.H. of this permit and submitted to the following address:

> NOTICE OF INTENT NYS DEC, Bureau of Water Permits 625 Broadway, 4th Floor Albany, New York 12233-3505

- 2. Beginning December 21, 2020 and in accordance with EPA's 2015 NPDES Electronic Reporting Rule (40 CFR Part 127), the *owner or operator* must submit the NOI electronically using the *Department's* online NOI.
- 3. The *owner or operator* shall have the SWPPP preparer sign the "SWPPP Preparer Certification" statement on the NOI prior to submitting the form to the Department.
- 4. As of the date the NOI is submitted to the Department, the *owner or operator* shall make the NOI and SWPPP available for review and copying in accordance with the requirements in Part VII.F. of this permit.

C. Permit Authorization

- 1. An *owner or operator* shall not *commence construction activity* until their authorization to *discharge* under this permit goes into effect.
- 2. Authorization to *discharge* under this permit will be effective when the *owner or operator* has satisfied all of the following criteria:
 - a. project review pursuant to the State Environmental Quality Review Act ("SEQRA") have been satisfied, when SEQRA is applicable. See the Department's website (http://www.dec.ny.gov/) for more information,
 - b. where required, all necessary Department permits subject to the *Uniform Procedures Act ("UPA")* (see 6 NYCRR Part 621), or the equivalent from another New York State agency, have been obtained, unless otherwise notified by the Department pursuant to 6 NYCRR 621.3(a)(4). *Owners or operators* of *construction activities* that are required to obtain *UPA* permits

must submit a preliminary SWPPP to the appropriate DEC Permit Administrator at the Regional Office listed in Appendix F at the time all other necessary *UPA* permit applications are submitted. The preliminary SWPPP must include sufficient information to demonstrate that the *construction activity* qualifies for authorization under this permit,

- c. the final SWPPP has been prepared, and
- d. a complete NOI has been submitted to the Department in accordance with the requirements of this permit.
- 3. An owner or operator that has satisfied the requirements of Part II.C.2 above will be authorized to discharge stormwater from their construction activity in accordance with the following schedule:
 - a. For *construction activities* that are <u>not</u> subject to the requirements of a regulated, traditional land use control MS4:
 - (i) Five (5) business days from the date the Department receives a complete electronic version of the NOI (eNOI) for *construction activities* with a SWPPP that has been prepared in conformance with the design criteria in the technical standard referenced in Part III.B.1 and the *performance criteria* in the technical standard referenced in Parts III.B., 2 or 3, for *construction activities* that require post-construction stormwater management practices pursuant to Part III.C.; or
 - (ii) Sixty (60) business days from the date the Department receives a complete NOI (electronic or paper version) for *construction activities* with a SWPPP that has <u>not</u> been prepared in conformance with the design criteria in technical standard referenced in Part III.B.1. or, for *construction activities* that require post-construction stormwater management practices pursuant to Part III.C., the *performance criteria* in the technical standard referenced in Parts III.B., 2 or 3, or;
 - (iii) Ten (10) business days from the date the Department receives a complete paper version of the NOI for construction activities with a SWPPP that has been prepared in conformance with the design criteria in the technical standard referenced in Part III.B.1 and the performance criteria in the technical standard referenced in Parts III.B., 2 or 3, for construction activities that require post-construction stormwater management practices pursuant to Part III.C.

- b. For *construction activities* that are subject to the requirements of a regulated, traditional land use control MS4:
 - Five (5) business days from the date the Department receives both a complete electronic version of the NOI (eNOI) and signed "MS4 SWPPP Acceptance" form, or
 - (ii) Ten (10) business days from the date the Department receives both a complete paper version of the NOI and signed "MS4 SWPPP Acceptance" form.
- 4. Coverage under this permit authorizes stormwater discharges from only those areas of disturbance that are identified in the NOI. If an owner or operator wishes to have stormwater discharges from future or additional areas of disturbance authorized, they must submit a new NOI that addresses that phase of the development, unless otherwise notified by the Department. The owner or operator shall not commence construction activity on the future or additional areas until their authorization to discharge under this permit goes into effect in accordance with Part II.C. of this permit.

D. General Requirements For Owners or Operators With Permit Coverage

- 1. The *owner or operator* shall ensure that the provisions of the SWPPP are implemented from the *commencement of construction activity* until all areas of disturbance have achieved *final stabilization* and the Notice of Termination ("NOT") has been submitted to the Department in accordance with Part V. of this permit. This includes any changes made to the SWPPP pursuant to Part III.A.4. of this permit.
- 2. The owner or operator shall maintain a copy of the General Permit (GP-0-20-001), NOI, NOI Acknowledgment Letter, SWPPP, MS4 SWPPP Acceptance form, inspection reports, responsible contractor's or subcontractor's certification statement (see Part III.A.6.), and all documentation necessary to demonstrate eligibility with this permit at the construction site until all disturbed areas have achieved final stabilization and the NOT has been submitted to the Department. The documents must be maintained in a secure location, such as a job trailer, on-site construction office, or mailbox with lock. The secure location must be accessible during normal business hours to an individual performing a compliance inspection.
- 3. The *owner or operator* of a *construction activity* shall not disturb greater than five (5) acres of soil at any one time without prior written authorization from the Department or, in areas under the jurisdiction of a *regulated*, *traditional land*

use control MS4, the regulated, traditional land use control MS4 (provided the regulated, traditional land use control MS4 is not the owner or operator of the construction activity). At a minimum, the owner or operator must comply with the following requirements in order to be authorized to disturb greater than five (5) acres of soil at any one time:

- a. The owner or operator shall have a qualified inspector conduct at least two (2) site inspections in accordance with Part IV.C. of this permit every seven (7) calendar days, for as long as greater than five (5) acres of soil remain disturbed. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
- b. In areas where soil disturbance activity has temporarily or permanently ceased, the application of soil stabilization measures must be initiated by the end of the next business day and completed within seven (7) days from the date the current soil disturbance activity ceased. The soil stabilization measures selected shall be in conformance with the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016.
- c. The *owner or operator* shall prepare a phasing plan that defines maximum disturbed area per phase and shows required cuts and fills.
- d. The *owner or operator* shall install any additional site-specific practices needed to protect water quality.
- e. The *owner or operator* shall include the requirements above in their SWPPP.
- 4. In accordance with statute, regulations, and the terms and conditions of this permit, the Department may suspend or revoke an *owner's or operator's* coverage under this permit at any time if the Department determines that the SWPPP does not meet the permit requirements or consistent with Part VII.K..
- 5. Upon a finding of significant non-compliance with the practices described in the SWPPP or violation of this permit, the Department may order an immediate stop to all activity at the site until the non-compliance is remedied. The stop work order shall be in writing, describe the non-compliance in detail, and be sent to the *owner or operator*.
- 6. For *construction activities* that are subject to the requirements of a *regulated, traditional land use control MS4*, the *owner or operator* shall notify the

regulated, traditional land use control MS4 in writing of any planned amendments or modifications to the post-construction stormwater management practice component of the SWPPP required by Part III.A. 4. and 5. of this permit. Unless otherwise notified by the regulated, traditional land use control MS4, the owner or operator shall have the SWPPP amendments or modifications reviewed and accepted by the regulated, traditional land use control MS4 prior to commencing construction of the post-construction stormwater management practice.

E. Permit Coverage for Discharges Authorized Under GP-0-15-002

 Upon renewal of SPDES General Permit for Stormwater Discharges from Construction Activity (Permit No. GP-0-15-002), an owner or operator of a construction activity with coverage under GP-0-15-002, as of the effective date of GP- 0-20-001, shall be authorized to discharge in accordance with GP- 0-20-001, unless otherwise notified by the Department.

An *owner or operator* may continue to implement the technical/design components of the post-construction stormwater management controls provided that such design was done in conformance with the technical standards in place at the time of initial project authorization. However, they must comply with the other, non-design provisions of GP-0-20-001.

F. Change of Owner or Operator

- 1. When property ownership changes or when there is a change in operational control over the construction plans and specifications, the original *owner or operator* must notify the new *owner or operator*, <u>in writing</u>, of the requirement to obtain permit coverage by submitting a NOI with the Department. For *construction activities* subject to the requirements of a *regulated, traditional land use control MS4*, the original *owner or operator* must also notify the MS4, in writing, of the change in ownership at least 30 calendar days prior to the change in ownership.
- 2. Once the new owner or operator obtains permit coverage, the original owner or operator shall then submit a completed NOT with the name and permit identification number of the new owner or operator to the Department at the address in Part II.B.1. of this permit. If the original owner or operator maintains ownership of a portion of the construction activity and will disturb soil, they must maintain their coverage under the permit.
- 3. Permit coverage for the new *owner or operator* will be effective as of the date the Department receives a complete NOI, provided the original *owner or*

operator was not subject to a sixty (60) business day authorization period that has not expired as of the date the Department receives the NOI from the new owner or operator.

Part III. STORMWATER POLLUTION PREVENTION PLAN (SWPPP)

A. General SWPPP Requirements

- 1. A SWPPP shall be prepared and implemented by the owner or operator of each construction activity covered by this permit. The SWPPP must document the selection, design, installation, implementation and maintenance of the control measures and practices that will be used to meet the effluent limitations in Part I.B. of this permit and where applicable, the post-construction stormwater management practice requirements in Part I.C. of this permit. The SWPPP shall be prepared prior to the submittal of the NOI. The NOI shall be submitted to the Department prior to the commencement of construction activity. A copy of the completed, final NOI shall be included in the SWPPP.
- 2. The SWPPP shall describe the erosion and sediment control practices and where required, post-construction stormwater management practices that will be used and/or constructed to reduce the *pollutants* in stormwater *discharges* and to assure compliance with the terms and conditions of this permit. In addition, the SWPPP shall identify potential sources of pollution which may reasonably be expected to affect the quality of stormwater *discharges*.
- 3. All SWPPs that require the post-construction stormwater management practice component shall be prepared by a *qualified professional* that is knowledgeable in the principles and practices of stormwater management and treatment.
- 4. The owner or operator must keep the SWPPP current so that it at all times accurately documents the erosion and sediment controls practices that are being used or will be used during construction, and all post-construction stormwater management practices that will be constructed on the site. At a minimum, the owner or operator shall amend the SWPPP, including construction drawings:
 - a. whenever the current provisions prove to be ineffective in minimizing *pollutants* in stormwater *discharges* from the site;

- whenever there is a change in design, construction, or operation at the construction site that has or could have an effect on the discharge of pollutants;
- c. to address issues or deficiencies identified during an inspection by the *qualified inspector*, the Department or other regulatory authority; and
- d. to document the final construction conditions.
- 5. The Department may notify the *owner or operator* at any time that the SWPPP does not meet one or more of the minimum requirements of this permit. The notification shall be in writing and identify the provisions of the SWPPP that require modification. Within fourteen (14) calendar days of such notification, or as otherwise indicated by the Department, the *owner or operator* shall make the required changes to the SWPPP and submit written notification to the Department that the changes have been made. If the *owner or operator* does not respond to the Department's comments in the specified time frame, the Department may suspend the *owner's or operator's* coverage under this permit or require the *owner or operator* to obtain coverage under an individual SPDES permit in accordance with Part II.D.4. of this permit.
- 6. Prior to the commencement of construction activity, the owner or operator must identify the contractor(s) and subcontractor(s) that will be responsible for installing, constructing, repairing, replacing, inspecting and maintaining the erosion and sediment control practices included in the SWPPP; and the contractor(s) and subcontractor(s) that will be responsible for constructing the post-construction stormwater management practices included in the SWPPP. The owner or operator shall have each of the contractors and subcontractors identify at least one person from their company that will be responsible for implementation of the SWPPP. This person shall be known as the trained contractor. The owner or operator shall ensure that at least one trained contractor is on site on a daily basis when soil disturbance activities are being performed.

The *owner or operator* shall have each of the contractors and subcontractors identified above sign a copy of the following certification statement below before they commence any *construction activity*:

"I hereby certify under penalty of law that I understand and agree to comply with the terms and conditions of the SWPPP and agree to implement any corrective actions identified by the *qualified inspector* during a site inspection. I also understand that the *owner or operator* must comply with

the terms and conditions of the most current version of the New York State Pollutant Discharge Elimination System ("SPDES") general permit for stormwater *discharges* from *construction activities* and that it is unlawful for any person to cause or contribute to a violation of *water quality standards*. Furthermore, I am aware that there are significant penalties for submitting false information, that I do not believe to be true, including the possibility of fine and imprisonment for knowing violations"

In addition to providing the certification statement above, the certification page must also identify the specific elements of the SWPPP that each contractor and subcontractor will be responsible for and include the name and title of the person providing the signature; the name and title of the *trained contractor* responsible for SWPPP implementation; the name, address and telephone number of the contracting firm; the address (or other identifying description) of the site; and the date the certification statement is signed. The *owner or operator* shall attach the certification statement(s) to the copy of the SWPPP that is maintained at the *construction site*. If new or additional contractors are hired to implement measures identified in the SWPPP after construction has commenced, they must also sign the certification statement and provide the information listed above.

7. For projects where the Department requests a copy of the SWPPP or inspection reports, the *owner or operator* shall submit the documents in both electronic (PDF only) and paper format within five (5) business days, unless otherwise notified by the Department.

B. Required SWPPP Contents

- 1. Erosion and sediment control component All SWPPPs prepared pursuant to this permit shall include erosion and sediment control practices designed in conformance with the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016. Where erosion and sediment control practices are not designed in conformance with the design criteria included in the technical standard, the *owner or operator* must demonstrate *equivalence* to the technical standard. At a minimum, the erosion and sediment control component of the SWPPP shall include the following:
 - a. Background information about the scope of the project, including the location, type and size of project

- b. A site map/construction drawing(s) for the project, including a general location map. At a minimum, the site map shall show the total site area; all improvements; areas of disturbance; areas that will not be disturbed; existing vegetation; on-site and adjacent off-site surface water(s); floodplain/floodway boundaries; wetlands and drainage patterns that could be affected by the construction activity; existing and final contours; locations of different soil types with boundaries; material, waste, borrow or equipment storage areas located on adjacent properties; and location(s) of the stormwater discharge(s);
- c. A description of the soil(s) present at the site, including an identification of the Hydrologic Soil Group (HSG);
- d. A construction phasing plan and sequence of operations describing the intended order of *construction activities*, including clearing and grubbing, excavation and grading, utility and infrastructure installation and any other activity at the site that results in soil disturbance;
- e. A description of the minimum erosion and sediment control practices to be installed or implemented for each *construction activity* that will result in soil disturbance. Include a schedule that identifies the timing of initial placement or implementation of each erosion and sediment control practice and the minimum time frames that each practice should remain in place or be implemented;
- f. A temporary and permanent soil stabilization plan that meets the requirements of this general permit and the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016, for each stage of the project, including initial land clearing and grubbing to project completion and achievement of *final stabilization*;
- g. A site map/construction drawing(s) showing the specific location(s), size(s), and length(s) of each erosion and sediment control practice;
- h. The dimensions, material specifications, installation details, and operation and maintenance requirements for all erosion and sediment control practices. Include the location and sizing of any temporary sediment basins and structural practices that will be used to divert flows from exposed soils;
- i. A maintenance inspection schedule for the contractor(s) identified in Part III.A.6. of this permit, to ensure continuous and effective operation of the erosion and sediment control practices. The maintenance inspection

schedule shall be in accordance with the requirements in the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016;

- j. A description of the pollution prevention measures that will be used to control litter, construction chemicals and construction debris from becoming a pollutant source in the stormwater discharges;
- k. A description and location of any stormwater discharges associated with industrial activity other than construction at the site, including, but not limited to, stormwater discharges from asphalt plants and concrete plants located on the construction site; and
- Identification of any elements of the design that are not in conformance with the design criteria in the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016.
 Include the reason for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is equivalent to the technical standard.
- 2. Post-construction stormwater management practice component The owner or operator of any construction project identified in Table 2 of Appendix B as needing post-construction stormwater management practices shall prepare a SWPPP that includes practices designed in conformance with the applicable sizing criteria in Part I.C.2.a., c. or d. of this permit and the performance criteria in the technical standard, New York State Stormwater Management Design Manual dated January 2015

Where post-construction stormwater management practices are not designed in conformance with the *performance criteria* in the technical standard, the *owner or operator* must include in the SWPPP the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.

The post-construction stormwater management practice component of the SWPPP shall include the following:

 a. Identification of all post-construction stormwater management practices to be constructed as part of the project. Include the dimensions, material specifications and installation details for each post-construction stormwater management practice;

- b. A site map/construction drawing(s) showing the specific location and size of each post-construction stormwater management practice;
- c. A Stormwater Modeling and Analysis Report that includes:
 - Map(s) showing pre-development conditions, including watershed/subcatchments boundaries, flow paths/routing, and design points;
 - (ii) Map(s) showing post-development conditions, including watershed/subcatchments boundaries, flow paths/routing, design points and post-construction stormwater management practices;
 - (iii) Results of stormwater modeling (i.e. hydrology and hydraulic analysis) for the required storm events. Include supporting calculations (model runs), methodology, and a summary table that compares pre and post-development runoff rates and volumes for the different storm events;
 - (iv) Summary table, with supporting calculations, which demonstrates that each post-construction stormwater management practice has been designed in conformance with the *sizing criteria* included in the Design Manual;
 - (v) Identification of any *sizing criteria* that is not required based on the requirements included in Part I.C. of this permit; and
 - (vi) Identification of any elements of the design that are not in conformance with the *performance criteria* in the Design Manual. Include the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the Design Manual;
- d. Soil testing results and locations (test pits, borings);
- e. Infiltration test results, when required; and
- f. An operations and maintenance plan that includes inspection and maintenance schedules and actions to ensure continuous and effective operation of each post-construction stormwater management practice. The plan shall identify the entity that will be responsible for the long term operation and maintenance of each practice.

3. Enhanced Phosphorus Removal Standards - All construction projects identified in Table 2 of Appendix B that are located in the watersheds identified in Appendix C shall prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the applicable *sizing criteria* in Part I.C.2. b., c. or d. of this permit and the *performance criteria*, Enhanced Phosphorus Removal Standards included in the Design Manual. At a minimum, the post-construction stormwater management practice component of the SWPPP shall include items 2.a - 2.f. above.

C. Required SWPPP Components by Project Type

Unless otherwise notified by the Department, *owners or operators* of *construction activities* identified in Table 1 of Appendix B are required to prepare a SWPPP that only includes erosion and sediment control practices designed in conformance with Part III.B.1 of this permit. *Owners or operators* of the *construction activities* identified in Table 2 of Appendix B shall prepare a SWPPP that also includes post-construction stormwater management practices designed in conformance with Part III.B.2 or 3 of this permit.

Part IV. INSPECTION AND MAINTENANCE REQUIREMENTS

A. General Construction Site Inspection and Maintenance Requirements

- 1. The *owner or operator* must ensure that all erosion and sediment control practices (including pollution prevention measures) and all post-construction stormwater management practices identified in the SWPPP are inspected and maintained in accordance with Part IV.B. and C. of this permit.
- 2. The terms of this permit shall not be construed to prohibit the State of New York from exercising any authority pursuant to the ECL, common law or federal law, or prohibit New York State from taking any measures, whether civil or criminal, to prevent violations of the laws of the State of New York or protect the public health and safety and/or the environment.

B. Contractor Maintenance Inspection Requirements

1. The owner or operator of each construction activity identified in Tables 1 and 2 of Appendix B shall have a trained contractor inspect the erosion and sediment control practices and pollution prevention measures being implemented within the active work area daily to ensure that they are being maintained in effective operating condition at all times. If deficiencies are identified, the contractor shall

begin implementing corrective actions within one business day and shall complete the corrective actions in a reasonable time frame.

- 2. For construction sites where soil disturbance activities have been temporarily suspended (e.g. winter shutdown) and *temporary stabilization* measures have been applied to all disturbed areas, the *trained contractor* can stop conducting the maintenance inspections. The *trained contractor* shall begin conducting the maintenance inspections in accordance with Part IV.B.1. of this permit as soon as soil disturbance activities resume.
- 3. For construction sites where soil disturbance activities have been shut down with partial project completion, the *trained contractor* can stop conducting the maintenance inspections if all areas disturbed as of the project shutdown date have achieved *final stabilization* and all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational.

C. Qualified Inspector Inspection Requirements

The *owner or operator* shall have a *qualified inspector* conduct site inspections in conformance with the following requirements:

[Note: The *trained contractor* identified in Part III.A.6. and IV.B. of this permit **cannot** conduct the *qualified inspector* site inspections unless they meet the *qualified inspector* qualifications included in Appendix A. In order to perform these inspections, the *trained contractor* would have to be a:

- licensed Professional Engineer,
- Certified Professional in Erosion and Sediment Control (CPESC),
- New York State Erosion and Sediment Control Certificate Program holder
- Registered Landscape Architect, or
- someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided they have received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity].
- 1. A *qualified inspector* shall conduct site inspections for all *construction activities* identified in Tables 1 and 2 of Appendix B, <u>with the exception of</u>:
 - a. the construction of a single family residential subdivision with 25% or less *impervious cover* at total site build-out that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres and is not located

- in one of the watersheds listed in Appendix C and <u>not</u> directly discharging to one of the 303(d) segments listed in Appendix E;
- b. the construction of a single family home that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres and is <u>not</u> located in one of the watersheds listed in Appendix C and <u>not</u> directly discharging to one of the 303(d) segments listed in Appendix E;
- c. construction on agricultural property that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres; and
- d. construction activities located in the watersheds identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.
- 2. Unless otherwise notified by the Department, the *qualified inspector* shall conduct site inspections in accordance with the following timetable:
 - a. For construction sites where soil disturbance activities are on-going, the *qualified inspector* shall conduct a site inspection at least once every seven (7) calendar days.
 - b. For construction sites where soil disturbance activities are on-going and the owner or operator has received authorization in accordance with Part II.D.3 to disturb greater than five (5) acres of soil at any one time, the qualified inspector shall conduct at least two (2) site inspections every seven (7) calendar days. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
 - c. For construction sites where soil disturbance activities have been temporarily suspended (e.g. winter shutdown) and temporary stabilization measures have been applied to all disturbed areas, the qualified inspector shall conduct a site inspection at least once every thirty (30) calendar days. The owner or operator shall notify the DOW Water (SPDES) Program contact at the Regional Office (see contact information in Appendix F) or, in areas under the jurisdiction of a regulated, traditional land use control MS4, the regulated, traditional land use control MS4 (provided the regulated, traditional land use control MS4 is not the owner or operator of the construction activity) in writing prior to reducing the frequency of inspections.

- d. For construction sites where soil disturbance activities have been shut down with partial project completion, the qualified inspector can stop conducting inspections if all areas disturbed as of the project shutdown date have achieved *final stabilization* and all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational. The owner or operator shall notify the DOW Water (SPDES) Program contact at the Regional Office (see contact information in Appendix F) or, in areas under the jurisdiction of a regulated, traditional land use control MS4, the regulated, traditional land use control MS4 (provided the regulated, traditional land use control MS4 is not the owner or operator of the *construction activity*) in writing prior to the shutdown. If soil disturbance activities are not resumed within 2 years from the date of shutdown, the owner or operator shall have the qualified inspector perform a final inspection and certify that all disturbed areas have achieved final stabilization, and all temporary, structural erosion and sediment control measures have been removed; and that all post-construction stormwater management practices have been constructed in conformance with the SWPPP by signing the "Final Stabilization" and "Post-Construction" Stormwater Management Practice" certification statements on the NOT. The owner or operator shall then submit the completed NOT form to the address in Part II.B.1 of this permit.
- e. For construction sites that directly *discharge* to one of the 303(d) segments listed in Appendix E or is located in one of the watersheds listed in Appendix C, the *qualified inspector* shall conduct at least two (2) site inspections every seven (7) calendar days. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
- 3. At a minimum, the *qualified inspector* shall inspect all erosion and sediment control practices and pollution prevention measures to ensure integrity and effectiveness, all post-construction stormwater management practices under construction to ensure that they are constructed in conformance with the SWPPP, all areas of disturbance that have not achieved *final stabilization*, all points of *discharge* to natural surface waterbodies located within, or immediately adjacent to, the property boundaries of the *construction site*, and all points of *discharge* from the *construction site*.
- 4. The *qualified inspector* shall prepare an inspection report subsequent to each and every inspection. At a minimum, the inspection report shall include and/or address the following:

- a. Date and time of inspection;
- b. Name and title of person(s) performing inspection;
- c. A description of the weather and soil conditions (e.g. dry, wet, saturated) at the time of the inspection;
- d. A description of the condition of the runoff at all points of *discharge* from the *construction site*. This shall include identification of any *discharges* of sediment from the *construction site*. Include *discharges* from conveyance systems (i.e. pipes, culverts, ditches, etc.) and overland flow;
- e. A description of the condition of all natural surface waterbodies located within, or immediately adjacent to, the property boundaries of the construction site which receive runoff from disturbed areas. This shall include identification of any discharges of sediment to the surface waterbody;
- f. Identification of all erosion and sediment control practices and pollution prevention measures that need repair or maintenance;
- g. Identification of all erosion and sediment control practices and pollution prevention measures that were not installed properly or are not functioning as designed and need to be reinstalled or replaced;
- h. Description and sketch of areas with active soil disturbance activity, areas that have been disturbed but are inactive at the time of the inspection, and areas that have been stabilized (temporary and/or final) since the last inspection;
- Current phase of construction of all post-construction stormwater management practices and identification of all construction that is not in conformance with the SWPPP and technical standards;
- j. Corrective action(s) that must be taken to install, repair, replace or maintain erosion and sediment control practices and pollution prevention measures; and to correct deficiencies identified with the construction of the post-construction stormwater management practice(s);
- Identification and status of all corrective actions that were required by previous inspection; and

- I. Digital photographs, with date stamp, that clearly show the condition of all practices that have been identified as needing corrective actions. The qualified inspector shall attach paper color copies of the digital photographs to the inspection report being maintained onsite within seven (7) calendar days of the date of the inspection. The qualified inspector shall also take digital photographs, with date stamp, that clearly show the condition of the practice(s) after the corrective action has been completed. The qualified inspector shall attach paper color copies of the digital photographs to the inspection report that documents the completion of the corrective action work within seven (7) calendar days of that inspection.
- 5. Within one business day of the completion of an inspection, the *qualified inspector* shall notify the *owner or operator* and appropriate contractor or subcontractor identified in Part III.A.6. of this permit of any corrective actions that need to be taken. The contractor or subcontractor shall begin implementing the corrective actions within one business day of this notification and shall complete the corrective actions in a reasonable time frame.
- 6. All inspection reports shall be signed by the *qualified inspector*. Pursuant to Part II.D.2. of this permit, the inspection reports shall be maintained on site with the SWPPP.

Part V. TERMINATION OF PERMIT COVERAGE

A. Termination of Permit Coverage

- An owner or operator that is eligible to terminate coverage under this permit
 must submit a completed NOT form to the address in Part II.B.1 of this permit.
 The NOT form shall be one which is associated with this permit, signed in
 accordance with Part VII.H of this permit.
- 2. An *owner or operator* may terminate coverage when one or more the following conditions have been met:
 - a. Total project completion All construction activity identified in the SWPPP has been completed; <u>and</u> all areas of disturbance have achieved *final* stabilization; <u>and</u> all temporary, structural erosion and sediment control measures have been removed; <u>and</u> all post-construction stormwater management practices have been constructed in conformance with the SWPPP and are operational;

- b. Planned shutdown with partial project completion All soil disturbance activities have ceased; <u>and</u> all areas disturbed as of the project shutdown date have achieved *final stabilization*; <u>and</u> all temporary, structural erosion and sediment control measures have been removed; <u>and</u> all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational;
- c. A new *owner or operator* has obtained coverage under this permit in accordance with Part II.F. of this permit.
- d. The *owner or operator* obtains coverage under an alternative SPDES general permit or an individual SPDES permit.
- 3. For *construction activities* meeting subdivision 2a. or 2b. of this Part, the *owner or operator* shall have the *qualified inspector* perform a final site inspection prior to submitting the NOT. The *qualified inspector* shall, by signing the "*Final Stabilization*" and "Post-Construction Stormwater Management Practice certification statements on the NOT, certify that all the requirements in Part V.A.2.a. or b. of this permit have been achieved.
- 4. For construction activities that are subject to the requirements of a regulated, traditional land use control MS4 and meet subdivision 2a. or 2b. of this Part, the owner or operator shall have the regulated, traditional land use control MS4 sign the "MS4 Acceptance" statement on the NOT in accordance with the requirements in Part VII.H. of this permit. The regulated, traditional land use control MS4 official, by signing this statement, has determined that it is acceptable for the owner or operator to submit the NOT in accordance with the requirements of this Part. The regulated, traditional land use control MS4 can make this determination by performing a final site inspection themselves or by accepting the qualified inspector's final site inspection certification(s) required in Part V.A.3. of this permit.
- 5. For *construction activities* that require post-construction stormwater management practices and meet subdivision 2a. of this Part, the *owner or operator* must, prior to submitting the NOT, ensure one of the following:
 - a. the post-construction stormwater management practice(s) and any right-ofway(s) needed to maintain such practice(s) have been deeded to the municipality in which the practice(s) is located,

- b. an executed maintenance agreement is in place with the municipality that will maintain the post-construction stormwater management practice(s),
- c. for post-construction stormwater management practices that are privately owned, the *owner or operator* has a mechanism in place that requires operation and maintenance of the practice(s) in accordance with the operation and maintenance plan, such as a deed covenant in the *owner or* operator's deed of record,
- d. for post-construction stormwater management practices that are owned by a public or private institution (e.g. school, university, hospital), government agency or authority, or public utility; the *owner or operator* has policy and procedures in place that ensures operation and maintenance of the practices in accordance with the operation and maintenance plan.

Part VI. REPORTING AND RETENTION RECORDS

A. Record Retention

The *owner or operator* shall retain a copy of the NOI, NOI Acknowledgment Letter, SWPPP, MS4 SWPPP Acceptance form and any inspection reports that were prepared in conjunction with this permit for a period of at least five (5) years from the date that the Department receives a complete NOT submitted in accordance with Part V. of this general permit.

B. Addresses

With the exception of the NOI, NOT, and MS4 SWPPP Acceptance form (which must be submitted to the address referenced in Part II.B.1 of this permit), all written correspondence requested by the Department, including individual permit applications, shall be sent to the address of the appropriate DOW Water (SPDES) Program contact at the Regional Office listed in Appendix F.

Part VII. STANDARD PERMIT CONDITIONS

A. Duty to Comply

The *owner or operator* must comply with all conditions of this permit. All contractors and subcontractors associated with the project must comply with the terms of the SWPPP. Any non-compliance with this permit constitutes a violation of the Clean Water

Act (CWA) and the ECL and is grounds for an enforcement action against the *owner or operator* and/or the contractor/subcontractor; permit revocation, suspension or modification; or denial of a permit renewal application. Upon a finding of significant non-compliance with this permit or the applicable SWPPP, the Department may order an immediate stop to all *construction activity* at the site until the non-compliance is remedied. The stop work order shall be in writing, shall describe the non-compliance in detail, and shall be sent to the *owner or operator*.

If any human remains or archaeological remains are encountered during excavation, the *owner or operator* must immediately cease, or cause to cease, all *construction activity* in the area of the remains and notify the appropriate Regional Water Engineer (RWE). *Construction activity* shall not resume until written permission to do so has been received from the RWE.

B. Continuation of the Expired General Permit

This permit expires five (5) years from the effective date. If a new general permit is not issued prior to the expiration of this general permit, an *owner or operator* with coverage under this permit may continue to operate and *discharge* in accordance with the terms and conditions of this general permit, if it is extended pursuant to the State Administrative Procedure Act and 6 NYCRR Part 621, until a new general permit is issued.

C. Enforcement

Failure of the *owner or operator*, its contractors, subcontractors, agents and/or assigns to strictly adhere to any of the permit requirements contained herein shall constitute a violation of this permit. There are substantial criminal, civil, and administrative penalties associated with violating the provisions of this permit. Fines of up to \$37,500 per day for each violation and imprisonment for up to fifteen (15) years may be assessed depending upon the nature and degree of the offense.

D. Need to Halt or Reduce Activity Not a Defense

It shall not be a defense for an *owner or operator* in an enforcement action that it would have been necessary to halt or reduce the *construction activity* in order to maintain compliance with the conditions of this permit.

E. Duty to Mitigate

The *owner or operator* and its contractors and subcontractors shall take all reasonable steps to *minimize* or prevent any *discharge* in violation of this permit which has a reasonable likelihood of adversely affecting human health or the environment.

F. Duty to Provide Information

The *owner or operator* shall furnish to the Department, within a reasonable specified time period of a written request, all documentation necessary to demonstrate eligibility and any information to determine compliance with this permit or to determine whether cause exists for modifying or revoking this permit, or suspending or denying coverage under this permit, in accordance with the terms and conditions of this permit. The NOI, SWPPP and inspection reports required by this permit are public documents that the *owner or operator* must make available for review and copying by any person within five (5) business days of the *owner or operator* receiving a written request by any such person to review these documents. Copying of documents will be done at the requester's expense.

G. Other Information

When the *owner or operator* becomes aware that they failed to submit any relevant facts, or submitted incorrect information in the NOI or in any of the documents required by this permit, or have made substantive revisions to the SWPPP (e.g. the scope of the project changes significantly, the type of post-construction stormwater management practice(s) changes, there is a reduction in the sizing of the post-construction stormwater management practice, or there is an increase in the disturbance area or *impervious area*), which were not reflected in the original NOI submitted to the Department, they shall promptly submit such facts or information to the Department using the contact information in Part II.A. of this permit. Failure of the *owner or operator* to correct or supplement any relevant facts within five (5) business days of becoming aware of the deficiency shall constitute a violation of this permit.

H. Signatory Requirements

- 1. All NOIs and NOTs shall be signed as follows:
 - a. For a corporation these forms shall be signed by a responsible corporate officer. For the purpose of this section, a responsible corporate officer means:

- (i) a president, secretary, treasurer, or vice-president of the corporation in charge of a principal business function, or any other person who performs similar policy or decision-making functions for the corporation; or
- (ii) the manager of one or more manufacturing, production or operating facilities, provided the manager is authorized to make management decisions which govern the operation of the regulated facility including having the explicit or implicit duty of making major capital investment recommendations, and initiating and directing other comprehensive measures to assure long term environmental compliance with environmental laws and regulations; the manager can ensure that the necessary systems are established or actions taken to gather complete and accurate information for permit application requirements; and where authority to sign documents has been assigned or delegated to the manager in accordance with corporate procedures;
- b. For a partnership or sole proprietorship these forms shall be signed by a general partner or the proprietor, respectively; or
- c. For a municipality, State, Federal, or other public agency these forms shall be signed by either a principal executive officer or ranking elected official. For purposes of this section, a principal executive officer of a Federal agency includes:
 - (i) the chief executive officer of the agency, or
 - (ii) a senior executive officer having responsibility for the overall operations of a principal geographic unit of the agency (e.g., Regional Administrators of EPA).
- 2. The SWPPP and other information requested by the Department shall be signed by a person described in Part VII.H.1. of this permit or by a duly authorized representative of that person. A person is a duly authorized representative only if:
 - The authorization is made in writing by a person described in Part VII.H.1.
 of this permit;
 - b. The authorization specifies either an individual or a position having responsibility for the overall operation of the regulated facility or activity, such as the position of plant manager, operator of a well or a well field,

superintendent, position of *equivalent* responsibility, or an individual or position having overall responsibility for environmental matters for the company. (A duly authorized representative may thus be either a named individual or any individual occupying a named position) and,

- c. The written authorization shall include the name, title and signature of the authorized representative and be attached to the SWPPP.
- 3. All inspection reports shall be signed by the *qualified inspector* that performs the inspection.
- 4. The MS4 SWPPP Acceptance form shall be signed by the principal executive officer or ranking elected official from the *regulated, traditional land use control MS4*, or by a duly authorized representative of that person.

It shall constitute a permit violation if an incorrect and/or improper signatory authorizes any required forms, SWPPP and/or inspection reports.

I. Property Rights

The issuance of this permit does not convey any property rights of any sort, nor any exclusive privileges, nor does it authorize any injury to private property nor any invasion of personal rights, nor any infringement of Federal, State or local laws or regulations. *Owners or operators* must obtain any applicable conveyances, easements, licenses and/or access to real property prior to *commencing construction activity*.

J. Severability

The provisions of this permit are severable, and if any provision of this permit, or the application of any provision of this permit to any circumstance, is held invalid, the application of such provision to other circumstances, and the remainder of this permit shall not be affected thereby.

K. Requirement to Obtain Coverage Under an Alternative Permit

1. The Department may require any owner or operator authorized by this permit to apply for and/or obtain either an individual SPDES permit or another SPDES general permit. When the Department requires any discharger authorized by a general permit to apply for an individual SPDES permit, it shall notify the discharger in writing that a permit application is required. This notice shall

include a brief statement of the reasons for this decision, an application form, a statement setting a time frame for the owner or operator to file the application for an individual SPDES permit, and a deadline, not sooner than 180 days from owner or operator receipt of the notification letter, whereby the authorization to discharge under this general permit shall be terminated. Applications must be submitted to the appropriate Permit Administrator at the Regional Office. The Department may grant additional time upon demonstration, to the satisfaction of the Department, that additional time to apply for an alternative authorization is necessary or where the Department has not provided a permit determination in accordance with Part 621 of this Title.

2. When an individual SPDES permit is issued to a discharger authorized to discharge under a general SPDES permit for the same discharge(s), the general permit authorization for outfalls authorized under the individual SPDES permit is automatically terminated on the effective date of the individual permit unless termination is earlier in accordance with 6 NYCRR Part 750.

L. Proper Operation and Maintenance

The *owner or operator* shall at all times properly operate and maintain all facilities and systems of treatment and control (and related appurtenances) which are installed or used by the *owner or operator* to achieve compliance with the conditions of this permit and with the requirements of the SWPPP.

M. Inspection and Entry

The *owner or operator* shall allow an authorized representative of the Department, EPA, applicable county health department, or, in the case of a *construction site* which *discharges* through an *MS4*, an authorized representative of the *MS4* receiving the discharge, upon the presentation of credentials and other documents as may be required by law, to:

- Enter upon the owner's or operator's premises where a regulated facility or activity is located or conducted or where records must be kept under the conditions of this permit;
- 2. Have access to and copy at reasonable times, any records that must be kept under the conditions of this permit; and

- Inspect at reasonable times any facilities or equipment (including monitoring and control equipment), practices or operations regulated or required by this permit.
- 4. Sample or monitor at reasonable times, for purposes of assuring permit compliance or as otherwise authorized by the Act or ECL, any substances or parameters at any location.

N. Permit Actions

This permit may, at any time, be modified, suspended, revoked, or renewed by the Department in accordance with 6 NYCRR Part 621. The filing of a request by the *owner or operator* for a permit modification, revocation and reissuance, termination, a notification of planned changes or anticipated noncompliance does not limit, diminish and/or stay compliance with any terms of this permit.

O. Definitions

Definitions of key terms are included in Appendix A of this permit.

P. Re-Opener Clause

- 1. If there is evidence indicating potential or realized impacts on water quality due to any stormwater discharge associated with construction activity covered by this permit, the owner or operator of such discharge may be required to obtain an individual permit or alternative general permit in accordance with Part VII.K. of this permit or the permit may be modified to include different limitations and/or requirements.
- Any Department initiated permit modification, suspension or revocation will be conducted in accordance with 6 NYCRR Part 621, 6 NYCRR 750-1.18, and 6 NYCRR 750-1.20.

Q. Penalties for Falsification of Forms and Reports

In accordance with 6NYCRR Part 750-2.4 and 750-2.5, any person who knowingly makes any false material statement, representation, or certification in any application, record, report or other document filed or required to be maintained under this permit, including reports of compliance or noncompliance shall, upon conviction, be punished in accordance with ECL §71-1933 and or Articles 175 and 210 of the New York State Penal Law.

R. Other Permits

Nothing in this permit relieves the *owner or operator* from a requirement to obtain any other permits required by law.

APPENDIX A – Acronyms and Definitions

Acronyms

APO - Agency Preservation Officer

BMP - Best Management Practice

CPESC - Certified Professional in Erosion and Sediment Control

Cpv – Channel Protection Volume

CWA – Clean Water Act (or the Federal Water Pollution Control Act, 33 U.S.C. §1251 et seq)

DOW - Division of Water

EAF – Environmental Assessment Form

ECL - Environmental Conservation Law

EPA – U. S. Environmental Protection Agency

HSG – Hydrologic Soil Group

MS4 – Municipal Separate Storm Sewer System

NOI – Notice of Intent

NOT – Notice of Termination

NPDES - National Pollutant Discharge Elimination System

OPRHP - Office of Parks, Recreation and Historic Places

Qf – Extreme Flood

Qp - Overbank Flood

RRv - Runoff Reduction Volume

RWE – Regional Water Engineer

SEQR - State Environmental Quality Review

SEQRA - State Environmental Quality Review Act

SHPA – State Historic Preservation Act

SPDES – State Pollutant Discharge Elimination System

SWPPP - Stormwater Pollution Prevention Plan

TMDL - Total Maximum Daily Load

UPA – Uniform Procedures Act

USDA - United States Department of Agriculture

WQv - Water Quality Volume

Definitions

All definitions in this section are solely for the purposes of this permit.

Agricultural Building – a structure designed and constructed to house farm implements, hay, grain, poultry, livestock or other horticultural products; excluding any structure designed, constructed or used, in whole or in part, for human habitation, as a

structure designed, constructed or used, in whole or in part, for human habitation, as a place of employment where agricultural products are processed, treated or packaged, or as a place used by the public.

Agricultural Property –means the land for construction of a barn, *agricultural building*, silo, stockyard, pen or other structural practices identified in Table II in the "Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State" prepared by the Department in cooperation with agencies of New York Nonpoint Source Coordinating Committee (dated June 2007).

Alter Hydrology from Pre to Post-Development Conditions - means the post-development peak flow rate(s) has increased by more than 5% of the pre-developed condition for the design storm of interest (e.g. 10 yr and 100 yr).

Combined Sewer - means a sewer that is designed to collect and convey both "sewage" and "stormwater".

Commence (Commencement of) Construction Activities - means the initial disturbance of soils associated with clearing, grading or excavation activities; or other construction related activities that disturb or expose soils such as demolition, stockpiling of fill material, and the initial installation of erosion and sediment control practices required in the SWPPP. See definition for "Construction Activity(ies)" also.

Construction Activity(ies) - means any clearing, grading, excavation, filling, demolition or stockpiling activities that result in soil disturbance. Clearing activities can include, but are not limited to, logging equipment operation, the cutting and skidding of trees, stump removal and/or brush root removal. Construction activity does not include routine maintenance that is performed to maintain the original line and grade, hydraulic capacity, or original purpose of a facility.

Construction Site – means the land area where *construction activity(ies)* will occur. See definition for "*Commence (Commencement of) Construction Activities*" and "*Larger Common Plan of Development or Sale*" also.

Dewatering – means the act of draining rainwater and/or groundwater from building foundations, vaults or excavations/trenches.

Direct Discharge (to a specific surface waterbody) - means that runoff flows from a *construction site* by overland flow and the first point of discharge is the specific surface waterbody, or runoff flows from a *construction site* to a separate storm sewer system

and the first point of discharge from the separate storm sewer system is the specific surface waterbody.

Discharge(s) - means any addition of any pollutant to waters of the State through an outlet or *point source*.

Embankment –means an earthen or rock slope that supports a road/highway.

Endangered or Threatened Species – see 6 NYCRR Part 182 of the Department's rules and regulations for definition of terms and requirements.

Environmental Conservation Law (ECL) - means chapter 43-B of the Consolidated Laws of the State of New York, entitled the Environmental Conservation Law.

Equivalent (Equivalence) – means that the practice or measure meets all the performance, longevity, maintenance, and safety objectives of the technical standard and will provide an equal or greater degree of water quality protection.

Final Stabilization - means that all soil disturbance activities have ceased and a uniform, perennial vegetative cover with a density of eighty (80) percent over the entire pervious surface has been established; or other equivalent stabilization measures, such as permanent landscape mulches, rock rip-rap or washed/crushed stone have been applied on all disturbed areas that are not covered by permanent structures, concrete or pavement.

General SPDES permit - means a SPDES permit issued pursuant to 6 NYCRR Part 750-1.21 and Section 70-0117 of the ECL authorizing a category of discharges.

Groundwater(s) - means waters in the saturated zone. The saturated zone is a subsurface zone in which all the interstices are filled with water under pressure greater than that of the atmosphere. Although the zone may contain gas-filled interstices or interstices filled with fluids other than water, it is still considered saturated.

Historic Property – means any building, structure, site, object or district that is listed on the State or National Registers of Historic Places or is determined to be eligible for listing on the State or National Registers of Historic Places.

Impervious Area (Cover) - means all impermeable surfaces that cannot effectively infiltrate rainfall. This includes paved, concrete and gravel surfaces (i.e. parking lots, driveways, roads, runways and sidewalks); building rooftops and miscellaneous impermeable structures such as patios, pools, and sheds.

Infeasible – means not technologically possible, or not economically practicable and achievable in light of best industry practices.

Larger Common Plan of Development or Sale - means a contiguous area where multiple separate and distinct *construction activities* are occurring, or will occur, under one plan. The term "plan" in "larger common plan of development or sale" is broadly defined as any announcement or piece of documentation (including a sign, public notice or hearing, marketing plan, advertisement, drawing, permit application, State Environmental Quality Review Act (SEQRA) environmental assessment form or other documents, zoning request, computer design, etc.) or physical demarcation (including boundary signs, lot stakes, surveyor markings, etc.) indicating that *construction activities* may occur on a specific plot.

For discrete construction projects that are located within a larger common plan of development or sale that are at least 1/4 mile apart, each project can be treated as a separate plan of development or sale provided any interconnecting road, pipeline or utility project that is part of the same "common plan" is not concurrently being disturbed.

Minimize – means reduce and/or eliminate to the extent achievable using control measures (including best management practices) that are technologically available and economically practicable and achievable in light of best industry practices.

Municipal Separate Storm Sewer (MS4) - a conveyance or system of conveyances (including roads with drainage systems, municipal streets, catch basins, curbs, gutters, ditches, man-made channels, or storm drains):

- (i) Owned or operated by a State, city, town, borough, county, parish, district, association, or other public body (created by or pursuant to State law) having jurisdiction over disposal of sewage, industrial wastes, stormwater, or other wastes, including special districts under State law such as a sewer district, flood control district or drainage district, or similar entity, or an Indian tribe or an authorized Indian tribal organization, or a designated and approved management agency under section 208 of the CWA that discharges to surface waters of the State;
- (ii) Designed or used for collecting or conveying stormwater;
- (iii) Which is not a combined sewer; and
- (iv) Which is not part of a Publicly Owned Treatment Works (POTW) as defined at 40 CFR 122.2.

National Pollutant Discharge Elimination System (NPDES) - means the national system for the issuance of wastewater and stormwater permits under the Federal Water Pollution Control Act (Clean Water Act).

Natural Buffer –means an undisturbed area with natural cover running along a surface water (e.g. wetland, stream, river, lake, etc.).

New Development – means any land disturbance that does not meet the definition of Redevelopment Activity included in this appendix.

New York State Erosion and Sediment Control Certificate Program – a certificate program that establishes and maintains a process to identify and recognize individuals who are capable of developing, designing, inspecting and maintaining erosion and sediment control plans on projects that disturb soils in New York State. The certificate program is administered by the New York State Conservation District Employees Association.

NOI Acknowledgment Letter - means the letter that the Department sends to an owner or operator to acknowledge the Department's receipt and acceptance of a complete Notice of Intent. This letter documents the owner's or operator's authorization to discharge in accordance with the general permit for stormwater discharges from *construction activity*.

Nonpoint Source - means any source of water pollution or pollutants which is not a discrete conveyance or *point source* permitted pursuant to Title 7 or 8 of Article 17 of the Environmental Conservation Law (see ECL Section 17-1403).

Overbank –means flow events that exceed the capacity of the stream channel and spill out into the adjacent floodplain.

Owner or Operator - means the person, persons or legal entity which owns or leases the property on which the *construction activity* is occurring; an entity that has operational control over the construction plans and specifications, including the ability to make modifications to the plans and specifications; and/or an entity that has day-to-day operational control of those activities at a project that are necessary to ensure compliance with the permit conditions.

Performance Criteria – means the design criteria listed under the "Required Elements" sections in Chapters 5, 6 and 10 of the technical standard, New York State Stormwater Management Design Manual, dated January 2015. It does not include the Sizing Criteria (i.e. WQv, RRv, Cpv, Qp and Qf) in Part I.C.2. of the permit.

Point Source - means any discernible, confined and discrete conveyance, including but not limited to any pipe, ditch, channel, tunnel, conduit, well, discrete fissure, container, rolling stock, concentrated animal feeding operation, vessel or other floating craft, or landfill leachate collection system from which *pollutants* are or may be discharged.

Pollutant - means dredged spoil, filter backwash, solid waste, incinerator residue, sewage, garbage, sewage sludge, munitions, chemical wastes, biological materials, radioactive materials, heat, wrecked or discarded equipment, rock, sand and industrial, municipal, agricultural waste and ballast discharged into water; which may cause or might reasonably be expected to cause pollution of the waters of the state in contravention of the standards or guidance values adopted as provided in 6 NYCRR Parts 700 et seq.

Qualified Inspector - means a person that is knowledgeable in the principles and practices of erosion and sediment control, such as a licensed Professional Engineer, Certified Professional in Erosion and Sediment Control (CPESC), Registered Landscape Architect, New York State Erosion and Sediment Control Certificate Program holder or other Department endorsed individual(s).

It can also mean someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided that person has training in the principles and practices of erosion and sediment control. Training in the principles and practices of erosion and sediment control means that the individual working under the direct supervision of the licensed Professional Engineer or Registered Landscape Architect has received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity. After receiving the initial training, the individual working under the direct supervision of the licensed Professional Engineer or Registered Landscape Architect shall receive four (4) hours of training every three (3) years.

It can also mean a person that meets the *Qualified Professional* qualifications in addition to the *Qualified Inspector* qualifications.

Note: Inspections of any post-construction stormwater management practices that include structural components, such as a dam for an impoundment, shall be performed by a licensed Professional Engineer.

Qualified Professional - means a person that is knowledgeable in the principles and practices of stormwater management and treatment, such as a licensed Professional Engineer, Registered Landscape Architect or other Department endorsed individual(s). Individuals preparing SWPPPs that require the post-construction stormwater management practice component must have an understanding of the principles of hydrology, water quality management practice design, water quantity control design, and, in many cases, the principles of hydraulics. All components of the SWPPP that involve the practice of engineering, as defined by the NYS Education Law (see Article 145), shall be prepared by, or under the direct supervision of, a professional engineer licensed to practice in the State of New York.

Redevelopment Activity(ies) – means the disturbance and reconstruction of existing impervious area, including impervious areas that were removed from a project site within five (5) years of preliminary project plan submission to the local government (i.e. site plan, subdivision, etc.).

Regulated, Traditional Land Use Control MS4 - means a city, town or village with land use control authority that is authorized to discharge under New York State DEC's

SPDES General Permit For Stormwater Discharges from Municipal Separate Stormwater Sewer Systems (MS4s) or the City of New York's Individual SPDES Permit for their Municipal Separate Storm Sewer Systems (NY-0287890).

Routine Maintenance Activity - means *construction activity* that is performed to maintain the original line and grade, hydraulic capacity, or original purpose of a facility, including, but not limited to:

- Re-grading of gravel roads or parking lots,
- Cleaning and shaping of existing roadside ditches and culverts that maintains the approximate original line and grade, and hydraulic capacity of the ditch,
- Cleaning and shaping of existing roadside ditches that does not maintain the approximate original grade, hydraulic capacity and purpose of the ditch if the changes to the line and grade, hydraulic capacity or purpose of the ditch are installed to improve water quality and quantity controls (e.g. installing grass lined ditch).
- Placement of aggregate shoulder backing that stabilizes the transition between the road shoulder and the ditch or *embankment*,
- Full depth milling and filling of existing asphalt pavements, replacement of concrete pavement slabs, and similar work that does not expose soil or disturb the bottom six (6) inches of subbase material.
- Long-term use of equipment storage areas at or near highway maintenance facilities.
- Removal of sediment from the edge of the highway to restore a previously existing sheet-flow drainage connection from the highway surface to the highway ditch or embankment,
- Existing use of Canal Corp owned upland disposal sites for the canal, and
- Replacement of curbs, gutters, sidewalks and guide rail posts.

Site limitations – means site conditions that prevent the use of an infiltration technique and or infiltration of the total WQv. Typical site limitations include: seasonal high groundwater, shallow depth to bedrock, and soils with an infiltration rate less than 0.5 inches/hour. The existence of site limitations shall be confirmed and documented using actual field testing (i.e. test pits, soil borings, and infiltration test) or using information from the most current United States Department of Agriculture (USDA) Soil Survey for the County where the project is located.

Sizing Criteria – means the criteria included in Part I.C.2 of the permit that are used to size post-construction stormwater management control practices. The criteria include; Water Quality Volume (WQv), Runoff Reduction Volume (RRv), Channel Protection Volume (Cpv), *Overbank* Flood (Qp), and Extreme Flood (Qf).

State Pollutant Discharge Elimination System (SPDES) - means the system established pursuant to Article 17 of the ECL and 6 NYCRR Part 750 for issuance of permits authorizing discharges to the waters of the state.

Steep Slope – means land area designated on the current United States Department of Agriculture ("USDA") Soil Survey as Soil Slope Phase "D", (provided the map unit name is inclusive of slopes greater than 25%), or Soil Slope Phase E or F, (regardless of the map unit name), or a combination of the three designations.

Streambank – as used in this permit, means the terrain alongside the bed of a creek or stream. The bank consists of the sides of the channel, between which the flow is confined.

Stormwater Pollution Prevention Plan (SWPPP) – means a project specific report, including construction drawings, that among other things: describes the construction activity(ies), identifies the potential sources of pollution at the *construction site*; describes and shows the stormwater controls that will be used to control the pollutants (i.e. erosion and sediment controls; for many projects, includes post-construction stormwater management controls); and identifies procedures the *owner or operator* will implement to comply with the terms and conditions of the permit. See Part III of the permit for a complete description of the information that must be included in the SWPPP.

Surface Waters of the State - shall be construed to include lakes, bays, sounds, ponds, impounding reservoirs, springs, rivers, streams, creeks, estuaries, marshes, inlets, canals, the Atlantic ocean within the territorial seas of the state of New York and all other bodies of surface water, natural or artificial, inland or coastal, fresh or salt, public or private (except those private waters that do not combine or effect a junction with natural surface waters), which are wholly or partially within or bordering the state or within its jurisdiction. Waters of the state are further defined in 6 NYCRR Parts 800 to 941.

Temporarily Ceased – means that an existing disturbed area will not be disturbed again within 14 calendar days of the previous soil disturbance.

Temporary Stabilization - means that exposed soil has been covered with material(s) as set forth in the technical standard, New York Standards and Specifications for Erosion and Sediment Control, to prevent the exposed soil from eroding. The materials can include, but are not limited to, mulch, seed and mulch, and erosion control mats (e.g. jute twisted yarn, excelsior wood fiber mats).

Total Maximum Daily Loads (TMDLs) - A TMDL is the sum of the allowable loads of a single pollutant from all contributing point and *nonpoint sources*. It is a calculation of the maximum amount of a pollutant that a waterbody can receive on a daily basis and still meet *water quality standards*, and an allocation of that amount to the pollutant's sources. A TMDL stipulates wasteload allocations (WLAs) for *point source* discharges, load allocations (LAs) for *nonpoint sources*, and a margin of safety (MOS).

Trained Contractor - means an employee from the contracting (construction) company, identified in Part III.A.6., that has received four (4) hours of Department endorsed

training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity. After receiving the initial training, the *trained contractor* shall receive four (4) hours of training every three (3) years.

It can also mean an employee from the contracting (construction) company, identified in Part III.A.6., that meets the *qualified inspector* qualifications (e.g. licensed Professional Engineer, Certified Professional in Erosion and Sediment Control (CPESC), Registered Landscape Architect, New York State Erosion and Sediment Control Certificate Program holder, or someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided they have received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity).

The *trained contractor* is responsible for the day to day implementation of the SWPPP.

Uniform Procedures Act (UPA) Permit - means a permit required under 6 NYCRR Part 621 of the Environmental Conservation Law (ECL), Article 70.

Water Quality Standard - means such measures of purity or quality for any waters in relation to their reasonable and necessary use as promulgated in 6 NYCRR Part 700 et seq.

APPENDIX B – Required SWPPP Components by Project Type

Table 1 Construction Activities that Require the Preparation of a SWPPP That Only Includes Erosion and Sediment Controls

The following construction activities that involve soil disturbances of one (1) or more acres of land, but less than five (5) acres:

- Single family home <u>not</u> located in one of the watersheds listed in Appendix C or <u>not</u> *directly discharging* to one of the 303(d) segments listed in Appendix E
- Single family residential subdivisions with 25% or less impervious cover at total site build-out and <u>not</u> located in one of the watersheds listed in Appendix C and <u>not</u> directly discharging to one of the 303(d) segments listed in Appendix E
- Construction of a barn or other agricultural building, silo, stock yard or pen.

The following construction activities that involve soil disturbances between five thousand (5000) square feet and one (1) acre of land:

All construction activities located in the watersheds identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.

- Installation of underground, linear utilities; such as gas lines, fiber-optic cable, cable TV, electric, telephone, sewer mains, and water mains
- Environmental enhancement projects, such as wetland mitigation projects, stormwater retrofits and stream restoration projects
- · Pond construction
- Linear bike paths running through areas with vegetative cover, including bike paths surfaced with an impervious cover
- · Cross-country ski trails and walking/hiking trails
- Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are not part of residential, commercial or institutional development;
- Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that include incidental shoulder or curb work along an existing highway to support construction of the sidewalk, bike path or walking path.
- · Slope stabilization projects
- Slope flattening that changes the grade of the site, but does not significantly change the runoff characteristics

Table 1 (Continued) Construction Activities that Require the Preparation of a SWPPP

THAT ONLY INCLUDES EROSION AND SEDIMENT CONTROLS

- · Spoil areas that will be covered with vegetation
- Vegetated open space projects (i.e. recreational parks, lawns, meadows, fields, downhill ski trails) excluding projects that alter hydrology from pre to post development conditions,
- Athletic fields (natural grass) that do not include the construction or reconstruction of *impervious* area and do not alter hydrology from pre to post development conditions
- Demolition project where vegetation will be established, and no redevelopment is planned
- Overhead electric transmission line project that does not include the construction of permanent access roads or parking areas surfaced with *impervious cover*
- Structural practices as identified in Table II in the "Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State", excluding projects that involve soil disturbances of greater than five acres and construction activities that include the construction or reconstruction of impervious area
- Temporary access roads, median crossovers, detour roads, lanes, or other temporary impervious areas that will be restored to pre-construction conditions once the construction activity is complete

Table 2

CONSTRUCTION ACTIVITIES THAT REQUIRE THE PREPARATION OF A SWPPP THAT INCLUDES POST-CONSTRUCTION STORMWATER MANAGEMENT PRACTICES

- Single family home located in one of the watersheds listed in Appendix C or directly discharging to one of the 303(d) segments listed in Appendix E
- · Single family home that disturbs five (5) or more acres of land
- Single family residential subdivisions located in one of the watersheds listed in Appendix C or directly discharging to one of the 303(d) segments listed in Appendix E
- Single family residential subdivisions that involve soil disturbances of between one (1) and five (5) acres of land with greater than 25% impervious cover at total site build-out
- Single family residential subdivisions that involve soil disturbances of five (5) or more acres of land, and single family residential subdivisions that involve soil disturbances of less than five (5) acres that are part of a larger common plan of development or sale that will ultimately disturb five or more acres of land
- Multi-family residential developments; includes duplexes, townhomes, condominiums, senior housing complexes, apartment complexes, and mobile home parks
- Airports
- Amusement parks
- · Breweries, cideries, and wineries, including establishments constructed on agricultural land
- Campgrounds
- Cemeteries that include the construction or reconstruction of impervious area (>5% of disturbed area) or alter the hydrology from pre to post development conditions
- · Commercial developments
- Churches and other places of worship
- Construction of a barn or other *agricultural building* (e.g. silo) and structural practices as identified in Table II in the "Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State" that include the construction or reconstruction of *impervious area*, excluding projects that involve soil disturbances of less than five acres.
- · Golf courses
- · Institutional development; includes hospitals, prisons, schools and colleges
- · Industrial facilities; includes industrial parks
- Landfills
- Municipal facilities; includes highway garages, transfer stations, office buildings, POTW's, water treatment plants, and water storage tanks
- Office complexes
- · Playgrounds that include the construction or reconstruction of impervious area
- Sports complexes
- Racetracks; includes racetracks with earthen (dirt) surface
- Road construction or reconstruction, including roads constructed as part of the construction activities listed in Table 1

Table 2 (Continued)

CONSTRUCTION ACTIVITIES THAT REQUIRE THE PREPARATION OF A SWPPP THAT INCLUDES POST-CONSTRUCTION STORMWATER MANAGEMENT PRACTICES

- Parking lot construction or reconstruction, including parking lots constructed as part of the construction activities listed in Table 1
- Athletic fields (natural grass) that include the construction or reconstruction of impervious area (>5% of disturbed area) or alter the hydrology from pre to post development conditions
- Athletic fields with artificial turf
- Permanent access roads, parking areas, substations, compressor stations and well drilling pads, surfaced with *impervious cover*, and constructed as part of an over-head electric transmission line project, wind-power project, cell tower project, oil or gas well drilling project, sewer or water main project or other linear utility project
- Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are part of a residential, commercial or institutional development
- Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are part of a highway construction or reconstruction project
- All other construction activities that include the construction or reconstruction of *impervious area* or alter the hydrology from pre to post development conditions, and are not listed in Table 1

APPENDIX C – Watersheds Requiring Enhanced Phosphorus Removal

Watersheds where *owners or operators* of construction activities identified in Table 2 of Appendix B must prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the Enhanced Phosphorus Removal Standards included in the technical standard, New York State Stormwater Management Design Manual ("Design Manual").

- Entire New York City Watershed located east of the Hudson River Figure 1
- Onondaga Lake Watershed Figure 2
- Greenwood Lake Watershed -Figure 3
- Oscawana Lake Watershed Figure 4
- Kinderhook Lake Watershed Figure 5

Figure 1 - New York City Watershed East of the Hudson

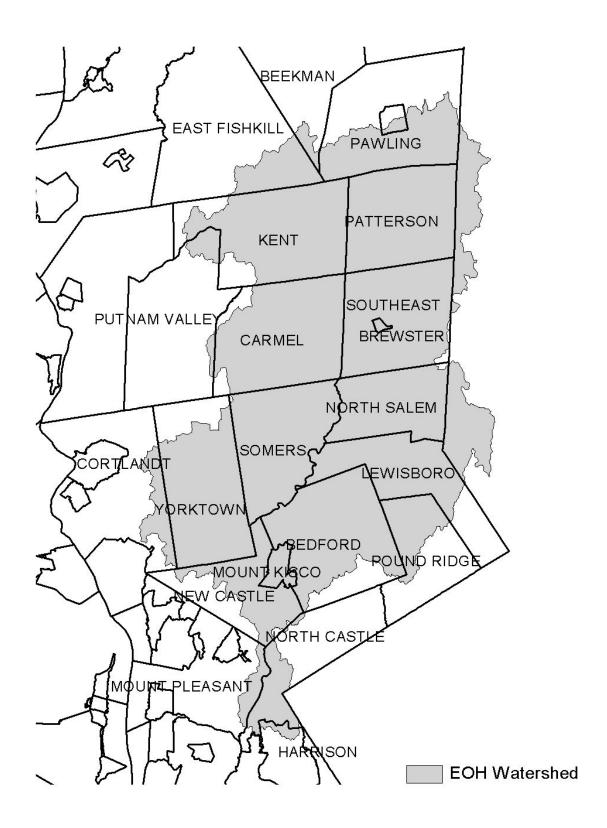


Figure 2 - Onondaga Lake Watershed



Figure 3 - Greenwood Lake Watershed

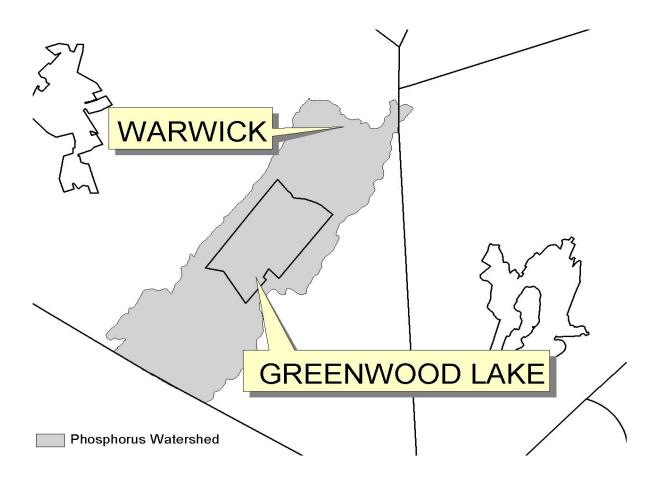


Figure 4 - Oscawana Lake Watershed

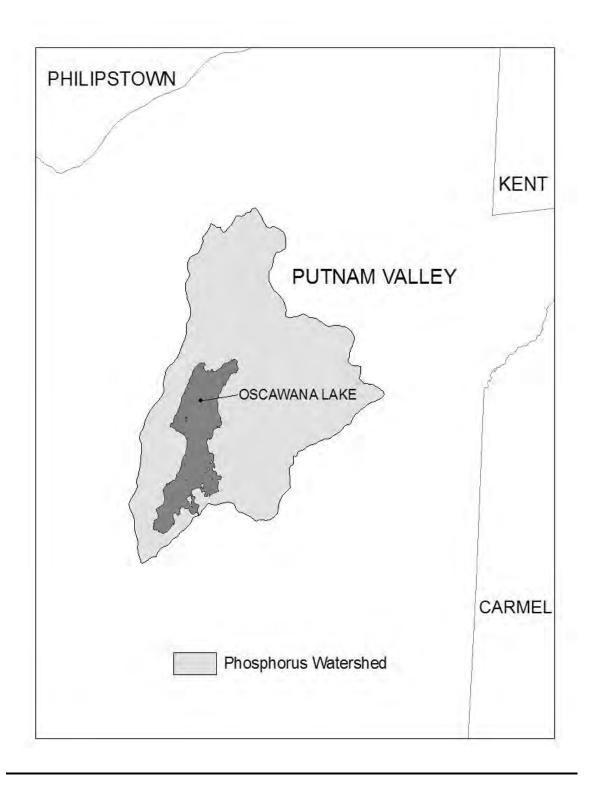
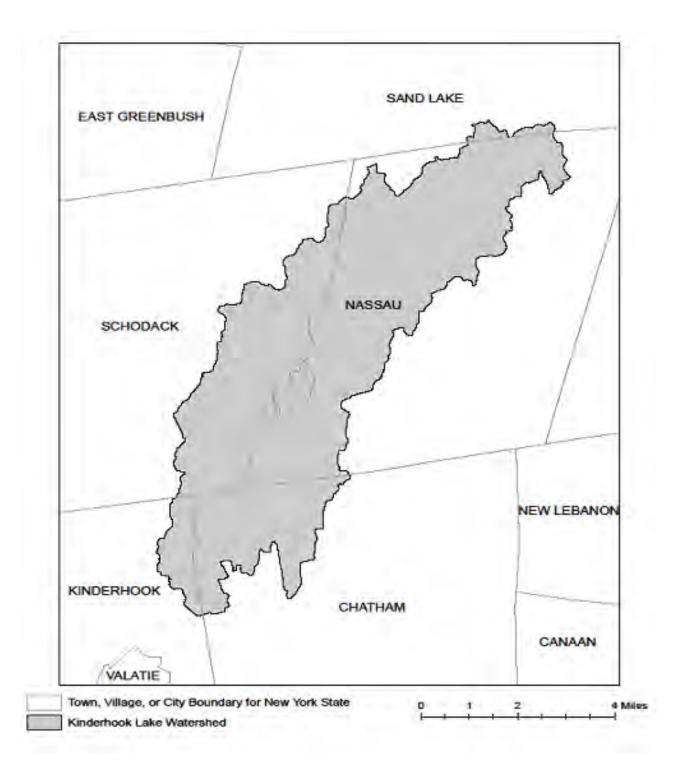


Figure 5 - Kinderhook Lake Watershed



APPENDIX D – Watersheds with Lower Disturbance Threshold

Watersheds where *owners or operators* of construction activities that involve soil disturbances between five thousand (5000) square feet and one (1) acre of land must obtain coverage under this permit.

Entire New York City Watershed that is located east of the Hudson River - See Figure 1 in Appendix C

APPENDIX E – 303(d) Segments Impaired by Construction Related Pollutant(s)

List of 303(d) segments impaired by pollutants related to *construction activity* (e.g. silt, sediment or nutrients). The list was developed using "The Final New York State 2016 Section 303(d) List of Impaired Waters Requiring a TMDL/Other Strategy" dated November 2016. *Owners or operators* of single family home and single family residential subdivisions with 25% or less total impervious cover at total site build-out that involve soil disturbances of one or more acres of land, but less than 5 acres, and *directly discharge* to one of the listed segments below shall prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the New York State Stormwater Management Design Manual ("Design Manual"), dated January 2015.

COUNTY	WATERBODY	POLLUTANT
Albany	Ann Lee (Shakers) Pond, Stump Pond	Nutrients
Albany	Basic Creek Reservoir Nutrients	
Allegany	Amity Lake, Saunders Pond Nutrients	
Bronx	Long Island Sound, Bronx Nutrients	
Bronx	Van Cortlandt Lake	Nutrients
Broome	Fly Pond, Deer Lake, Sky Lake	Nutrients
Broome	Minor Tribs to Lower Susquehanna (north)	Nutrients
Broome	Whitney Point Lake/Reservoir	Nutrients
Cattaraugus	Allegheny River/Reservoir	Nutrients
Cattaraugus	Beaver (Alma) Lake	Nutrients
Cattaraugus	Case Lake	Nutrients
Cattaraugus	Linlyco/Club Pond	Nutrients
Cayuga	Duck Lake	Nutrients
Cayuga	Little Sodus Bay Nutrien	
Chautauqua	Bear Lake	Nutrients
Chautauqua	qua Chadakoin River and tribs Nutrients	
Chautauqua	Chautauqua Chautauqua Lake, North Nutrien	
Chautauqua	Chautauqua Lake, South	Nutrients
Chautauqua	Findley Lake	Nutrients
Chautauqua	Hulburt/Clymer Pond	Nutrients
Clinton	Great Chazy River, Lower, Main Stem	Silt/Sediment
Clinton	Lake Champlain, Main Lake, Middle	Nutrients
Clinton	Lake Champlain, Main Lake, North	Nutrients
Columbia		
Columbia	Robinson Pond	Nutrients
Cortland	tland Dean Pond Nutrients	

Dutchess	Fall Kill and tribs	Nutrients
Dutchess	Hillside Lake Nutrients	
Dutchess	Wappingers Lake	Nutrients
Dutchess	Wappingers Lake Silt/Sedime	
Erie	Beeman Creek and tribs Nutrients	
Erie	Ellicott Creek, Lower, and tribs	Silt/Sediment
Erie	Ellicott Creek, Lower, and tribs	Nutrients
Erie	Green Lake	Nutrients
Erie	Little Sister Creek, Lower, and tribs	Nutrients
Erie	Murder Creek, Lower, and tribs	Nutrients
Erie	Rush Creek and tribs	Nutrients
Erie	Scajaquada Creek, Lower, and tribs	Nutrients
Erie	Scajaquada Creek, Middle, and tribs	Nutrients
Erie	Scajaquada Creek, Upper, and tribs	Nutrients
Erie	South Branch Smoke Cr, Lower, and tribs	Silt/Sediment
Erie	South Branch Smoke Cr, Lower, and tribs	Nutrients
Essex	Lake Champlain, Main Lake, South	Nutrients
Essex	Lake Champlain, South Lake	Nutrients
Essex	Willsboro Bay	Nutrients
Genesee	Bigelow Creek and tribs	Nutrients
Genesee	Black Creek, Middle, and minor tribs	Nutrients
Genesee	Black Creek, Upper, and minor tribs	Nutrients
Genesee	Bowen Brook and tribs	Nutrients
Genesee	LeRoy Reservoir	Nutrients
Genesee	Oak Orchard Cr, Upper, and tribs	Nutrients
Genesee	Tonawanda Creek, Middle, Main Stem	Nutrients
Greene	Schoharie Reservoir	Silt/Sediment
Greene	Sleepy Hollow Lake	Silt/Sediment
Herkimer	Steele Creek tribs	Silt/Sediment
Herkimer	Steele Creek tribs	Nutrients
Jefferson	Moon Lake	Nutrients
Kings	Hendrix Creek Nutrients	
Kings	Prospect Park Lake	Nutrients
Lewis	Mill Creek/South Branch, and tribs	Nutrients
Livingston	Christie Creek and tribs	Nutrients
Livingston	Conesus Lake	Nutrients
Livingston	Mill Creek and minor tribs Silt/Sedimen	
Monroe	Black Creek, Lower, and minor tribs Nutrients	
Monroe	Buck Pond	Nutrients
Monroe	Cranberry Pond	Nutrients

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Monroe	Lake Ontario Shoreline, Western	Nutrients
Monroe	Long Pond Nutrients	
Monroe	Mill Creek and tribs	Nutrients
Monroe	Mill Creek/Blue Pond Outlet and tribs	Nutrients
Monroe	Minor Tribs to Irondequoit Bay	Nutrients
Monroe	Rochester Embayment - East	Nutrients
Monroe	Rochester Embayment - West	Nutrients
Monroe	Shipbuilders Creek and tribs	Nutrients
Monroe	Thomas Creek/White Brook and tribs	Nutrients
Nassau	Beaver Lake	Nutrients
Nassau	Camaans Pond	Nutrients
Nassau	East Meadow Brook, Upper, and tribs	Silt/Sediment
Nassau	East Rockaway Channel	Nutrients
Nassau	Grant Park Pond	Nutrients
Nassau	Hempstead Bay	Nutrients
Nassau	Hempstead Lake	Nutrients
Nassau	Hewlett Bay	Nutrients
Nassau	Hog Island Channel	Nutrients
Nassau	Long Island Sound, Nassau County Waters	Nutrients
Nassau	Massapequa Creek and tribs	Nutrients
Nassau	Milburn/Parsonage Creeks, Upp, and tribs	Nutrients
Nassau	Reynolds Channel, west	Nutrients
Nassau	Tidal Tribs to Hempstead Bay	Nutrients
Nassau	Tribs (fresh) to East Bay	Nutrients
Nassau	Tribs (fresh) to East Bay	Silt/Sediment
Nassau	Tribs to Smith/Halls Ponds	Nutrients
Nassau	Woodmere Channel	Nutrients
New York	Harlem Meer	Nutrients
New York	The Lake in Central Park	Nutrients
Niagara	Bergholtz Creek and tribs	Nutrients
Niagara	Hyde Park Lake	Nutrients
Niagara	Lake Ontario Shoreline, Western	Nutrients
Niagara	Lake Ontario Shoreline, Western	Nutrients
Oneida	Ballou, Nail Creeks and tribs	Nutrients
Onondaga	Harbor Brook, Lower, and tribs	Nutrients
Onondaga	Ley Creek and tribs	Nutrients
Onondaga	Minor Tribs to Onondaga Lake	Nutrients
Onondaga	Ninemile Creek, Lower, and tribs	Nutrients
Onondaga	Onondaga Creek, Lower, and tribs	Nutrients
Onondaga	Onondaga Creek, Middle, and tribs	Nutrients
	<u> </u>	1

Onondaga	Onondaga Lake, northern end	Nutrients
Onondaga	Onondaga Lake, southern end Nutrients	
Ontario	Great Brook and minor tribs Silt/Sedime	
Ontario	Great Brook and minor tribs Nutrients	
Ontario	Hemlock Lake Outlet and minor tribs Nutrients	
Ontario	Honeoye Lake	Nutrients
Orange	Greenwood Lake	Nutrients
Orange	Monhagen Brook and tribs	Nutrients
Orange	Orange Lake	Nutrients
Orleans	Lake Ontario Shoreline, Western	Nutrients
Orleans	Lake Ontario Shoreline, Western	Nutrients
Oswego	Lake Neatahwanta	Nutrients
Oswego	Pleasant Lake	Nutrients
Putnam	Bog Brook Reservoir	Nutrients
Putnam	Boyd Corners Reservoir	Nutrients
Putnam	Croton Falls Reservoir	Nutrients
Putnam	Diverting Reservoir	Nutrients
Putnam	East Branch Reservoir	Nutrients
Putnam	Lake Carmel	Nutrients
Putnam	Middle Branch Reservoir	Nutrients
Putnam	Oscawana Lake	Nutrients
Putnam	Palmer Lake	Nutrients
Putnam	West Branch Reservoir	Nutrients
Queens	Bergen Basin	Nutrients
Queens	Flushing Creek/Bay	Nutrients
Queens	Jamaica Bay, Eastern, and tribs (Queens)	Nutrients
Queens	Kissena Lake	Nutrients
Queens	Meadow Lake	Nutrients
Queens	Willow Lake	Nutrients
Rensselaer	Nassau Lake	Nutrients
Rensselaer	Snyders Lake Nutrients	
Richmond	Grasmere Lake/Bradys Pond	Nutrients
Rockland	Congers Lake, Swartout Lake Nutrients	
Rockland	Rockland Lake	Nutrients
Saratoga	Ballston Lake	Nutrients
Saratoga	Dwaas Kill and tribs	Silt/Sediment
Saratoga	Dwaas Kill and tribs	Nutrients
Saratoga	Lake Lonely Nutrients Nutrients	
Saratoga	Round Lake	Nutrients
Saratoga	Tribs to Lake Lonely	Nutrients

Schenectady	Collins Lake	Nutrients
Schenectady	Duane Lake Nutrients	
Schenectady	Mariaville Lake Nutrients	
Schoharie	Engleville Pond Nutrients	
Schoharie	Summit Lake Nutrients	
Seneca	Reeder Creek and tribs Nutrients	
St.Lawrence	Black Lake Outlet/Black Lake	Nutrients
St.Lawrence	Fish Creek and minor tribs	Nutrients
Steuben	Smith Pond	Nutrients
Suffolk	Agawam Lake	Nutrients
Suffolk	Big/Little Fresh Ponds	Nutrients
Suffolk	Canaan Lake	Silt/Sediment
Suffolk	Canaan Lake	Nutrients
Suffolk	Flanders Bay, West/Lower Sawmill Creek	Nutrients
Suffolk	Fresh Pond	Nutrients
Suffolk	Great South Bay, East	Nutrients
Suffolk	Great South Bay, Middle	Nutrients
Suffolk	Great South Bay, West	Nutrients
Suffolk	Lake Ronkonkoma	Nutrients
Suffolk	Long Island Sound, Suffolk County, West	Nutrients
Suffolk	Mattituck (Marratooka) Pond	Nutrients
Suffolk	Meetinghouse/Terrys Creeks and tribs	Nutrients
Suffolk	Mill and Seven Ponds	Nutrients
Suffolk	Millers Pond	Nutrients
Suffolk	Moriches Bay, East	Nutrients
Suffolk	Moriches Bay, West	Nutrients
Suffolk	Peconic River, Lower, and tidal tribs	Nutrients
Suffolk	Quantuck Bay	Nutrients
Suffolk	Shinnecock Bay and Inlet	Nutrients
Suffolk	Tidal tribs to West Moriches Bay Nutrients	
Sullivan	Bodine, Montgomery Lakes Nutrients	
Sullivan	Davies Lake	Nutrients
Sullivan	Evens Lake	Nutrients
Sullivan	Pleasure Lake	Nutrients
Tompkins	Cayuga Lake, Southern End	Nutrients
Tompkins	Cayuga Lake, Southern End	Silt/Sediment
Tompkins	Owasco Inlet, Upper, and tribs Nutrients	
Ulster	Ashokan Reservoir	Silt/Sediment
Ulster	Esopus Creek, Upper, and minor tribs	Silt/Sediment
Warren	Hague Brook and tribs	Silt/Sediment

Warren	Huddle/Finkle Brooks and tribs	Silt/Sediment	
Warren	Indian Brook and tribs		
Warren	Lake George Silt/Sediment		
Warren	Tribs to L.George, Village of L George Silt/Sedime		
Washington	Cossayuna Lake Nutrients		
Washington	Lake Champlain, South Bay	Nutrients	
Washington	Tribs to L.George, East Shore	Silt/Sediment	
Washington	Wood Cr/Champlain Canal and minor tribs	Nutrients	
Wayne	Port Bay	Nutrients	
Westchester	Amawalk Reservoir	Nutrients	
Westchester	Blind Brook, Upper, and tribs	Silt/Sediment	
Westchester	Cross River Reservoir	Nutrients	
Westchester	Lake Katonah	Nutrients	
Westchester	Lake Lincolndale	Nutrients	
Westchester	Lake Meahagh	Nutrients	
Westchester	Lake Mohegan	Nutrients	
Westchester	Lake Shenorock	Nutrients	
Westchester	Long Island Sound, Westchester (East)	Nutrients	
Westchester	Mamaroneck River, Lower	Silt/Sediment	
Westchester	Mamaroneck River, Upper, and minor tribs	Silt/Sediment	
Westchester	Muscoot/Upper New Croton Reservoir	Nutrients	
Westchester	New Croton Reservoir	Nutrients	
Westchester	Peach Lake	Nutrients	
Westchester	Reservoir No.1 (Lake Isle)	Nutrients	
Westchester	Saw Mill River, Lower, and tribs	Nutrients	
Westchester	Saw Mill River, Middle, and tribs	Nutrients	
Westchester	Sheldrake River and tribs	Silt/Sediment	
Westchester	Sheldrake River and tribs	Nutrients	
Westchester	Silver Lake	Nutrients	
Westchester	Teatown Lake	Nutrients	
Westchester	Titicus Reservoir	Nutrients	
Westchester	Truesdale Lake	Nutrients	
Westchester	Wallace Pond	Nutrients	
Wyoming	Java Lake	Nutrients	
Wyoming	Silver Lake	Nutrients	

APPENDIX F – List of NYS DEC Regional Offices

<u>Region</u>	COVERING THE FOLLOWING COUNTIES:	DIVISION OF ENVIRONMENTAL PERMITS (DEP) PERMIT ADMINISTRATORS	DIVISION OF WATER (DOW) WATER (SPDES) PROGRAM
1	NASSAU AND SUFFOLK	50 CIRCLE ROAD STONY BROOK, NY 11790 Tel. (631) 444-0365	50 CIRCLE ROAD STONY BROOK, NY 11790-3409 Tel. (631) 444-0405
2	BRONX, KINGS, NEW YORK, QUEENS AND RICHMOND	1 HUNTERS POINT PLAZA, 47-40 21st St. LONG ISLAND CITY, NY 11101-5407 TEL. (718) 482-4997	1 HUNTERS POINT PLAZA, 47-40 21ST ST. LONG ISLAND CITY, NY 11101-5407 TEL. (718) 482-4933
3	DUTCHESS, ORANGE, PUTNAM, ROCKLAND, SULLIVAN, ULSTER AND WESTCHESTER	21 SOUTH PUTT CORNERS ROAD NEW PALTZ, NY 12561-1696 TEL. (845) 256-3059	100 HILLSIDE AVENUE, SUITE 1W WHITE PLAINS, NY 10603 TEL. (914) 428 - 2505
4	ALBANY, COLUMBIA, DELAWARE, GREENE, MONTGOMERY, OTSEGO, RENSSELAER, SCHENECTADY AND SCHOHARIE	1150 NORTH WESTCOTT ROAD SCHENECTADY, NY 12306-2014 Tel. (518) 357-2069	1130 NORTH WESTCOTT ROAD SCHENECTADY, NY 12306-2014 Tel. (518) 357-2045
5	CLINTON, ESSEX, FRANKLIN, FULTON, HAMILTON, SARATOGA, WARREN AND WASHINGTON	1115 STATE ROUTE 86, Po Box 296 Ray Brook, Ny 12977-0296 Tel. (518) 897-1234	232 GOLF COURSE ROAD WARRENSBURG, NY 12885-1172 TEL. (518) 623-1200
6	HERKIMER, JEFFERSON, LEWIS, ONEIDA AND ST. LAWRENCE	STATE OFFICE BUILDING 317 WASHINGTON STREET WATERTOWN, NY 13601-3787 TEL. (315) 785-2245	STATE OFFICE BUILDING 207 GENESEE STREET UTICA, NY 13501-2885 TEL. (315) 793-2554
7	BROOME, CAYUGA, CHENANGO, CORTLAND, MADISON, ONONDAGA, OSWEGO, TIOGA AND TOMPKINS	615 ERIE BLVD. WEST SYRACUSE, NY 13204-2400 TEL. (315) 426-7438	615 ERIE BLVD. WEST SYRACUSE, NY 13204-2400 TEL. (315) 426-7500
8	CHEMUNG, GENESEE, LIVINGSTON, MONROE, ONTARIO, ORLEANS, SCHUYLER, SENECA, STEUBEN, WAYNE AND YATES	6274 EAST AVON-LIMA ROADAVON, NY 14414-9519 TEL. (585) 226-2466	6274 EAST AVON-LIMA RD. AVON, NY 14414-9519 TEL. (585) 226-2466
9	ALLEGANY, CATTARAUGUS, CHAUTAUQUA, ERIE, NIAGARA AND WYOMING	270 MICHIGAN AVENUE BUFFALO, NY 14203-2999 TEL. (716) 851-7165	270 MICHIGAN AVENUE BUFFALO, NY 14203-2999 TEL. (716) 851-7070

APPENDIX F

NEW YORK STATE HISTORIC PRESERVATION OFFICE (SHPO) "NO EFFECT LETTER"



ANDREW M. CUOMO Governor **ERIK KULLESEID**Commissioner

September 13, 2019

Mr. Andrew Dangler USACE Update Regulatory Field Office 1 Buffington Street Building 10, 3rd Floor North Watervliet, NY 12819

Re: USACE

Albany Port District Commission Industrial Park Project City of Albany, Town of Bethlehem, Albany County, NY 18PR07273

Dear Mr. Dangler:

Thank you for requesting the comments of the New York State Historic Preservation Office (SHPO). We have reviewed the visual simulation and the August 6, 2019 McFarland Johnson letter noting that the proposed building height has changed and could reach 85 feet in accordance with Section 106 of the National Historic Preservation Act of 1966. These comments are those of the SHPO and relate only to Historic/Cultural resources.

The visual simulation of the proposed building shows that the roof will be visible from the National Register eligible Papscanee Island Historic District. As noted in our November 2009 Determination of Eligibility for Papscanee Island, "Papscanee Island is historically and archaeologically significant for its association with the Upper Hudson Valley's predominate native people, the Mohican..."The rich soil along the flats and on Papscanee Island were flooded annually and generations of Mohicans cleared and cultivated these areas."

While some buildings have been introduced into the landscape, these buildings are not directly across from one of the few remaining cultivated areas on the Island. Since only the top of the building will be visible, the SHPO continues to recommend that this undertaking will have **No Adverse Effect** on historic properties with the **condition** that non-reflective, earth toned roofing materials are utilized. Maintaining a non-reflective roof will minimize any visual intrusions and help maintain the agricultural setting of the Papscanee Island Historic District.

If you have any questions, I can be reached at (518) 268-2179.

Sincerely,

Nancy Herter

Many Herter

Archaeology Unit Program Coordinator



KATHY HOCHUL Governor **ERIK KULLESEID**Commissioner

December 9, 2021

Jordan Tate
Environmental Analyst
McFarland Johnson
60 Railroad Place
Suite 402
Saratoga Springs, NY 12866

Re: USACE

Marmen/Welcon Offshore Wind Tower Manufacturing Plant

Town of Bethlehem, Albany County, NY

21PR04693

Dear Jordan Tate:

Thank you for requesting the comments of the New York State Historic Preservation Office (SHPO). We have reviewed the provided documentation in accordance with Section 106 of the National Historic Preservation Act of 1966. These comments are those of the SHPO and relate only to Historic/Cultural resources.

SHPO has reviewed the proposed cut/fill plan and construction depths, and the visual simulation from the Papscanee Island shoreline. We have no archaeological concerns with the proposed ground disturbing activities that will occur during this project. Based on the visual simulation, the SHPO concurs with the Stockbridge Munsee Community (SMC) THPO that the Marmen/Welcon Offshore Wind Tower Manufacturing Plant will have an adverse visual effect on the National Register eligible Papscanee Island Historic District (08303.000130).

SHPO will provide additional comments once the Acoustic Noise Assessment has been completed to measure the proposed project's noise impacts at the Papscanee Island Historic District and the SMC THPO's comments regarding noise impacts have been provided.

If you have any questions, I can be reached at Jessica.Schreyer@parks.ny.gov.

Sincerely,

Jessica Schreyer Scientist Archaeology

Jessica E. Schreyen

Stockbridge-Munsee Tribal Historic Preservation

Arvid E. Miller Library Museum N8510 Mohheconnuck Road Bowler. WI 54416 Extension Office 86 Spring Street Williamstown, MA 01267

Email: thpo@mohican-nsn.gov

March 3, 2022

Andrew Dangler
Biologist/Senior Project Manager
Upstate New York Section
DEPARTMENT OF THE ARMY
US Army Corps of Engineers, ATTN: CENAN-OP-RU
1 Buffington St., Bldg. 10, 3rd Fl. North
Watervliet, NY 12189
Via email only

Re: Port of Albany Expansion Project, Town of Bethlehem, Albany Co., NY SHPO #18PR07273 /21PR04693

Dear Mr. Dangler:

I am writing regarding the aforementioned project as part of our continuing Government-to-Government Section 106 consultation.

In review of the project's designs and the additional visual and audial assessments, Stockbridge-Munsee Community feels that its cultural resource concerns have now been satisfactorily addressed.

Our determination is that the Port of Albany project will have **No Adverse Effect** to Historic Properties. No further consultation is required unless the designs should change further.

If you have any questions, please feel free to contact our office.

Respectfully,

Bonney Hartley

BHartley

Tribal Historic Preservation Manager

Stockbridge-Munsee Community

Cc: John Eddins, ACHP *Via email only*Jessica Schreyer, NY SHPO *via email only*David Witt, Charles Vandrei, NY DEC, *via email only*

Robert Leslie, Town of Bethlehem, via email only

Megan Daly, Port of Albany, via email only

Steve Boisfort, David Rosa, Jordan Tate- Mc Farland Johnson, via email only



KATHY HOCHUL Governor **ERIK KULLESEID**Commissioner

March 25, 2022

Jordan Tate
Environmental Analyst
McFarland Johnson
60 Railroad Place
Suite 402
Saratoga Springs, NY 12866

Re: USACE

Marmen/Welcon Offshore Wind Tower Manufacturing Plant

Town of Bethlehem, Albany County, NY

21PR04693

Dear Jordan Tate:

Thank you for requesting the comments of the New York State Historic Preservation Office (SHPO). We have reviewed the provided documentation in accordance with Section 106 of the National Historic Preservation Act of 1966. These comments are those of the SHPO and relate only to Historic/Cultural resources.

SHPO has reviewed the Noise Assessment and updated Visual Simulations (provided via email, McFarland Johnson, Inc., 2/18/22) to evaluate the project's effects on the National Register eligible Papscanee Island Historic District (08303.000130) and the Site Plan (McFarland Johnson, Inc., 3/18/22) showing the proposed 3.30-acre deed restricted area containing the vegetated area along the Hudson River shoreline. The vegetated area will provide a visual and acoustic buffer between the Papscanee Island Historic District and the proposed manufacturing plant.

We note that the Stockbridge Munsee Community has issued their opinion (letter, dated 3/2/22) that this project will have No Adverse Effect on Historic Resources.

Based on this review, it is the opinion of the SHPO that no historic properties, including archaeological and/or historic resources, will be Adversely Affected by this undertaking with the condition that a Restrictive Deed Covenant is filed to protect and maintain the vegetated buffer along the Hudson River shoreline.

If you have any questions, I can be reached at Jessica.Schreyer@parks.ny.gov.

Sincerely,

Jessica Schreyer Scientist Archaeology

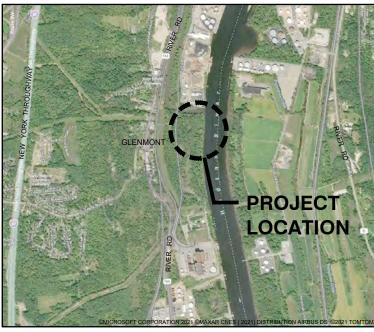
Lessica E. Schreye

APPENDIX G

DRAFT WHARF AND DREDGING E&SC PLANS









VICINITY AND LOCATION MAP SCALE: N.T.S.

NOTES:

- HORIZONTAL CONTROL REFERENCED TO NORTH AMERICAN DATUM OF 1983, STATE PLANE COORDINATE SYSTEM, NEW YORK, EAST ZONE, IN FEET.
- WATER LEVEL DATUM IS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88), AS FOLLOWS:
- MEAN HIGHER HIGH WATER LEVEL (MHHW) = +3.78 (NAVD88)
- MEAN HIGH WATER LEVEL (MHW) = +3.40 (NAVD88)
- MEAN TIDE LEVEL (MTL) = +0.91 (NAVD88)
- MEAN LOW WATER LEVEL (MLW) = -1.59 (NAVD88)
- MEAN LOWER LOW WATER LEVÉL (MLLW) = -1.81 (NAVD88)

PURPOSE: WHARF CONSTRUCTION PERMIT SUBMITTAL-NOT TO BE USED FOR CONSTRUCTION DATUM: NAVD88



m&n engineering, p.c.

OWNER/APPLICANT:

ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY

IN: HUI NEAR: SO

HUDSON RIVER SOUTH OF ALBANY

LOCATION: PORT OF ALBANY
106 SMITH BOULEVARD
ALBANY, NEW YORK 12202

WHARF DREDGING AND CONSTRUCTION

VICINITY AND LOCATION

SHEET 1 OF 5 DATE: (REV1) 2021-10-11

PLAN - EXISTING CONDITIONS



PURPOSE: WHARF CONSTRUCTION PERMIT SUBMITTAL-NOT TO BE USED FOR CONSTRUCTION DATUM: NAVD88

Active|_Permits|1094901P-02; Plotted; 10/13/2021 2:11 PM by COKER, MAEVE; Saved; 10/13/2021 12:21 PM by MCOKER

Q:INY110949-01120 CADDI



m&n engineering, p.c.

OWNER/APPLICANT: ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY

IN: HUDSON RIVER
NEAR: SOUTH OF ALBANY
LOCATION: PORT OF ALBANY

PORT OF ALBANY 106 SMITH BOULEVARD ALBANY, NEW YORK 12202 WHARF DREDGING AND CONSTRUCTION

PLAN - EXISTING CONDITIONS

SHEET 2 OF 5 DATE: (REV1) 2021-10-11

PLAN - PROPOSED CONDITIONS



PURPOSE: WHARF CONSTRUCTION PERMIT SUBMITTAL-NOT TO BE USED FOR CONSTRUCTION DATUM: NAVD88

Q:INY110949-01120 CADDI



m&n engineering, p.c.

OWNER/APPLICANT: ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY

HUDSON RIVER NEAR: SOUTH OF ALBANY LOCATION: PORT OF ALBANY

106 SMITH BOULEVARD ALBANY, NEW YORK 12202 WHARF DREDGING AND CONSTRUCTION

PLAN - PROPOSED CONDITIONS

SHEET 3 OF 5 DATE: (REV1) 2021-10-11

NOTE: DREDGE EQUIPMENT AND ASSOCIATED TURBIDITY CURTAIN/ ENVIRONMENTAL PROTECTION BARRIER LOCATIONS VARY.

10/13/2021 2:09 PM

Permits\1094901P-04 : Plotted:

Q:INY110949-01120 CADDI

PLAN - PROPOSED TEMPORARY **ENVIRONMENTAL PROTECTION**



PURPOSE: WHARF CONSTRUCTION PERMIT SUBMITTAL-NOT TO BE USED FOR CONSTRUCTION DATUM: NAVD88



OWNER/APPLICANT: ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY

HUDSON RIVER NFAR-SOUTH OF ALBANY LOCATION: PORT OF ALBANY

106 SMITH BOULEVARD ALBANY, NEW YORK 12202 WHARF DREDGING AND CONSTRUCTION

PLAN - PROPOSED TEMPORARY ENVIRONMENTAL PROTECTION

SHEET 4 OF 5 DATE: (REV1) 2021-10-11

SOUTH OF ALBANY

ALBANY, NEW YORK 12202

SHEET 5 OF 5

DATE: (REV1) 2021-10-11

PORT OF ALBANY 106 SMITH BOULEVARD

NEAR

m&n engineering, p.c.

LOCATION:

Q:INY110949-01120 CADD_Active_Permits11094901P-05; Plotted: 10/14/2021 10:16 AM by COKER, MAEVE; Saved: 10/13/2021 4:32 PM by MCOKER File:

APPENDIX H

SOIL MANAGEMENT PLAN



ATLANTIC TESTING LABORATORIES

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WBE certified company

October 23, 2020

McFarland Johnson, Inc. 60 Railroad Place, Suite 402 Saratoga Springs, New York 12866

Attn: David Rosa

Re: Soil Management Plan

Port of Albany Expansion Project

Beacon Island Parcel

Bethlehem, Albany County, New York

MJ Project No. 18641.02

ATL Report No. AT5596CE-05-10-20

Ladies/Gentlemen:

Enclosed is a copy of the Soil Management Plan prepared for the referenced site. This report was completed in accordance with the standard form of agreement between McFarland Johnson, Inc., and Atlantic Testing Laboratories, Limited.

Please contact our office should you have any questions, or if we may be of further assistance.

Sincerely,

ATLANTIC TESTING LABORATORIES. Limited

Cheyenne J. Dashnaw, P.E.

Senior Engineer

CJD/cjd

Enclosures

cc: Georgie Nugent, McFarland Johnson, Inc.

SOIL MANAGEMENT PLAN

PORT OF ALBANY EXPANSION PROJECT BEACON ISLAND PARCEL BETHLEHEM, ALBANY COUNTY, NEW YORK



WBE certified company

PREPARED BY:

ATLANTIC TESTING LABORATORIES, LIMITED 22 Corporate Drive Clifton Park, New York 12065

PREPARED FOR:

McFarland Johnson, Inc. 60 Railroad Place, Suite 402 Saratoga Springs, New York 12866 MJ Project No. 18641.02 Albany Port District Commission 106 Smith Boulevard Albany, New York 12202

ATL REPORT No. AT5596CE-05-10-20

October 23, 2020

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1.0 INTRODUCTION

1.1 Purpose

Atlantic Testing Laboratories, Limited (ATL) was retained by McFarland Johnson, Inc., on behalf of the Albany Port District Commission, to prepare a Soil Management Plan that can be used to address areas at the Beacon Island parcel that are impacted with ash material and related debris. The purpose of this Soil Management Plan is to summarize procedures to implement for planned excavation activities, installation of a soil cover system in areas of ash material or other potential impacted fill, and management of waste soil and/or groundwater. This Soil Management Plan also addresses protocol for monitoring and sampling and analysis during excavation and site work, and recommendations for installation of vapor barrier systems beneath proposed buildings.

1.2 Site Description

The project site is the Beacon Island parcel located to the east of River Road (County Route 144) and along the west side of the Hudson River, in the Town of Bethlehem, Albany County, New York. The Beacon Island parcel is comprised of approximately 80 acres, and is the site of a planned expansion for the Port of Albany. A Site Location Map, showing the approximate location of the subject site, is included in Appendix A.

Information provided to ATL by McFarland Johnson, Inc., indicates that planned redevelopment for the site includes land clearing, excavation and backfill operations, dredging sediment for the area along the Hudson River, and construction of facilities to be associated with the Port of Albany.

1.3 Plan Contents and Organization

This Soil Management Plan includes an introductory section (Section 1), a summary of information obtained from prior investigations (Section 2), pertinent coordination items when work is scheduled for impacted areas (Section 4) and a description of procedures that may be warranted for various site work activities (Section 3), a description of procedures to be implemented during specific site work activities (Sections 5 through 12), and a description of reports and records that should be maintained for work completed at the subject site (Section 13). Appendices are included to provide supplemental information that is considered pertinent to the items described in the Soil Management Plan and are referenced where applicable.

This Soil Management Plan is organized in a manner to allow for site representatives to review and identify applicable measures to be implemented for different areas of work and types of work activities being performed. Section 1.4 describes different areas of work and the associated work activities that may be applicable. A Soil Management Plan Flow Chart, contained in Appendix B, is provided to outline tasks to be implemented for management of existing on-site soil and soil that may be imported for use as fill.

1.4 Applicability

1.4.1 Areas to be Developed with Buildings/Structures

Areas to be developed with buildings or other structures will require appropriate soil management procedures, in association with the excavation, backfill, and grading for the

installation of foundation systems, and with the construction of slabs-on-grade for buildings. Following is a summary of the soil management procedures to be implemented, with reference to applicable sections of this Soil Management Plan.

- <u>Excavation for foundations in areas of known/suspect impacts from ash:</u> Refer to
 Section 5 and Item A of Soil Management Plan Flow Chart (Appendix B)
- Excavation for foundations in areas without known/suspect impacts from ash: Refer to **Section 6** and **Item B** of Soil Management Plan Flow Chart (Appendix B)
- <u>Backfill in areas of construction:</u> Refer to **Section 11** and **Items E and F** of Soil Management Plan Flow Chart (Appendix B)
- <u>Construction of slabs-on-grade for buildings:</u> Refer to **Section 9** and **Item E** of Soil Management Plan Flow Chart (Appendix B)

1.4.2 Areas to be Developed with Asphalt/Concrete Surfaces

Areas to be developed with asphalt or concrete surfaces (e.g., driveways, parking lots, walking paths) will require appropriate soil management procedures, in association with the excavation, backfill, and grading prior to installation of the asphalt or concrete surface cover. Following is a summary of the soil management procedures to be implemented, with reference to applicable sections of this Soil Management Plan.

- <u>Excavation and site preparation in areas of known/suspect impacts from ash:</u>
 Refer to **Section 5** and **Item A** of Soil Management Plan Flow Chart (Appendix B)
- Excavation and site preparation in areas without known/suspect impacts from ash:
 Refer to **Section 6** and **Item B** of Soil Management Plan Flow Chart (Appendix B)
- <u>Backfill in areas of construction:</u> Refer to **Section 11** and **Items E and F** of Soil Management Plan Flow Chart (Appendix B)

1.4.3 Areas to be Developed with Lawn/Landscaping

Areas to be redeveloped with lawn or landscaping will require appropriate soil management procedures, in association with the excavation, backfill, grading, and soil cover system installation. Following is a summary of the soil management procedures to be implemented, with reference to applicable sections of this Soil Management Plan.

- Excavation and site preparation in areas of known/suspect impacts from ash:
 Refer to **Section 5** and **Item A** of Soil Management Plan Flow Chart (Appendix B)
- Excavation and site preparation in areas without known/suspect impacts from ash: Refer to **Section 6** and **Item B** of Soil Management Plan Flow Chart (Appendix B)
- <u>Backfill and soil cover system in areas of lawns and landscaping:</u> Refer to Sections 8 and 11 and Items E and F of Soil Management Plan Flow Chart (Appendix B)

1.4.4 Areas to Remain Wooded

Areas of the subject site that are currently wooded and are planned to remain wooded will not require implementation of specific soil management procedures at this time. In the event that these areas are scheduled for redevelopment in the future, or if there are any ground intrusive activities performed, appropriate soil management procedures should then be provided.

1.4.5 Areas to be Dredged

Management of areas where sediment is planned for dredging is described in general for this Soil Management Plan; however, additional planning and coordination with the New York State Department of Environmental Conservation (NYSDEC), United States Army Corps of Engineers (USACE), and other applicable regulatory agencies will be necessary prior to performing the dredging operations and the handling and reuse or disposal of dredged sediments. Refer to **Section 10** and **Item D** of the Soil Management Plan Flow Chart (Appendix B).

2.0 BACKGROUND INFORMATION AND AREAS OF CONCERN

2.1 Summary of Previous Investigations

ATL performed sediment sampling at the subject site in June 2019 and August 2020, and a subsurface investigation and soil sampling in September 2020. Additionally, ATL was provided with a draft Phase II Environmental Site Assessment report prepared by Bergmann Associates for the Port of Albany and dated April 6, 2017.

The sediment sampling conducted by ATL in June 2019 included the advancement of 5 cores, and the sediment sampling conducted by ATL in August 2020 included the advancement of 10 cores. The cores were advanced in the areas scheduled for dredging as part of planned redevelopment for the site. Sediment samples were collected from the core locations and submitted for subsequent laboratory analysis. Laboratory analysis parameters for the June 2019 sampling event were selected to include compounds described in NYSDEC Technical and Operational Guidance Series (TOGS) 5.1.9, whereas the samples collected in August 2020 were analyzed for parameters to evaluate potential reuse options in addition to the NYSDEC TOGS 5.1.9 parameters. A complete summary of findings for the previously completed sediment sampling and analysis are provided in ATL Report No. CD4644CE-01-07-19, dated July 15, 2019, ATL Report No. CD4644CE-01-07-19 Addendum 1, dated August 2, 2019, and ATL Report No. AT5596CE-03-09-20 dated September 24, 2020.

The subsurface investigation and soil sampling conducted by ATL in September 2020 included the advancement of 45 probes. The probes were advanced in accessible areas throughout the site, to assess the presence or absence of ash material. Additionally, soil samples were collected from locations without ash material to evaluate potential reuse options for consideration during site redevelopment. The subsurface investigation identified multiple locations where ash material is present, but did not identify obvious visual or olfactive evidence of petroleum or chemical-related contamination. Soil samples were collected from areas without ash material, including 22 samples for analysis of volatile organic compounds (VOC), and 11 samples for analysis of semi-VOC, polychlorinated biphenyls (PCB), pesticides, metals, and cyanide. With a few exceptions, laboratory analysis results for the soil samples collected from areas without ash material were below 6 NYCRR Part 360 fill material pre-determined beneficial use criteria and below NYSDEC Unrestricted Use Soil Cleanup Objectives (SCO) listed in 6 NYCRR Part 375 and/or NYSDEC CP-51 document. A general summary of the findings for the subsurface investigation previously completed by ATL is provided as Table C-1 in Appendix C. A complete summary of findings is provided in ATL Report No. AT5596CE-04-10-20, dated October 22, 2020.

The Phase II ESA conducted by Bergmann Associates in February 2017 included the advancement of 12 test pits and 8 borings, and the installation of temporary monitor wells at 3 of the boring locations. Information in the draft Phase II ESA report indicates that coal ash was observed throughout the depths for 3 of the test pits and a fourth test pit exhibited the presence of railroad ties covered in a black tar-like substance at depths of 8 to 12 feet below ground surface. Of the 8 borings advanced during this investigation, 7 exhibited evidence of coal ash. A surface soil sample was collected from the initial 2 inches for each boring. Subsurface soil samples were also collected from the borings at varving depths. There were 3 temporary monitor wells installed for collection of groundwater samples. The soil and groundwater samples were laboratory analyzed for VOC, semi-VOC, cyanide, pesticides, PCB, and target compound list (TCL) metals. With the exception of metals, target compounds for the referenced analytical parameters were non-detect for each of the soil and groundwater samples. A general summary of the findings for the subsurface investigation previously completed by Bergmann Associates is provided as Tables C-2 and C-3 in Appendix C. The report prepared by Bergmann Associates and dated April 6, 2017, should be referenced for additional details pertaining to the findings of the subsurface investigation.

2.2 Known Locations of Impacted Soil

Data and information from the previous subsurface investigation activities indicates that ash material is present at the site in a widespread condition. The ash material has been predominantly observed on the west side of the subject site. No obvious visual or olfactive evidence of petroleum or chemical-related contamination was observed at the locations investigated.

The Aerial Overview of Affected Locations, contained in Appendix D, shows approximate locations for the borings, test pits, and probes previously advanced at the subject site, along with an indication of which exhibited the presence of ash material. The referenced drawing also shows an approximate delineation of areas where ash material is expected to be present, areas where ash material is not expected, and areas that are considered to potentially contain ash material. The areas shown on the drawing are based on existing available data and not intended to represent an exact delineation for the locations of ash material.

3.0 COORDINATION OF WORK

3.1 Roles and Responsibilities

The soil management procedures described herein should be coordinated and conducted by firms and individuals who are familiar with the conditions of the Soil Management Plan, have an understanding of the known or suspected conditions in different areas of the subject site, and have related experience and capabilities to implement the applicable work activities. While the Owner of the property has responsibility for the implementation of the Soil Management Plan, it is anticipated that performance of work activities associated with the Soil Management Plan would be coordinated and completed by design professionals, contractors, and environmental consultants who are retained by the Owner. The following table provides a summary of the primary roles and responsibilities for implementation of the Soil Management Plan.

Role	Responsibilities	
Owner	 Retain and coordinate with Design Professionals, Contractors, and Environmental Consultants for performance of site work pursuant to conditions of the Soil Management Plan Maintain site records and documentation for work completed pursuant to Soil Management Plan 	
Design Professionals	 Incorporate applicable provisions of the Soil Management Plan into design plans and specifications for planned site redevelopment Coordinate with Owner, Contractors, and Environmental Consultants during design and construction phases to confirm work is completed as planned 	
Contractors	 Correspond with NYSDEC (and other regulatory agencies, as applicable) for notifications of work activities Perform site work activities, including, but not limited to, excavation, grading, placement and compaction of backfill, dust control, groundwater management, soil cover system installation, vapor barrier system installation, construction, and waste transport and disposal 	
Environmental Consultants	 Provide guidance and assistance with implementation of the Soil Management Plan Correspond with NYSDEC (and other regulatory agencies, as applicable) to discuss clarifications or modifications to conditions of the Soil Management Plan Conduct monitoring and soil screening during performance of work activities that affect impacted or contaminated soil Conduct air monitoring during ground intrusive activities that affect impacted or contaminated soil Perform soil sampling and laboratory analysis for waste materials, fill materials, and excavation areas 	

3.2 Project Notifications

Within 14 days, and no less than 3 days, prior to commencing work activities that may affect areas of the subject site that are impacted with ash, the NYSDEC should be notified of the planned work. This notification should be performed by the Owner and/or Contractor performing the site work. The Design Professional and Environmental Consultant should also be similarly notified.

3.3 Spill Reporting/Administration

The subject site is known to have areas impacted with ash and related debris. Other types of contamination (i.e., petroleum, chemical) have not been encountered at locations of past investigations. The NYSDEC must be notified in the event that petroleum- or chemical-related contaminated soil is discovered on the project site. This notification will need to be provided directly to the NYSDEC Spill Hotline (telephone number 1-800-457-7362).

4.0 GENERAL SITE WORK AND SOIL MANAGEMENT PLAN CONDITIONS

4.1 Health and Safety

In addition to construction site health and safety, site personnel should be aware of the contaminants of concern associated with the ash material (metals) and utilize appropriate control methods, personal protective clothing, and personal protective equipment during the handling and management of impacted materials. Contractors working at the subject site should perform work pursuant to a health and safety plan that is specific to their scope of work and associated hazards or potential hazards.

4.2 Groundwater Removal and Management (If Applicable)

In the event that there is significant groundwater inflow in a zone of contaminated soil, a vacuum truck should be provided to remove the infiltrated groundwater as the excavation progresses or at the completion of excavation activities. Alternatively, groundwater can be pumped into a frac tank(s) or other appropriate receptacles and temporarily stored on-site prior to on-site treatment and discharge or transfer and disposal off-site.

4.3 Dust Control and Air Monitoring

Fugitive dust and vapors should be minimized or mitigated during the excavation and handling of contaminated soil, if encountered. In the event that particulates and/or vapors represent a potential concern for the work area and/or surrounding areas, particulates and/or vapors should be monitored during ground intrusive activities associated with contaminated soil by setting up real-time instrumentation at locations upwind and downwind of the project area. Assessment for airborne dust would be performed using particulate monitors capable of measuring particulate matter less than 10 microns (PM10). Assessment for vapors (applicable to areas where petroleum- or chemical-related contamination is encountered) would be performed using a photoionization detector (PID) to screen the ambient air for the measurable presence of VOC.

If air monitoring for particulates is conducted, an action level of 0.15 milligrams per cubic meter (mg/m³) should be used for PM10 concentrations associated with the project work area. If screening is performed for ambient airborne VOC concentrations, an action level of 5 parts per million (ppm) should be used for the project work area. These action levels are consistent with the NYSDEC DER-10 "Technical Guidance for Site Investigation and Remediation" and the New York State Department of Health (NYSDOH) "Generic Community Air Monitoring Plan."

In the event that the PM10 action level is exceeded for the work site (downwind monitoring station), the upwind background level should be immediately confirmed and it should be determined whether the work site (downwind) level exceeds the upwind background by greater than 0.1 mg/m³. For any such exceedance, work activities should temporarily cease and dust suppression techniques should be implemented. Dust suppression techniques may include some or all of the following (as cited from Appendix 1B of the NYSDEC DER-10):

- Applying water on haul roads
- Wetting equipment and excavation faces
- Spraying water on buckets during excavation and dumping
- Hauling materials in properly tarped or watertight containers

- Restricting vehicle speeds to 10 mph
- Covering excavated areas and material after excavtion activity ceases
- Reducing the excavation size and/or number of excavations

In the event that the VOC action level is exceeded for the work site (downwind monitoring station), the upwind background level should be immediately confirmed and it should be determined whether the work site (downwind) level exceeds the upwind background by greater than 5 ppm. For any such exceedance, work activities should temporarily cease while monitoring continues. If the concentrations readily decrease below 5 ppm over background, work activities can resume. If the concentrations do not readily decrease and a definitive source can not be eliminated, the work site and on-site work activities would require further evaluation to determine an appropriate course of action.

4.4 Personnel and Equipment Decontamination

Equipment that is in contact with contaminated soil should be decontaminated, as necessary to prevent cross-contamination to other areas. Equipment and tools can be decontaminated by initially scrubbing the bulk material from the item, cleaning with a phosphate-free detergent and tap water wash, rinsing with tap water, and rinsing with distilled water. In order to contain decontamination liquids, a decontamination pad, of sufficient size to accommodate the affected portions of equipment, can be constructed using double layers of polyethylene sheeting as a base and a suitable material (i.e., lumber, clean soil, hay bales) for a perimeter berm. A more durable setup would be necessary if larger, heavier items need to be decontaminated. The polyethylene sheeting should be wrapped around the perimeter berm. Wastewater generated from decontamination activities shall be disposed of pursuant to applicable local, state and federal requirements.

5.0 EXCAVATION IN AREAS IMPACTED WITH ASH AND DEBRIS

5.1 Soil Removal and Stockpile

Soil that is impacted with ash and requires excavation for planned site redevelopment activities will need to be transported off-site for disposal. In consideration of the ash materials being widespread at various locations of the subject site, and the soil cover system that will be implemented as described in other sections of this Soil Management Plan, the areal extent of excavation for ash and debris wastes will be only as necessary to complete the scheduled site redevelopment. It is intended that the depths of removal be similarly limited to scheduled depths of excavations; however, if existing available information suggests that waste ash/debris exists at only a limited distance below scheduled depths of excavations, removal of the additional material should be conducted to limit the amount of material that would remain below permanent structures or site features to be constructed.

Excavated soil should be field examined for the visual and/or olfactive indicators of the presence of ash and debris materials or the potential presence of petroleum- or chemical-related impacts. In the event that petroleum- or chemical-related impacts are identified, procedures described in Section 7 should implemented.

Excavated soil should be segregated between soil that is impacted with ash and overburden soil that does not exhibit visual evidence of these wastes. The impacted soil should be stockpiled or directly loaded for subsequent transport and disposal. The

overburden soil can be processed for reuse on-site, provided applicable conditions are satisfied (reference Section 11).

For impacted soil that is stockpiled on-site, the selected location(s) should be an area not susceptible to flooding or inundation of water during precipitation events, readily accessible to equipment that will be utilized for loading and hauling the material, and located away from stormwater or site drainage components. Any contaminated soil stockpile would need to be placed on and covered with 6-mil polyethylene sheeting or other comparable impervious material that can be readily removed and disposed of. The following items should be applicable to stockpiles for contaminated soil materials.

- Polyethylene sheeting or other impervious membrane used for the base of the soil stockpile should be placed with sheets overlapping a minimum of 1 foot.
- The base of the soil stockpile should be bermed at the perimeter to contain the soil stockpile and potential runoff during precipitation events. The berm materials, which can be comprised of mounds of clean soil material, hay bales, lumber, or other readily available suitable materials, should be placed along the perimeter and wrapped with the polyethylene sheeting or other impervious membrane that is used for the base of the soil stockpile. To minimize extraneous handling of materials and the size of the completed soil stockpile area, the berm perimeter can initially be constructed along 2 sides, and the remaining 2 sides can be constructed after all soil material is placed in the stockpile or temporarily bermed at the end of each workday.
- The height and slopes of the soil stockpile should be limited such that slope stability is not compromised during storage or the loading process.
- The soil stockpile should be covered with the polyethylene sheeting upon placement of all impacted soil material or at the end of each workday. Seams should be overlapped a minimum of 1 foot. The stockpile cover should be sufficiently weighted to contain the stored soil and resist damage from wind. Materials used to weigh down and stabilize the stockpile cover should consist of readily available materials that will not tend to damage the cover upon placement (e.g., clean soil material, sand bags, tires).
- Any temporary on-site soil stockpiles should be periodically inspected to ensure that material continues to be contained and is not released to the surrounding environment. The temporary on-site soil stockpiles will need to be properly protected and maintained until removal and off-site disposal. Polyethylene sheeting should be repaired or replaced as needed.
- Water from precipitation events that ponds on the surface of the stockpile cover should be removed upon discovery. The ponded water can be discharged onsite provided there is no contact with the petroleum-contaminated soil, and provided such activities are compliant with any stormwater discharge permits that may be applicable for the site or active construction work. Water that contacts the petroleum-impacted soil shall be properly containerized and managed as impacted waste water.
- Stockpiles with impacted soil should not remain on-site in excess of 60 days.

5.2 Excavation Monitoring and Soil Sampling

A representative of the Environmental Consultant should be on-site during excavation activities in the known or suspect areas of ash materials, to examine exposed soil for the presence of ash. The on-site representative should assist with determinations for the segregation of soil material that is considered relatively clean overburden to be reused

and soil material that would be classified as contaminated for off-site disposal. The onsite representative would also be available to provide guidance relative to the management of the contaminated subsurface materials.

Since it is planned to manage ash materials in-place for various locations at the subject site, soil samples are not proposed for excavation area(s) where waste ash/debris is removed, unless other potential contaminants of concern are encountered or suspected. If soil samples are to be collected from these excavation areas, the Environmental Consultant should coordinate with the NYSDEC to confirm analytical parameters, sampling locations, and quantity of samples.

5.3 Soil Reuse or Disposal

Overburden soil scheduled for reuse should be managed pursuant to procedures described in Section 11. Waste soil materials scheduled for disposal should be managed pursuant to procedures described in Section 12.

6.0 EXCAVATION IN NON-IMPACTED AREAS

6.1 Soil Removal and Stockpile

Soil that is excavated from areas without known or suspect impacts from ash can be removed and handled pursuant to routine construction and site work methods. Contractors performing the excavation work should be cognizant of the potential for impacted soil and should visually monitor the soil as removed to determine if it may be potentially affected. If ash material is identified, the excavation and soil management procedures should transition to the methods described in Section 5. In the event that petroleum- or chemical-related impacts are identified, procedures described in Section 7 should implemented.

6.2 Excavation Monitoring

As indicated in Section 6.1, a representative of the Contractor should examine exposed soil for visual and/or olfactive indicators of potential contamination. If suspect impacted materials are encountered, a representative of the Environmental Consultant should be on-site for further assessment and monitoring in the affected area.

Unless suspect contamination is encountered, soil samples are not proposed for the excavations. If soil samples are to be collected from these excavation areas, the Environmental Consultant should coordinate with the NYSDEC to confirm analytical parameters, sampling locations, and quantity of samples.

6.3 Soil Reuse or Disposal

The excavated soil that is scheduled for reuse should be managed pursuant to procedures described in Section 11. In the event that the soil materials need to be disposed of, transport and disposal should be performed pursuant to procedures described in Section 12.

7.0 EXCAVATION IN AREAS OF PETROLEUM/CHEMICAL SPILLS

7.1 Soil Removal and Stockpile

If petroleum- or chemical-related contamination is encountered during site work, a spill will need to be reported (reference Section 3.3) and contaminated soil will need to be removed for disposal. The areal extent and depths of excavation for material affected by a spill should be inclusive of the entirety of the contaminated material, if feasible and practical. If the affected materials cannot be completely removed, an alternate approach to site remediation should be coordinated through the NYSDEC.

Excavated soil should be field examined for the visual and/or olfactive indicators of the petroleum- or chemical-related impacts, and field screened for the measurable presence of VOC with a photoionization detector (PID), equipped with the 10.6 eV lamp. In general, soil exhibiting obvious visual or olfactive evidence of contamination and/or greater than 10 ppm via ambient PID screening should be removed from the excavation, and processed for subsequent disposal. Overburden soil that does not exhibit these characteristics should be stockpiled on-site for subsequent sampling and evaluation of reuse options.

For petroleum-contaminated soil that is stockpiled on-site, the selected location(s) should be an area not susceptible to flooding or inundation of water during precipitation events, readily accessible to equipment that will be utilized for loading and hauling the material, and located away from stormwater or site drainage components. Any contaminated soil stockpile would need to be placed on and covered with 6-mil polyethylene sheeting or other comparable impervious material that can be readily removed and disposed of. The following items should be applicable to stockpiles for contaminated soil materials.

- Polyethylene sheeting or other impervious membrane used for the base of the soil stockpile should be placed with sheets overlapping a minimum of 1 foot.
- The base of the soil stockpile should be bermed at the perimeter to contain the soil stockpile and potential runoff during precipitation events. The berm materials, which can be comprised of mounds of clean soil material, hay bales, lumber, or other readily available suitable materials, should be placed along the perimeter and wrapped with the polyethylene sheeting or other impervious membrane that is used for the base of the soil stockpile. To minimize extraneous handling of materials and the size of the completed soil stockpile area, the berm perimeter can initially be constructed along 2 sides, and the remaining 2 sides can be constructed after all soil material is placed in the stockpile or temporarily bermed at the end of each workday.
- The height and slopes of the soil stockpile should be limited such that slope stability is not compromised during storage or the loading process.
- The soil stockpile should be covered with the polyethylene sheeting upon placement of all impacted soil material or at the end of each workday. Seams should be overlapped a minimum of 1 foot. The stockpile cover should be sufficiently weighted to contain the stored soil and resist damage from wind. Materials used to weigh down and stabilize the stockpile cover should consist of readily available materials that will not tend to damage the cover upon placement (e.g., clean soil material, sand bags, tires).
- Any temporary on-site soil stockpiles should be periodically inspected to ensure that material continues to be contained and is not released to the surrounding environment. The temporary on-site soil stockpiles will need to be properly

protected and maintained until removal and off-site disposal. Polyethylene sheeting should be repaired or replaced as needed.

- Water from precipitation events that ponds on the surface of the stockpile cover should be removed upon discovery. The ponded water can be discharged onsite provided there is no contact with the petroleum-contaminated soil, and provided such activities are compliant with any stormwater discharge permits that may be applicable for the site or active construction work. Water that contacts the petroleum-impacted soil shall be properly containerized and managed as impacted waste water.
- Stockpiles with impacted soil should not remain on-site in excess of 60 days.

7.2 Excavation Monitoring and Sampling

A representative of the Environmental Consultant should be on-site during excavation activities in the areas affected by a petroleum- or chemical-related spill, to examine exposed soil for visual and/or olfactive indicators of petroleum- or chemical-related impacts. Additionally, field screening for the measurable presence of VOC should be performed at the time of the excavation activities, using a portable PID, equipped with a 10.6 eV lamp.

The on-site representative should assist with determinations for the segregation of soil material that is considered relatively clean overburden to be reused and soil material that would be classified as contaminated for off-site disposal. The on-site representative would also be available to provide guidance relative to the management of the contaminated subsurface materials.

Post-excavation soil samples should be collected from the walls and floor of the excavation area(s) where petroleum- or chemical-contaminated soil is removed. The quantities of soil samples to be collected from these excavation areas should be selected pursuant to the following criteria:

- For excavations with a perimeter of less than 20 feet, 1 bottom and 1 sidewall sample should be collected.
- For excavations with a perimeter between 20 and 300 feet, samples from sidewalls should be collected at a frequency of 1 per 30 linear feet and samples from the bottom should be collected at a frequency of 1 per 900 square feet.
- For excavations with a perimeter of greater than 300 linear feet, the quantity of samples to be collected should be coordinated through the NYSDEC, or selected pursuant to the same criteria specified for an excavation perimeter between 20 and 300 feet.

The post-excavation soil samples should be laboratory analyzed for VOC, in accordance with EPA Method 8260; and semi-VOC, in accordance with EPA Method 8270 (base/neutral extractables).

7.3 Soil Reuse or Disposal

Overburden soil scheduled for reuse should be managed pursuant to procedures described in Section 11. Waste soil materials scheduled for disposal should be managed pursuant to procedures described in Section 12.

8.0 SOIL COVER SYSTEM INSTALLATION

A soil cover should be installed in areas of the site that are impacted with ash material and will be utilized as lawn or landscaped areas. The following criteria should be applicable to the soil cover system.

- The upper 6 inches of the soil cover should be suitable to sustain growth of appropriate vegetation at the ground surface.
- A minimum of 1 foot of soil cover should be placed above the ash material.
- The upper 1 foot of the soil cover should not have concentrations of contaminants that exceed the Restricted Residential Soil Cleanup Objectives (SCO) set forth in 6 NYCRR Part 375-6.
- Fill that is placed at a depth below the upper 1 foot of soil cover should not have concentrations of contaminants that exceed the Commercial SCO set forth in 6 NYCRR Part 375-6.
- A demarcation layer should be provided between the soil cover layer and underlying impacted soil, unless approval is obtained from the NYSDEC to forego installation of a demarcation layer.
- In the event that the soil cover system is breached, penetrated, or temporarily removed, restoration to original conditions (or equivalent) should be performed.
- Areas with a soil cover should be inspected at least annually, to assess existing
 conditions and determine if any restoration or repairs are necessary. Inspections
 should also be performed after severe weather events or significant site
 operations that may have adversely affected the soil cover system.

9.0 VAPOR BARRIER SYSTEM INSTALLATION

A vapor barrier system could be considered as an option for buildings that are constructed at the subject site, especially for buildings that would be occupied on a routine basis. While risks with vapor migration from contaminants associated with ash material is relatively low, installation of a vapor barrier system is generally an inexpensive addition to the construction of a new building. A vapor barrier system could consist of a gas permeable layer (i.e., crushed stone) and a soil gas retarder membrane (i.e., polyethylene or polyolefin sheeting) between the gas permeable layer and concrete slab. Soil gas collector pipes could also be installed in the gas permeable layer, and established as a passive system, active system, or passive with capability to be transitioned to an active system. If the Owner opts for installation of a vapor barrier system for buildings, the vapor barrier system should be incorporated into design plans and specifications for the specific building(s) being constructed.

10.0 DREDGING OF SEDIMENT

10.1 Sediment Removal and Management

Dredging of sediment would need to be conducted pursuant to conditions of applicable permits, as determined through the joint application for permits process with state agencies and the USACE. A dredging plan should also be developed to identify the dredging methods and management options. Direct coordination with the NYSDEC and reference to NYSDEC TOGS 5.1.9 would be necessary to ensure that necessary criteria for the dredging operations are addressed.

10.2 Sediment Reuse or Disposal

6 NYCRR Part 360.12(c)(1)(iv) describes conditions for pre-determined beneficial use of navigational dredged material; however, laboratory analysis data for previously collected samples at the site are not indicative of the sediment material meeting the requisite criteria. For navigational dredged material that does not meet the pre-determined beneficial use criteria, a petition for a case-specific beneficial use determination (BUD) could be considered.

Laboratory analysis results from previously collected sediment samples have identified elevated concentrations for metals and PCB, and as such, dredged sediment (or affected portions thereof) should be disposed of at a permitted solid waste management facility. If reuse is desired for portions that may exhibit lesser contaminant concentrations, a plan would need to be developed for segregation and sampling and analysis, along with submitting the petition for a case-specific BUD.

11.0 BACKFILL AND SOIL REUSE

11.1 Suitable On-Site Soil

Laboratory analysis results for samples previously collected from locations on the subject site not impacted with ash indicate that concentrations of contaminants generally do not exceed the 6 NYCRR Part 375 Commercial SCO and the 6 NYCRR Part 360 fill material pre-determined beneficial use criteria. This material should be suitable for on-site reuse below the upper 1 foot of soil cover. Additional sampling and analysis may be needed for areas not previously investigated and for previously sampled areas where exceedances were identified relative to the 6 NYCRR Part 375 Commercial SCO and/or the 6 NYCRR Part 360 fill material pre-determined beneficial use criteria. If additional sampling and analysis is performed, the quantity of samples and analytical parameters should be selected pursuant to the Sampling and Analysis Schedule for Fill in Appendix E.

11.2 Imported Fill

Fill material may need to be imported to the site, for use as the upper 1 foot of soil cover system or for other areas specific types of fill material. Imported fill material should be sampled and analyzed prior to delivery to the site, to confirm the material satisfies criteria established for use as a soil cover (reference Section 8) or criteria for use as general fill, restricted use fill, or limited use fill per 6 NYCRR Part 360.13. The quantity of samples and analytical parameters for imported fill should be selected pursuant to the Sampling and Analysis Schedule for Fill in Appendix E.

12.0 WASTE TRANSPORT AND DISPOSAL

The Contractor should provide for loading and transporting contaminated soil to a permitted solid waste management facility. Transport of waste materials will require use of trucks with applicable permits pursuant to 6 NYCRR Part 364 criteria. The disposal of waste soil materials should be documented via waste manifests and/or copies of waste disposal receipts.

Waste characterization soil samples should be collected and laboratory analyzed from the impacted material, pursuant to requirements of the selected disposal facility. The selected disposal facility should be contacted prior to excavation work to identify applicable

laboratory analysis parameters and quantity of samples, and to process waste profile documentation.

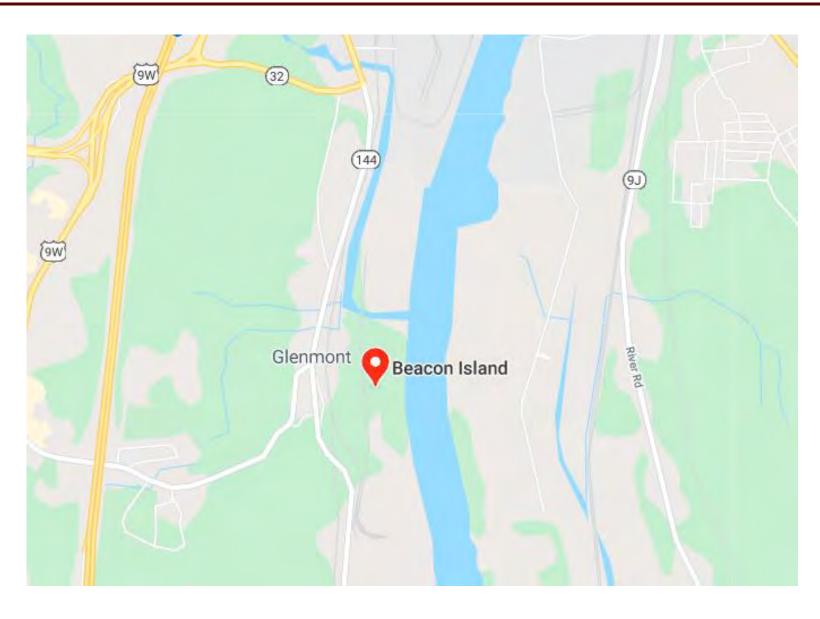
13.0 REPORTING AND RECORDKEEPING

Reports and records of site work should be maintained, as needed to document site conditions and soil management procedures that are completed. Reports and records to be maintained in association with this Soil Management Plan include, but may not be limited to, the following:

- As-built plans
- Waste manifests and/or disposal receipts for ash, soil, and groundwater
- Air monitoring data
- Excavation monitoring data
- Soil sampling and laboratory analysis data
- Site observation reports

APPENDIX A

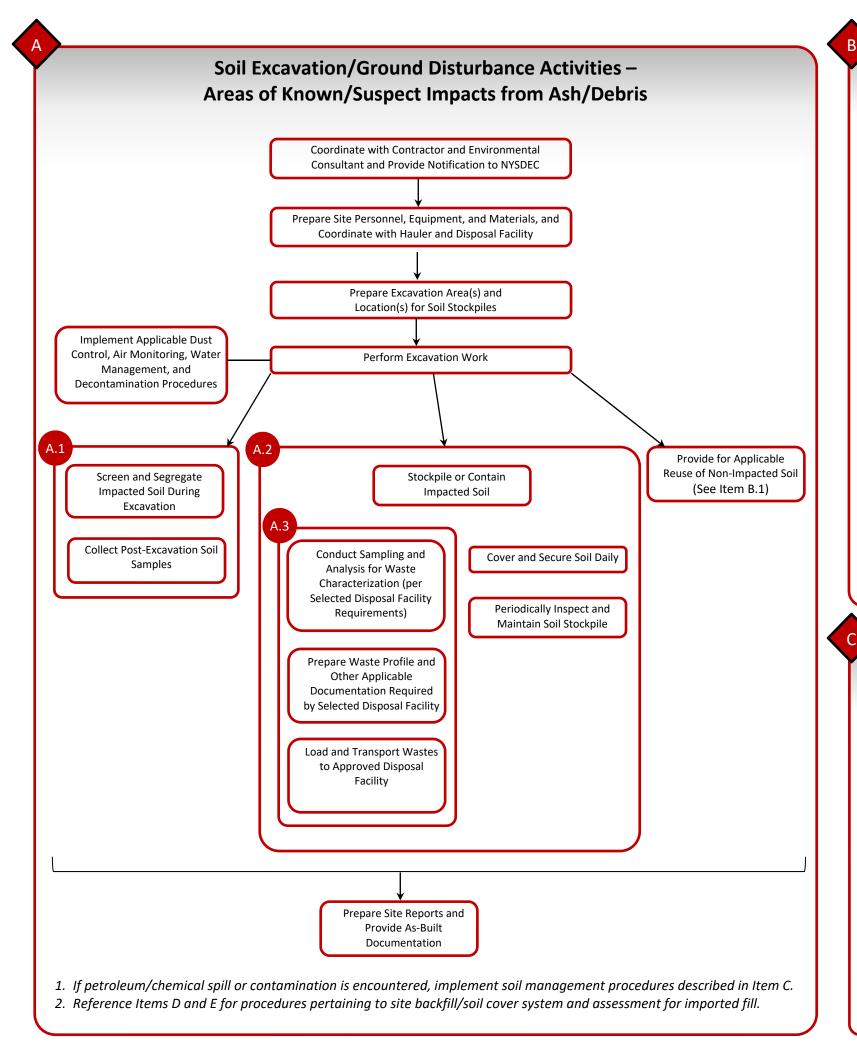
Site Location Map



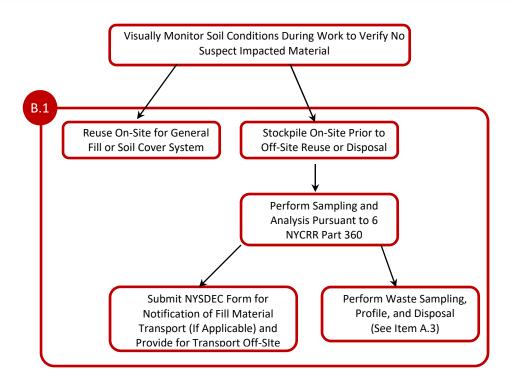
Site Location Map	Drawn by:		Scale:	Project No.:	Date:
	TSP		Not to scale	AT5596	May 2020
Beacon Island Parcel Bethlehem, Albany County, New York	Albany, NY Poughkeepsie,	ATLANTI Binghamton, N Syracuse, N	·	Elmira, NY	e d Plattsburgh, NY Watertown, NY

APPENDIX B

Soil Management Plan Flow Chart

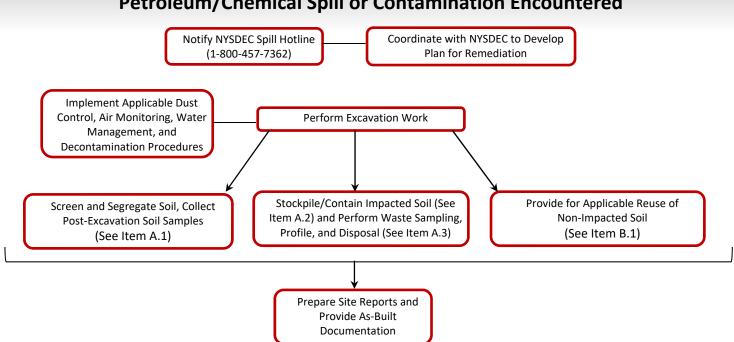


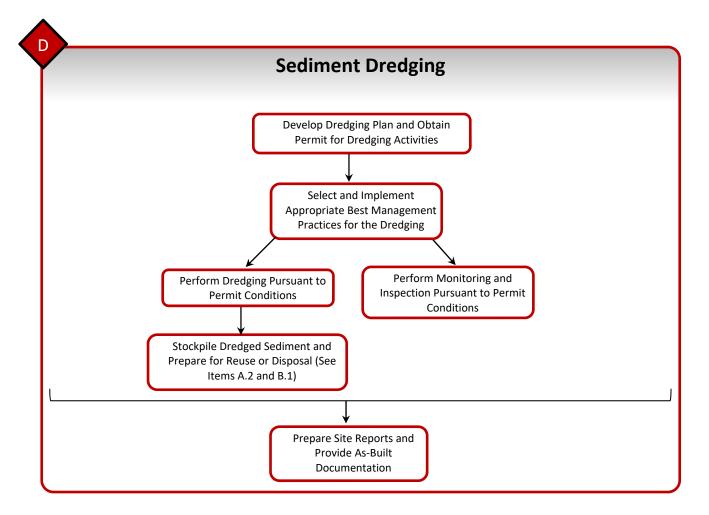
Soil Excavation/Ground Disturbance Activities – Areas without Known/Suspect Impacts from Ash/Debris

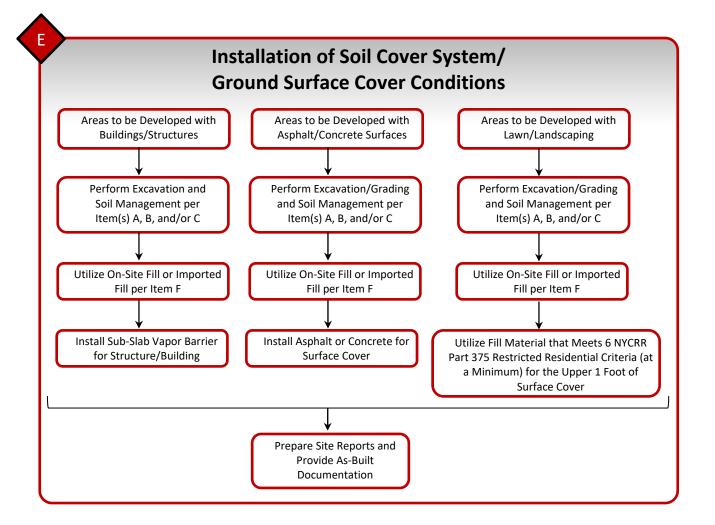


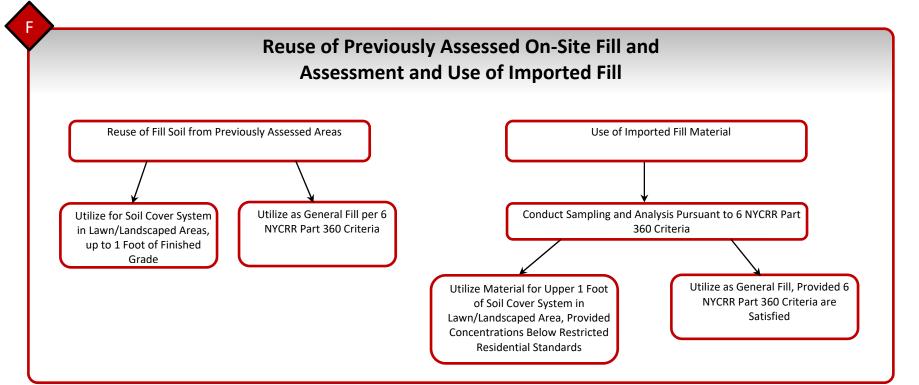
- 1. If ash/debris material is encountered, implement soil management procedures described in Item A.
- 2. If petroleum/chemical spill or contamination is encountered, implement soil management procedures described in Item C.
- 3. Reference Items D and E for procedures pertaining to site backfill/soil cover system and assessment for imported fill.

Soil Excavation/Ground Disturbance Activities – Petroleum/Chemical Spill or Contamination Encountered









APPENDIX C

Summary of Data from Previous Investigations

Table C-1
Summary of Information from September 2020 Investigation – Probes
(Information Available from Environmental Subsurface Investigation and Soil Sampling Report prepared by ATL and dated October 22, 2020)

Probe ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Samples Collected for Analysis of VOC	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO	Samples Collected for Analysis of Semi-VOC, PCB, Metals, Pesticides, and Cyanide	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO
B-1	20'	Coal Ash @ 0'.5 – 2'	ND				
B-2	20'	Coal Ash @ 0' – 20'	ND				
B-3	20'	Coal Ash @ 0' – 20'	ND				
B-4	20'	Coal Ash @ 0' – 18'	ND				
B-5	20'		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-6 and B-8)	Iron
B-6	20'		ND	Soil @ 10' – 15'		Soil @ 0' – 20' (Composite with B-5 and B-8)	See B-5
B-7	20'	Coal Ash @ 0' – 11'	ND				
B-8	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-5 and B-6)	See B-5
B-9	20'	Coal Ash @ 0.5' – 2.5'	ND – 18.2			,	
B-10	20'		ND			Soil @ 0' – 20' (Composite with B-11 and B-12)	4,4'-DDD, Arsenic, Iron, Vanadium
B-11	20'	Coal Ash @ 8' – 11.5'	ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-10 and B-12)	See B-10

Table C-1 (continued)
Summary of Information from September 2020 Investigation – Probes
(Information Available from Environmental Subsurface Investigation and Soil Sampling Report prepared by ATL and dated October 22, 2020)

Probe ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Samples Collected for Analysis of VOC	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO	Samples Collected for Analysis of Semi-VOC, PCB, Metals, Pesticides, and Cyanide	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO
B-12	20'		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-10 and B-11)	See B-10
B-13	20'		ND	Soil @ 10' – 15'	Acetone	Soil @ 0' – 20' (Composite with B-15 and B-16)	Iron, Vanadium
B-14	20'		ND				
B-15	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-13 and B-16)	See B-13
B-16	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-13 and B-15)	See B-13
B-17	20'		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-18 and B-19)	Iron, Vanadium
B-18	20'		ND	Soil @ 10' – 15'		Soil @ 0' – 20' (Composite with B-17 and B-19)	See B-17
B-19	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-17 and B-18)	See B-17
B-20	20'	Coal Ash @ 0' – 2'	ND				
B-21	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-22 and B-23)	Iron
B-22	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-21 and B-23)	See B-21
B-23	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-21 and B-22)	See B-21
B-24	20'		ND			Soil @ 0' – 20' (Composite with B-25)	Aluminum, Iron
B-25	20'		ND			Soil @ 0' – 20' (Composite with B-24)	See B-24
B-26	5.1' (Refusal)		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-27)	Iron
B-27	20'		ND			Soil @ 0' – 20' (Composite with B-26)	See B-26
B-28	20'		ND	Soil @ 10' – 15'		Soil @ 0' – 20' (Composite with B-29)	Iron

Table C-1 (continued)
Summary of Information from September 2020 Investigation – Probes
(Information Available from Environmental Subsurface Investigation and Soil Sampling Report prepared by ATL and dated October 22, 2020)

Probe ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Samples Collected for Analysis of VOC	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO	Samples Collected for Analysis of Semi-VOC, PCB, Metals, Pesticides, and Cyanide	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO
B-29	20'		ND			Soil @ 0' – 20' (Composite with B-28)	See B-28
B-30	10' (Refusal)		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-31)	Iron
B-31	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-30)	See B-30
B-32	20'		ND				
B-33	20'		ND				
B-34	20'		ND				
B-35	20'	Coal Ash @ 0' – 12.5'	ND				
B-36	20'	Coal Ash @ 0.5' – 6'	ND				
B-37	20'	Coal Ash @ 0.5' – 7.5'	ND				
B-38	20'	Coal Ash @ 0' – 11.5'	ND				
B-39	20'	Coal Ash @ 0' – 15'	ND				
B-40	20'	Coal Ash @ 0.5' – 20'	ND				
B-41	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-43)	4,4'-DDE, 4,4'-DDD, Aluminum, Calcium, Iron
B-42	20'	Coal Ash @ 0' – 8'	ND				
B-43	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-41)	See B-41

Table C-1 (continued)

Summary of Information from September 2020 Investigation – Probes

(Information Available from Environmental Subsurface Investigation and Soil Sampling Report prepared by ATL and dated October 22, 2020)

B-44 20' ND Soil @ 0' – 5' Soil @ 0' – 20' (Composite with B-45)	ing 6 NYCRR Unrestricted	Compou Exceeding 6 Part 375 Unre Use SC	Samples Collected for Analysis of Semi-VOC, PCB, Metals, Pesticides, and Cyanide	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO	Samples Collected for Analysis of VOC	VOC Field Screening (ppm)	Coal Ash/Debris Observations	Depth Advanced	Probe ID**
with B-40)	Iron	Iron	Soil @ 0' – 20' (Composite with B-45)		Soil @ 0' – 5'	ND		20'	B-44
B-45 20' ND Soil @ 10' - Acetone Soil @ 0' - 20' (Composite with B-44) See	e B-44	See B-4		Acetone	_	ND		20'	B-45

^{**} Approximate locations of probes are shown on the Aerial Overview of Affected Locations plan in Appendix D.

Table C-2 Summary of Information from February 2017 Investigation – Borings/Monitor Wells (Information Available from Draft Phase II Environmental Site Assessment Report prepared by Bergmann Associates and dated April 6, 2017)

Boring/ Monitor Well ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Groundwater Observations	Samples Collected for Metals Analysis	Metals Exceeding 6 NYCRR Part 375 Unrestricted Use Soil Cleanup Objectives				
B-1	100' (environmental assessment to 12')	Coal Ash @	0.0	Water @ 12.9'	0" - 2" (Soil)	Arsenic, Barium, Nickel				
		0' – 12'			10' – 12' (Soil)	Arsenic, Barium				
B-2	50' (environmental	Coal Ash @	0.0 – 2.9	Water @ 6'	0" - 2" (Soil)	Arsenic, Barium, Silver				
D Z	assessment to 10')	0' – 10'	0.0 2.3	Water @ 0	4' - 6' (Soil)	Arsenic, Barium, Chromium, Selenium, Silver				
B-3/ MW-	150'				0" - 2" (Soil)	Nickel				
1	(environmental	Coal Ash @	0.0 – 13.7	Water @ 14.9'	2' - 4' (Soil)	Silver				
•	assessment to 16')	· .	-	- · · · · · · · · · · · · · · · · · · ·	`	0' – 6'			Groundwater (Screened @ 12' – 22')	Iron, Manganese
					0" - 2" (Soil)	Arsenic, Barium, Mercury				
B-4/ MW- 3	100' (environmental assessment to 12')	(environmental	Coal Ash @ 0' – 12'	0.0 – 0.9		2' - 4' (Soil)	Arsenic, Barium, Mercury			
		0 12			Groundwater (Screened @ 5' – 15')	Iron, Sodium				
	50' (environmental assessment to 14')						0" - 2" (Soil)	Arsenic, Barium, Silver		
B-5/ MW- 2			2.9 – 22.9		4' - 6' (Soil)	Arsenic, Selenium, Silver				
		assessment to 14')	assessment to 14)				Groundwater (Screened @ 11' – 21')	Iron, Manganese		
B-6	-6 50' (environmental	Coal Ash @	0.0 - 0.2	Water @ 7.8'	0" – 2" (Soil)	Arsenic, Barium, Chromium, Nickel, Silver				
	assessment to 14')	0' – 14'			4' - 6' (Soil)	Arsenic, Barium, Nickel				
B-7	50' (environmental	Coal Ash @	0.1 – 0.2	Water @ 2.5'	0" - 2" (Soil)	Arsenic, Barium, Nickel, Silver				
D-1	assessment to 20')	0' – 18	0.1 – 0.2	vvalei @ 2.5	1' - 4' (Soil)	Arsenic, Barium, Chromium, Mercury, Nickel				
B-8	50' (environmental	Coal Ash @	0.1 – 0.6		0" - 2" (Soil)					
	assessment to 18')	6' – 18'			6' – 8' (Soil)					

Table C-3

Summary of Information from February 2017 Investigation – Test Pits

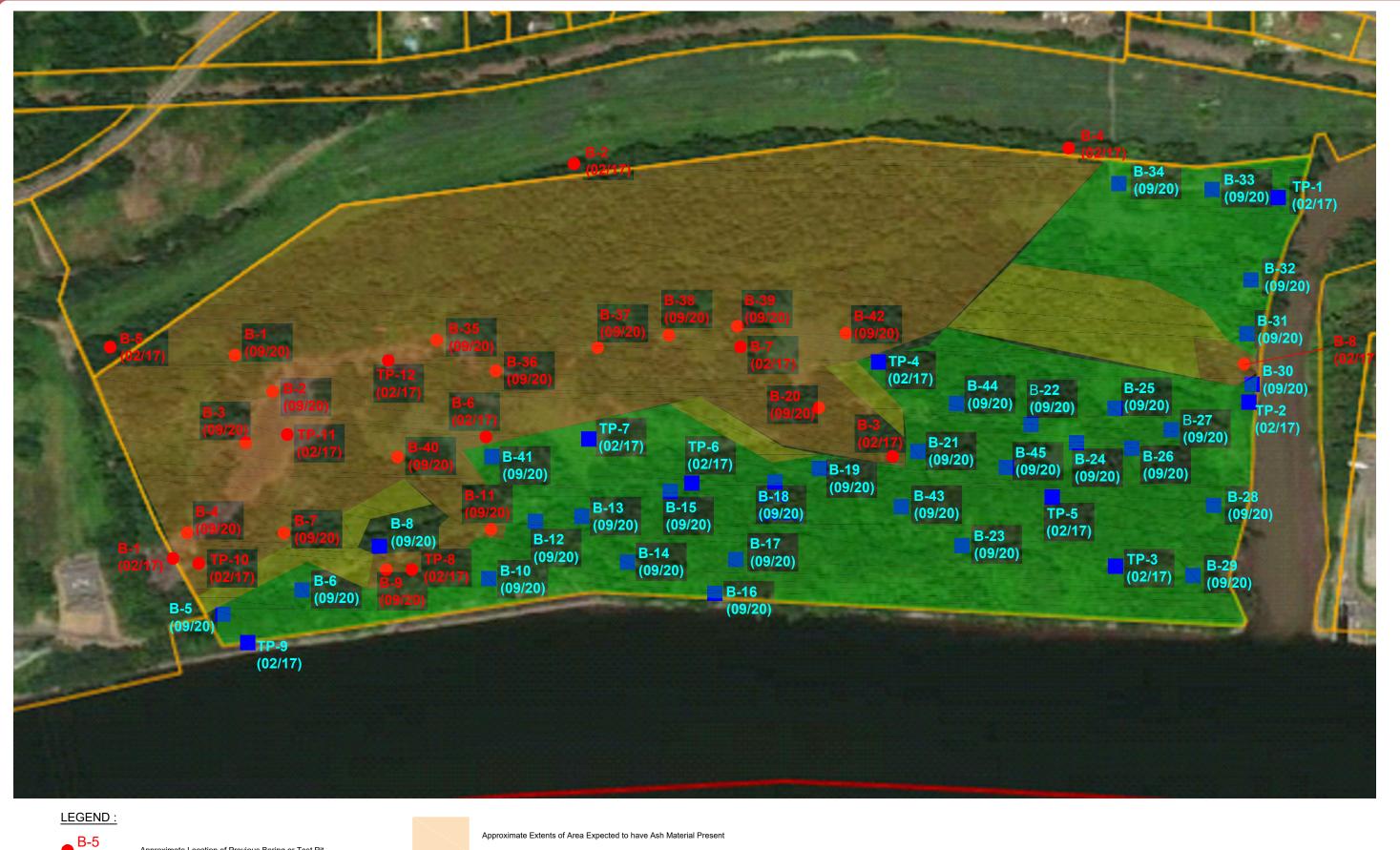
(Information Available from Draft Phase II Environmental Site Assessment Report prepared by Bergmann Associates and dated April 6, 2017)

Test Pit ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)
TP-1	12'		0.0 – 0.1
TP-2	12'		0.0 – 0.1
TP-3	12'		0.0 – 0.2
TP-4	12'		0.1 – 0.2
TP-5	12'		0.0 – 0.1
TP-6	12'		0.0
TP-7	12'		0.0
TP-8	12'	Railroad ties covered in black tar-like substance @ 8' – 12'	0.0 – 10.1
TP-9	10'		0.0
TP-10	12'	Coal Ash @ 0' – 12'	0.1
TP-11	12'	Coal Ash @ 0' – 12'	0.0 – 0.1
TP-12	12'	Coal Ash @ 0' – 12'	0.1

^{**} Approximate locations of test pits are shown on the Aerial Overview of Affected Locations plan in Appendix D.

APPENDIX D

Aerial Overview of Affected Locations



Approximate Location of Previous Boring or Test Pit with or Debris Ash Material Present (and Month/Year of Investigation)

(02/17)

Approximate Location of Previous Boring or Test Pit without Ash Material Present (and Month/Year of Investigation) Approximate Extents of Area with Potential to have Ash Material Present

AERIAL OVERVIEW OF AFFECTED LOCATIONS Drawn By: CJD Drawing:

Scale: As Noted Project No.: Date:

AT5596 October 2020

Approximate Extents of Area Not Expected to have Ash Material Present

Beacon Island Parcel Bethlehem, Albany County, New York



ATLANTIC TESTING LABORATORIES, Limited

Albany, NY Binghamton, NY Canton, NY Elmira, NY Poughkeepsie, NY Plattsburgh, NY Rochester, NY Syracuse, NY Utica, NY Watertown, NY

APPENDIX E

Sampling and Analysis Schedule for Fill

Sampling Criteria for Fill Material per 6 NYCRR Part 360.13(e)

	Number of Discrete Samples	Number of Composite Samples ¹	
Soil Quantity (cubic yards)	Volatile Organic Compounds (VOC)	Semi-VOC, Inorganics, Polychlorinated Biphenyls (PCB), and Pesticides	
0 – 300	2	1	
300 – 1,000	4	2	
1,000 - 10,000	6	3	
>10,000	2 for every additional 10,000 cubic yards	1 for every additional 10,000 cubic yards	

Notes: ¹Each composite sample will be comprised of 3 to 5 discrete samples from different locations within the fill material.

APPENDIX I

SEDIMENT BASIN CALCULATIONS

TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

Computed by	NSO	Date _	1/20/22	Checked by		Date
	of Albany				1/ WQ	v Pond #2
Location Expa				basin (≤50 Ac.)		
			N SIZE I			
						Top of Zone Elev
=	zone volume $= 3,600$ cu. f	t. x numbe	er of drainage	area acres = $19,0$	<u>80</u> cu. ft., To	op of Zone Elev
=	dth ratio = <u>3.6:1</u>	_				
	at 50% of sediment storag					
	below top of riser			0.00		0.15
5. Minimum su	rface area is larger of 0.01	l Q ₍₁₀₎	0.13 or, 0.	015 DA = 0.06	use _	U.15 acres
	DESIGN	OF SP	ILLWAY	S & ELEVAT	ΓIONS	
Runoff						n 1 (WQv Pond #2) has
	14.96	cfs (A	Attach runoff	computation sheets	s) to fun	uate storage and surface area action as a temporary nent basin. All pipes and
Pipe Spillway (Q						ures within basin are to be
	illway cap., $Q_{ps} = 0.2 x_{-}$				conct	red with filter fabric during ruction. Sediment cleanout is
	e is no emergency spillwa			$Q_{p(10)} = _{c}$		e place once final stabilization
8. H, head =	ft. Barrel length =	=	_ft		is rea	ched.
	inches; $Q_{ps} = (0)$					
	inches; Length				V	
11. Trash Rack:	Diameter =inch	es; H, hei	ght =	inches		
Emergency Spill	way Design					
12. Emergency S	Spillway Flow, $Q_{es} = Q_p$ - ($Q_{ps} = _{_{_{_{_{_{_{_{_{_{_{_{_{_{_{_{_{1}}}}}}}}$		=	cf	s.
13. Width	ft.; H _p ft	Crest ele	evation	; Design H	igh Water El	ev
Entrance cha	nnel slope			Γop of Dam Elev		
Exit channel	slope		%			
	ANTI-SEEP COI	LLAR/S	SEEPAG	E DIAPHRA	AGM DE	SIGN
Collars:						
	_ft.; z =:1; pipe	slope =	0/2 1	= ft		
	collars,i					
Diaphragms:	conars,	nenes squa	arc, projectio	nı —ıı.		
	_ width ft.	height	ft			
"						
	DEW	ATER	ING ORI	FICE SIZIN	\mathbf{G}	
	(Determ	nined fron	n the Dewater	ring Device Standa	rd)	
15. Dewatering of16. Design dewa	orifice diameter = days	inches. s (Min. 2 o	Skimmerlays required	or Riser (c)	heck one)	

TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

Computed by NSO	Date 1/20/22	Checked by	Date
Project Port of Albany		Basin # 2	
Location Expansion Site	Total Area draining to	basin (≤50 Ac.) <u>15.2</u>	Acres
	BASIN SIZE I	DESIGN	
 Sediment storage zone volume = 1,00 Dewatering zone volume = 3,600 cu. 	ft. x number of drainage		
3. Length to width ratio = 9.2:1			
4. A. Cleanout at 50% of sediment storaB. Distance below top of riser4.		6.75'	
5. Minimum surface area is larger of 0.0		015 DA = 0.23	use 0.57 acres
DESIGN	OF SPILLWAY	S & ELEVATIO	NS
Runoff			
6. $Q_{p(10)} = _{\underline{}}$	cfs (Attach runoff	computation sheets)	
Pipe Spillway (Q _{ps})			
7. Min. pipe spillway cap., $Q_{ps} = 0.2 x$			
Note: If there is no emergency spillw		$Q_{p(10)} = _{} cfs.$	
8. H, head = $\frac{5}{100}$ ft. Barrel length		c > 0.00 3.70	C
9. Barrel: Diam. 12 inches; $Q_{ps} = 10$. Riser: Diam. 15 inches; Length	(Q) 4.41 x (cor.	fac.) $0.80 = 3.78$	CIS.
11. Trash Rack: Diameter = 21 inc	n.; n = hes: H height =	inches	11.0
		micnes	
Emergency Spillway Design 12. Emergency Spillway Flow, Q _{es} = Q _p -	0 - 56.95	3 79 _ 53 16	S of
12. Emergency Spiriway Flow, $Q_{es} = Q_p$ - 13. Width 15 ft.; H_p 1 ft	$Q_{ps} = 00.90$ - Crest elevation	$\frac{0.79}{12.0} = \frac{33.10}{12.0}$	one CIS. Vater Elev. 13.0
Entrance channel slope 1		T <u>2.0</u> , Design High W Ton of Dam Elev 1	4 0
Entrance channel slope 1 Exit channel slope 3		rep er Bum Brev	
ANTI-SEEP CO	LLAR/SEEPAG	E DIAPHRAGN	A DESIGN
Collars:			
14. $y = 4.5$ ft.; $z = 2$:1; pipe	e slope =	$_{\rm s} = $ 27 ft.	
Use 2 collars, 4 - 0	inches square; projection	on = 1.4 ft.	
Diaphragms:			
# width ft	heightft.		
DEV	VATERING ORI	FICE SIZING	
(Deter	mined from the Dewater	ring Device Standard)	
15. Dewatering orifice diameter = 5 16. Design dewatering time 2 day	inches. Skimmer> /s (Min. 2 days required	check or Riser (check	one)

TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

Computed by NSO Date Date Date
Project Port of Albany Basin # 3
Location Expansion Site Total Area draining to basin (≤50 Ac.) 33.0 Acres
BASIN SIZE DESIGN
 Sediment storage zone volume = 1,000 cu. ft. x number of disturbed acres = 33,000 cu. ft., Top of Zone Elev. 7.5 Dewatering zone volume = 3,600 cu. ft. x number of drainage area acres = 118,800 cu. ft., Top of Zone Elev. 11.0 Length to width ratio = 11.6:1
 4. A. Cleanout at 50% of sediment storage zone volume, Elev. 6.75 B. Distance below top of riser 4.25 feet
5. Minimum surface area is larger of $0.01 Q_{(10)} = 1.11$ or, $0.015 DA = 1.49$ use 1.11 acres
DESIGN OF SPILLWAYS & ELEVATIONS
Runoff 6. $Q_{p(10)} = \underline{\hspace{1cm}}$ cfs (Attach runoff computation sheets)
Pipe Spillway (Q _{ps})
7. Min. pipe spillway cap., $Q_{ps} = 0.2 \text{ x}$ Drainage Area, acres = 6.6 cfs
Note: If there is no emergency spillway, then required $Q_{ps} = Q_{p(10)} = \underline{\hspace{1cm}}$ cfs.
8. H, head =5ft. Barrel length =115 _ft 9. Barrel: Diam15inches; Q _{ps} = (Q)7.78x (cor.fac.)0.85 _ =6.61cfs.
10. Riser: Diam. 18 inches; Length 4.5 ft.; $h = 1$ ft. Crest Elev. 11.0
11. Trash Rack: Diameter = 27 inches; H, height = 8 inches
Emergency Spillway Design
12. Emergency Spillway Flow, $Q_{es} = Q_p - Q_{ps} = 110.93$ - 6.61 = 104.32 cfs.
13. Width 30 ft.: H. 1 ft Crest elevation 12.0 : Design High Water Elev. 13.0
Entrance channel slope 1 %; Top of Dam Elev. 14.0 Exit channel slope 3 %
Exit channel slope%
ANTI-SEEP COLLAR/SEEPAGE DIAPHRAGM DESIGN
Collars:
14. $y = 4.5$ ft.; $z = 3$:1; pipe slope = 0.5 %, $L_s = 31.5$ ft.
Use 2 collars, 4 - 3 inches square; projection = 1.6 ft.
Diaphragms:
width ft. height ft.
DEWATERING ORIFICE SIZING
(Determined from the Dewatering Device Standard)
15. Dewatering orifice diameter = 7inches. Skimmer x or Riser (check one) 16. Design dewatering time days (Min. 2 days required)

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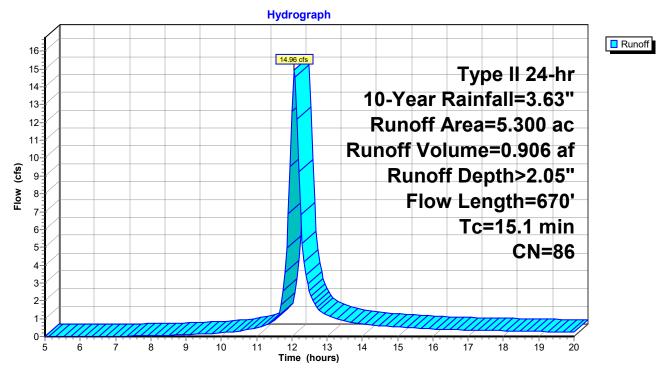
Summary for Subcatchment DA1: (new Subcat)

Runoff = 14.96 cfs @ 12.07 hrs, Volume= 0.906 af, Depth> 2.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area	(ac) C	N Desc	cription						
	0.850 96 Gravel surface, HSG D									
	2.	200 8	30 >759	>75% Grass cover, Good, HSG D						
_	2.250 89 Dirt roads, HSG D									
	5.	300 8	36 Wei	ghted Aver	age					
	5.	300	100.	00% Pervi	ous Area					
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.5	150	0.0200	0.72		Sheet Flow,				
						n= 0.023 P2= 2.40"				
	11.6	520	0.0025	0.75		Shallow Concentrated Flow,				
						Grassed Waterway Kv= 15.0 fps				
_	15 1	670	Total							

Subcatchment DA1: (new Subcat)



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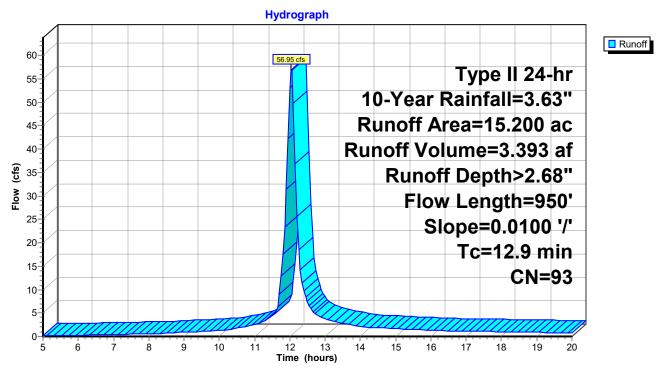
Summary for Subcatchment DA2: (new Subcat)

Runoff = 56.95 cfs @ 12.04 hrs, Volume= 3.393 af, Depth> 2.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area (ac) CN Description			cription		
*	6.	.900 98 Bldg A				
_				roads, HS	G D	
	15.200 93 Weighted Average			ghted Avei	age	
	8.300 54.61% Pervious Area					
	6.900 45.39% Impervious Area				/ious Area	
	Tc	Length		Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.6	150	0.0100	0.54		Sheet Flow,
						n= 0.023 P2= 2.40"
	8.3	800	0.0100	1.61		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	12 9	950	Total			

Subcatchment DA2: (new Subcat)



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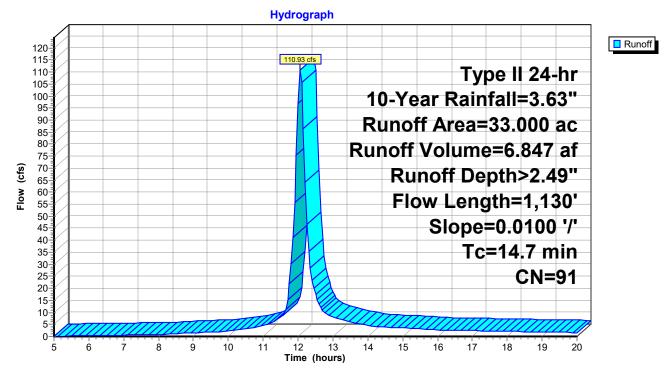
Summary for Subcatchment DA3: (new Subcat)

Runoff = 110.93 cfs @ 12.06 hrs, Volume= 6.847 af, Depth> 2.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type II 24-hr 10-Year Rainfall=3.63"

_	Area (ac) CN Description						
*	7.	000	98 Bldg B C D				
	26.000 89 Dirt roads, HSG D			roads, HS0	G D		
	33.000 91 Weighted Average			ghted Aver	age		
	26.000 78.79% Pervious Area					us Area	
	7.000 21.21% Impervious Area					ious Area	
	Tc (min)	Lengtl (feet		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	4.6	150	0.0	0100	0.54		Sheet Flow,
	10.1	980	0.0	0100	1.61		n= 0.023 P2= 2.40" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
	14.7	1,130) To	otal			

Subcatchment DA3: (new Subcat)



18641.00-Construction Activity

Type II 24-hr 10-Year Rainfall=3.63" Printed 1/25/2022

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Summary for Pond 2P: (new Pond)

Volume	Invert Ava	ail.Storage	Storage Description				
#1	6.00'	71,786 cf	Custom Stage Data (Irregular) Listed below (Recalc)				
Elevation (feet)	Surf.Area (sq-ft)		Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)		
6.00	9,449	976.0	0	0	9,449		
7.00	11,415	988.9	10,417	10,417	11,693		
7.50	12,407	995.0	5,954	16,370	12,776		
11.00	19,527	1,039.0	55,416	71,786	20,738		

Prepared by McFarland Johnson

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Summary for Pond 3p: (new Pond)

Volume	Invert	Avail	.Storage	Storage Description	n			
#1	6.00'	156,085 cf		Custom Stage Data (Irregular) Listed below (Recalc)				
Elevation (feet)	Surf (s	Area sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)		
6.00	21	,679	1,328.0	0	0	21,679		
6.50	23	3,679	1,338.0	11,336	11,336	23,903		
7.00	25	,694	1,347.0	12,340	23,676	25,940		
7.50	27	,044	1,353.0	13,183	36,859	27,395		
11.00	41	,606	1,419.0	119,226	156,085	42,740		

APPENDIX J

DRAFT NOI

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NOI for coverage under Stormwater General Permit for Construction Activity

version 1.35

(Submission #: HPE-0QXG-AE8EZ, version 1)

Details

Originally Started By Natalie Olivieri

Alternate Identifier Marmen-Welcon Tower Manufacturing Plant

Submission ID HPE-0QXG-AE8EZ

Submission Reason New

Status Draf

Active Steps Form Submitted

Form Input

Owner/Operator Information

Owner/Operator Name (Company/Private Owner/Municipality/Agency/Institution, etc.)

Albany Port District Commission

Owner/Operator Contact Person Last Name (NOT CONSULTANT)

Hendrick

Owner/Operator Contact Person First Name

Richard

Owner/Operator Mailing Address

106 Smith Boulevard

City

Albany

State

New York

Zip

12205

Phone

5184638763

Emai

rhendrick@portofalbany.us

Federal Tax ID

14-6002520

Project Location

Project/Site Name

Marmen-Welcon Tower Manufacturing Plant

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Street Address (Not P.O. Box)

309 River Road

Side of Street

East

City/Town/Village (THAT ISSUES BUILDING PERMIT)

Town of Bethlehem

State

NY

Zip

12077

DEC Region

4

County

ALBANY

Name of Nearest Cross Street

Old River Road

Distance to Nearest Cross Street (Feet)

970

Project In Relation to Cross Street

South

Tax Map Numbers Section-Block-Parcel

98.00-2-10.23

Tax Map Numbers

98.01-2-1.0

1. Coordinates

Provide the Geographic Coordinates for the project site. The two methods are:

- Navigate to the project location on the map (below) and click to place a marker and obtain the XY coordinates.
- The "Find Me" button will provide the lat/long for the person filling out this form. Then pan the map to the correct location and click the map to place a marker and obtain the XY coordinates.

Navigate to your location and click on the map to get the X,Y coordinates

42.602283629058164,-73.76555834600738

Project Details

2. What is the nature of this project?

New Construction

3. Select the predominant land use for both pre and post development conditions.

Pre-Development Existing Landuse

Forest

Post-Development Future Land Use

Industrial

3a. If Single Family Subdivision was selected in question 3, enter the number of subdivision lots.

NONE PROVIDED

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^{4.} In accordance with the larger common plan of development or sale, enter the total project site acreage, the acreage to be disturbed and the future impervious area (acreage) within the disturbed area.

*** ROUND TO THE NEAREST TENTH OF AN ACRE. *** **Total Site Area (acres)** 108.6 **Total Area to be Disturbed (acres)** 72.7 **Existing Impervious Area to be Disturbed (acres) Future Impervious Area Within Disturbed Area (acres)** 65.9 5. Do you plan to disturb more than 5 acres of soil at any one time? Yes 6. Indicate the percentage (%) of each Hydrologic Soil Group(HSG) at the site. A (%) 3.2 B (%) C (%) D (%) 96.8 7. Is this a phased project? Yes 8. Enter the planned start and end dates of the disturbance activities. **Start Date** 6/1/2022 **End Date** 9/1/2023 9. Identify the nearest surface waterbody(ies) to which construction site runoff will discharge. Hudson River, Normans Kill, Wetland 9a. Type of waterbody identified in question 9? Wetland/Federal Jurisdiction On Site (Answer 9b) River On Site Stream/Creek On Site Other Waterbody Type Off Site Description NONE PROVIDED 9b. If "wetland" was selected in 9A, how was the wetland identified? Delineated by Consultant 10. Has the surface waterbody(ies in question 9 been identified as a 303(d) segment in Appendix E of GP-0-20-001? No 11. Is this project located in one of the Watersheds identified in Appendix C of GP-0-20-001? 12. Is the project located in one of the watershed areas associated with AA and AA-S classified waters? No

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If No, skip question 13.

13. Does this construction activity disturb land with no existing impervious cover and where the Soil Slope Phase is identified as D (provided the map unit name is inclusive of slopes greater than 25%), E or F on the USDA Soil Survey?

NONE PROVIDED

If Yes, what is the acreage to be disturbed?

NONE PROVIDED

- 14. Will the project disturb soils within a State regulated wetland or the protected 100 foot adjacent area? Yes
- 15. Does the site runoff enter a separate storm sewer system (including roadside drains, swales, ditches, culverts, etc)?

No

- **16. What is the name of the municipality/entity that owns the separate storm sewer system?**NONE PROVIDED
- 17. Does any runoff from the site enter a sewer classified as a Combined Sewer?
- 18. Will future use of this site be an agricultural property as defined by the NYS Agriculture and Markets Law?
- 19. Is this property owned by a state authority, state agency, federal government or local government? Yes
- 20. Is this a remediation project being done under a Department approved work plan? (i.e. CERCLA, RCRA, Voluntary Cleanup Agreement, etc.)
 No

Required SWPPP Components

- 21. Has the required Erosion and Sediment Control component of the SWPPP been developed in conformance with the current NYS Standards and Specifications for Erosion and Sediment Control (aka Blue Book)?
 Yes
- 22. Does this construction activity require the development of a SWPPP that includes the post-construction stormwater management practice component (i.e. Runoff Reduction, Water Quality and Quantity Control practices/techniques)?

Yes

If you answered No in question 22, skip question 23 and the Post-construction Criteria and Post-construction SMP Identification sections.

- 23. Has the post-construction stormwater management practice component of the SWPPP been developed in conformance with the current NYS Stormwater Management Design Manual?

 No
- **24.** The Stormwater Pollution Prevention Plan (SWPPP) was prepared by: Professional Engineer (P.E.)

SWPPP Preparer

Adam Frosino

Contact Name (Last, Space, First)

Frosino, Adam

Mailing Address

60 Railroad Place, Suite 402

City

Saratoga Springs

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State

NY

Zip

12866

Phone

5185809380

Email

afrosino@mjinc.com

Download SWPPP Preparer Certification Form

Please take the following steps to prepare and upload your preparer certification form:

- 1) Click on the link below to download a blank certification form
- 2) The certified SWPPP preparer should sign this form
- 3) Scan the signed form
- 4) Upload the scanned document

Download SWPPP Preparer Certification Form

Please upload the SWPPP Preparer Certification

SWPPP Preparer Cert_Signed.pdf - 05/24/2022 10:45 AM

Comment

NONE PROVIDED

Erosion & Sediment Control Criteria

25. Has a construction sequence schedule for the planned management practices been prepared? Yes

26. Select all of the erosion and sediment control practices that will be employed on the project site:

Temporary Structural

Check Dams

Construction Road Stabilization

Dust Control

Perimeter Dike/Swale

Sediment Basin

Sediment Traps

Silt Fence

Stabilized Construction Entrance

Storm Drain Inlet Protection

Biotechnical

None

Vegetative Measures

Mulching

Seeding

Temporary Swale

Topsoiling

Permanent Structural

Lined Waterway (Rock)

Land Grading

Retaining Wall

Rock Outlet Protection

Streambank Protection

Other

NONE PROVIDED

Post-Construction Criteria

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* IMPORTANT: Completion of Questions 27-39 is not required if response to Question 22 is No.

27. Identify all site planning practices that were used to prepare the final site plan/layout for the project.

Preservation of Undisturbed Area Preservation of Buffers

Reduction of Clearing and Grading

27a. Indicate which of the following soil restoration criteria was used to address the requirements in Section 5.1.6("Soil Restoration") of the Design Manual (2010 version).

All disturbed areas will be restored in accordance with the Soil Restoration requirements in Table 5.3 of the Design Manual (see page 5-22).

28. Provide the total Water Quality Volume (WQv) required for this project (based on final site plan/layout). (Acre-feet) 6.29

29. Post-construction SMP Identification

Use the Post-construction SMP Identification section to identify the RR techniques (Area Reduction), RR techniques(Volume Reduction) and Standard SMPs with RRv Capacity that were used to reduce the Total WQv Required (#28).

Identify the SMPs to be used by providing the total impervious area that contributes runoff to each technique/practice selected. For the Area Reduction Techniques, provide the total contributing area (includes pervious area) and, if applicable, the total impervious area that contributes runoff to the technique/practice.

Note: Redevelopment projects shall use the Post-Construction SMP Identification section to identify the SMPs used to treat and/or reduce the WQv required. If runoff reduction techniques will not be used to reduce the required WQv, skip to question 33a after identifying the SMPs.

30. Indicate the Total RRv provided by the RR techniques (Area/Volume Reduction) and Standard SMPs with RRv capacity identified in question 29. (acre-feet)

1.45

31. Is the Total RRv provided (#30) greater than or equal to the total WQv required (#28)?

If Yes, go to question 36. If No, go to question 32.

32. Provide the Minimum RRv required based on HSG. [Minimum RRv Required = (P) (0.95) (Ai) / 12, Ai=(s) (Aic)] (acre-feet)

1.32

32a. Is the Total RRv provided (#30) greater than or equal to the Minimum RRv Required (#32)? Yes

If Yes, go to question 33.

Note: Use the space provided in question #39 to summarize the specific site limitations and justification for not reducing 100% of WQv required (#28). A detailed evaluation of the specific site limitations and justification for not reducing 100% of the WQv required (#28) must also be included in the SWPPP.

If No, sizing criteria has not been met; therefore, NOI can not be processed. SWPPP preparer must modify design to meet sizing criteria.

33. SMPs

Use the Post-construction SMP Identification section to identify the Standard SMPs and, if applicable, the Alternative SMPs to be used to treat the remaining total WQv (=Total WQv Required in #28 - Total RRv Provided in #30).

Also, provide the total impervious area that contributes runoff to each practice selected.

NOTE: Use the Post-construction SMP Identification section to identify the SMPs used on Redevelopment projects.

33a. Indicate the Total WQv provided (i.e. WQv treated) by the SMPs identified in question #33 and Standard SMPs with RRv Capacity identified in question #29. (acre-feet) 4.85

Note: For the standard SMPs with RRv capacity, the WQv provided by each practice = the WQv calculated using the contributing drainage area to the practice - provided by the practice. (See Table 3.5 in Design Manual)

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34. Provide the sum of the Total RRv provided (#30) and the WQv provided (#33a).

6.31

35. Is the sum of the RRv provided (#30) and the WQv provided (#33a) greater than or equal to the total WQv required (#28)?

Yes

If Yes, go to question 36.

If No, sizing criteria has not been met; therefore, NOI can not be processed. SWPPP preparer must modify design to meet sizing criteria.

36. Provide the total Channel Protection Storage Volume (CPv required and provided or select waiver (#36a), if applicable.

CPv Required (acre-feet)

0.93

CPv Provided (acre-feet)

1.17

36a. The need to provide channel protection has been waived because:

NONE PROVIDED

37. Provide the Overbank Flood (Qp) and Extreme Flood (Qf) control criteria or select waiver (#37a), if applicable.

Overbank Flood Control Criteria (Qp)

Pre-Development (CFS)

73.24

Post-Development (CFS)

12.46

Total Extreme Flood Control Criteria (Qf)

Pre-Development (CFS)

163.60

Post-Development (CFS)

30.97

37a. The need to meet the Qp and Qf criteria has been waived because:

NONE PROVIDED

38. Has a long term Operation and Maintenance Plan for the post-construction stormwater management practice(s) been developed?

Yes

If Yes, Identify the entity responsible for the long term Operation and Maintenance

Albany Port District Commission

39. Use this space to summarize the specific site limitations and justification for not reducing 100% of WQv required (#28). (See question #32a) This space can also be used for other pertinent project information.

The proposed Facility requires 85 acres of usable manufacturing and storage space along the Hudson River. This site was chosen given it is located adjacent to the existing Port of Albany and is directly on the Hudson River. However, the usable portion of the site adjacent to the Hudson River, is only 66-acre area. Therefore, the entirety of the site is needed for the OSW manufacturing process, with an ancillary receiving site located at 700 Smith Boulevard.

Responses to questions 36 and 37 are related only to Analysis Point #1A. Analysis Points #1, #2, and #3 have direct discharge to tidal waters and therefore are waived from meeting the CPv, Qp, and Qf requirements.

Post-Construction SMP Identification

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Runoff Reduction (RR) Techniques, Standard Stormwater Management Practices (SMPs) and Alternative SMPs

Identify the Post-construction SMPs to be used by providing the total impervious area that contributes runoff to each technique/practice selected. For the Area Reduction Techniques, provide the total contributing area (includes pervious area) and, if applicable, the total impervious area that contributes runoff to the technique/practice.

RR Techniques (Area Reduction)

Round to the nearest tenth

Total Contributing Acres for Conservation of Natural Area (RR-1)

4.0

Total Contributing Impervious Acres for Conservation of Natural Area (RR-1)

0

Total Contributing Acres for Sheetflow to Riparian Buffers/Filter Strips (RR-2)

NONE PROVIDED

Total Contributing Impervious Acres for Sheetflow to Riparian Buffers/Filter Strips (RR-2)

NONE PROVIDED

Total Contributing Acres for Tree Planting/Tree Pit (RR-3)

NONE PROVIDED

Total Contributing Impervious Acres for Tree Planting/Tree Pit (RR-3)

NONE PROVIDED

Total Contributing Acres for Disconnection of Rooftop Runoff (RR-4)

NONE PROVIDED

RR Techniques (Volume Reduction)

Total Contributing Impervious Acres for Disconnection of Rooftop Runoff (RR-4)

NONE PROVIDED

Total Contributing Impervious Acres for Vegetated Swale (RR-5)

NONE PROVIDED

Total Contributing Impervious Acres for Rain Garden (RR-6)

NONE PROVIDED

Total Contributing Impervious Acres for Stormwater Planter (RR-7)

NONE PROVIDED

Total Contributing Impervious Acres for Rain Barrel/Cistern (RR-8)

NONE PROVIDED

Total Contributing Impervious Acres for Porous Pavement (RR-9)

NONE PROVIDED

Total Contributing Impervious Acres for Green Roof (RR-10)

NONE PROVIDED

Standard SMPs with RRv Capacity

Total Contributing Impervious Acres for Infiltration Trench (I-1)

NONE PROVIDED

Total Contributing Impervious Acres for Infiltration Basin (I-2)

1

Total Contributing Impervious Acres for Dry Well (I-3)

NONE PROVIDED

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Total Contributing Impervious Acres for Underground Infiltration System (I-4)

23.7

Total Contributing Impervious Acres for Bioretention (F-5)

NONE PROVIDED

Total Contributing Impervious Acres for Dry Swale (O-1)

0.05

Standard SMPs

Total Contributing Impervious Acres for Micropool Extended Detention (P-1)

5 1

Total Contributing Impervious Acres for Wet Pond (P-2)

NONE PROVIDED

Total Contributing Impervious Acres for Wet Extended Detention (P-3)

NONE PROVIDED

Total Contributing Impervious Acres for Multiple Pond System (P-4)

NONE PROVIDED

Total Contributing Impervious Acres for Pocket Pond (P-5)

NONE PROVIDED

Total Contributing Impervious Acres for Surface Sand Filter (F-1)

NONE PROVIDED

Total Contributing Impervious Acres for Underground Sand Filter (F-2)

NONE PROVIDED

Total Contributing Impervious Acres for Perimeter Sand Filter (F-3)

NONE PROVIDED

Total Contributing Impervious Acres for Organic Filter (F-4)

NONE PROVIDED

Total Contributing Impervious Acres for Shallow Wetland (W-1)

NONE PROVIDED

Total Contributing Impervious Acres for Extended Detention Wetland (W-2)

NONE PROVIDED

Total Contributing Impervious Acres for Pond/Wetland System (W-3)

NONE PROVIDED

Total Contributing Impervious Acres for Pocket Wetland (W-4)

NONE PROVIDED

Total Contributing Impervious Acres for Wet Swale (O-2)

NONE PROVIDED

Alternative SMPs (DO NOT INCLUDE PRACTICES BEING USED FOR PRETREATMENT ONLY)

Total Contributing Impervious Area for Hydrodynamic

NONE PROVIDED

Total Contributing Impervious Area for Wet Vault

NONE PROVIDED

Total Contributing Impervious Area for Media Filter

NONE PROVIDED

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"Other" Alternative SMP?

Contech Jellyfish Filter

Total Contributing Impervious Area for "Other"

54.7

Provide the name and manufaturer of the alternative SMPs (i.e. proprietary practice(s)) being used for WQv treatment.

Note: Redevelopment projects which do not use RR techniques, shall use questions 28, 29, 33 and 33a to provide SMPs used, total WQv required and total WQv provided for the project.

Manufacturer of Alternative SMP

Contech

Name of Alternative SMP

Jellyfish Filter

Other Permits

40. Identify other DEC permits, existing and new, that are required for this project/facility.

Endangered or Threatened Species (Incidental Take Permit)

If SPDES Multi-Sector GP, then give permit ID

NONE PROVIDED

If Other, then identify

Wetland Joint Permit, Air State Facility Permit

41. Does this project require a US Army Corps of Engineers Wetland Permit?

Yes

If "Yes," then indicate Size of Impact, in acres, to the nearest tenth

0.9

42. If this NOI is being submitted for the purpose of continuing or transferring coverage under a general permit for stormwater runoff from construction activities, please indicate the former SPDES number assigned.

NONE PROVIDED

MS4 SWPPP Acceptance

43. Is this project subject to the requirements of a regulated, traditional land use control MS4?

Yes - Please attach the MS4 Acceptance form below

If No, skip question 44

44. Has the "MS4 SWPPP Acceptance" form been signed by the principal executive officer or ranking elected official and submitted along with this NOI?

NONE PROVIDED

MS4 SWPPP Acceptance Form Download

Download form from the link below. Complete, sign, and upload. MS4 SWPPP Acceptance Form

MS4 Acceptance Form Upload

NONE PROVIDED Comment

NONE PROVIDED

Owner/Operator Certification

Owner/Operator Certification Form Download

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Download the certification form by clicking the link below. Complete, sign, scan, and upload the form. <u>Owner/Operator Certification Form (PDF, 45KB)</u>

Upload Owner/Operator Certification Form

POA - eNOI Owner Cert_Signed.pdf - 05/24/2022 11:52 AM

Comment

NONE PROVIDED

Attachments

Date	Attachment Name	Context	User
5/24/2022 11:52 AM	POA - eNOI Owner Cert_Signed.pdf	Attachment	Natalie Olivieri
5/24/2022 10:45 AM	SWPPP Preparer Cert_Signed.pdf	Attachment	Natalie Olivieri

Status History

	User	Processing Status
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Under Review	DAVID GASPER	
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APPENDIX K

UNIFORM PROCEDURES ACT EXCEPTION LETTER

NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION

Division of Environmental Permits
625 Broadway, 4th Floor, Albany, New York 12233-1750
P: (518) 402-9167 | F: (518) 402-9168 | deppermitting@dec.ny.gov
www.dec.ny.gov

March 30, 2022

VIA EMAIL

Richard Hendrick Albany Port District Commission 106 Smith Boulevard Albany, NY 12202 rhendrick@portofalbany.us

RE: SPDES GP-0-20-001 - Commencement of Limited Construction Activities

Port of Albany Expansion Project

Beacon Island Parcel, Bethlehem NY, Albany County

DEC # 4-0122-00322/00002

Dear Mr. Hendrick:

By letter dated March 25, 2022, Albany Port District Commission (APDC) requested to commence limited construction activities (i.e., tree clearing), and authorization to discharge pursuant to the Stormwater State Pollutant Discharge Elimination System (SPDES) General Permit for Construction Activity (GP-0-20-001), for the Port of Albany Expansion Project (Project) prior to obtaining all necessary permits from New York State Department of Environmental Conservation (NYSDEC or Department). APDC has not obtained an Air State Facility (ASF) permit, individual SPDES permit, Part 182 permit, Protection of Waters permits and Water Quality Certification (WQC) ("Uniform Procedures Act (UPA) Permits"). APDC asserts in its request that good cause exists based on its committed construction schedule and specific requirements for site preparation, construction, and operational components. Pursuant to 6 NYCRR 621.3(a)(4), based on permitting considerations and the specific circumstances presented here, NYSDEC reviewed the March 25, 2022 request from APDC and determined that there is good cause to allow the commencement of limited construction activities² as further described herein, without all UPA Permits having been obtained.

² Construction [Activities] are defined in GP-0-20-001 as, "any clearing, grading, excavation, filling, demolition or stockpiling activities that result in soil disturbance. Clearing activities can include, but are not limited to, logging equipment operation, the cutting and skidding of trees, stump removal and/or brush root removal. Construction activity does not include routine maintenance that is performed to maintain the original line and grade, hydraulic capacity, or original purpose of a facility."



¹According to Part II(C)(1) of GP-0-20-001, an owner or operator shall not commence any construction activity in any location until the authorization to discharge under the General Permit goes into effect. Additionally, under Part II(C)(2)(b) of GP-0-20-001, authorization to discharge under the permit will be effective, among other requirements, when the owner or operator has obtained, "all necessary Department permits subject to the Uniform Procedures Act ("UPA") (see 6 NYCRR Part 621), or the equivalent from another New York State agency" unless otherwise notified by the Department pursuant to 6 NYCRR 621.3(a)(4).

Demonstration of Good Cause

In evaluating whether there is good cause for NYSDEC to grant an exception to the authorization criterion contained in Part II(C)(2)(b) of SPDES GP-0-20-0001, and allow authorization to discharge and the commencement of limited construction activities prior to obtaining all other necessary UPA permits, NYSDEC has considered the following factors:

- Pursuant to UPA regulations, Section 621.3(a)(4), APDC has submitted all applications for UPA Permits for the Project.
- The requirements of the State Environmental Quality Review Act (SEQR Article 8 of the ECL) have been satisfied,³ as follows: (i) The Town of Bethlehem Planning Board was established as SEQR Lead Agency (Lead Agency) and a positive declaration was issued requiring a Draft Generic Environmental Impact Statement (GEIS) for the Project; (ii) a Final GEIS was accepted as complete and a SEQR Findings Statement was adopted by the Lead Agency on June 2, 2020 for the Project; (iii) the Lead Agency determined the Project may have potential to create one or more significant adverse environmental impacts not evaluated within the Final GEIS and issued a Positive Declaration requiring a Supplemental Draft EIS on July 6, 2021; and (iv) a Supplemental Final EIS was accepted as complete and a SEQR Findings Statement was adopted by the Lead Agency on March 15, 2022 for the Project.
- The requirements of the State Historic Preservation Act (SHPA),⁴ have been complied with for the Project, as follows:
 - The Stockbridge Munsee Community issued their opinion in a March 2, 2022 letter that the Project will have No Adverse Effect on Historic Resources.
 - o The New York State Historic Preservation Office (SHPO) issued a letter on March 25, 2022, stating that that no historic properties, including archaeological and/or historic resources, will be Adversely Affected by the Project, provided that a Restrictive Deed Covenant is filed to protect and maintain the vegetated buffer along the Hudson River shoreline.
- APDC has prepared a Stormwater Pollution Prevention Plan (SWPPP) for tree clearing activities.
- On March 29, 2022, the Town of Bethlehem as a regulated, traditional land use control Municipal Separate Stormwater Sewer Systems (MS4) accepted the SWPPP for tree clearing activities.
- APDC has indicated that to meet its contractual obligations with Equinor to be operational by December 1, 2023, tree clearing must take place by mid-April 2022 to facilitate site preparation, including implementation of a 3-month surcharge program to address poor soils and settlement concerns.
- APDC has indicated that the UPA Permits for the operational components of the Project (ASF and individual SPDES permits) require selection of manufacturing and processing equipment that must follow the Port of Albany procurement process and therefore, not all information is available prior to the construction bid. This information is required for NYSDEC to issue the ASF and individual SPDES permits.

³ See Part II.C(2)(a) of SPDES GP-0-20-001

⁴ See Part I.F(8)(b)(iv) of SPDES GP-0-20-001

Commencement of Limited Construction Activities

In consideration of the factors identified above, NYSDEC is hereby granting a limited exception to the authorization criterion contained in Part II(C)(2)(b) of SPDES GP-0-20-001. Upon submission of a complete eNOI, APDC would be authorized to commence limited construction activities, (i.e., tree clearing), under SPDES GP-0-20-001 and pursuant to the SWPPP approved by the Town of Bethlehem on March 29, 2022, subject to the following limitations:

- 1. No permanent construction, including building supports and foundations, can commence until the Air State Facility permit is obtained.⁵
- 2. No construction of the Project's wastewater treatment facility can commence until the individual SPDES permit is issued and plan approval for the wastewater treatment facility has been obtained from NYSDEC.
- 3. No excavation, fill, or dredging activities can commence in any wetlands or other waters of the U.S., including the Hudson River, Normans Kill, and federally regulated wetlands, until the following Permits are issued: Part 182, Protection of Waters, and WQC.
- 4. If tree clearing is conducted within federal wetlands, it must only be done using hand equipment and no stumps shall be removed.
- 5. No trees shall be removed within the vegetated buffer area, located along the Hudson River, in contravention of the Restrictive Deed Covenant that APDC has agreed to establish.
- 6. If any bats are observed flying from a tree that will be cut, work activities shall be stopped immediately and NYSDEC shall be contacted for guidance (see #5 in the following link: https://www.dec.ny.gov/animals/106090.html).
- 7. All other applicable terms and conditions of SPDES GP-0-20-001 are satisfied and complied with.

This exception to Part II(C)(2)(b) of SPDES GP-0-20-001 for the limited construction activities (i.e., tree clearing) is only authorized until May 15, 2022, or until NYSDEC issues all UPA Permits, whichever comes first. Please also note that granting of this exception does not guarantee issuance of the individual permits identified above as the permits are still subject to public review and comment, and other applicable provisions of 6 NYCRR Part 621. Further, this exception does not apply to construction activities that would be commenced beyond tree clearing. As a result, APDC assumes all risks in commencing construction.

Please contact me at karen.gaidasz@dec.ny.gov if you have any questions or concerns.

Sincerely,

(Maen M. Gridan

Karen M. Gaidasz, Chief

Offshore Wind & Hydroelectric Section Bureau of Energy Project Management

⁵ NYCRR 201-2.1(b)(9), specifically excludes site clearing and excavation activities, it states, "[t]he initiation of physical on-site construction activities which are of a permanent nature excluding site clearing and excavation. Such activities include, but are not limited to, installation of building supports and foundations, laying underground pipework and construction of permanent storage structures."

APPENDIX L

5 ACRE WAIVER REQUEST



60 Railroad Place, Suite 402 • Saratoga Springs, NY 12866 Phone: (518) 580-9380 • Fax: (518) 580-9383 www.mjinc.com

May 20, 2022

Paul Penman, P.E.
Town Engineer, Deputy Commissioner of Public Works
Town of Bethlehem
445 Delaware Avenue
Delmar, New York 12054

Re: SPDES General Permit for Storm Water Discharges from Construction Activity – Marmen-Welcon Tower Manufacturing Plant

Mr. Penman,

We are hereby requesting approval to disturb more than 5 acres of soil at a time for the Marmen-Welcon Tower Manufacturing Plant project.

Activities related to the above construction site will comply with all other requirements under GP-0-20-001. As such, SWPPP inspections will be conducted twice weekly while more than 5 acres of soil are disturbed.

The project has been split into five (5) phases spanning 20 months as shown on the project's Erosion and Sediment Control plans. The maximum soil disturbance at one time is anticipated to be around 12-15 acres as partial disturbance in two phases may occur simultaneously for short durations given the nature of the project. The anticipated soil disturbance areas and durations for each phase are as follows:

SOIL DISTURBANCE PHASING		
PHASE	DISTURBANCE AREA	DURATION
1	8.5 ACRES	2 MONTHS
2	11.3 ACRES	2 MONTHS
3	11.0 ACRES MAX	
3A	9.7 ACRES	
3B	9.6 ACRES	C NAONITUG
3C	10.0 ACRES	6 MONTHS
3D	10.1 ACRES	
3E	10.0 ACRES	
3F	3.5 ACRES	
4	NO NEW AREAS	4 MONTHS
5	5.1 ACRES	8 MONTHS

Disturbances associated with Phases 1 and 2 are expected to take place concurrently over a 2-month period. During these phases the construction entrance (including rock hammering), staging area, and site access roads will be established, as well as temporary sediment basins #1, #2, and #3. Any additional sediment controls not installed during the site tree cutting are to be installed during this phase.

During Phase 3 the site will be grubbed, and mass site grading will occur in preparation for the stone aggregate surcharging. Approximately 98,000 CY of on-site cut material will be used as fill to balance out the site. In addition, approximately 150,000-200,000 CY of suitable fill will be brought in to bring the site up to the sub-grade elevation.

The large grubbing area as well as the large amount of mass grading required resulted in breaking up Phase 3 into sub-phases of roughly 10 acres each. The sub-phases were determined based on overall project sequencing to start at the south end with Building A preparation, as well as establishing approximate areas where borrowing and fill will occur within each sub-area. Limits of disturbance to be minimized in each sub-phase by stabilizing areas within 2 days of achieving final grade. The sub-phase areas will be disturbed and stabilized in a rolling operation as the earthwork progresses from the south end of the site to the north end with disturbance ranging from 8-11 acres. The disturbance envelope ranges from 700 feet initially to 400 feet as earthwork progresses. To avoid stockpiling, available cut material from one sub-phase area that no longer requires any additional fill may be deposited and stabilized within another sub-phase area; however, the overall total disturbed area during Phase 3 shall not exceed 11.0 acres. Fine earthwork grading and subgrade preparation under the surcharge areas in accordance with the project's geotechnical report will also occur during this phase. In accordance with the SWPPP, all areas which are not active will be temporarily stabilized.

During Phase 4, approximately 700,000 CY of stone aggregate will be imported and stockpiled on the proposed building pads as a temporary building pad surcharge and will be used as the future stone yard area. It is anticipated that the subbase stone will begin to be brought into the site as the building footprint subgrade is completed for each sub-phase of Phase 3. As the stone aggregate is brought onto the site and placed in the surcharge areas it will act as permanent stabilization therefore decreasing the disturbed area. Given the volume of material to be brought into the site, this will take some time and will be completed in a rolling fashion in a similar fashion to Phase 3. The first building's surcharge import (Building A) will be completed to enable the surcharging compaction timeframe to start prior to placing the stone aggregate surcharge on the next building pad. Any peripheral subgrade areas previously disturbed or disturbed as part of the surcharge operations and no longer active will be temporarily stabilized in accordance with the SWPPP.

Phase 5 includes spreading the stone aggregate surcharge material to establish the stone yard area and all remaining construction on the project. Once the proposed drainage system and second pond have been installed and are operational, the temporary sediment basins will be removed as well as the conversion and installation of the permanent stormwater ponds. All

previously disturbed areas that are to remain pervious will need to achieve final stabilization during this phase prior to issuance of the Notice of Termination.

The attached Phasing Plans demonstrates the intended construction sequence for the Marmen-Welcon Tower Manufacturing Plant project.

If you have any questions, or require anything further, please let us know. Thank you.

Sincerely,

McFarland-Johnson, Inc.

Adam J. Frosino, PE, PTOE

Project Manager

cc: Robert Leslie, Town of Bethlehem

Richard Hendrick, Port of Albany

Megan Daly, Port of Albany

Steve Boisvert, McFarland-Johnson

APPENDIX M

NATIONAL GRID ENVIRONMENTAL GUIDANCE



Doc No.:	EG-501NYN
Rev. No.:	5
Page No.:	1 of 2
Date:	03/05/2020

SUBJECT REFERENCE	
SOBJECT NET ENERGE	
Release Notifications in New York North EP-5	

Purpose / Objective: This guidance document provides instructions for reporting a release of oil, chemical, or hazardous material.

Who: All National Grid employees and contractors working on National Grid projects or properties.

What to Do:

Report all releases to the National Grid Regional Control Center (RCC) immediately, regardless of the volume or location.

EASTERN RCC	(518) 356-6471
CENTRAL RCC	(315) 460-2796
WESTERN RCC	(716) 398-5308

Provide the following information to the RCC concerning the release:

- Name and contact information
- Time of discovery
- Location (be specific)
- Material and quantity
- Source (vehicle number, transformer, gas meter, HVAC unit, tank number, etc.)
- Cause (i.e., equipment malfunction, motor vehicle accident, storm, human factor, other)
- Description of impacted area and resources (land, water, air)
- Request cleanup crew

REGIONAL CONTROL CENTER:

- 1. Upon notification of a release, contact New York State Spill Hotline (1-800-457-7362) within 2 hours (of discovery time).
- 2. If release is reported at an Environmental SIR Site, contact Environmental immediately (see below).
- 3. Record release in the Incident Management System (IMS).
- 4. Contact Divisional Environmental Engineer, as applicable.



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SUBJECT REFERENCE
Release Notifications in New York North EP-5

ENVIRONMENTAL MANAGEMENT:

- 1. Communicate with RCC and/or field crews regarding additional reporting requirements (e.g., releases to water and PCB releases require reporting to the National Response Center (1-800-424-8802).
- 2. In IMS categorize the release as Category 1 or Category 2 (EG-1502) and classify/complete/close out the incident.
- 3. Confirm clean up, provide additional information to state agency to close out the release as requested.

RELEASE REPORTING ON NEW YORK SIR MGP SITES

Environmental Site Investigation and Remediation has entered into Consent Orders with the New York State Department of Environmental Conservation (NYSDEC) to evaluate and, where necessary, remediate former manufactured gas plant (MGP) sites. These sites are managed by a National Grid project manager (PM). As agreed to with NYSDEC, in the event of an accidental release or spill of material at an MGP site which will require subsurface excavation work for cleanup:

- Report release using procedures above.
- The National Grid PM must be notified as soon as possible to coordinate work.
- The National Grid PM would document the release in IMS.

HELP: Contact the local Environmental Representative if you have questions.

EASTERN: Matt Root 518-227-7508

CENTRAL: Rich Fox 315-546-4011

WESTERN: Lisa Montesano 716-479-5339



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SUBJECT REFERENCE

Release Clean Up in New York North EP-5; Release Response

Purpose / Objective:

The purpose of this guidance document is to provide instructions in the clean-up of oil and other chemical releases.

Who:

This guidance applies to New York North National Grid personnel who may be assigned to respond and/or clean up a release.

What To Do:

Immediate Actions:

- Secure the area
- Attempt to contain release. Utilize release kit contained on most company vehicles.
- Use absorbent/containment materials to minimize or eliminate the spread of contamination.
- Do not walk through or touch the released material; step away from the release area.
- Using physical barriers, visible warnings (i.e., caution tape, cones, etc.), or other means, restrict access to the release area. Prevent unauthorized persons from entering the area.

Note: Large releases should be cleaned up by qualified Hazardous Materials personnel. If the release is large and/or PCB containing, or has reached a water body, contact Regional Control or the Divisional Environmental Engineer for assistance in obtaining help with the clean-up.

Clean up Requirements:

Assess the release. Determine material released. If hazardous material such as mercury, acid or PCB oil, contact Regional Control for help in securing Hazardous Materials personnel or release contractor.

Don personnel protective equipment (PPE) as necessary. PPE may include, but not be limited to gloves, hardhats, safety glasses, steel toed shoes, coveralls, etc. If working near roadway, appropriate cones shall be placed, and high visibility clothing shall be worn. Follow all Safety procedures.

Note: All releases are unique. The clean-up methodology employed will depend upon the nature of the release, the amount released, location, etc. The guidance listed below is meant to be general and not prescriptive.

Non-PCB oil releases to land:



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SUBJECT REFERENCE

Release Clean Up in New York North EP-5; Release Response

Non-PCB oil releases include non-PCB labeled transformers, hydraulic oil, diesel fuel and motor oil. Clean up requires removal of visible stained oil from the surface. Soil removal, use of oil sorbent pads, Speedi Dri, and use of a water-based cleaner may all be used for release clean-up.

- Remove all visible traces of oil.
- Document clean-up efforts and provide to divisional environmental engineer.
- Containerize waste in appropriate containers and label.

Note: NYS DEC guidance and clean up criteria vary between Regions in NYS. Effort shall be made to clean the area to as close as possible to pre-release conditions.

Unlabeled transformer oil releases to land:

If an unlabeled transformer has released, obtain a sample of the oil from the unit and conduct a field PCB test using a CLOR-N-OIL kit. Collect an additional sample for laboratory analysis. If results reveal ≥ 50 ppm, waste clean-up debris must be handled as PCB contaminated and labeled as such until laboratory results determine otherwise. If CLOR-N-OIL results reveal < 50 ppm, the oil and waste may be handled as non-PCB until laboratory results are received. If no oil is left in the unit or a sample cannot be obtained, collect oily soil or debris and send to laboratory for analysis.

- Clean up release as noted above.
- Collect additional soil sample or wipe samples to verify clean up.
- Containerize waste and label appropriately.
- Document clean up and provide to divisional environmental engineer.
- Clean up should be completed within 48 hours. Otherwise, fully document reason for the delay.
- Clean up all reusable equipment using rags and/or cleaners as necessary.
- If PCB results confirm that the oil release was PCB contaminated or PCB oil, an EPA Identification Number may be required prior to disposal of material. Contact the Divisional Engineer for assistance.

Divisional Environmental Engineer Contacts

Western	Lisa Montesano	716-479-5339
Central	Rich Fox	315-546-4011
Eastern	Matt Root	518-227-7508

Documentation

Official record of all releases is maintained in the Incident Management System (IMS.)



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SUBJECT REFERENCE
Release Clean Up in New York North EP-5; Release Response

Regional Control centers will initiate the IMS report upon notification from the field and document time of incident, notification from field time, regulatory notification time, release details (material released, amount, location, response measures). Regional control follows National Grid Distribution Control Center System Operations Operating Guide 3.7 "Oil Release Reporting."

If the release is of sensitive or serious nature (based on public exposure, environmental impact, or public relations issue) such as those involving bodies of water or public buildings in addition to immediate notification to the divisional engineer, notify and document in the Shift Supervisor log book.

Document remediation efforts including release area and property items/materials impacted amount of clean up necessary. Submit documentation to Divisional Environmental Engineer.

Any contact with members of the public, emergency agencies or regulatory personnel should be documented by the response crew.

Divisional Environmental Engineers shall maintain and complete the release documentation in the IMS system and ensure release is closed out.

HELP:

Contact the local Environmental Representative if you have questions.