

STORMWATER POLLUTION PREVENTION PLAN (SWPPP)

For

MARMEN-WELCON TOWER MANUFACTURING PLANT

PREPARED FOR:



ALBANY PORT DISTRICT COMMISSION
106 SMITH BOULEVARD
ALBANY, NY 12202
(518) 463-8763
www.portofalbany.us

PREPARED BY:



60 RAILROAD PLACE, SUITE 402
SARATOGA SPRINGS, NY 12866

FINAL SITE PLAN SUBMISSION

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1. INTRODUCTION

A stormwater management assessment has been conducted for the proposed project in order to protect the waters of the State of New York from the adverse impacts of stormwater runoff. This report presents an analysis of the project in accordance with the *New York State Department of Environmental Conservation SPDES General Permit for Stormwater Discharges from Construction Activity Permit No. GP-0-20-001*. A separate Drainage Design Report (included as Appendix C of this report) has been developed to address the *New York State Stormwater Management Design Manual* (“The Manual”). As required, the Stormwater Pollution Prevention Plan is designed, where appropriate, to incorporate green infrastructure techniques that preserve natural resources and utilize the existing hydrology of the site, provide runoff reduction practices, water quality treatment practices, apply volume and peak control practices for channel protection, overbank flood control, and extreme flood control as appropriate.

In accordance with Appendix B, Table 2 of the SPDES General Permit for Construction Activity, GP-0-20-001 (included as Appendix E of this report), industrial facilities that involve a soil disturbance of one or more acres require the preparation of a full SWPPP that includes post-construction stormwater management practices. In total, approximately 72.7 acres of soil disturbance is expected during the construction of this project. Therefore, this project includes the development of erosion and sediment controls, green infrastructure site planning techniques, runoff reduction volume practices and post-construction stormwater management practices.

The general contractor and subcontractors performing any activity that involves soil disturbance will be required to comply with the terms and conditions of the SWPPP for the project identified as a condition of authorization to discharge stormwater. The Contractor shall provide signed certifications (Form CONR 5) for itself and all applicable subcontractors at the preconstruction meeting. These signed certifications shall be included as part of the SWPPP. The SPDES General Permit and SWPPP must be kept on file at the Project Field Office. As required by the conditions described in the SPDES general permit, the SWPPP shall be kept current, and updates will be made to reflect changes in the design, construction and operation, or maintenance of the project.

The complete set of construction drawings and specifications are provided as separate documents; however, they should be considered an integral component of the SWPPP and are referenced throughout this document. Prior to the start of construction activities, a Notice of Intent (NOI) must be filed and accepted by the NYSDEC. A Draft NOI has been included in this document as Appendix J. The applicant must retain all documentation for 5 years after NYSDEC accepts the Notice of Termination (NOT).

1.1 Scope of the Project

The proposed development is an offshore wind (OSW) manufacturing operation that will produce wind turbine tower components. The site development includes 603,500 +/- square feet of OSW manufacturing spread over four (4) buildings with ancillary impervious areas including parking for automobiles and trucks, roadway, bridge, and a maritime wharf. The remainder of the site will be used for tower storage and be made up of dense graded aggregate (compacted gravel). There will also be small pervious areas of grass and unaltered brush and trees.

1.2 Location of Project

The Project is situated on 81.62 acres of land on Beacon Island (“Expansion Site”), located at the confluence of the Normans Kill and Hudson River. The project also includes development within 4.4 acres

of the adjoining parcel owned by National Grid, the extension and improvement of Normanskill Street (Normanskill Street Improvements) and widening of Rt. 144 (Offsite Improvements). The project owner, Albany Port District Commission (APDC), is proposing to develop the vacant parcels of land (tax parcels 98.00-2-10.23 and 98.01-2-1.0) to expand the existing Port of Albany in the Town of Bethlehem, Albany County, New York. Refer to the Location Map in Appendix A.

The project is not located within a TMDL and does not discharge into a 303(d) listed waterbody.

Table 1 - Location Table

Approximate Coordinate Position @ Center of Project	
Latitude	42° 36' 10.8" N
Longitude	73° 45' 57.0" W

1.3 Project Type and Size

The project is a new development construction project that has a disturbance area of approximately 72.7 +/- acres. The new impervious area is approximately 65.9 acres.

1.4 Project Description

The proposed project will include development of an OSW tower manufacturing (Marmen-Welcon) facility consisting of five (5) separate buildings totaling up to 625,539 +/- square feet of floor space. The following is a breakdown of the function and size of each building:

- Building A Plate Preparation & Welding (299,250 SF)
- Building B Welding Finishing (111,023 SF)
- Building C Blast Metallization Plant (131,968 SF)
- Building D Internal Assembly Finishing (61,550 SF)
- Building E Material Receiving (21,748 SF)

Tower production will occur within four (4) buildings (Buildings A-D) at the main facility on the Port Expansion property located in the Town of Bethlehem. The 5th building (Building E) will be located at 700 Smith Boulevard within the existing Port District in the City of Albany. A proposed gated bridge over the Normans Kill will provide a truck transportation route in and out of the main facility, by connecting Beacon Island and the 14.7-acre offsite parcel at 700 Smith Boulevard. In conjunction with the proposed bridge, Normanskill Street is to be extended from its existing end point to the bridge. The existing pavement will be improved to accommodate the proposed trucking route. River Road (Rt. 144) will be widened to accommodate the employee entrance. Employee parking will be situated on the adjoining land owned by National Grid with access from River Road. A proposed 500 LF wharf and associated dredging along the Hudson River will be used to load and ship completed tower sections. A separate stormwater analysis and SWPPP has been prepared for the 14.7-acre Building E site at 700 Smith Boulevard and the portion of Normanskill Street, located in the City of Albany, as the sites are separated by approximately 1-mile and are under separate MS4 jurisdictions.

The purpose of this report is to assess the stormwater quality, quantity, and erosion and sediment control for the development of the site. This report has been developed in accordance with the New York State Department of Environmental Conservation (NYSDEC) State Pollution Discharge Elimination System (SPDES) General Permit for Stormwater Discharges from Construction Activity, GP-0-20-001 (Permit) and the NYSDEC Stormwater Management Design Manual (The Manual). The project site is located within the

Town of Bethlehem, Albany County, New York, which is an MS4 community, requiring this report and project to receive approval from the Town.

The soil disturbance area addressed in this report is contained within the Town of Bethlehem. This report does not include coverage for work within the Mean High Water (MHW) elevation of the Hudson River or the Normans Kill. Work within the MHW line will be covered under a separate permit.

The total disturbance area is 72.7 +/- acres and includes the Expansion Site, Normanskill Street Improvements and Offsite Improvement. The existing impervious area is approximately 5.16 +/- acres, 7.09% of the total disturbance area. The proposed site development will consist of 65.9 +/- acres of impervious cover, 90.6% of the total disturbance area.

Due to the amount of soil disturbance proposed for this project, a 5-acre disturbance waiver is being requested. The 5-acre waiver request along with all required documentation is included as Appendix L of this report.

1.5 Cultural Resources

A Supplemental Environmental Impact Statement (SEIS) has been developed as part of the SEQR process for the Port of Albany Expansion Project. A SHPO review was conducted, and the current status reflects "No Adverse Effect". The SHPO review letter for the GEIS review process, dated September 13, 2019. A follow up SEIS SHPO review letter, dated December 9, 2021, resulted in a follow up noise study and coordination with the Stockbridge-Munsee Tribal Historic Preservation (SMTHP). Multiple coordination meetings were conducted resulting in some modifications to the site design and additional information provided. As a result, the SMTHP provided a follow up letter dated March 3, 2022, confirming the project has "No Adverse Effect". In response to the SMTHP letter, SPHO has issued a letter of "No Adverse Effect" dated March 25, 2022, contingent upon a deed restriction to be filed by the Owner to protect the Tree and Vegetation buffer area during the construction phase as well as permanently after construction is completed. All referenced letters have been included in Appendix F of this report.

1.6 On-site Wetlands

As part of the Draft Generic Environmental Impact Statement (DGEIS) and SEIS, impact to aquatic resources, including wetlands, were evaluated. The New York State Freshwater Wetland and Tidal Wetlands mapping of the project site indicates there are no NYSDEC jurisdictional wetlands within or adjacent to the project area. Review of USFWS National Wetlands Inventory (NWI) mapping of the project site indicates that the majority of the project area is mapped as palustrine emergent wetlands (PEM) and palustrine forested wetlands (PFO). It should be noted that NWI mapping does not have any regulatory consequence, but rather indicates areas that may meet federal wetland criteria as identified by the USFWS using aerial photography.

A wetland delineation was conducted in April 2019 by McFarland Johnson (MJ) for the FGEIS. The results of the delineation indicated that there are 8 freshwater wetlands located within the project limits. These wetlands are hereafter referred to as Wetlands 1, 3, 4, 5, 6, 7, 8, and 9. Wetlands within the original study area totaled approximately 2.33 acres. A Supplemental Wetland Delineation was performed by MJ in April 2021 within the 18.22 acres on the National Grid Parcel. One contiguous wetland, comprising of approximately 7.13 acres, was delineated within the 18.22-acre area. The delineated wetland represents an extension of the 2019 wetland delineation and previously identified as Wetland 1. Wetland 1 drains in a northerly direction into 40-inch corrugated metal pipe (CMP) which discharges directly to the Normans Kill.

The Project will result in direct impacts to 0.81 acres of Wetland 1 located in Beacon Island (original Project Area) and 0.01 acres of direct impact to Wetland 1 on National Grid property for the construction of a retaining wall. In addition, there is a 0.04-acre impact to Wetland 9 for the bridge over the Normans Kill and a 0.02-acre impact to Wetland 7 for roadway improvements. There will also be approximately 0.33 acres of temporary impacts to wetlands during construction. Total permanent wetland impacts are estimated to be approximately 0.86 acre.

Compensatory wetland mitigation will be satisfied through a federally approved In-Lieu Fee Mitigation Program or off-site mitigation bank (The Wetland Trust). Mitigation in accordance with USACE rules and regulations will ensure no net loss of wetlands and will be included as part of the Joint application Permit submitted to the USACE and NYSDEC.

2. PROJECT MAPS AND PLANS

2.1 Location Map

See Appendix A

2.2 Soil Maps

See Appendix E of the Drainage Design Report (included as Appendix C of this report)

2.3 Erosion and Sediment Control Plans

See Appendix B of this report

2.4 Existing and Proposed Subcatchment Maps

See Appendix A and B of the Drainage Design Report (included as Appendix C of this report)

3. PROJECT SOILS

3.1 NRCS Soil Map

See Appendix E of the Drainage Design Report (included as Appendix C of this report)

3.2 Soil Types

The following soil type(s) and hydrologic group(s) are present within the project area of disturbance:

Table 2 – Soil Types

Symbol	Soil Name	Hydrologic Soil Group
HuE	Hudson silt loam, 25 to 45 percent slopes	C/D
NrD	Nassau very channery silt loam, hilly, very rocky	D
Ug	Udorthents, loamy	A
Ur	Urban land	
Wo	Wayland soils complex, non-calcareous substratum, 0 to 3 percent slopes, frequently flooded	B/D

3.3 Discussion of Soil Characteristics and Soil Erosion Hazard Potential

According to the Natural Resources Conservation Service (NRCS) web soil survey, there are five (5) mapped soil units identified within the project boundary. See Appendix E of the Drainage Design Report (included as Appendix C of this report). The majority of the soil at the expansion site falls within the hydrologic soil group B/D. The first letter corresponds to drained soil's properties under drained conditions and the second to saturated conditions. Group B soils have moderate infiltration and runoff rates while group D have a low infiltration rate and a high runoff rate. The soils with dual group identifiers have been modeled with the more conservative of the two, in this case a D soils group. Most of the soil adjacent to Normanskill Street is within soil group A. Group A soils have a high infiltration rate.

Geotechnical studies have been undertaken to evaluate the subsurface conditions of the site. These investigations have been summarized in the following reports:

- *Preliminary Geotechnical Evaluation and Interpretive Report*, CME Associates, Inc., April 5, 2017
- *Supplemental Geotechnical Report*, Dente Group, July 20, 2017

Copies of these reports were included in the TOWN OF BETHLEHEM PLANNING BOARD, DRAFT GENERIC ENVIRONMENTAL IMPACT STATEMENT For ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY EXPANSION PROJECT, Appendix E.

- *Draft Geotechnical Engineering Report*, Terracon, October 15, 2021

A copy of this reports is included in the TOWN OF BETHLEHEM PLANNING BOARD, SUPPLEMENTAL ENVIRONMENTAL IMPACT STATEMENT For ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY EXPANSION PROJECT.

Based on these previous investigations, the subsurface conditions of the Expansion site are generally characterized by historic fills of various depths overlying, in sequence with depth; river sediments, alluvial sands, glaciolacustrine silt/ clay, glacial till, and shale bedrock. The fill was noted at specific boring locations ranging from 6 to 23 feet below existing grade. The fill material is characterized as a random landfill deposit containing natural and solid waste deposits such as, but not limited to, foundry sand waste, sand, silt, coal ash, gravel, and organic matter. A predominant component of the fill was reported as coal ash.

Shale bedrock was found beneath the glacial till soils at select boring locations. The depth to rock ranged from approximately 61 feet below grade near the northwest portion of the site, to greater than 148 feet at the southeast portion of the site. The rock depths appear shallowest on the north and west sides of the site and increase to the east towards the Hudson River and in a south direction across the site. Based on the New York State Museum and Science Service's Geologic Map of New York: State Hudson-Mohawk Sheet, and the geotechnical rock core samples, the bedrock appears to be consistent with the Normanskill Shale Formation.

According to the geotechnical reports, shallow groundwater was observed at depths ranging from approximately 1.5 to 13.7 feet below existing grade. However, due to the subsurface conditions, the shallower observations could be representative of perched groundwater zones due to discontinuous impermeable layers. Shallow groundwater fluctuations should be expected to occur at this site depending on several factors such as rainfall, seasonal changes, prevailing climate, ambient weather conditions, and the tidal influences of the Hudson River.

Historically, the project site was composed of small islands and river channels subject to natural shifts due

to flows associated with the Hudson River and the former Island Creek, a side channel of the Hudson River. Island Creek historically flowed along the western side of the site through the current power line corridor and discharged to the Hudson River at the southern end of the site. Based on available mapping, sometime between 1936 and 1961, Island Creek channel was diverted at the north end of the site directly to the Hudson River, whereupon it was referred to solely as Normans Kill, the main tributary to this former channel. The site was subject to historic filling operations to create usable lands and a portion of the site was operated as a coal ash (fly ash) disposal site by Niagara Mohawk from approximately 1952 to 1970. As such, there are large areas of fly ash deposits on the site that must be considered during the design and construction of the site infrastructure and stormwater management facilities. Excavated fly ash material will need to be appropriately handled and properly disposed of.

Due to the presence of fly ash on the Expansion Site, in addition to a NYSDEC SPDES, a Site Management Plan (SMP) has been prepared in accordance with 6 NYCRR Part 375 and DER Technical Guidance for Site Investigation and Remediation and submitted to the NYSDEC, Division of Environmental Remediation and the NYSDOH. The SMP includes: a Health and Safety Plan (HASP), to inform and protect the contractor and their work force; a Community Air Monitoring Plan (CAMP), to monitor and protect the surrounding communities; and an Excavation Work Plan (EWP), to direct the activities of the contractor during construction. The EWP includes a detailed description of the work to be performed, the anticipated environmental conditions, and engineering controls to mitigate the movement of fly ash. The SMP pertains only to the Expansion Site portion of the project (see Appendix H of this report).

3.4 Soil Infiltration Test

Supplemental to the above noted geotechnical reports, additional subsurface investigation and infiltration testing was completed by Terracon on May 12, 13, and 18, 2022. Test pit locations were selected based on the potential for stormwater infiltration practices to be utilized. Test locations were along the shore of the Hudson River and Normans Kill as well as within the boundary of Infiltration Basin #1 and #2. The testing locations are shown on a map included in Appendix F of the Drainage Report (included as Appendix C to this report).

The subsurface investigation and infiltration testing concluded that locations IT-1, IT-1A, IT-7, IT-7A, IT-8, IT-10, IT-12, IT-12A, and IT-15 can provide an infiltration rate of 0.5 in/hr or greater. The remaining locations had test results below 0.5 in/hr which is not sufficient for infiltration chambers or infiltration basins. In addition to infiltration rate, a soil classification was also provided at the test depth. The soil classifications found were fill (coal ash with crushed stone and slag), sandy silt (ML), silt (ML), silt and clay (CL-ML), silt (ML), silt with sand (ML), silty sand (ML), silty clay (CL-ML), fill (sandy silt), and fill (coal ash). The entire subsurface investigation report including soil profiles is located in Appendix F of the Drainage Report (included as Appendix C to this report).

4. CONSTRUCTION PHASING

4.1 Sequence of Construction Activities

The Contractor's work schedule and methods shall be consistent with the SWPPP or amended SWPPP. Once approved, the progress schedule shall become a part of the SWPPP. It should be noted that there is a NYSDEC approved SMP for this site, which is included as Appendix H of this report. Any disturbance of the site must comply with the SMP.

The following list is a suggested sequence of major construction activities for the project to meet the NYSDEC Phase II erosion control requirements:

1. Conduct a pre-construction meeting with the MS4, Engineer, and Contractor to review the SWPPP.
2. Notify the NYSDEC within 14 days, and no less than 3 days, prior to commencing work activities that may affect areas of the subject site that are impacted with ash, as required by Section 3.2 of the SMP.
3. Clearly identify project work limits, identifying all areas where construction disturbance shall be permitted.
4. Install erosion control measures prior to commencing earthwork operations. Construct temporary earthen berms, diversion swales, sediment control dams and associated erosion control measures necessary to divert runoff from entering planned areas of disturbance and to protect the adjacent waterway.
5. All installed erosion and sediment control measures are to be inspected and certified as correctly installed by the owner's qualified inspector and Town of Bethlehem staff.
6. Establish temporary/permanent storm water management ponds/erosion control basins.
 - a. Consult the SMP for the appropriate measures to handle or dispose of any encountered contaminated soils.
7. Remove vegetation and dispose of off-site.
8. Strip and stockpile topsoil from proposed pavement, structural fill and cut areas (stockpile materials in locations as directed by owner's representative).
 - a. Consult the SMP for appropriate measures to handle or dispose of any encountered contaminated soils.
9. Establish mass earthwork subgrade elevations.
 - a. Consult the SMP the appropriate measures to handle or dispose of any encountered contaminated soils.
10. All temporary erosion and sediment control measures as well as stockpiles are to be mulched and seeded for temporary vegetative cover immediately following grading.
11. Import the aggregate fill material to serve as a surcharge for the proposed building and concrete pad areas.
12. After surcharging compaction is completed, place fabric and geogrid on the subgrade and spread the aggregate material in layers with additional geogrid as specified.
13. Construct utility lines (water/electric/gas/communications/sanitary sewers/storm sewers), construct building and install infrastructure improvements.
14. Box out roadway and pavement areas and install concrete curbing.
15. Construct asphalt pavement section, up to binder course.
16. Fine grade and spread topsoil, install landscaping plantings and hardscapes, site amenities and permanent seeding.
17. Town of Bethlehem (MS4) shall conduct a site inspection to determine (1) that the site has achieved 80% stabilization and (2) the installed stormwater facilities are operational.
18. Remove temporary erosion and sediment control features upon establishment of permanent ground cover and inspection/approval from a Town official or representative.
19. Notify owner's representative of completion of final site stabilization.
20. File Notice of Termination.

5. EROSION AND SEDIMENT CONTROL MEASURES

5.1 Erosion Control Plan

An erosion control plan has been developed in accordance with the “New York Standards and Specifications for Erosion and Sediment Control”. The erosion control plan employs permanent and temporary erosion and sediment control methods including silt fence, erosion control matting, construction entrances, and other appropriate measures. It should be noted that there is a NYSDEC approved SMP for the Expansion Site, which is included as Appendix H of this report. Any disturbance of this area must comply with the SMP. As stated in Section 3.2 of the SMP, NYSDEC must be notified within 14 days, and no less than 3 days, prior to commencing work activities that may affect areas of the subject site that are impacted with ash.

5.1.1 Temporary Surface Stabilization

All work and prior NYSDEC notification shall be in accordance with the SMP. Areas within the project limits that may be disturbed more than once during the construction activities will be stabilized using temporary seed and mulch item or as directed by the Engineer. Areas remaining unpaved and undisturbed for more than seven (7) days during construction operations shall be stabilized temporarily. Other areas that might need to be stabilized temporarily will be at the discretion of the Engineer.

5.1.2 Drainage Pipe Inlet / Outlet Stabilization

As part of the permanent erosion control measure, the inlet and outlet of the culvert pipes will be provided with either stone riprap apron or an apron consisting of erosion control product with vegetation to provide the required erosion control which blends in with the surrounding natural features and topography. The location and type of stabilization to be provided is shown on project plans.

5.1.3 De-watering

Any groundwater that is suspected of being contaminated shall be handled in accordance with Section 4.2 of the SMP. If required, de-watering of miscellaneous areas within the site will be performed utilizing a pump and filter bag system. The filter bags should be made of non-woven geotextile material capable of trapping particles larger than 150 microns. Filter bags should be replaced when they are half full or a no longer functioning per the manufacturer’s requirements. Filter bags should be located in a well vegetated/grassy area and discharge into stable erosions resistant areas. Where this is not possible a geotextile flow path should be established. Bags shall not be placed on slopes greater than 5%. The pump discharge hose shall be inserted into the bags in the manner specified by the manufacturer and securely clamped. Pumping rate shall not be greater than 750 GPM or ½ the maximum specified by the manufacturer, whichever is less. Pump intakes shall be floated and screened.

5.1.4 Construction Entrance

As required, at least one (1) stabilized construction entrance will be constructed to access the Contractors Staging/Storage Area. This entrance/area shall conform to the details. Refer to the Erosion and Sediment Control (E&SC) Plans (included as Appendix B of this report) for location of construction entrance(s).

5.1.5 Concrete Truck Washout / Concrete Batch Plant Protection

As required, a temporary excavated or above ground lined pit where concrete truck mixers and equipment can be washed after their loads have been discharged, to prevent highly alkaline runoff from entering storm drainage systems or leaching into soil shall be constructed. See E&SC Plans (included Appendix B of

this report) for location of concrete washout. If a concrete batch plant is installed at the site, temporary containment to prevent discharge of runoff from entering storm drainage systems or leaching into soil shall be constructed.

5.1.6 Permanent Stabilization

Stabilization of the graded surfaces will be accomplished by using various seed mixtures for establishing permanent vegetation.

5.1.7 Dust Control

Dust shall be controlled and monitored in accordance with Section 4.3 of the SMP. The contractor will be required to minimize dust generation during the construction activities. Provisions such as applying water on haul roads, wetting equipment, and excavation faces, spraying water on buckets during excavation and dumping, hauling materials in properly tarped or watertight containers, restricting vehicle speeds to 10 mph, covering excavated areas and material after excavation activity ceases, and reducing the excavation size and/or number of excavations have proven effective in dust control.

5.1.8 Silt Fence

Silt fence will be placed per the E&SC Plans (Appendix B of this report), down slope of all disturbed areas, soil stockpiles, and spoil areas. Along the bank of the Normans Kill, two layers of silt fence are to be installed due to the proximity to the Mean Higher High Water (MHHW) level. The purpose of the silt fence is to remove sediment from sheet flow in these areas. Silt fence shall remain in place and functional until the contributing area has been permanently stabilized. Sediment socks or mulch dikes may be used in lieu of silt fence, where approved by the Engineer of Record. Erosion Control shall be in accordance with the SMP.

5.1.9 Temporary Sediment Basins

Temporary sediment basins have been designed to store sediment runoff from the Expansion Site. Basin #1 will be converted into a permanent stormwater quality pond. All basins have been designed in accordance with Section 5 of the NYS Standards and Specifications for Erosion and Sediment Control (Blue Book). Calculations for the basins are included as Appendix I to this report. Locations and a detail of the basins are included in the E&SC Plans (Appendix B of this report).

5.1.10 Weekly Inspections

A qualified inspector shall conduct site inspections at least once every seven (7) calendar days. After a 5-acre waiver is granted; site inspections shall occur at least twice every seven (7) calendar days while there are more than 5 acres of soil disturbance. The qualified inspector shall inspect all erosion and sediment control practices and pollution prevention measures to ensure integrity and effectiveness; all post-construction stormwater management practices under construction to ensure that they are constructed in conformance with the SWPPP; all areas of disturbance that have not achieved final stabilization, all points of discharge to natural surface waterbodies located within, or immediately adjacent to, the property boundaries of the construction site; and all points of discharge from the construction site. The qualified construction inspector shall also prepare an inspection report after every inspection. Complete inspection and maintenance requirements can be found in Part IV of the SPDES General Permit GP-0-20-001 (included as Appendix E of this report). Inspection reports shall be submitted to the Town's Stormwater Program Manager.

5.1.11 Final Inspection

Prior to the project being finally accepted, it shall be inspected for any evidence of erosion or slope failure. If any such condition becomes apparent upon final inspection, temporary soil erosion and sediment controls shall be installed immediately as directed by the Engineer. The situation shall be corrected per a schedule agreed to by the MS4 (Town of Bethlehem).

5.1.12 Wharf E&SC

Erosion and sediment control measures associated with the construction of the wharf and dredging of the Hudson River are to be designed and approved prior to disturbance below the Mean High High Water (MHHW) elevation. These E&SC measures are being designed in conjunction with the NYSDEC, USACE and other State agencies through a separate permitting process. All additional permits required for the wharf and dredging will also be in place prior to disturbance below the MHHW. Draft conceptual E&SC Plans associated with the wharf construction and dredging are included in Appendix G of this report.

5.2 Permanent Erosion and Sediment Control Measures

Table 3 – List of Permanent Erosion & Sediment Control Measures

Permanent Feature	Converted Temporary Practice?	Location: ESC Plan	Receiving Waterbody Protected (where applicable)
Riprap outlet protection	Yes	See Plans	Hudson River, Normans Kill
Soil Stabilization	Yes	See Plans	Hudson River, Normans Kill
Check Dam	Yes	See Plans	N/A
Diversion Dike	Yes	See Plans	N/A

5.3 Installation Sequence

See the intended sequence of construction activities noted in Section 4 above.

5.4 Maintenance Schedule

The Contractor is required to inspect all E&SC devices in their active work area daily and after each rain event; and repair any deficiencies in accordance with the SPDES permit.

5.5 SWPPP Implementation Responsibilities

Implementation of all E&SC devices will be by the Contractor as indicated in the contract documents.

6. POLLUTION PREVENTION MEASURES

6.1 Material Management Practices

All waste materials, including construction debris and trash that occur onsite shall be handled and disposed of in a lawful manner that is in accordance with state and local regulations. No waste material shall be buried on site.

- An effort will be made to store only enough products required for the project.
- All materials stored within the site will be stored in a neat orderly manner in their appropriate containers and if possible, an enclosed area.
- Products shall be kept in their original containers with the original manufacturer's labels.

Manufacturer's recommendations for proper use and disposal shall be followed.

- Hazardous materials shall be disposed of in a lawful manner and in accordance with State and Local regulations.
- Sanitary waste will be collected from portable units as required and shall be disposed of in a lawful manner.

The following materials are expected to be on-site during construction:

- Concrete
- Asphalt
- Paints (Enamel and Latex)
- Petroleum based products
- Fertilizers
- Metal building components
- Detergents
- Cleaning Solvents
- Roofing Materials
- Tar

These materials and other materials used during construction with the potential to impact stormwater will be stored, managed, used, and disposed of in a lawful manner that minimizes the potential for releases to the environment and especially into stormwater.

Emergency contacts for the project will be posted at the project office and are included at the end of this section.

6.2 Spill Control Practices

The contractor will be responsible for preparing a project area specific spill control plan in accordance with Local and NYSDEC regulations. At a minimum, this plan shall:

1. Stop the source of the spill.
2. Contain the spill.
3. Reduce stormwater contact if there is a spill.
4. Dispose of contaminated material in lawful manner and in accordance with manufacturer's procedures and NYSDEC regulations.
5. Identify responsible trained personnel.
6. Ensure spill area is well ventilated.

For any work within National Grid property, the National Grid Environmental Guidance EG 501 regarding reporting of a release of oil, chemical or hazardous material must be followed. National Grid EG 501 has been included as Appendix M of this document.

6.3 General Material Handling Practices

The following general practices will be used throughout the project to reduce the potential for spills:

1. Potential pollutants will be stored and used in a manner consistent with the manufacturer's instructions in a secure location. To the extent practicable, material storage areas should not be located near storm drain inlets and should be equipped with covers, roofs, or secondary containment as needed to prevent stormwater from contacting stored materials. Potential pollutants should not be stored within 100 feet of a water course or wetland. Chemicals that are

not compatible shall be stored in segregated areas so that spilled materials cannot combine and react.

2. Materials disposal will be in accordance with manufacturer's instructions and applicable local state and federal regulations.
3. Materials no longer required for construction will be removed from the site as soon as practicable.
4. Adequate garbage, construction waste, and sanitary waste handling and disposal facilities will be provided/utilized to the extent necessary to keep the site clear of obstruction and Best Management Practices (BMPs) clear and functional.

6.4 Product Specific Practices

The following product specific practices will be followed within the project area.

6.4.1 *Petroleum Products*

All project related vehicles shall be monitored for leaks and receive regular preventative maintenance to reduce the potential of leakage. Petroleum products shall be stored in tightly sealed containers, which are clearly labeled. Any asphalt substances used during construction shall be applied according to manufacturer's recommendations.

6.4.2 *Fertilizers*

Fertilizers used shall be applied only in the minimum amounts recommended by the manufacturer. Once applied, fertilizer shall be worked into the soil to limit exposure to stormwater. Fertilizers shall be stored in covered or other contained areas.

6.4.3 *Paints*

All containers shall be tightly sealed and stored when not required for use. Excess paint shall not be discharged into the storm sewer system but shall be disposed of according to manufacturer's instructions or State regulations.

6.4.4 *Concrete Trucks*

Concrete Trucks shall be allowed to wash out within project areas that the contractor provides an area which collects and contains any concrete / slurry material washed from trucks for recovery and disposal at a later time. No concrete or slurry shall be discharged from the property at any time of construction. The concrete washout area shall conform to the detail found on sheet ESC-06 (Appendix B of this report).

6.5 Spill Response

The primary objective in responding to a spill is to quickly contain the material(s) and prevent or minimize their migration into stormwater runoff or conveyance systems. If the release has impacted on-site stormwater, it is critical to contain the released material on-site and prevent their release into receiving waters.

If a spill of pollutants threatens stormwater on-site, the spill response procedures outline below must be implemented in a timely manner to prevent release of the pollutant:

1. The site superintendent will be notified immediately when a spill or the threat of a spill is observed. The superintendent will assess the situation and determine the appropriate response.
2. If spills represent an imminent threat of escaping E&SC facilities and entering the receiving waters, facility personnel will respond immediately to contain the release and notify the superintendent after the situation has been stabilized.
3. Spill kits containing materials and equipment for spill response and clean-up will be maintained

onsite. Each spill kit may contain:

- Oil absorbent pads (one bale)
 - Oil absorbent booms (40 feet)
 - 55-gallon drums (2)
 - 9-mil plastic bags (10)
 - Personal protective equipment including gloves and goggles
4. If an oil sheen is observed on surface water, absorbent pads and/or booms will be applied to contain and remove the oil. The source of the oil sheen will also be identified and removed or repaired as necessary to prevent further releases.
 5. The site superintendent, or their designee, will be responsible for completing a spill reporting form to the appropriate state or local agency.
 6. Spill response equipment will be inspected and maintained as necessary to replace any materials used in spill response activities.

6.6 Notification

In the event of a spill, make the appropriate notification(s) consistent with the following procedures:

1. Any spill of oil which a) violates water quality standards, b) produces a sheen on a surface water, c) causes a sludge or emulsion must be reported immediately by telephone to the National Response Center Hotline at (800) 424-8802.
2. Any oil, hazardous substance, or hazardous waste release which exceeds the reportable quantity must be reported immediately by telephone to the National Response Center Hotline at (800) 424-8802.
3. Any spill of oil or hazardous substance to waters of the state must be reported immediately by telephone to the NYSDEC.
4. Any release of hazardous substance that may be a threat to human health or the environment must be reported to the NYSDEC immediately upon discovery.

7. EXISTING SITE CONDITIONS

The existing site is Beacon Island, located in the Town of Bethlehem, Albany County, New York. The site is currently vacant and consists primarily of brush and trees with a small gravel area as well as abandoned railroad tracks.

7.1 Existing Watershed Information

The project area is in close proximity and includes shorelines to both the Hudson River and Normans Kill, which are the receiving waterbodies for runoff from the current site.

The existing drainage condition is split up into seven (7) drainage areas. Drainage area DR-A drains to analysis point #1A, drainage areas DR-B and DR-F drain to analysis point #1, drainage areas DR-D and DR-E drain to analysis point #2. Drainage area DR-G drains to analysis point #3. Drainage area DR-C drains to a self-contained depression for storage. See Appendix A of the Drainage Design Report (included as Appendix C of this report) for the Pre-Development Site Drainage Areas Map.

Runoff from DR-A travels via sheet and shallow concentrated flow directly to a wetland located in the northwest corner of the site (Wetland 1). During large storm events the wetland overflows into an existing 40" pipe with direct outlet to the Normans Kill. Analysis of the existing capacity of the outlet pipe is

provided in section IV of the Drainage Design Report (included as Appendix C of this report). Runoff from areas DR-B, DR-D, DR-E, and DR-F travel via sheet and concentrated flow to low areas with eventual outfall directly to the Normans Kill and Hudson River. An approximately 30-acre internal portion of the site (DR-C) was determined to be self-contained within the site capable of storing and infiltrating the 100-year storm event. Runoff from area DR-G sheet flows to the west side of River Road and travels to a low spot adjacent to the roadway where it is stored and eventually infiltrated.

The existing site falls within the Normans Kill watershed of the Middle Hudson Sub-Basin for the Lower Hudson River Basin (HUC10: 0202000602, Water Index No H-221-4) which is listed as a Class C water. Neither the Normans Kill nor the Hudson River are listed in the Manual’s Appendix C as a watershed where enhanced phosphorus removal standards are required. Additionally, neither are listed in the Manual’s Appendix E as a watershed impaired by pollutants related to construction activity.

7.2 Table of Receiving Waterbodies

Table 4: Receiving Waterbodies

<i>Stormwater Structure</i>	<i>Receiving Waterbody</i>	<i>NYSDEC Regulated</i>
None	Hudson River	Yes – Class C
40” Outlet Pipe	Normans Kill	Yes – Class C

8. STORMWATER MANAGEMENT ASSESSMENT

8.1 Methodology

To analyze the hydrologic impacts of the proposed development, a storm water management model was developed in accordance with the Manual. HydroCAD™, by HydroCAD Software Solutions LLC was used to model both the existing and proposed conditions: soil data from the NRCS Web Soil Survey was entered into the software; land coverage areas were estimated using aerial photography and site visits; watershed areas were developed using the surveyed topography; time of concentrations were estimated using USDA, Urban Hydrology for Small Watersheds, TR-55 (TR-55) methodology; and finally runoff and routing calculations were performed using the SCS Unit Hydrograph method.

Green Infrastructure practices were designed in accordance with the Manual using the NYSDEC Runoff Reduction Worksheets available through the NYSDEC’s Construction Stormwater Toolbox, available on their website.

The following general steps are followed when conducting a stormwater design:

1. **Site Planning:** The existing natural resource areas and drainage patterns including wetlands, waterways, floodplains, and soils are identified. Conservation of natural resources are maximized given the proposed site.
2. **Pre and Post-Development Conditions Analysis:** The pre and post-development stormwater runoff conditions for the 1, 10, and 100-year storm events are determined using HydroCAD (detailed HydroCAD reports for this project can be found in Appendix A and B or the Drainage Design Report, provided in Appendix C of this report).
3. **Water Quality:** The Water Quality Volume and Runoff Reduction Volume are calculated using Chapter 4 of the Manual and Green Infrastructure Worksheets (see Appendix C of the Drainage Design Report, provided in Appendix C of this report).

4. **Water Quantity:** Peak runoff and stormwater retention/detention are evaluated using the Manual.

8.1.1 Water Quality Volume (WQv) / Runoff Reduction Volume (RRv)

Section 4.2 of the Manual states that Water Quality Volume (WQv) is intended to improve the water quality by capturing and treating runoff from small, frequent storm events that contain higher pollutant levels created through the increase of impervious surfaces. Impervious surfaces accumulate pollutants that quickly wash off and rapidly enter downstream waters as well as prevent natural groundwater recharge.

The WQv required for the proposed site is based upon the 90% rainfall event number, percent of impervious cover, and the total site area. Calculations were done using the Green Infrastructure worksheets and can be found in Appendix C of the Drainage Report (included as Appendix C of this report). The total WQv required is 273,874 cubic feet.

Runoff Reduction Volume (RRv) is the reduction of the total WQv by application of green infrastructure techniques and stormwater management practices to replicate pre-development hydrology more closely. The intent of RRv is to recognize the water quality benefits of certain site design practices to address flow as a pollutant of concern. Calculations were done using the Green Infrastructure worksheets and can be found in Appendix C of the Drainage Report (included as Appendix C of this report). The minimum RRv was determined to be 57,313 cubic feet.

Due to the level of contamination present in the existing soils across the Expansion Site, stormwater infiltration practices were located only in areas along the Hudson River and Normans Kill where contamination is not expected to be present. However, the Normanskill Street project area does not contain contaminated soils, so all treatment practices selected in this area utilize infiltration and therefore include RRv.

The total Water Quality Volume and Runoff Reduction Volume requirements are met for this project.

8.1.2 Channel Protection Volume (CPv)

Stream Channel Protection Volume Requirements (CPv) are designed to protect stream channels from erosion. The Manual was used to determine the water quantity requirements of CPv; specifically, providing 24-hour extended detention for the 1-year storm event or discharging directly to tidal waters.

According to Section 4.4 of the Manual, the Stream Channel Protection Volume (CPV) requirement does not apply when the site discharges to a tidal waterbody.

The CPv requirement does not apply in certain conditions, including the following:

- Reduction of the entire CPv volume is achieved at a site through green infrastructure or infiltration systems.
- The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, 24-hour extended detention of the 1-year storm event is not required for drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and

analyzed as Analysis Point #1A. Hydrologic analysis for the 1-year storm event from existing to proposed is provided in Appendix A and B of the Drainage Report (included as Appendix C of this report) and summarized in Table 8.

8.1.3 Overbank Flood Control (Q_p)

The primary purpose of the overbank flood control sizing criterion is to prevent an increase in the frequency and magnitude of out-of-bank flooding generated by urban development. The Manual was used to determine the water quantity requirements of Q_p ; specifically, providing sufficient retention volume to discharge all runoff from the proposed 10-year storm event at a rate equal to or less than the existing peak 10-year runoff rate or discharging directly to tidal waters.

According to Section 4.5 of the Manual, the Overbank Flood Control Criteria (Q_p) requirement does not apply when the site discharges to a tidal waterbody.

The overbank flood control requirement (Q_p) does not apply in certain conditions, including:

- The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, 24-hour extended detention of the 10-year storm event is not required for drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and analyzed as Analysis Point #1A. Hydrologic analysis for the 10-year storm event from existing to proposed is provided in Appendix A and B of the Drainage Report (included as Appendix C of this report) and summarized in Table 8.

8.1.4 Extreme Flood Control (Q_f)

The intent of the extreme flood criteria is to prevent the increased risk of flood damage from large storm events, maintain the boundaries of the predevelopment 100-year floodplain, and protect the physical integrity of stormwater management practices. The Manual was used to determine the water quantity requirements of Q_f ; specifically, providing sufficient retention volume to discharge all runoff from the proposed 100-year storm event at a rate equal to or less than the existing peak 100-year runoff rate or discharging directly to tidal waters.

According to Section 4.6 of the Manual, the Extreme Flood Control Criteria (Q_f) requirement does not apply when the site discharges to a tidal waterbody.

The 100-year storm control requirement can be waived if:

- The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, 24-hour extended detention of the 100-year storm event is not required for drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and

analyzed as Analysis Point #1A. Hydrologic analysis for the 100-year storm event from existing to proposed is provided in Appendix A and B of the Drainage Report (included as Appendix C of this report) and summarized in Table 8.

8.2 Evaluation of Green Infrastructure

According to Section 4.3 of the Manual, meeting the RRv (through green infrastructure) may not be feasible due to limitations that prevent the use of an infiltration technique and/or infiltration of the total WQv. The Beacon Island portion of the project site does not allow for the infiltration of any stormwater runoff due to the presence of fly ash across the site. However, green infrastructure practices were evaluated for potential use.

8.2.1 *Conservation of Natural Areas*

The existing vegetation located along the bank of the Hudson River is conserved in a deed restricted area in the proposed plan. Credit has been applied.

8.2.2 *Sheetflow to Riparian Buffers and Filter Strips*

Riparian Buffers and Filter Strips were not utilized, due to the lack of space on the Port Authority owned land.

8.2.3 *Vegetated Swales*

The developed site contains vegetated swales where there is sufficient room. Due to the SMP not recommending infiltration within the Expansion Site, no credit has been applied.

8.2.4 *Tree Planting / Tree Pits*

New landscaping will complement the existing environment and provide aesthetics for the buildings and parking areas. No credit has been applied for proposed tree plantings.

8.2.5 *Disconnection of Rooftop Runoff*

Rooftop disconnection was not considered for this project, as the buildings will have large, sloped roofs in a single direction and would have to discharge to the compacted gravel areas that would potentially cause erosion and instability of the dense graded aggregate due to over saturation; as well as encourage infiltration into the fly ash sub-surface layer which is not recommended by the SMP.

8.2.6 *Stream Daylighting*

Stream daylighting is not available for the proposed project.

8.2.7 *Bioretention*

The developed site does not have sufficient area to accommodate Bioretention. The proposed stormwater treatment ponds designed for this site are located either partially or fully on the adjacent National Grid property. As required by National Grid, the treatment on their property must hold at least the 10-year storm. There is not adequate space to use bioretention systems instead of stormwater ponds in these locations given the quantity of water required to retain. This practice promotes infiltration into the fly ash sub-surface layer which is not recommended by the SMP.

8.2.8 *Green Roofs*

Green roofs were not considered to be feasible as pre-engineered metal buildings are proposed for this project.

8.2.9 Stormwater Planter

Stormwater Planters were not considered due to the poor soils, excessive rooftop runoff volume, and would promote infiltration into the fly ash sub-surface layer which is not recommended by the SMP.

8.2.10 Rain Barrels and Cisterns

The developed site does not have sufficient area for Rain Barrels or Cisterns to accommodate the storage of the roof runoff volume.

8.2.11 Porous Pavement

Porous pavement was not considered due to the large loads associated with the Tower sections being moved and stored on site that would cause the porous pavement surface to crumble. This practice also promotes infiltration, which is not recommended by the SMP.

8.2.12 Infiltration System

Two infiltration basins were designed to treat runoff from a portion of the Normanskill Street Improvements. Two dry swales were designed to treat runoff from the Offsite and a portion of the Normanskill Street Improvements. Three infiltration chamber systems were designed to provide runoff reduction along the Hudson River and Normans Kill.

9. POST CONSTRUCTION STORMWATER CONTROL PRACTICES

9.1 Table of Post Construction Practices

See Table 5 below.

9.2 Post Construction Practices Plan

Locations of Post Construction Practices are found in the Erosion & Sediment Control Plans and Details (included as Appendix B of this report).

To best mitigate the water quality requirements of the proposed site, two (2) stormwater quality ponds, six (6) manufactured stormwater filtering systems, three (3) infiltration chamber systems, two (2) infiltration basins, and two (2) dry swales were designed. All practices were designed in accordance with the Manual. Each practice was sized to provide WQv; however, they do not all provide storm event flow mitigation (see sections 8.1.2 through 8.1.4 above).

Drainage Areas DR-1 through DR-7 will provide WQv using manufactured water quality systems. Drainage Areas DR-8 and DR-9 will drain to stormwater ponds providing WQv. The total of all practices providing water quality volume is 211,395 cubic feet (cf). A full description of the designed stormwater treatment practices is provided in Section III.B of the Drainage Design Report (included as Appendix C of this report). The WQv is summarized in Table 5 below:

Table 5 – Water Quality Volume Practice Summary

Drainage Area	Stormwater Practice	WQv (cf)
DR-1	Filter Type 2	18,005
	Infiltration Chamber	2,802
DR-2	Filter Type 1	21,971
DR-3	Filter Type 1	43,939
DR-4	Filter Type 3	14,989
	Infiltration Chamber	2,052
DR-5	Infiltration Chamber	2,047
DR-6	Filter Type 1	48,060
DR-7	Filter Type 2	34,826
DR-8	Stormwater Pond #1	8,437
DR-9	Stormwater Pond #2	13,361
DR-14	Infiltration Basin #2	141
DR-15	Dry Swale #1	129
DR-17	Dry Swale #2	636
Total WQv		211,395

Due to the presence of fly ash across the Expansion Site, infiltration practices were located in areas not expected to be contaminated. However, the Normanskill Street and Offsite Improvement portions of this project are in an area of uncontaminated soil with high infiltration rates. Therefore, all treatment practices selected infiltrate into the ground and provide RRv. The total RRv provided is 63,333 CF. The RRv is summarized in Table 6 below:

Table 6 – Runoff Reduction Practice Summary

Drainage Area	Stormwater Practice	RRv (cf)
DR-1	Infiltration Chamber	21,248
DR-4	Infiltration Chamber	18,464
DR-5	Infiltration Chamber	18,426
DR-11	Conservation of Natural Areas	868
DR-13	Infiltration Basin #1	1,995
DR-14	Infiltration Basin #2	2,245
DR-15	Dry Swale #1	87
Total RRv		63,333

Drainage Areas DR-10, DR-11, DR-12, and DR-16 are to remain as naturally vegetated and therefore do not require water quality treatment.

However, Drainage Area DR-11 will be deed restricted to ensure the perpetual protection of the proposed area. Therefore, this area qualifies under the “Conservation of Natural Areas” volume reduction practice shown in the chart above.

9.3 Hydraulic Analysis of Pre- and Post-Development Conditions

The site was analyzed in both the pre- and post-construction stormwater conditions. Water quantity controls were required for drainage areas contributing to analysis point #1A as it is a Wetland. Using Chapter 4 of the Manual for new development, the project meets the total water quality volume required. Table 7 below summarizes the impervious cover of the pre- and post-development conditions.

Table 7 – Impervious Cover

	Pre-Development	Post-Development
Impervious Area	5.16 ac	65.9 ac
% Impervious Cover	7.1%	90.6%

The existing site has no water quality treatment measures. A portion of all stormwater not stored within the site is directly discharged into the Hudson River and Normans Kill. Per Chapter 4 of the Manual, new development projects are required to provide water quality treatment. As shown below, the project can meet the total water quality volume required. The peak discharge for all storm events draining to Analysis Point #1A is decreased in the post-development condition. The post-development peak discharge rates for the 1-year, 10-year and 100-year storm events exceed the pre-development peak discharge rates for the remaining analysis points; however, as described in Section 8.1 above, this requirement is waived when discharging directly to tidal waters. A summary of the peak discharge and stormwater management plan is shown in Table 8 below.

Table 8 – Peak Discharge and Stormwater Management Plan Summary

Storm Event	Pre-Development	Post-Development
Analysis Point #1A (Wetland #1)		
1-yr Discharge	27.32 cfs	4.77 cfs
10-yr Discharge	73.24 cfs	12.46 cfs
100-yr Discharge	163.60 cfs	30.97 cfs
Analysis Point #1		
1-yr Discharge	3.25 cfs	58.54 cfs
10-yr Discharge	14.96 cfs	124.96 cfs
100-yr Discharge	43.20 cfs	205.59 cfs
Analysis Point #2		
1-yr Discharge	7.17 cfs	82.79 cfs
10-yr Discharge	20.65 cfs	166.00 cfs
100-yr Discharge	48.06 cfs	290.19 cfs
Analysis Point #3		
1-yr Discharge	0.60 cfs	1.20 cfs
10-yr Discharge	1.84 cfs	2.62 cfs
100-yr Discharge	4.39 cfs	5.25 cfs
Total Area of Soil Disturbance	72.7 acres	
WQv Target	273,874 cf	
WQv Provided	274,728 cf	
RRv Target	57,313 cf	
RRv Provided	63,333 cf	

Analysis Point #1A analyzes the peak discharge at Wetland #1. In larger storm events, stormwater quality ponds #1 and #2 will provide a “first flush” treatment for up to a 10-year storm event with stabilized emergency spillways to direct flow to the surrounding area for storms greater than the 10-year event. Due to the topography of the surrounding undisturbed area, water will flow toward Wetland #1. In the post-development condition, Analysis Point #1A has a peak discharge less than the pre-development condition during all storm events, therefore the required water quantity controls are met.

In the post-development condition, Analysis Point #1 has a total drainage area of 0.12 square miles (75.28 acres). This point drains to the Normans Kill with a drainage area of 162 square miles (103,680 acres). The project area makes up approximately 0.07% of the total drainage area of the Normans Kill. With an overall project time of concentration of around 10 minutes, the proposed project will have a negligible impact on the total Normans Kill hydrology as the site-produced runoff will be conveyed prior to the Normans Kill peak and will not impact the overall flood conditions of the Normans Kill.

In the post-development condition, Analysis Point #2 has a total drainage area of 0.04 square miles (23.6 acres). This point drains to the Hudson River with a drainage area of 8,090 square miles (5,177,600 acres). The project area makes up approximately 0.0005% of the total drainage area of the Hudson. With an overall project time of concentration of around 10 minutes, the proposed project will have a negligible impact on the total Hudson River hydrology, as the site-produced runoff will be conveyed prior to the Hudson River peak and will not impact the overall flood conditions of the Hudson River.

At Analysis Point #3, the post-development discharge rates are higher than the pre-development condition. However, analysis point #3 drains to the surrounding area which stores runoff to be gradually infiltrated. Runoff from this analysis point does not flow to a stream or wetland.

9.4 Deviation from NYS Stormwater Management Design Manual

The proposed stormwater management design deviates from The Manual by utilizing manufactured stormwater filtering systems for new development.

The need for alternative stormwater management practices is rooted in the extremely limited space available as well as the current site conditions. The proposed Offshore Wind Manufacturing Facility requires 85 acres of usable manufacturing and storage space along the Hudson River. It also requires close proximity to an existing port. Such requirements narrow the available project locations to a select few plots of unoccupied land in the entire state and this site was selected through a solicitation process by the state for off-shore wind development. This site was chosen given it is located adjacent to the existing Port of Albany and is directly on the Hudson River. However, the usable portion of the site adjacent to the Hudson River, is only 66-acres. Therefore, the entirety of the site is needed for the OSW manufacturing process, with an ancillary receiving site located at 700 Smith Boulevard.

The Expansion Site also extends onto the adjacent National Grid property from which APDC is leasing approximately 4.4 acres. However, National Grid has prohibited the installation of permanent stormwater infiltration practices within their property.

In addition to space limitations, the existing soils conditions prevent infiltration from being utilized as a stormwater management practice over most of the site. The existing soils are classified as Hydrologic Group D and B/D which provide little to no infiltration and are underlaid by fly ash. Infiltration practices were utilized in the areas where greater than 0.5 in/hr infiltration rates were achieved.

To adequately satisfy the WQv requirements of the Manual, manufactured systems are needed. The Contech Jellyfish units designed meet both the performance and sizing requirements of Chapter 4 of the Manual. The units are also certified by Washington State Department of Ecology (TAPE) and the Maryland Department of the Environment, adequate sources accepted by the NYSDEC. Specifications and details for the proposed units are provided in Appendix D of the Design Report (included as Appendix C of this report).

9.5 Maintenance Schedule of Post-Construction Stormwater Control Practices

See Appendix D of this report for the maintenance inspection checklists and requirement for the facilities to be maintained as summarized below in Table 9.

Table 9 – Maintenance Schedule of Post-Construction Stormwater Management Facilities

Maintained By	Name of Entity
Name, Address, Phone of Responsible Party	Albany Port District Commission 106 Smith Boulevard Albany, NY 12202 (518) 463-8763
Facilities to be Maintained	Jellyfish Filter (9 units at 6 locations) Infiltration Chamber (3 systems) Stormwater Quality Ponds (2) Infiltration Basins (2) Dry Swales (2) Stormwater Collection & Conveyance Systems
Description of Maintenance Activity for each Facility and Frequency	See Appendix D for maintenance guidelines, as recommended by the manufacturer and NYSDEC.
Description of Applicable Easements	N/A
Access and Safety Issues	Maintenance forces have access to all drainage facilities within the site.
Local and Non-Local Permits	Joint Permit Application
Legal Agreements	N/A

9.6 Drainage Structure Catchment Areas

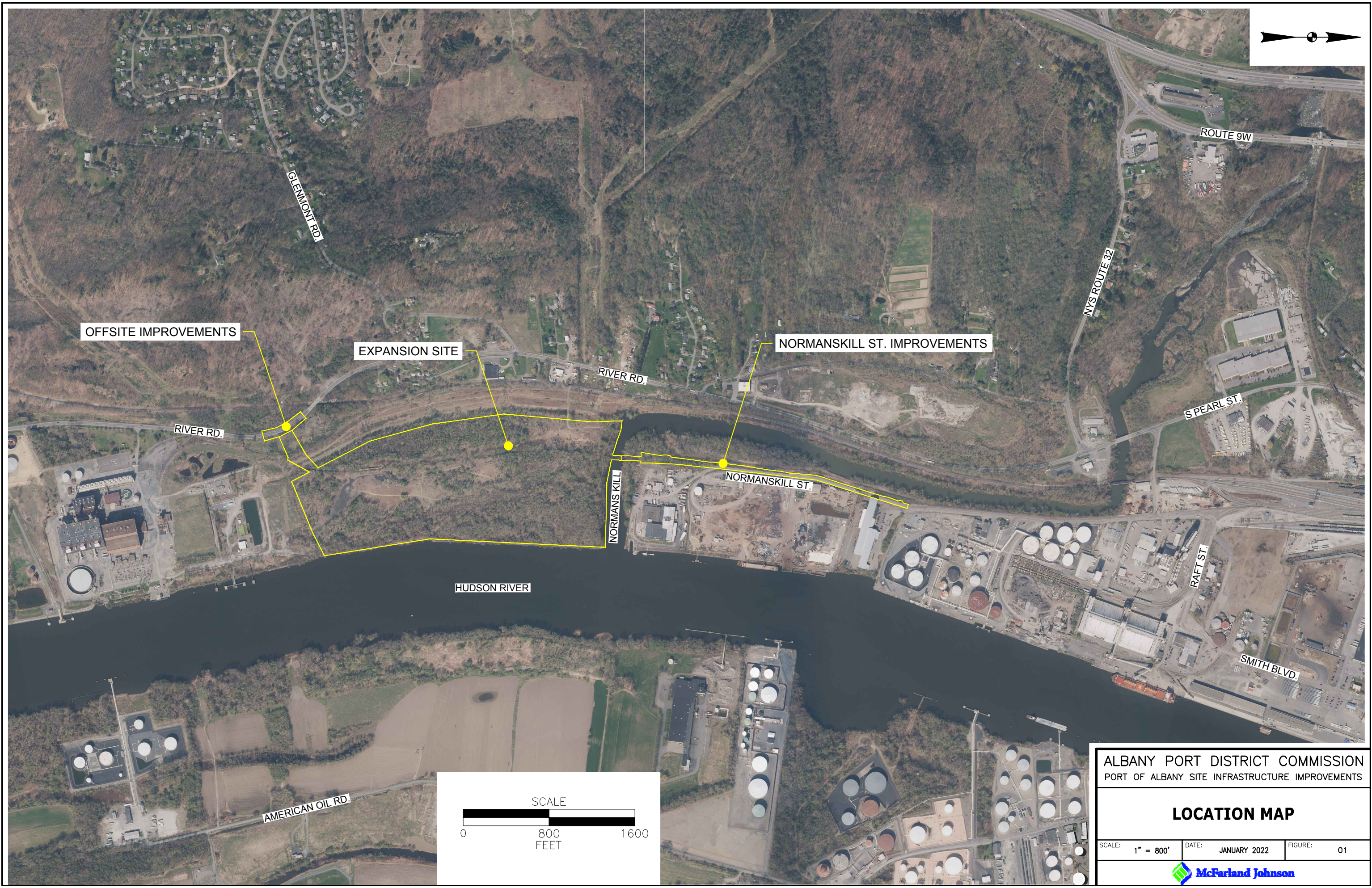
See Appendix C of the Drainage Design Report (included as Appendix C of this report).

9.7 Hydraulic Analysis of Stormwater Sewer System

All elements of the closed drainage system have been designed to be non-erosive during a 2-year storm event and capable of conveying a 10-year storm event. The profiles were created in AutoCAD Civil 3D which incorporates the rational method and Manning’s Equation to iteratively calculate the hydraulic capacity, grade lines, and inlet spreads. Printouts of the closed drainage system analysis are in Appendix C of the Drainage Design Report (included as Appendix C of this report).

APPENDIX A

LOCATION MAP



OFFSITE IMPROVEMENTS

EXPANSION SITE

NORMANSKILL ST. IMPROVEMENTS

RIVER RD.

RIVER RD.

NORMANSKILL ST.

NORMANS KILL

HUDSON RIVER

ROUTE 9W

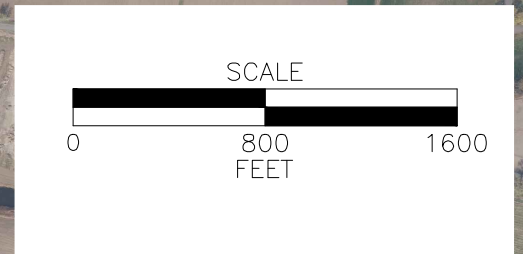
NYS ROUTE 32

S PEARL ST.

RAFT ST.

SMITH BLVD.

AMERICAN OIL RD.



ALBANY PORT DISTRICT COMMISSION
PORT OF ALBANY SITE INFRASTRUCTURE IMPROVEMENTS

LOCATION MAP

SCALE: 1" = 800'	DATE: JANUARY 2022	FIGURE: 01
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APPENDIX B

EROSION & SEDIMENT CONTROL PLANS, DETAILS &
NOTES



McFarland Johnson
 60 RAILROAD PLACE
 SUITE 402
 SARATOGA SPRINGS, NEW YORK 12866
 P: 518-580-9380 F: 518-580-9383
 SaratogaROM@mjinco.com

PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

CLIENT:
ALBANY PORT DISTRICT COMMISSION
 ALBANY, NEW YORK

PROJECT:
PORT OF ALBANY EXPANSION SITE

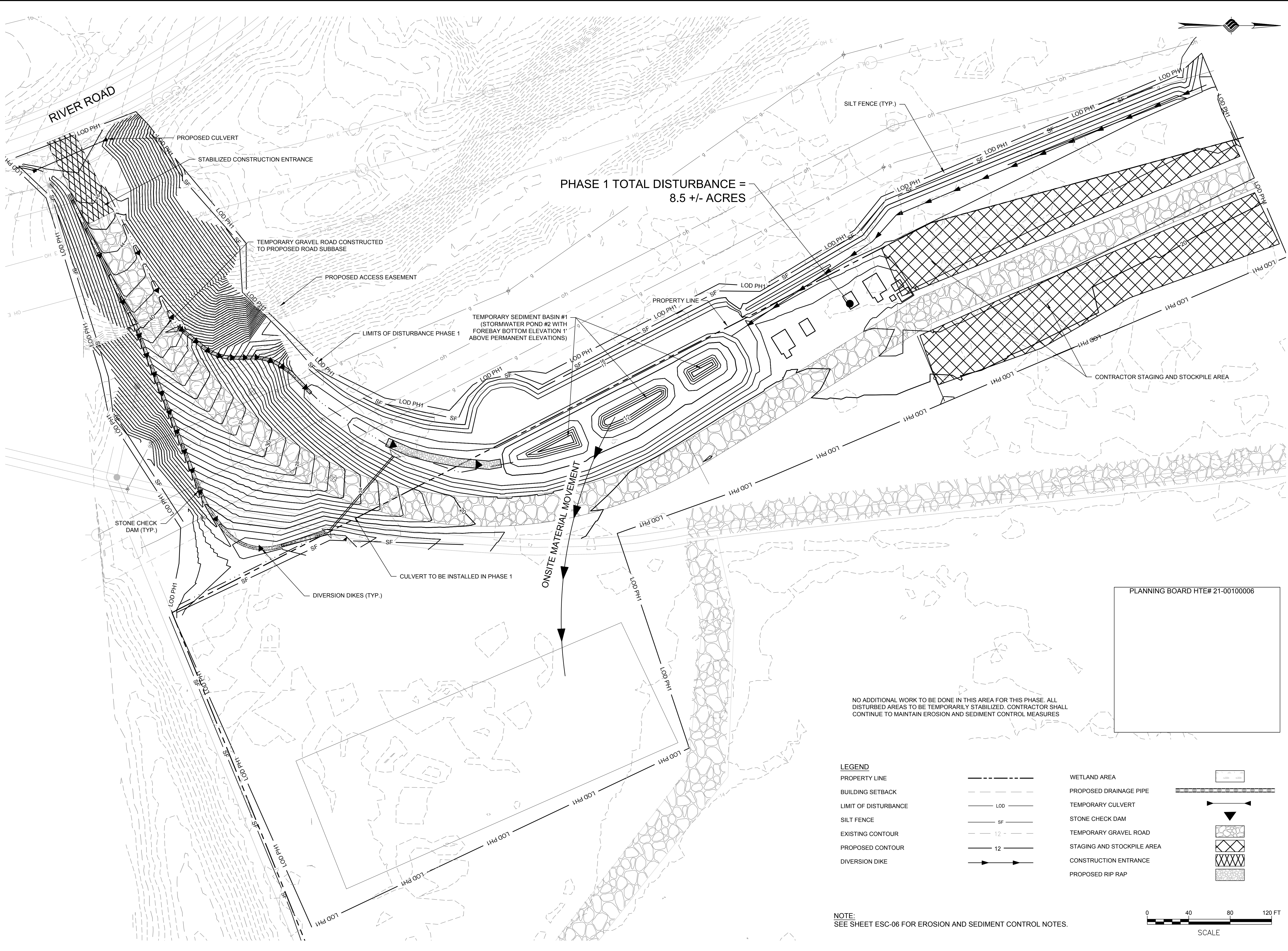
DRAWN	JES
DESIGNED	NSO
CHECKED	AJF
SCALE	AS SHOWN
DATE	05/10/2022
PROJECT	18641.00



IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECT DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR, TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION.

DRAWING TITLE
EROSION & SEDIMENT CONTROL PLAN-PH.1

DRAWING NUMBER
ESC-01



PHASE 1 TOTAL DISTURBANCE =
 8.5 +/- ACRES

NO ADDITIONAL WORK TO BE DONE IN THIS AREA FOR THIS PHASE. ALL DISTURBED AREAS TO BE TEMPORARILY STABILIZED. CONTRACTOR SHALL CONTINUE TO MAINTAIN EROSION AND SEDIMENT CONTROL MEASURES

LEGEND

PROPERTY LINE	---	WETLAND AREA	
BUILDING SETBACK	---	PROPOSED DRAINAGE PIPE	
LIMIT OF DISTURBANCE	LOD	TEMPORARY CULVERT	
SILT FENCE	SF	STONE CHECK DAM	
EXISTING CONTOUR	12	TEMPORARY GRAVEL ROAD	
PROPOSED CONTOUR	12	STAGING AND STOCKPILE AREA	
DIVERSION DIKE	▶▶	CONSTRUCTION ENTRANCE	
		PROPOSED RIP RAP	

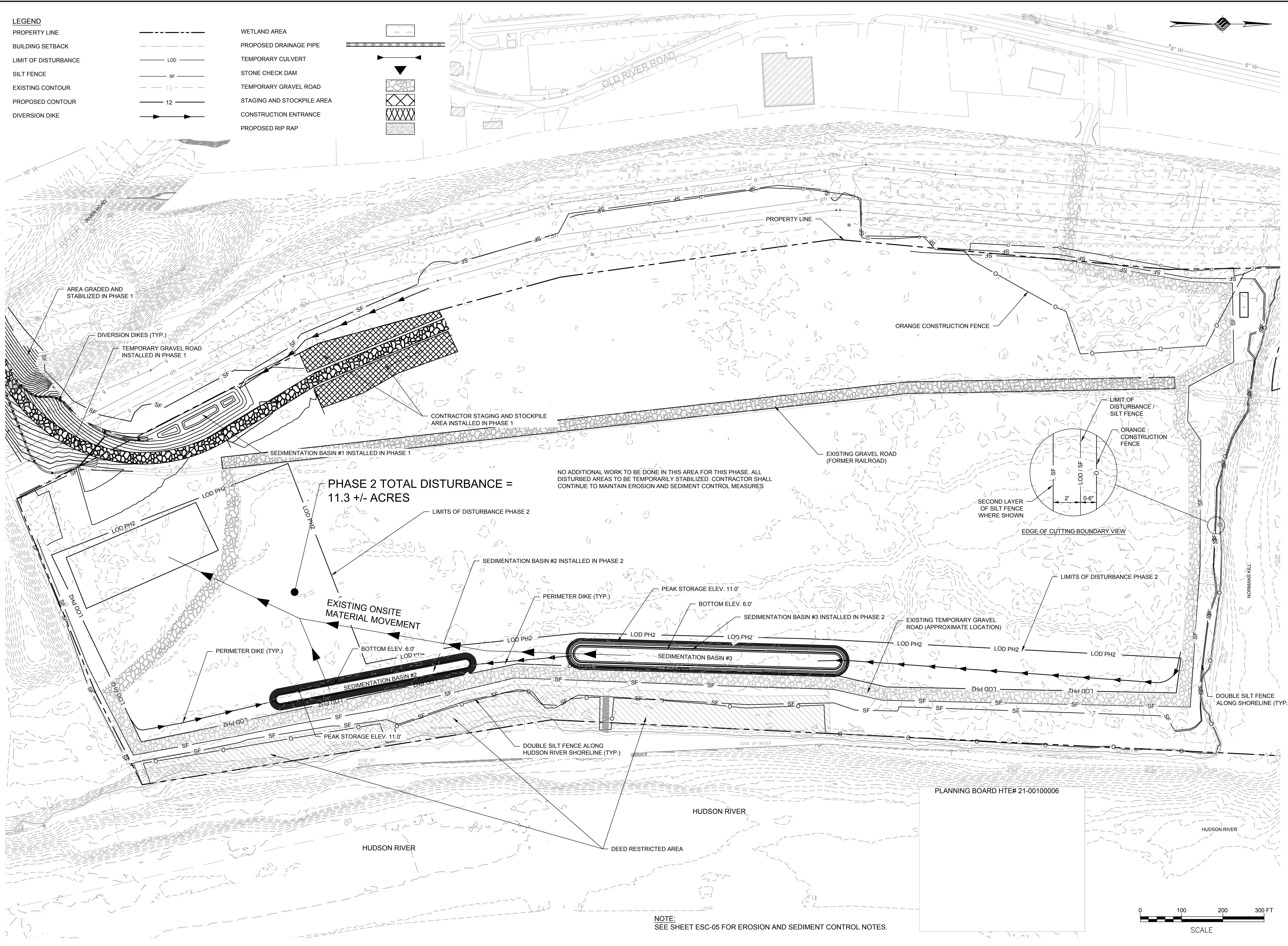
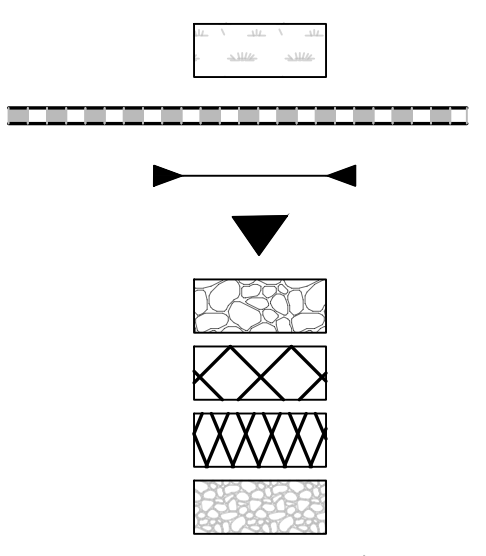
NOTE:
 SEE SHEET ESC-06 FOR EROSION AND SEDIMENT CONTROL NOTES.



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- LEGEND**
- PROPERTY LINE
 - BUILDING SETBACK
 - LIMIT OF DISTURBANCE
 - SILT FENCE
 - EXISTING CONTOUR
 - PROPOSED CONTOUR
 - DIVERSION DIKE

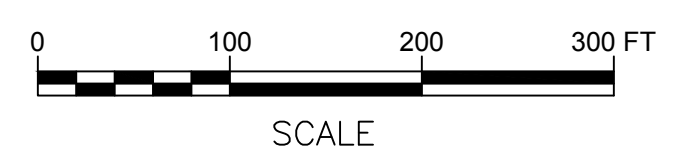
- WETLAND AREA
- PROPOSED DRAINAGE PIPE
- TEMPORARY CULVERT
- STONE CHECK DAM
- TEMPORARY GRAVEL ROAD
- STAGING AND STOCKPILE AREA
- CONSTRUCTION ENTRANCE
- PROPOSED RIP RAP



NO ADDITIONAL WORK TO BE DONE IN THIS AREA FOR THIS PHASE. ALL DISTURBED AREAS TO BE TEMPORARILY STABILIZED. CONTRACTOR SHALL CONTINUE TO MAINTAIN EROSION AND SEDIMENT CONTROL MEASURES

PLANNING BOARD HTE# 21-00100006

NOTE:
SEE SHEET ESC-05 FOR EROSION AND SEDIMENT CONTROL NOTES.



McFarland Johnson
60 RAILROAD PLACE
SUITE 402
SARATOGA SPRINGS, NEW YORK 12866
P: 518-580-9380 F: 518-580-9383
SaratogaROM@mjinc.com

PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

CLIENT:
ALBANY PORT DISTRICT COMMISSION
ALBANY, NEW YORK

PROJECT:
PORT OF ALBANY EXPANSION SITE

DRAWN	JES
DESIGNED	NSO
CHECKED	AJF
SCALE	AS SHOWN
DATE	05/10/2022
PROJECT	18641.00



IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECT DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR, TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION.

DRAWING TITLE
EROSION & SEDIMENT CONTROL PLAN-PH.2

DRAWING NUMBER
ESC-02



PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

CLIENT:
ALBANY PORT DISTRICT COMMISSION
 ALBANY, NEW YORK
 PROJECT:
PORT OF ALBANY EXPANSION SITE

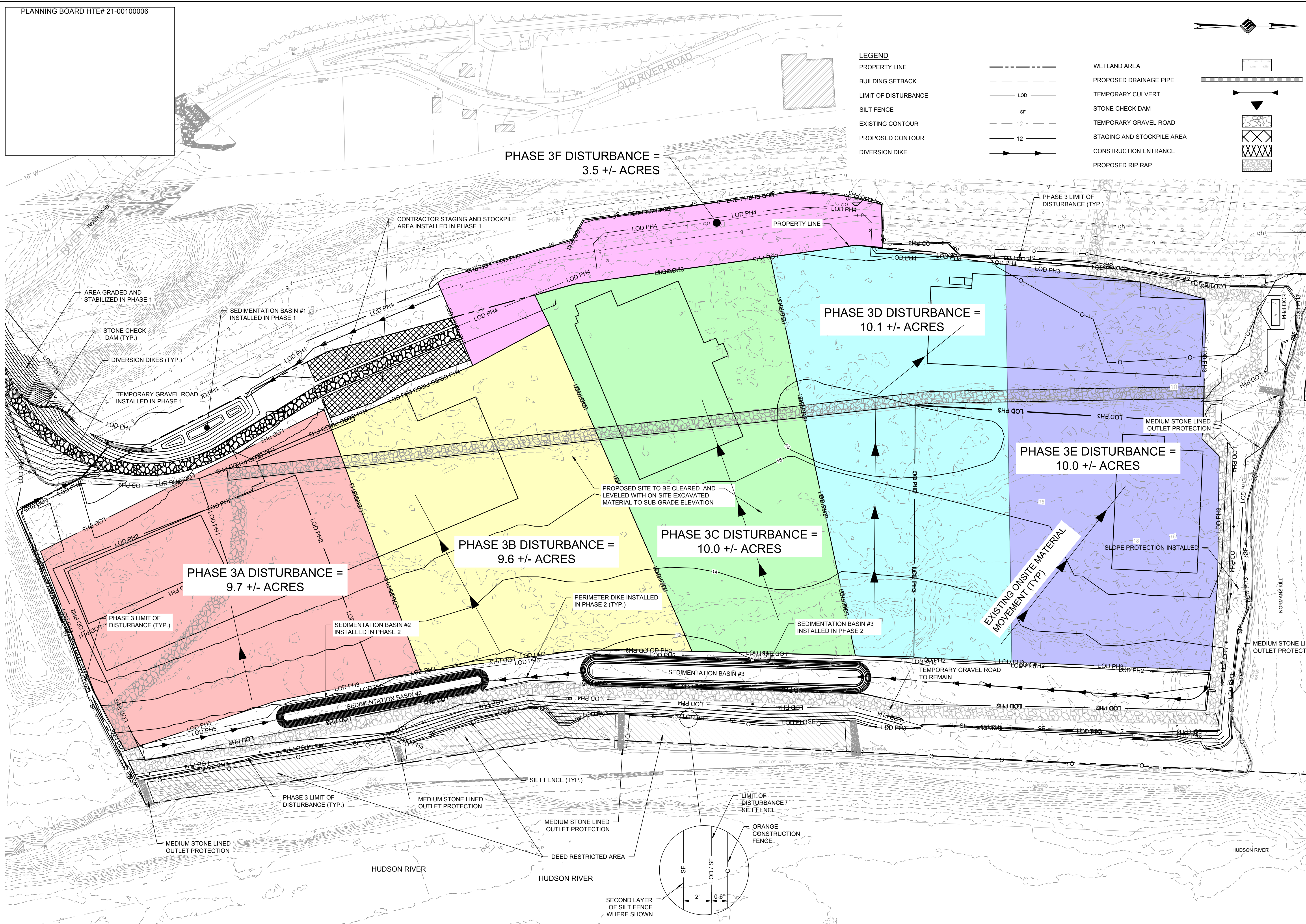
DRAWN	JES
DESIGNED	NSO
CHECKED	AJF
SCALE	AS SHOWN
DATE	05/10/2022
PROJECT	18641.00



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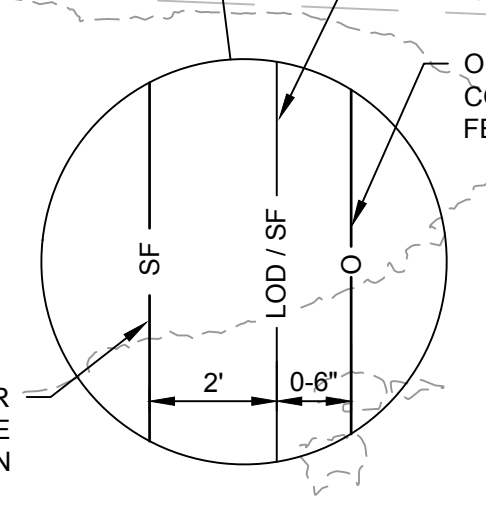
DRAWING TITLE
EROSION & SEDIMENT CONTROL PLAN-PH.3

DRAWING NUMBER
ESC-03

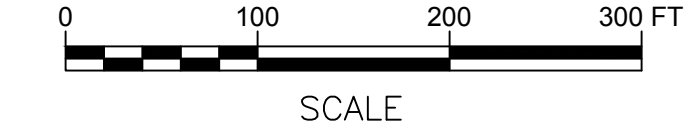


LEGEND

PROPERTY LINE	---	WETLAND AREA	[Hatched Pattern]
BUILDING SETBACK	---	PROPOSED DRAINAGE PIPE	---
LIMIT OF DISTURBANCE	LOD	TEMPORARY CULVERT	---
SILT FENCE	SF	STONE CHECK DAM	---
EXISTING CONTOUR	12	TEMPORARY GRAVEL ROAD	---
PROPOSED CONTOUR	12	STAGING AND STOCKPILE AREA	[Cross-hatched Pattern]
DIVERSION DIKE	---	CONSTRUCTION ENTRANCE	[Dashed Pattern]
		PROPOSED RIP RAP	[Stippled Pattern]



NOTE:
 SEE SHEET ESC-05 FOR EROSION AND SEDIMENT CONTROL NOTES.





NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

CLIENT: **ALBANY PORT DISTRICT COMMISSION**
ALBANY, NEW YORK
PROJECT: **PORT OF ALBANY EXPANSION SITE**

DRAWN	JES
DESIGNED	NSO
CHECKED	AJF
SCALE	AS SHOWN
DATE	05/10/2022
PROJECT	18641.00



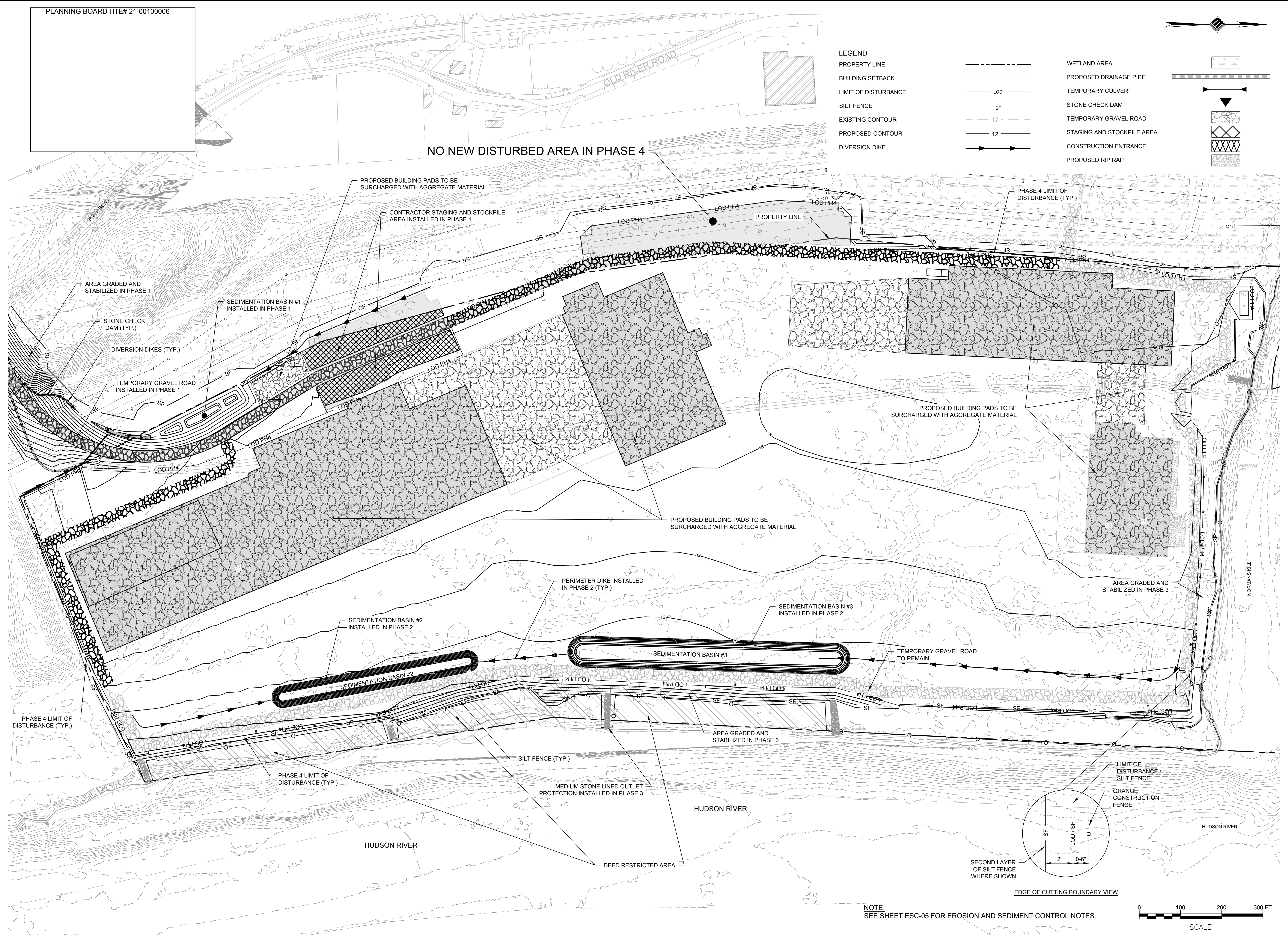
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DRAWING TITLE

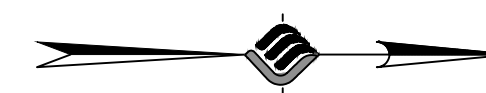
EROSION & SEDIMENT CONTROL PLAN-PH.4

DRAWING NUMBER

ESC-04



PLANNING BOARD HTE# 21-00100006



McFarland Johnson
 60 RAILROAD PLACE
 SUITE 402
 SARATOGA SPRINGS, NEW YORK 12866
 P: 518-580-9380 F: 518-580-9383
 SaratogaROM@mjinc.com

PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

CLIENT:
ALBANY PORT DISTRICT COMMISSION
 ALBANY, NEW YORK

PROJECT:
PORT OF ALBANY EXPANSION SITE

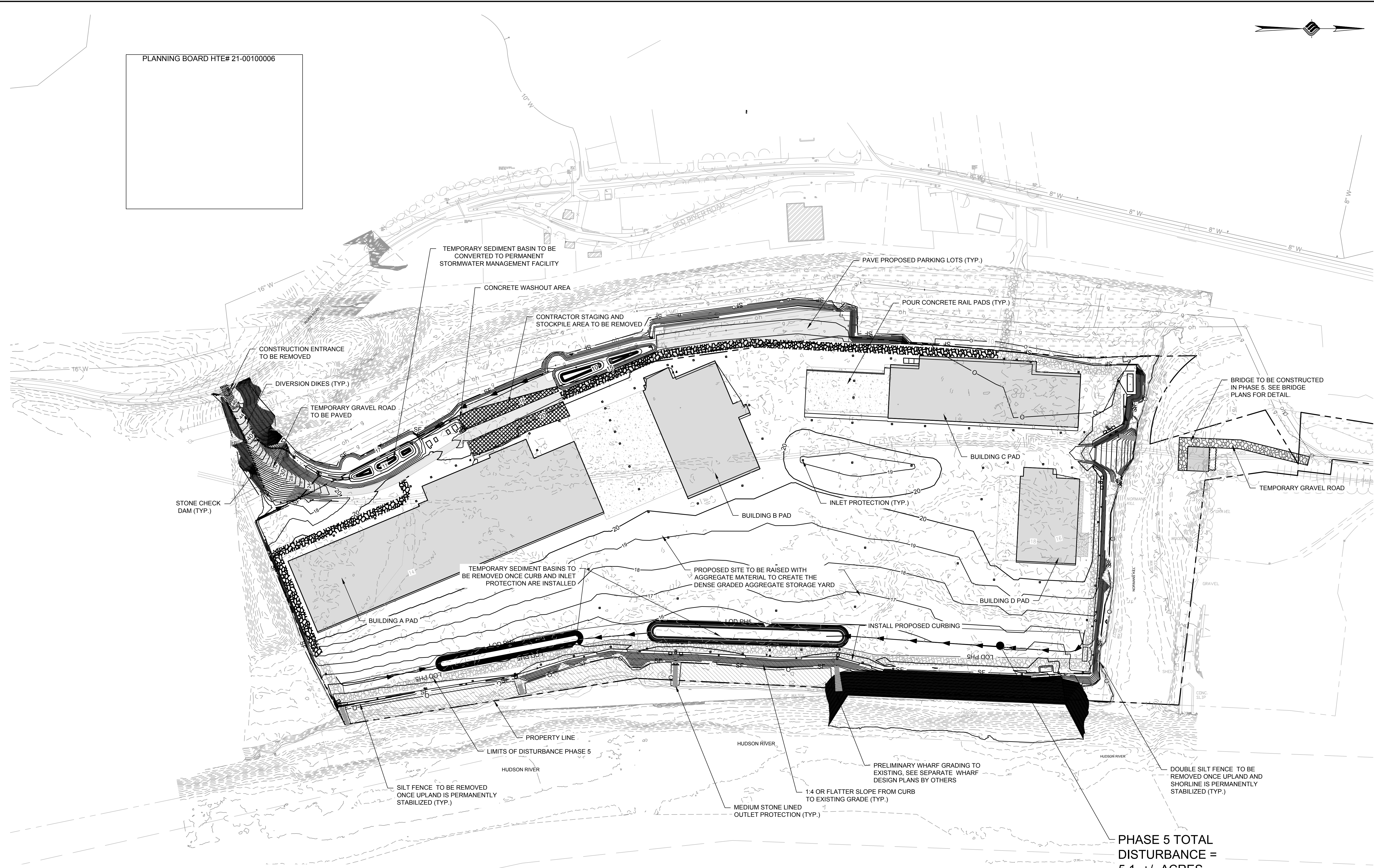
DRAWN	JES
DESIGNED	NSO
CHECKED	AJF
SCALE	AS SHOWN
DATE	05/10/2022
PROJECT	18641.00



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DRAWING TITLE
EROSION & SEDIMENT CONTROL PLAN-PH.5

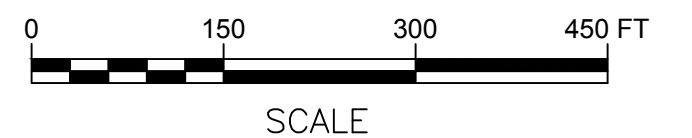
DRAWING NUMBER
ESC-05
 61 OF 68



PHASE 5 TOTAL DISTURBANCE = 5.1 +/- ACRES

LEGEND	
-----	PROPERTY LINE
-----	BUILDING SETBACK
-----	LIMIT OF DISTURBANCE
-----	SILT FENCE
-----	EXISTING CONTOUR
-----	PROPOSED CONTOUR
-----	DIVERSION DIKE
-----	WETLAND AREA
-----	PROPOSED DRAINAGE PIPE
-----	TEMPORARY CULVERT
-----	STONE CHECK DAM
-----	TEMPORARY GRAVEL ROAD
-----	STAGING AND STOCKPILE AREA
-----	CONSTRUCTION ENTRANCE
-----	PROPOSED RIP RAP

NOTE:
 SEE SHEET ESC-05 FOR EROSION AND SEDIMENT CONTROL NOTES.

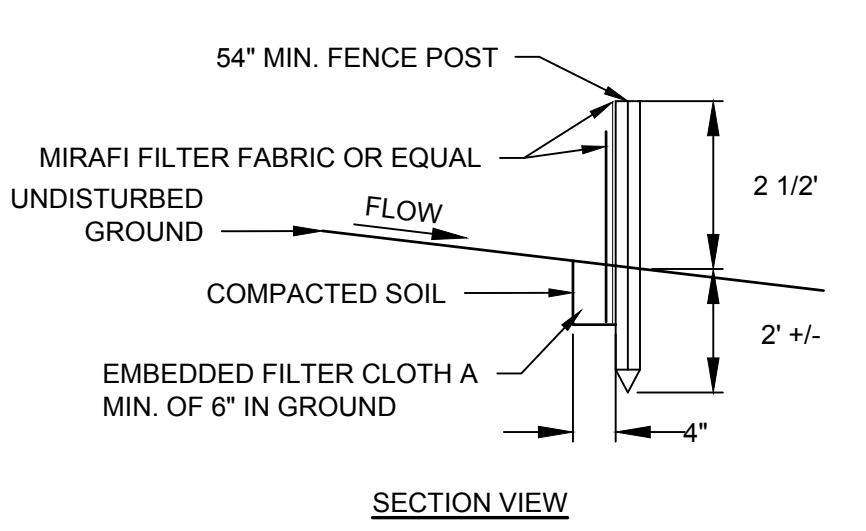
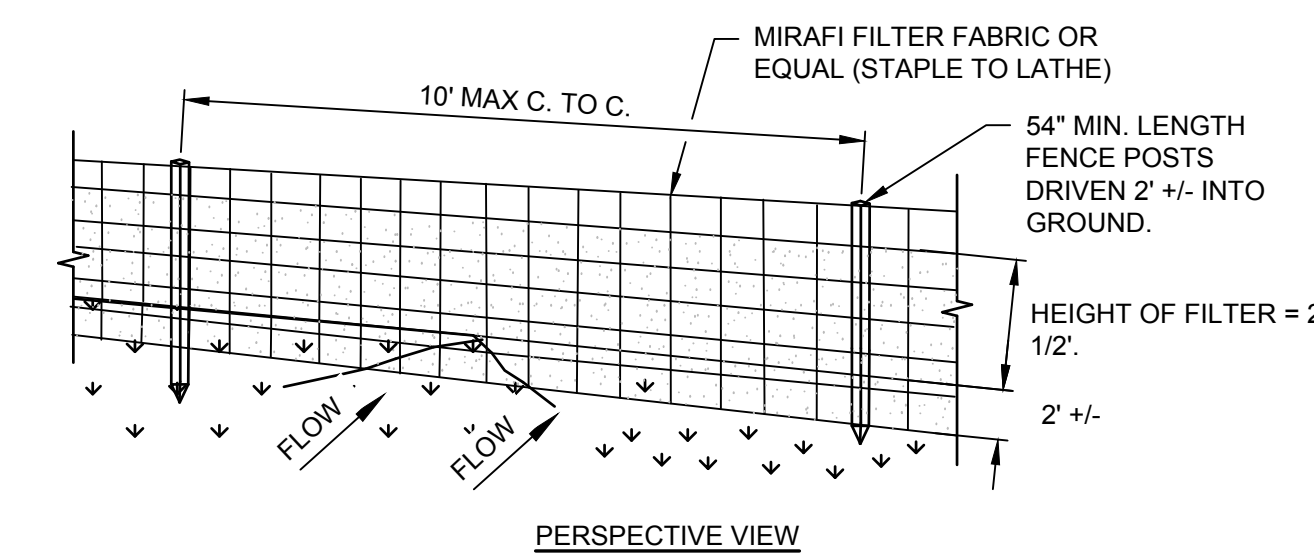


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PLANNING BOARD HTE# 21-00100006

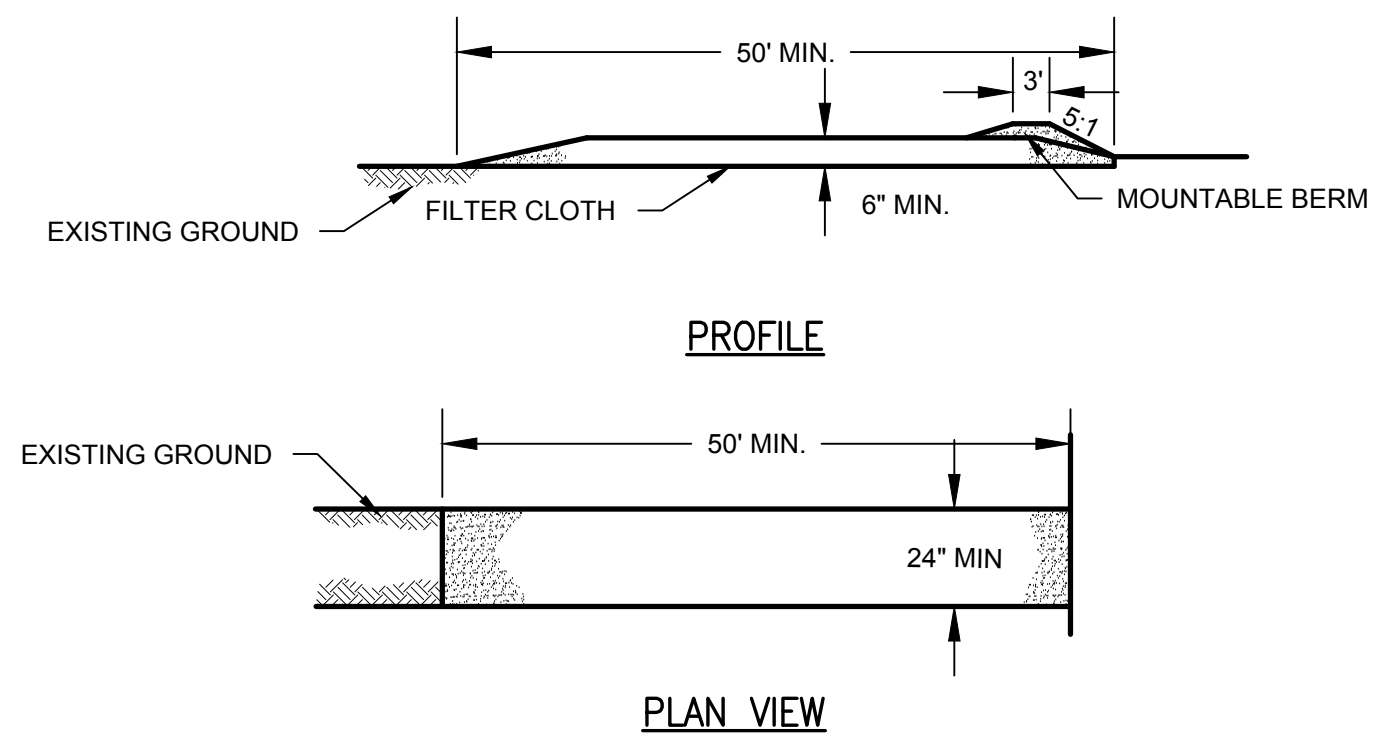
PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS



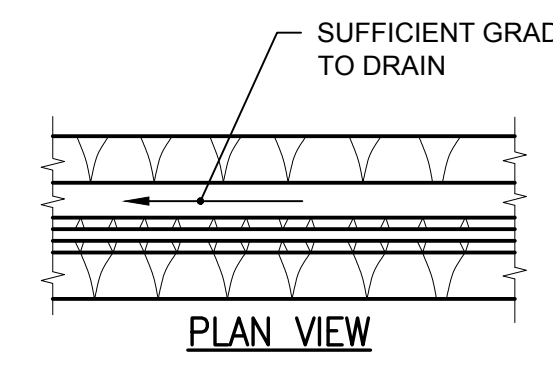
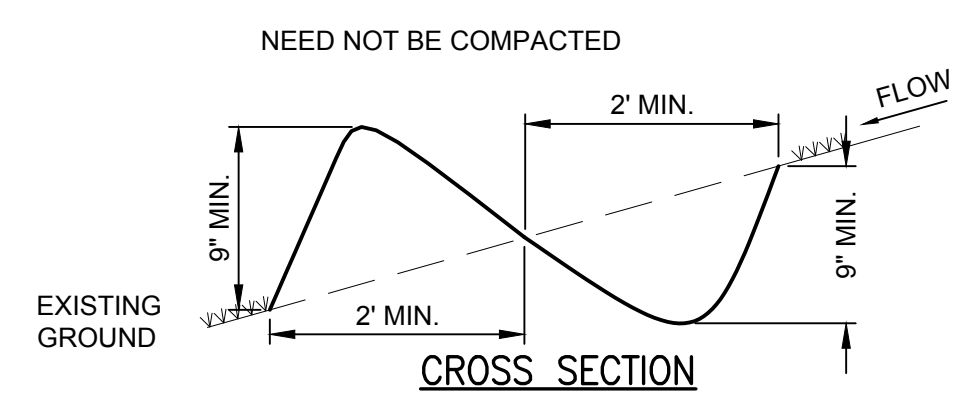
- NOTES:**
- MIRAFI FILTER FABRIC TO BE SECURED TO FENCE POSTS WITH STAPLES. POSTS SHALL BE STEEL EITHER "T" OR "U" TYPE OR HARDWOOD.
 - WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER THEY SHALL BE OVER-LAPPED BY SIX INCHES AND FOLDED.
 - MAINTENANCE SHALL BE PERFORMED AS NEEDED AND MATERIAL REMOVED WHEN "BULGES" DEVELOP IN THE SILT FENCE.

SILT FENCE
N.T.S.



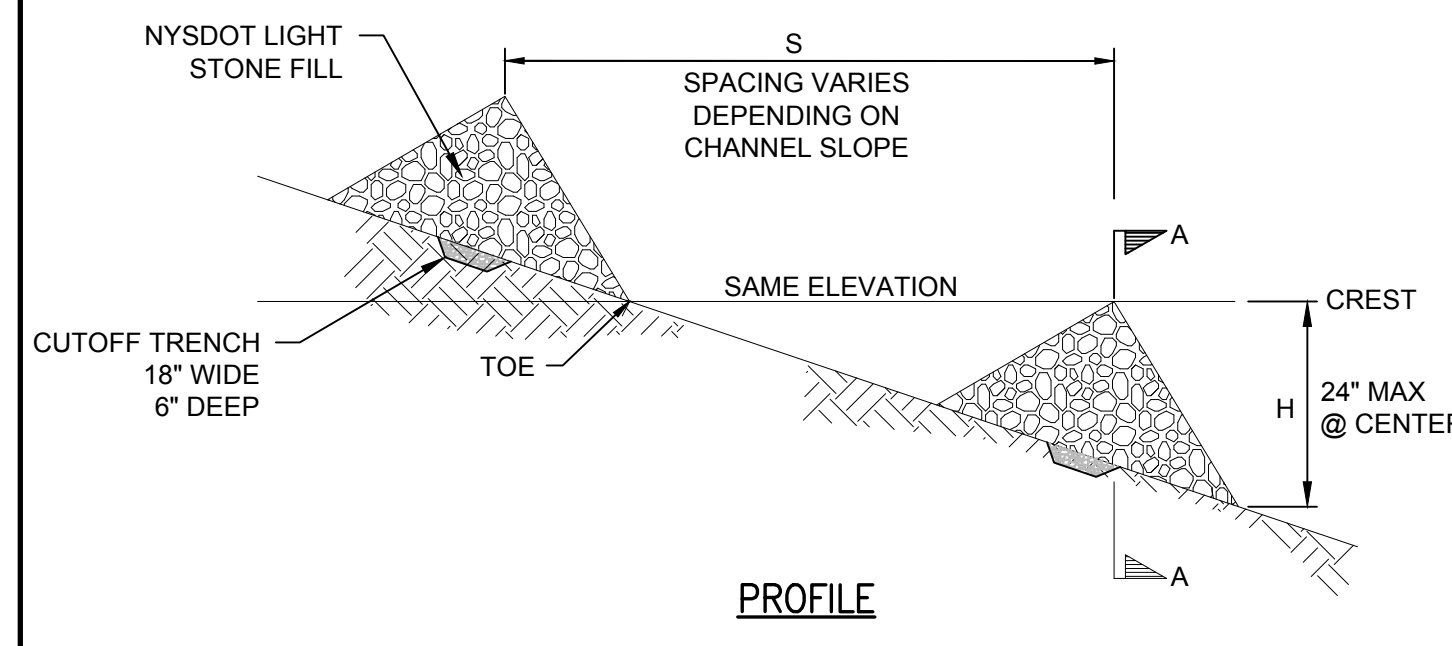
- NOTES:**
- STONE SIZE - USE #3 CRUSHED STONE OR GRAVEL (PER NYS DOT SECTION 209).
 - LENGTH - NOT LESS THAN 50 FEET.
 - THICKNESS - NOT LESS THAN SIX (6) INCHES.
 - WIDTH - TWENTY-FOUR (24) FOOT IF SINGLE ENTRANCE TO SITE.
 - FILTER CLOTH - WILL BE PLACED OVER THE ENTIRE AREA PRIOR TO PLACING OF STONE.
 - SURFACE WATER - ALL SURFACE WATER FLOWING OR DIVERTED TOWARD CONSTRUCTION ENTRANCES SHALL BE PIPED ACROSS THE ENTRANCE. IF PIPING IS IMPRACTICAL, A MOUNTABLE BERM WITH 5:1 SLOPES WILL BE PERMITTED.
 - MAINTENANCE - THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHTS-OF-WAY, ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACTED ONTO PUBLIC RIGHTS-OF-WAY MUST BE REMOVED IMMEDIATELY.
 - WHEN WASHING IS REQUIRED, IT SHALL BE DONE ON AN AREA STABILIZED WITH STONE AND WHICH DRAINS INTO AN APPROVED SEDIMENT TRAPPING DEVICE.
 - PERIODIC INSPECTION AND NEEDED MAINTENANCE SHALL BE PROVIDED AFTER EACH RAIN.

STABILIZED CONSTRUCTION ENTRANCE
N.T.S.

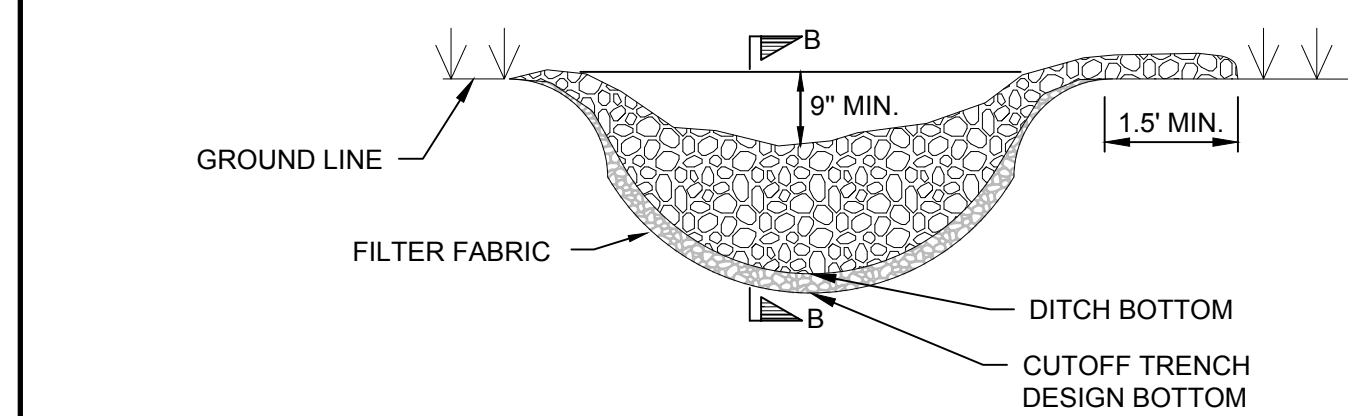


- NOTES:**
- ALL PERIMETER DIKE/SWALE SHALL HAVE UNINTERRUPTED POSITIVE GRADE TO AN OUTLET.
 - DIVERTED RUNOFF FROM A DISTURBED AREA SHALL BE CONVEYED TO A SEDIMENT TRAPPING DEVICE.
 - DIVERTED RUNOFF FROM AN UNDISTURBED AREA SHALL OUTLET INTO AN UNDISTURBED STABILIZED AREA AT NON-EROSION VELOCITY.
 - THE SWALE SHALL BE EXCAVATED OR SHAPED TO LINE GRADE, AND CROSS SECTION AS REQUIRED TO MEET THE CRITERIA SPECIFIED IN THE STANDARD.
 - STABILIZATION OF THE AREA DISTURBED BY THE DIKE AND SWALE SHALL BE DONE IN ACCORDANCE WITH THE STANDARD AND SPECIFICATIONS FOR TEMPORARY SEEDING AND MULCHING, AND SHALL BE DONE WITHIN 10 DAYS.
 - PERIODIC INSPECTION AND REQUIRED MAINTENANCE MUST BE PROVIDED AFTER EACH RAIN EVENT.

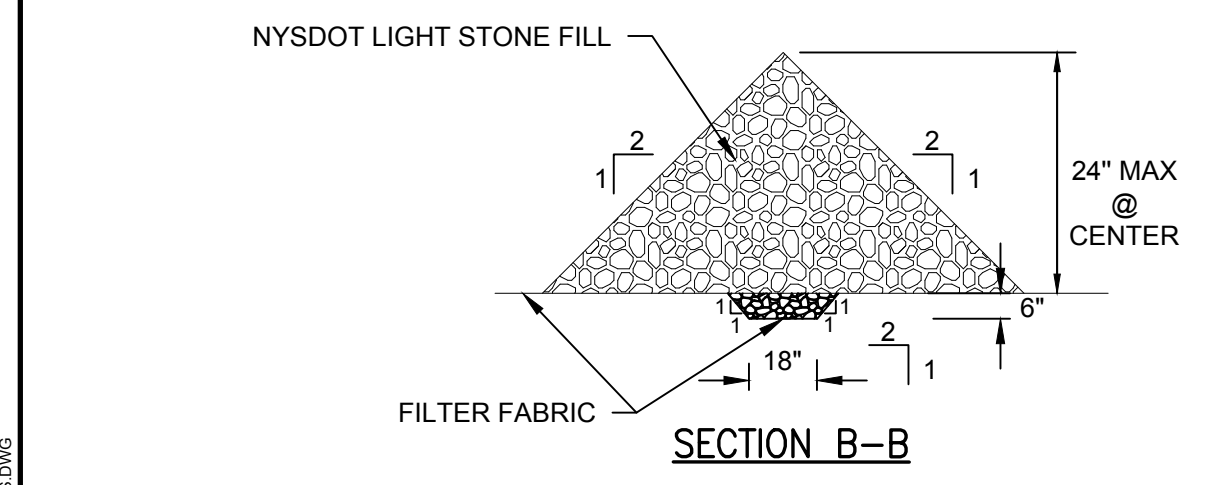
PERIMETER DIKE
N.T.S.



$$S = \frac{H (FT)}{\text{SLOPE (FT/FT)}}$$



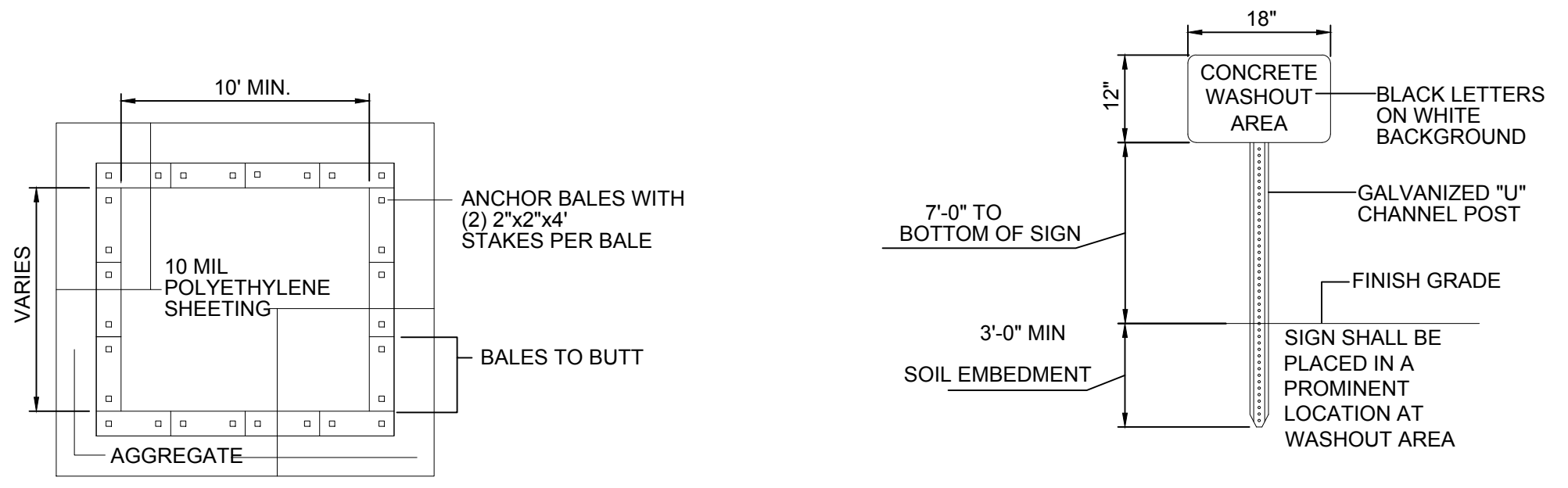
SECTION A-A



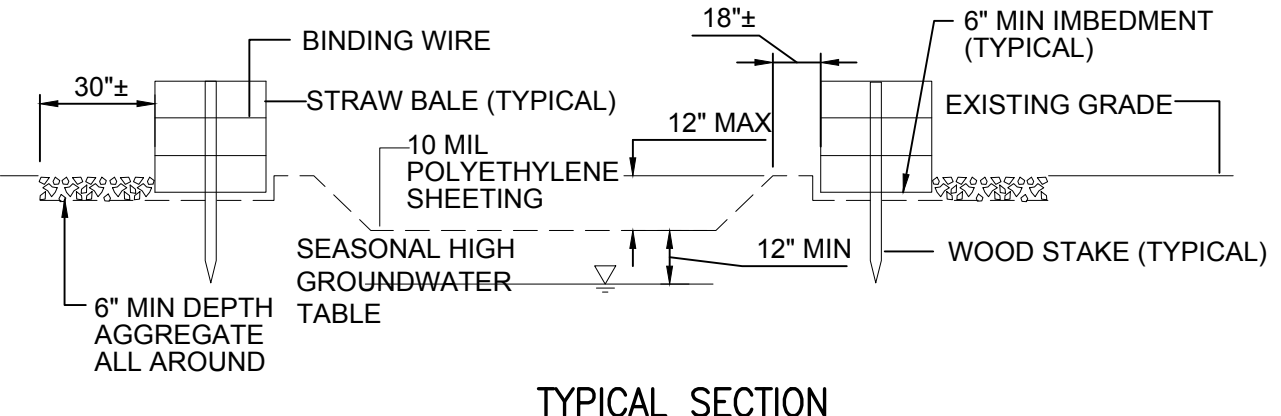
SECTION B-B

- CONSTRUCTION SPECIFICATIONS**
- STONE WILL BE PLACED ON A FILTER FABRIC FOUNDATION TO THE LINES GRADES AND LOCATIONS SHOWN ON THE PLAN.
 - SET SPACING OF CHECK DAMS TO ASSUME THAT THE ELEVATIONS OF THE CREST OF THE DOWNSTREAM DAM IS AT THE SAME ELEVATION OF THE TOE OF THE UPSTREAM DAM.
 - EXTEND THE STONE A MINIMUM OF 1.5' BEYOND THE DITCH BANKS TO PREVENT CUTTING AROUND THE DAM.
 - PROTECT THE CHANNEL DOWNSTREAM OF THE LOWEST CHECK DAM FROM SCOUR AND EROSION WITH STONE OR LINER AS APPROPRIATE.
 - ENSURE THAT CHANNEL APPURTENANCES SUCH AS CULVERT ENTRANCES BELOW CHECK DAMS ARE NOT SUBJECT TO DAMAGE OR BLOCKAGE FROM DISPLACED STONES.

LIGHT STONE CHECK DAM
N.T.S.



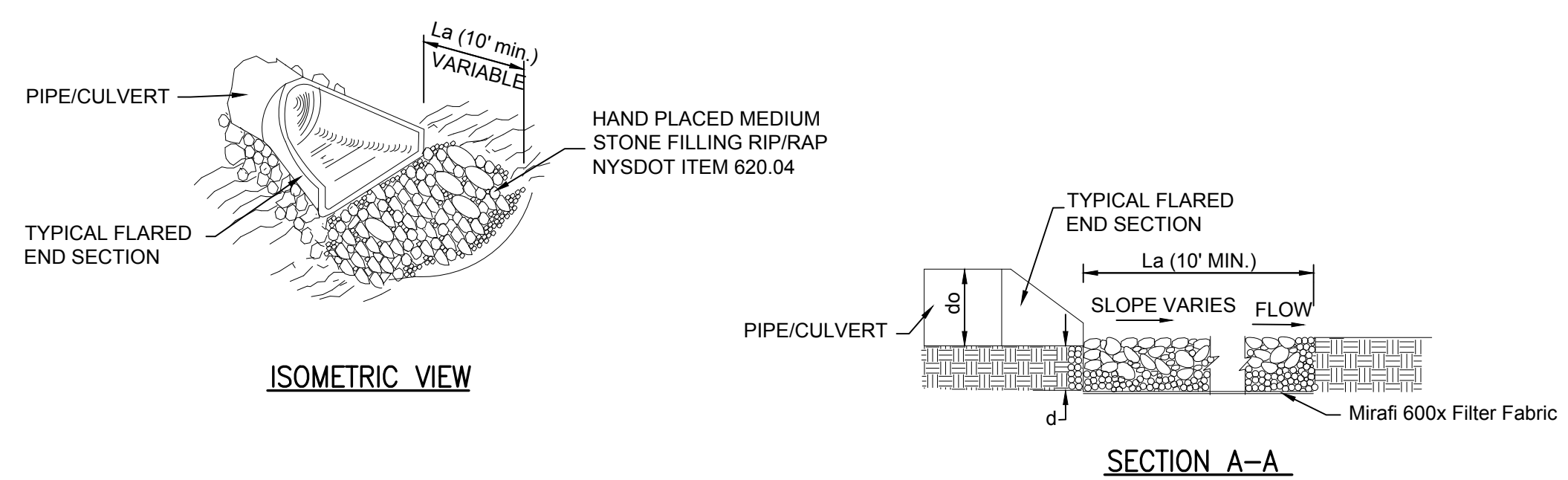
WASHOUT SIGN



TYPICAL SECTION

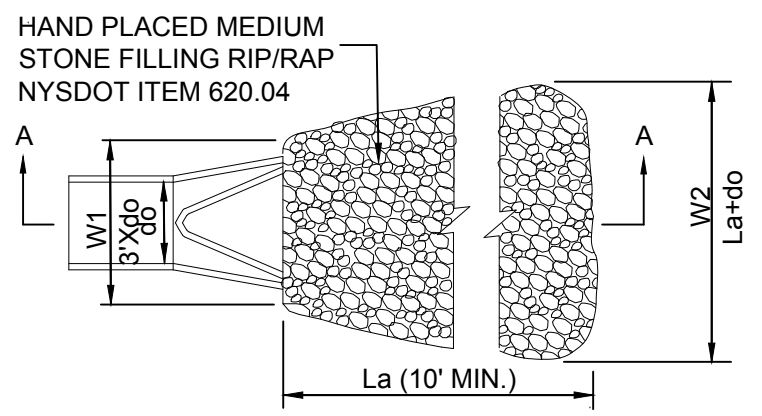
- NOTES:**
- CONTAINMENT MUST BE STRUCTURALLY SOUND AND LEAK FREE AND CONTAIN ALL LIQUID WASTES.
 - CONTAINMENT DEVICES MUST BE OF SUFFICIENT QUANTITY OR VOLUME TO COMPLETELY CONTAIN THE LIQUID WASTES GENERATED.
 - WASHOUT MUST BE CLEANED OR NEW FACILITIES CONSTRUCTED AND READY TO USE ONCE WASHOUT IS 75% FULL.
 - WASHOUT AREA(S) SHALL BE INSTALLED IN A LOCATION EASILY ACCESSIBLE BY CONCRETE TRUCKS.
 - ONE OR MORE AREAS MAY BE INSTALLED ON THE CONSTRUCTION SITE AND MAY BE RELOCATED AS CONSTRUCTION PROGRESSES.
 - AT LEAST WEEKLY REMOVE ACCUMULATION OF SAND AND AGGREGATE AND DISPOSE OF PROPERLY.

CONCRETE WASHOUT
N.T.S.



ISOMETRIC VIEW

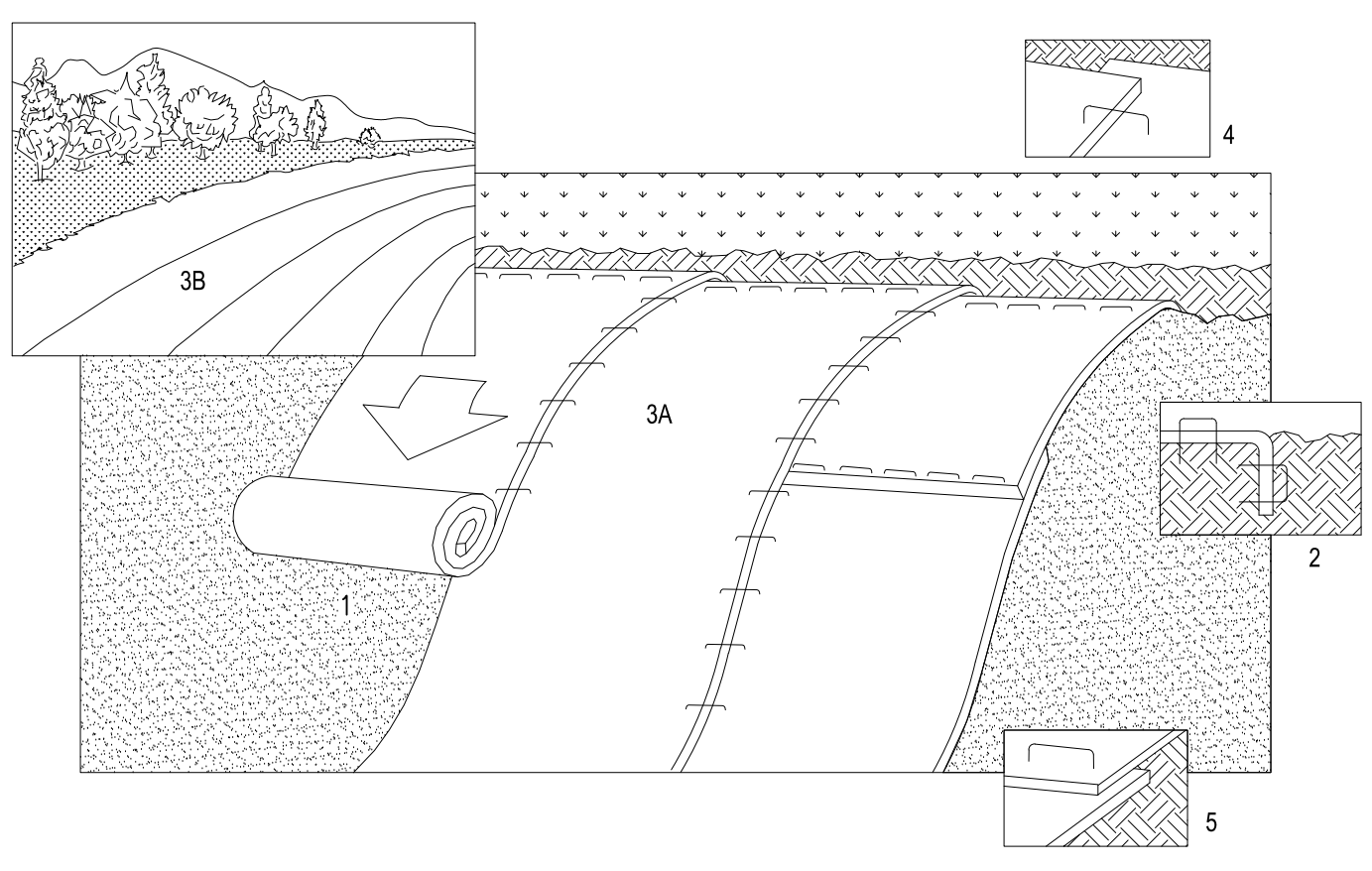
SECTION A-A



PLAN

- NOTES:**
- $d = 1.5$ TIMES THE MAXIMUM STONE DIAMETER BUT NO LESS THAN 6".
 - INSTALL FILTER MIRAFI 500X OR APPROVED EQUAL FILTER FABRIC BETWEEN RIP-RAP AND SUBGRADE.

OUTLET PROTECTION - RIP RAP
N.T.S.



- INSTALLATION OF GEOSYNTHETIC EROSION CONTROL MATS:**
- EROSION CONTROL MATS SHALL BE UTILIZED ON ALL SLOPES OF 3:1 OR GREATER REQUIRING PERMANENT STABILIZATION.
 - SLOPES SHALL BE PREPARED AND EROSION CONTROL MATS SHALL BE INSTALLED, ANCHORED AND SOIL FILLED IN ACCORDANCE WITH THE MANUFACTURER'S SPECIFICATIONS AND INSTALLATION PROCEDURES.
 - SEEDING SHALL BE COMPLETED IN ACCORDANCE WITH THE PERMANENT SEEDING SPECIFICATIONS ABOVE PRIOR TO PLACEMENT OF THE EROSION CONTROL MAT. A SECOND APPLICATION OF PERMANENT SEEDING SHALL BE APPLIED AFTER THE MAT IS IN PLACE, PRIOR TO SOIL FILLING THE MAT.
 - CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTENANCE, RESEEDING AND REPAIR OF MATS AND SLOPES UNTIL PERMANENT STABILIZATION IS ACHIEVED.

- NOTES:**
- REFER TO GENERAL STAPLE PATTERN GUIDE FOR CORRECT STAPLE PATTERN RECOMMENDATIONS FOR SLOPE INSTALLATIONS.
- PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING APPLICATION OF LIME, FERTILIZER, AND SEED. NOTE: WHEN USING CELL-O-SEED DO NOT SEED PREPARED AREA. CELL-O-SEED MUST BE INSTALLED WITH PAPER SIDE DOWN.
 - BEGIN AT THE TOP OF THE SLOPE BY ANCHORING THE BLANKET IN 6" DEEP X 6" WIDE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING.
 - ROLL THE BLANKETS (A) DOWN OR (B) HORIZONTALLY ACROSS THE SLOPE.
 - THE EDGES OF PARALLEL BLANKETS MUST BE STAPLED WITH APPROXIMATELY 2" OVERLAP.
 - WHEN BLANKETS MUST BE SPLICED DOWN THE SLOPE, PLACE BLANKETS END OVER END (SHINGLE STYLE) WITH APPROXIMATELY 4" OVERLAP. STAPLE THROUGH OVERLAPPED AREA, APPROXIMATELY 12" APART.
 - MANUFACTURER'S INSTALLATION INSTRUCTIONS SHALL SUPERCEDE THIS DETAIL.

EROSION CONTROL MAT INSTALLATION
N.T.S.

CLIENT:
ALBANY PORT DISTRICT COMMISSION
ALBANY, NEW YORK

PROJECT:
PORT OF ALBANY EXPANSION SITE

DRAWN	JES
DESIGNED	NSO
CHECKED	AJF
SCALE	AS SHOWN
DATE	05/10/2022
PROJECT	18641.00



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EROSION & SEDIMENT CONTROL DETAILS

DRAWING NUMBER

ESC-07



McFarland Johnson
 60 RAILROAD PLACE
 SUITE 402
 SARATOGA SPRINGS, NEW YORK 12866
 P: 518-580-9380 F: 518-580-9383
 SaratogaROM@mjinco.com

PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

CLIENT:
ALBANY PORT DISTRICT COMMISSION
 ALBANY, NEW YORK

PROJECT:
PORT OF ALBANY EXPANSION SITE

DRAWN	JES
DESIGNED	NSO
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SCALE	AS SHOWN
DATE	05/10/2022
PROJECT	18641.00



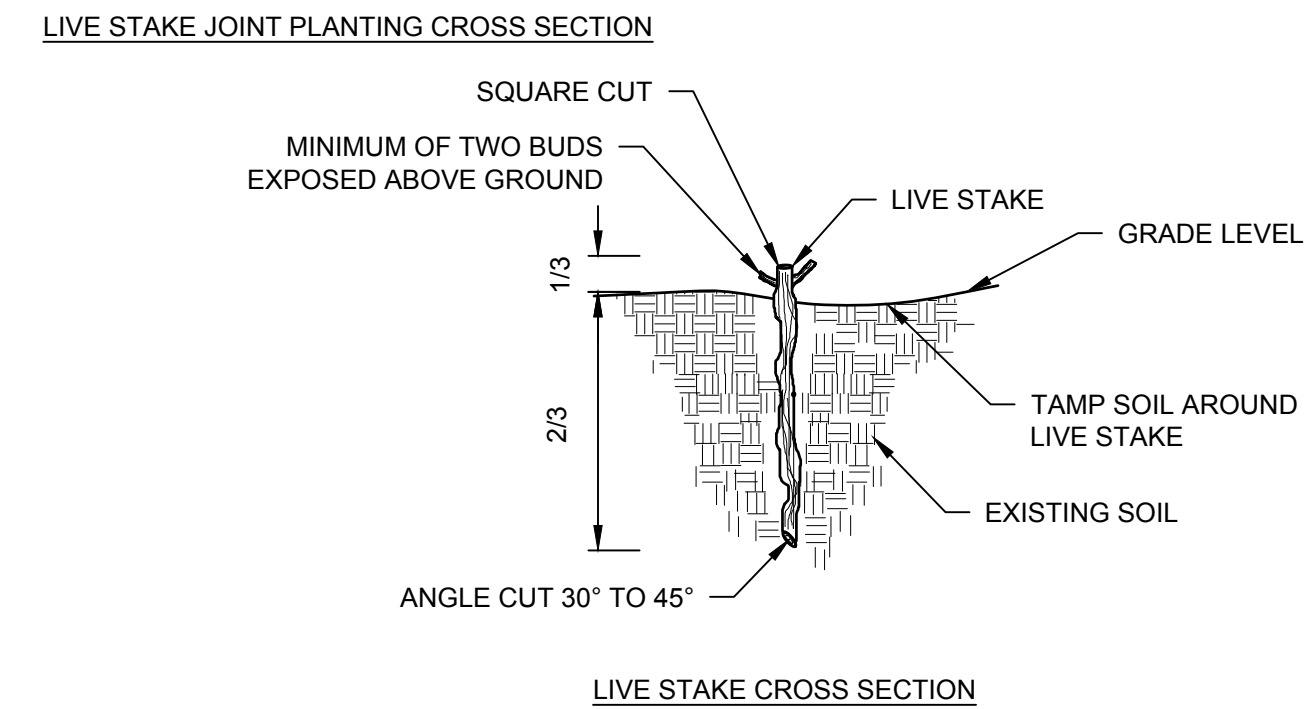
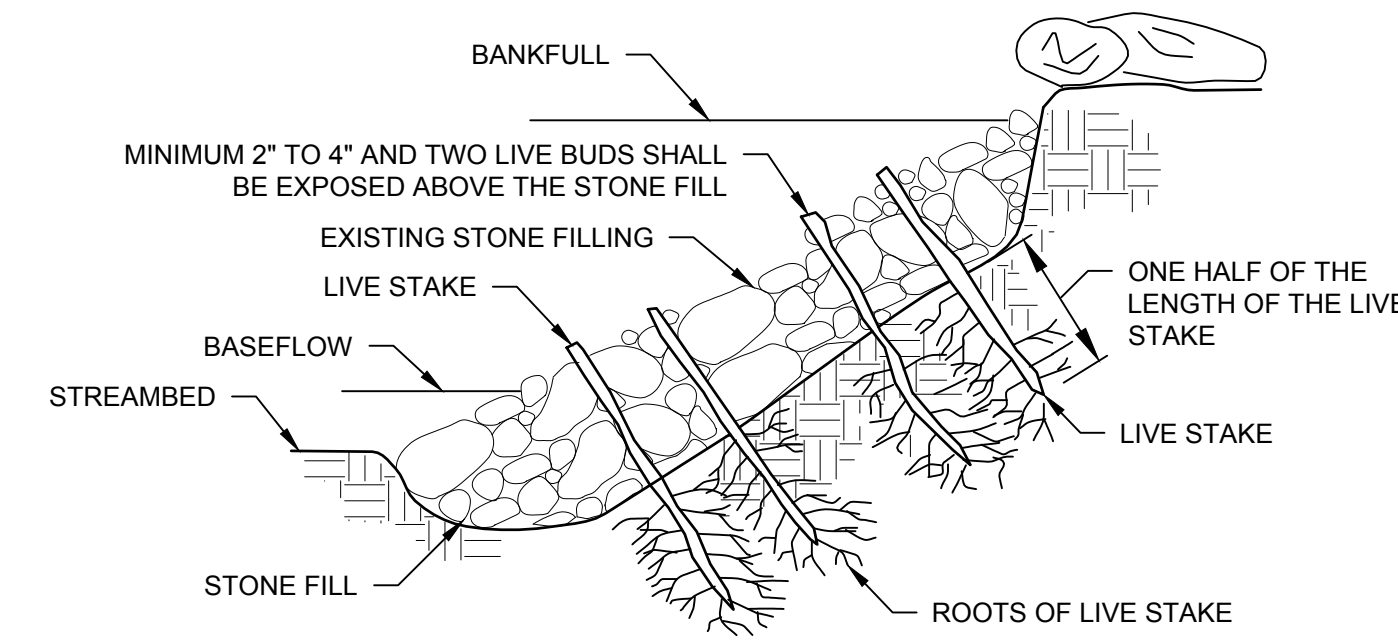
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DRAWING TITLE
EROSION & SEDIMENT CONTROL DETAILS

DRAWING NUMBER

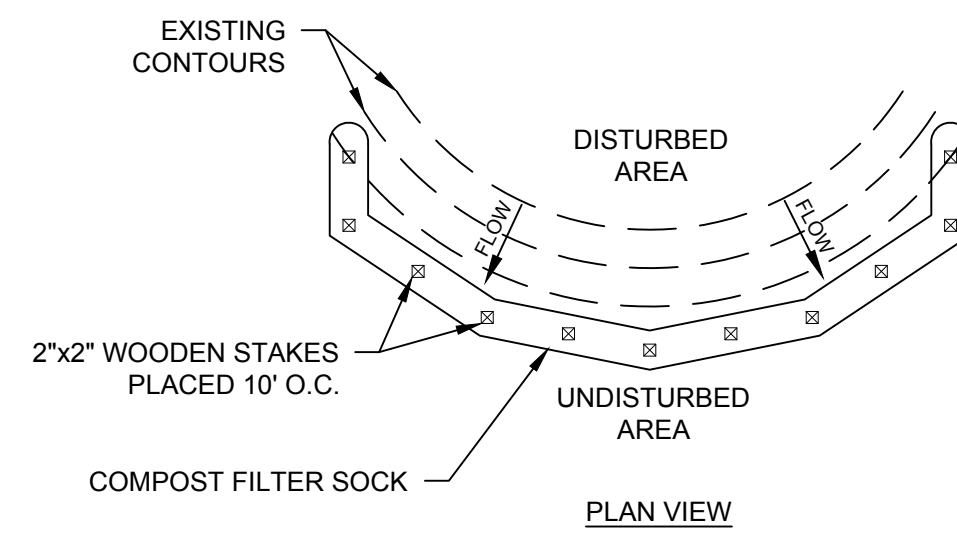
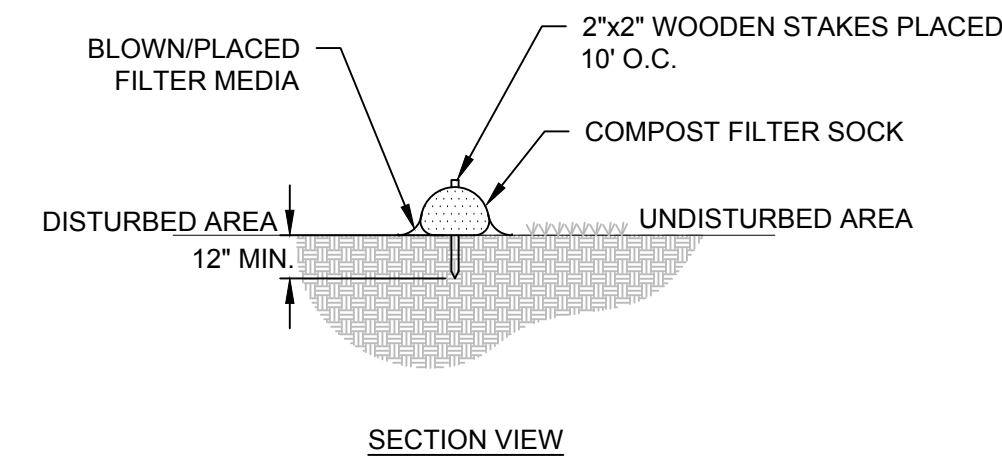
ESC-08

- NOTES:
- CARE SHALL BE TAKEN NOT TO DAMAGE THE LIVE STAKES DURING INSTALLATION. THOSE DAMAGED SHALL BE LEFT IN PLACE AND SUPPLEMENTED WITH AN INTACT LIVE STAKE.
 - THE LENGTHS OF LIVE STAKES DEPENDS UPON THE APPLICATION. THE LENGTH SHALL EXTEND THROUGH THE SURFACE OF THE STONE FILL AT LEAST HALF THE LENGTH SHALL BE INSERTED IN TO THE SOIL, BELOW THE STONE FILL.
 - A PILOT HOLE IS REQUIRED TO ENSURE THAT THE LIVE STAKE IS NOT DAMAGED WHEN DRIVEN THROUGH THE STONE FILLING. ACCESS SHALL BE MADE THROUGH THE USE OF A DIBBLE BAR, OR SIMILAR TOOL TO WORK AN OPENING THROUGH THE ROCK LAYER.
 - MINIMUM 2" TO 4" AND TWO LIVE BUDS OF THE LIVE STAKE SHALL BE EXPOSED ABOVE THE STONE FILLING.
 - LIVE STAKES SHALL RANGE FROM 1" TO 4" IN DIAMETER AND BE FROM 5' TO 6' IN LENGTH.
 - LIVE STAKES SHALL BE CUT TO A POINT ON THE BASAL END FOR INSERTION IN THE GROUND.
 - USE A DEAD BLOW HAMMER TO DRIVE STAKES INTO THE GROUND. (HAMMER HEAD FILLED WITH SHOT OR SAND). A DIBBLE, IRON BAR, OR SIMILAR TOOL SHALL BE USED TO MAKE A PILOT HOLE TO PREVENT DAMAGING THE MATERIAL DURING INSTALLATION.
 - WHEN POSSIBLE, TAMP SOIL AROUND LIVE STAKES.



LIVE STAKE

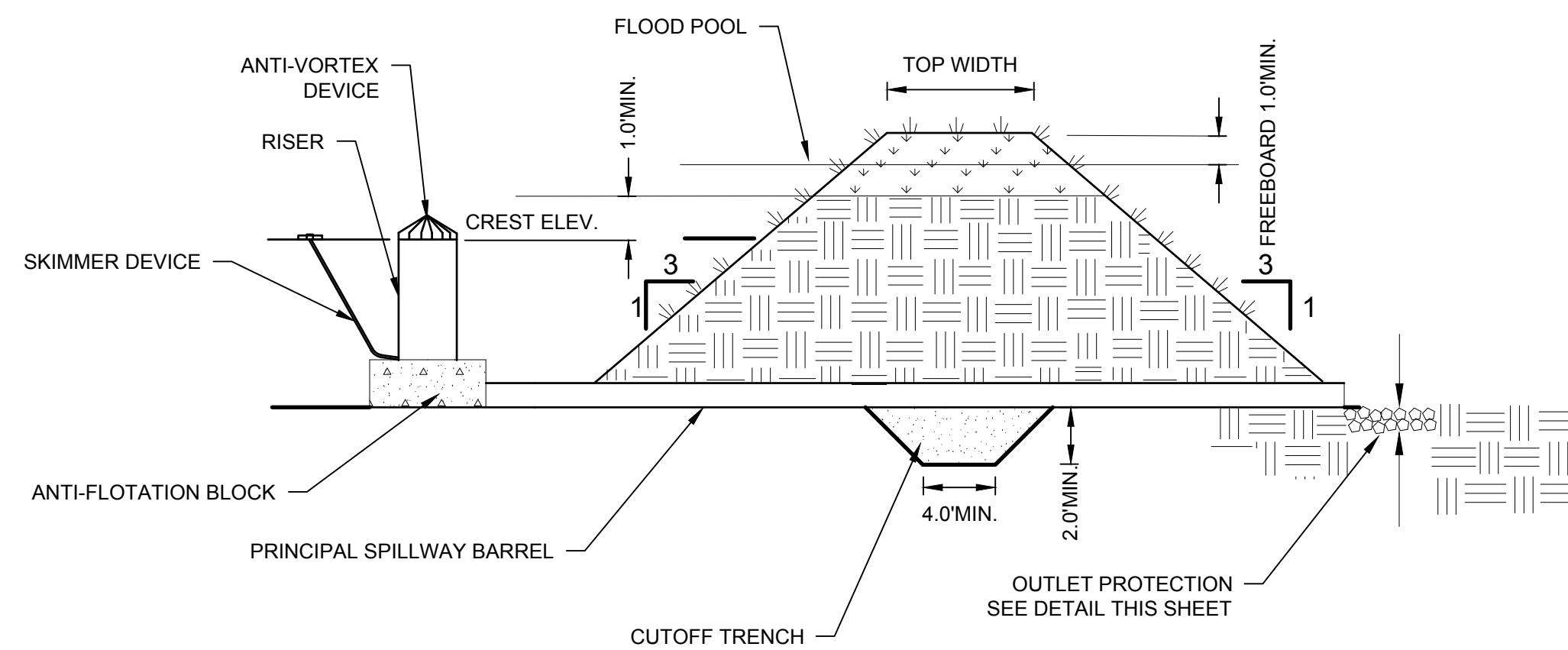
- NOTES:
- SOCK FABRIC SHALL MEET STANDARDS OF TABLE 5.1 OF NYS STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL. COMPOST FILTER SOCK SHALL MEET THE STANDARDS LISTED ON TABLE 5.2 OF NYS STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL.
 - COMPOST FILTER SOCK SHALL BE PLACED AT EXISTING LEVEL GRADE. BOTH ENDS OF THE SOCK SHALL BE EXTENDED AT LEAST 8 FEET UP SLOPE AT 45° TO THE MAIN SOCK ALIGNMENT. MAXIMUM SLOPE LENGTH ABOVE ANY SOCK SHALL NOT EXCEED THAT SHOWN ON FIGURE X.X OF NYS STANDARDS AND SPECIFICATIONS FOR EROSION AND SEDIMENT CONTROL. STAKES MAY BE INSTALLED IMMEDIATELY DOWN SLOPE OF THE SOCK IF SO SPECIFIED BY THE MANUFACTURER.
 - TRAFFIC SHALL NOT BE PERMITTED TO CROSS FILTER SOCKS.
 - ACCUMULATED SEDIMENT SHALL BE REMOVED WHEN IT REACHES HALF THE ABOVEGROUND HEIGHT OF THE SOCK AND DISPOSED IN THE MANNER DESCRIBED ELSEWHERE IN THE PLAN.
 - SOCKS SHALL BE INSPECTED WEEKLY AND AFTER EACH RUNOFF EVENT. DAMAGED SOCKS SHALL BE REPAIRED ACCORDING TO MANUFACTURER'S SPECIFICATIONS OR REPLACED WITHIN 24 HOURS OF INSPECTION.
 - BIODEGRADABLE FILTER SOCKS SHALL BE REPLACED AFTER 6 MONTHS; PHOTODEGRADABLE SOCKS AFTER 1 YEAR. POLYPROPYLENE SOCKS SHALL BE REPLACED ACCORDING TO MANUFACTURER'S RECOMMENDATIONS.
 - UPON STABILIZATION OF THE AREA TRIBUTARY TO THE SOCKS, STAKES SHALL BE REMOVED. THE SOCK MAY BE LEFT IN PLACE AND VEGETATED OR REMOVED. IN THE LATTER CASE, THE MESH SHALL BE CUT OPEN AND THE MULCH SPREAD AS A SOIL SUPPLEMENT.



COMPOST FILTER SOCK

N.T.S.

PLANNING BOARD HTE# 21-00100006

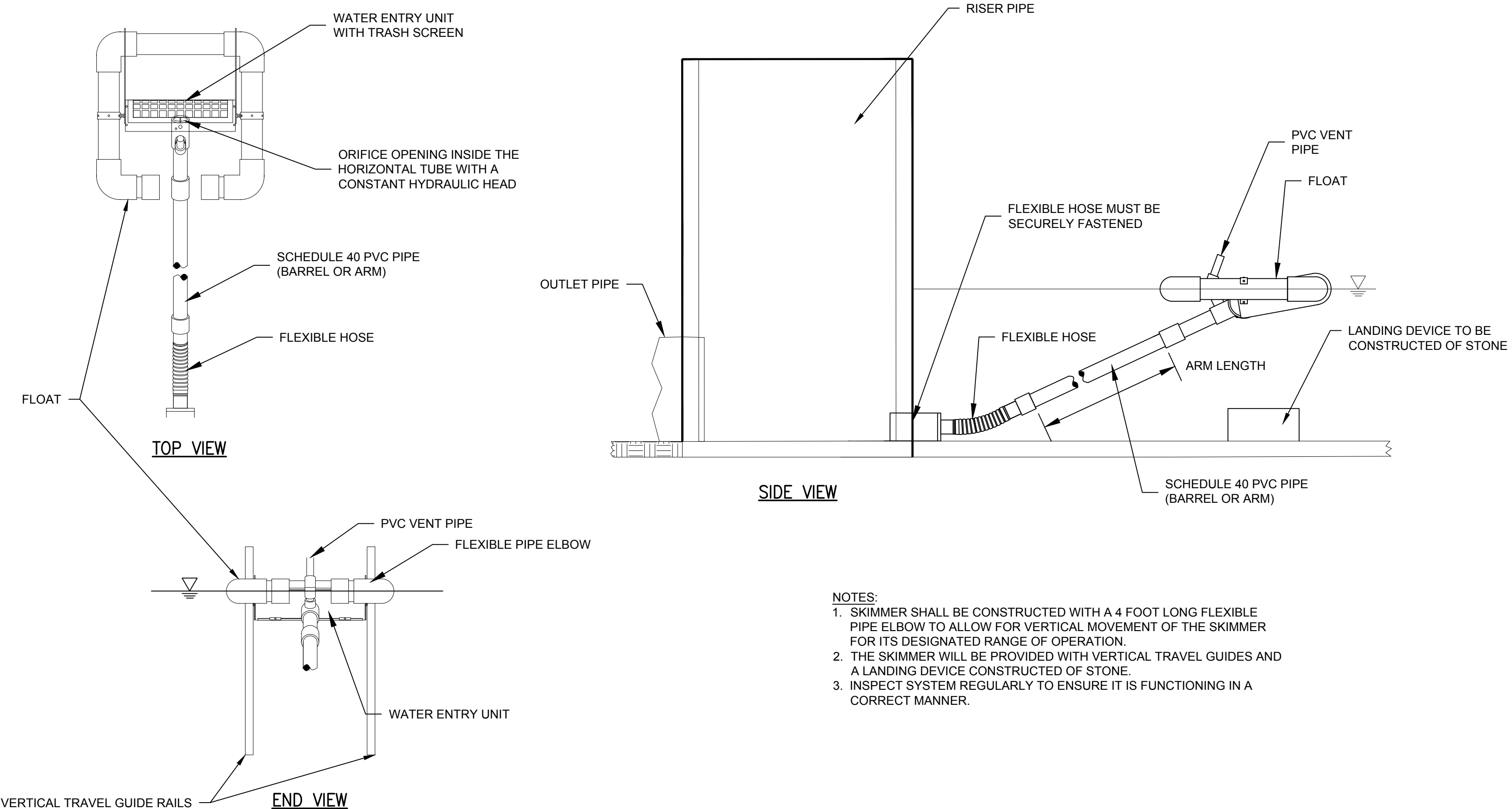


BASIN NUMBER	BOTTOM ELEV. (FT)	TOP OF DAM ELEV. (FT)	TOP OF RISER ELEV. (FT)	INV. OUT (FT)	SEDIMENT STORAGE ZONE VOLUME REQ'D (FT³)	SEDIMENT STORAGE ZONE VOLUME PROVIDED (FT³)	SEDIMENT STORAGE ZONE ELEV. (FT)	DEWATERING ZONE VOLUME REQ'D (FT³)	DEWATERING ZONE VOLUME PROVIDED (FT³)	DEWATERING ZONE ELEV. (FT)	CLEANOUT ELEVATION (FT.)
1	10	14	-	-	5300	5300	-	19080	19080	-	-
2	6	14	11	6.5	15200	16370	7.5	54720	55416	11	6.75
3	6	14	11	6.5	33000	36859	7.5	118800	119226	11	6.75

- NOTES:
- TEMPORARY SEDIMENT BASIN 1 CALCULATIONS HAVE BEEN SHOWN FOR CAPACITY VERIFICATION ONLY.
 - BASIN 1 WILL BE GRADED OUT PER WQV POND DETAIL ON SHEET GR-14. ALL OUTLET STRUCTURES ARE TO BE COVERED WITH FILTER FABRIC DURING CONSTRUCTION. EXCAVATION OF BASIN 1 TO FINAL GRADE ELEVATIONS SHALL OCCUR ONCE FINAL STABILIZATION HAS BEEN REACHED.
 - EMBANKMENT MUST BE COMPACTED TO DESIGN SPECIFICATIONS.
 - EROSION PROTECTION MUST BE INSTALLED ALONG THE EMBANKMENT AND AT THE DISCHARGE END OF THE PIPE.

TEMPORARY SEDIMENT BASIN

N.T.S.



- NOTES:
- SKIMMER SHALL BE CONSTRUCTED WITH A 4 FOOT LONG FLEXIBLE PIPE ELBOW TO ALLOW FOR VERTICAL MOVEMENT OF THE SKIMMER FOR ITS DESIGNATED RANGE OF OPERATION.
 - THE SKIMMER WILL BE PROVIDED WITH VERTICAL TRAVEL GUIDES AND A LANDING DEVICE CONSTRUCTED OF STONE.
 - INSPECT SYSTEM REGULARLY TO ENSURE IT IS FUNCTIONING IN A CORRECT MANNER.

BASIN NUMBER	WATER SURFACE ELEVATION (FT)	ARM LENGTH (FT)	ARM DIA. (in)	ORIFICE SIZE (in)	TOP OF LANDING DEVICE ELEVATION (FT)	FLEXIBLE HOSE LENGTH (in)	FLEXIBLE HOSE ATTACHMENT ELEVATION (FT)
2	11	16	5	5	7.5	12	6
3	11	16	7	7	7.5	12	6

SKIMMER DEWATERING DEVICE DETAILS

N.T.S.



McFarland Johnson
 60 RAILROAD PLACE
 SUITE 402
 SARATOGA SPRINGS, NEW YORK 12866
 P:518-580-9380 F:518-580-9383
 SaratogaROM@mjinc.com

PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS
2	06/06/22	TOWN COMMENTS

CLIENT:
ALBANY PORT DISTRICT COMMISSION
 ALBANY, NEW YORK

PROJECT:
NORMANSKILL ST. REHAB

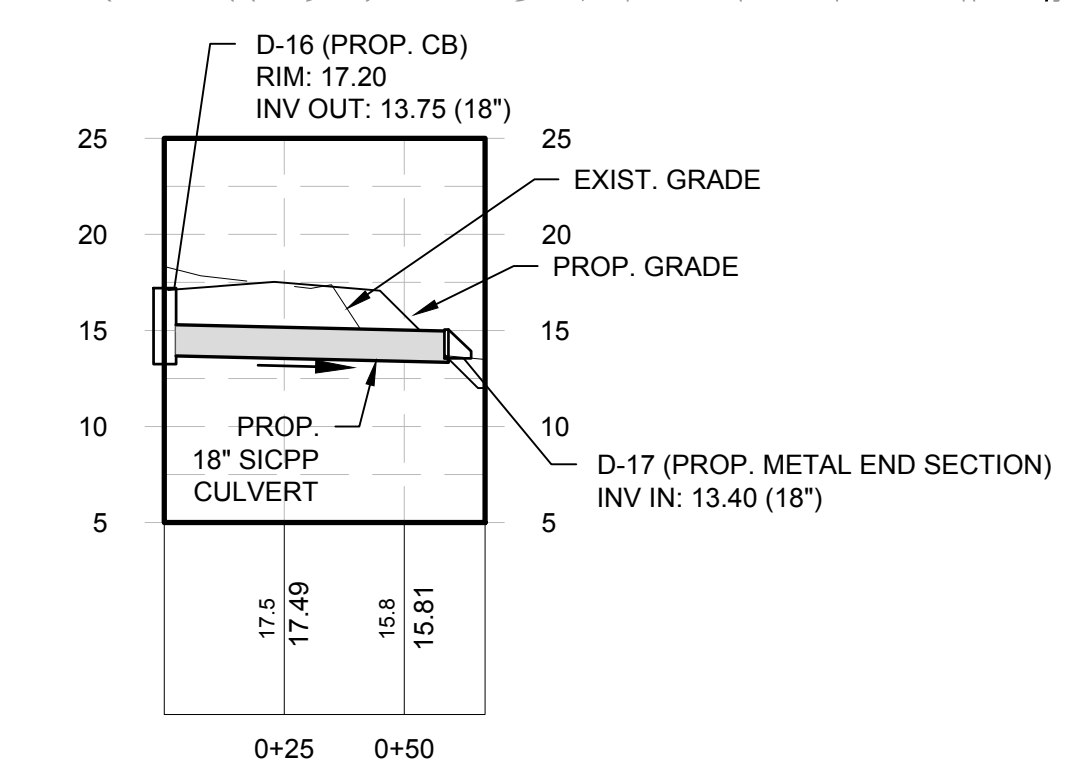
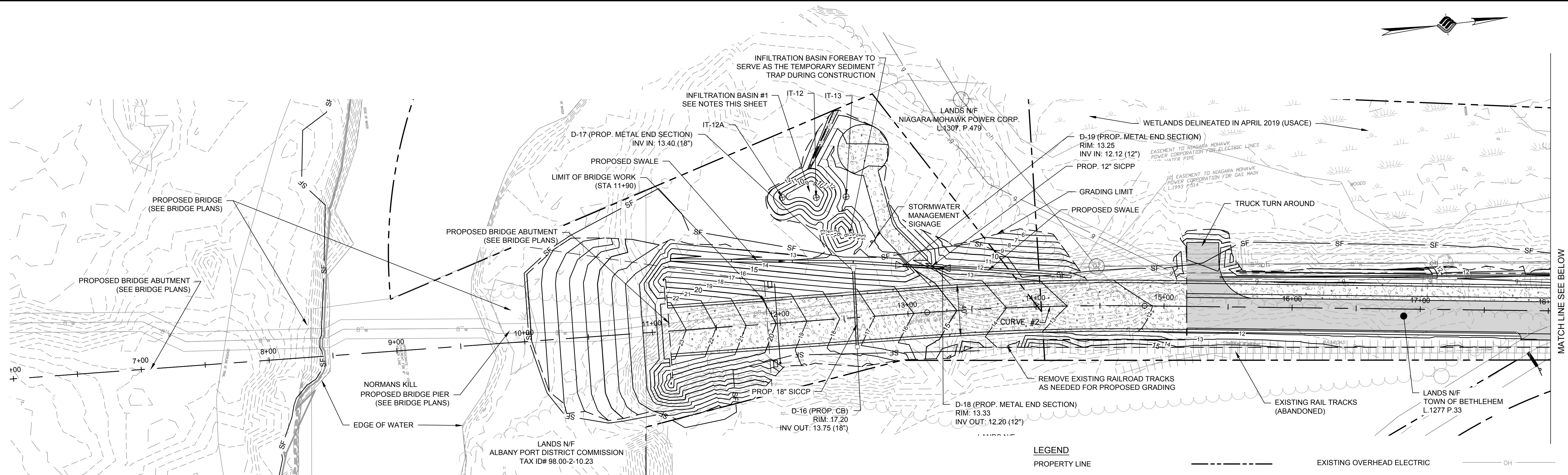
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DESIGNED	NSO
CHECKED	AJF
SCALE	1"=40'
DATE	05-10-2022
PROJECT	18641.00



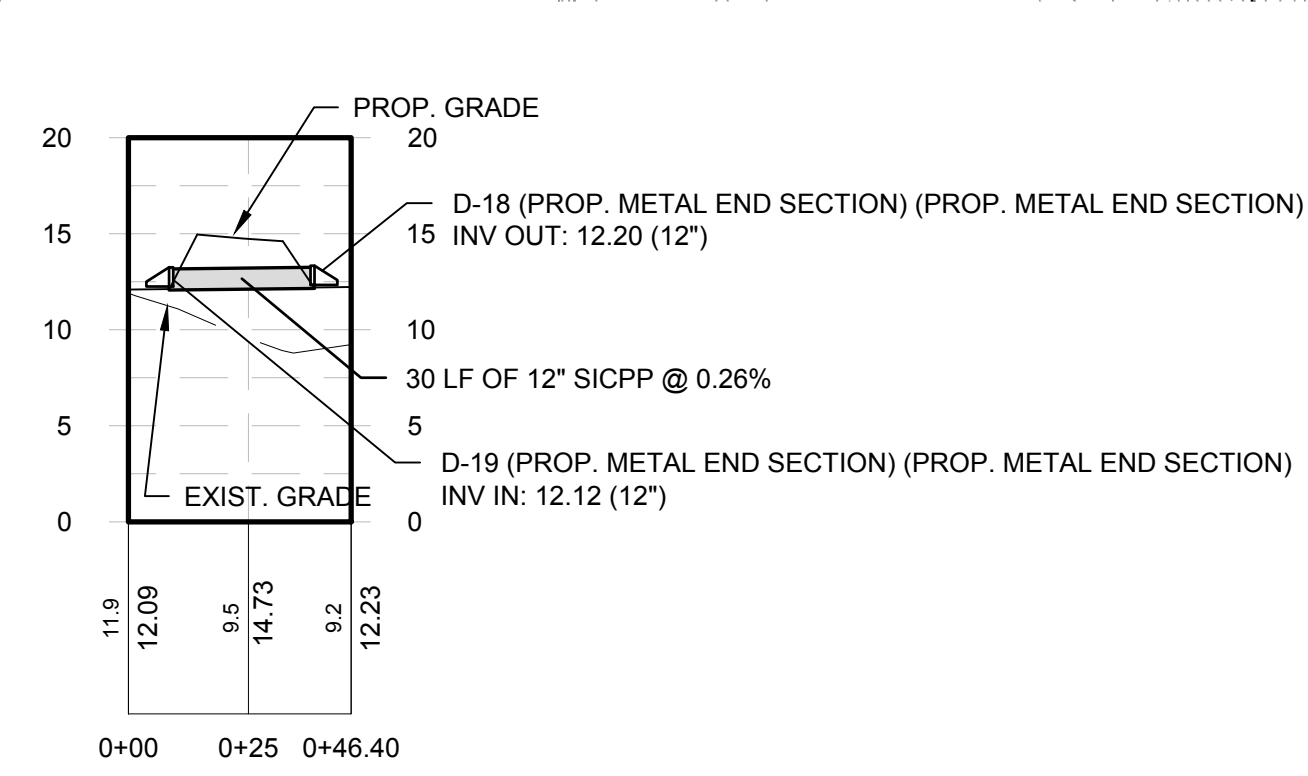
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DRAWING TITLE
GRADING, DRAINAGE, EROSION AND SEDIMENT CONTROL

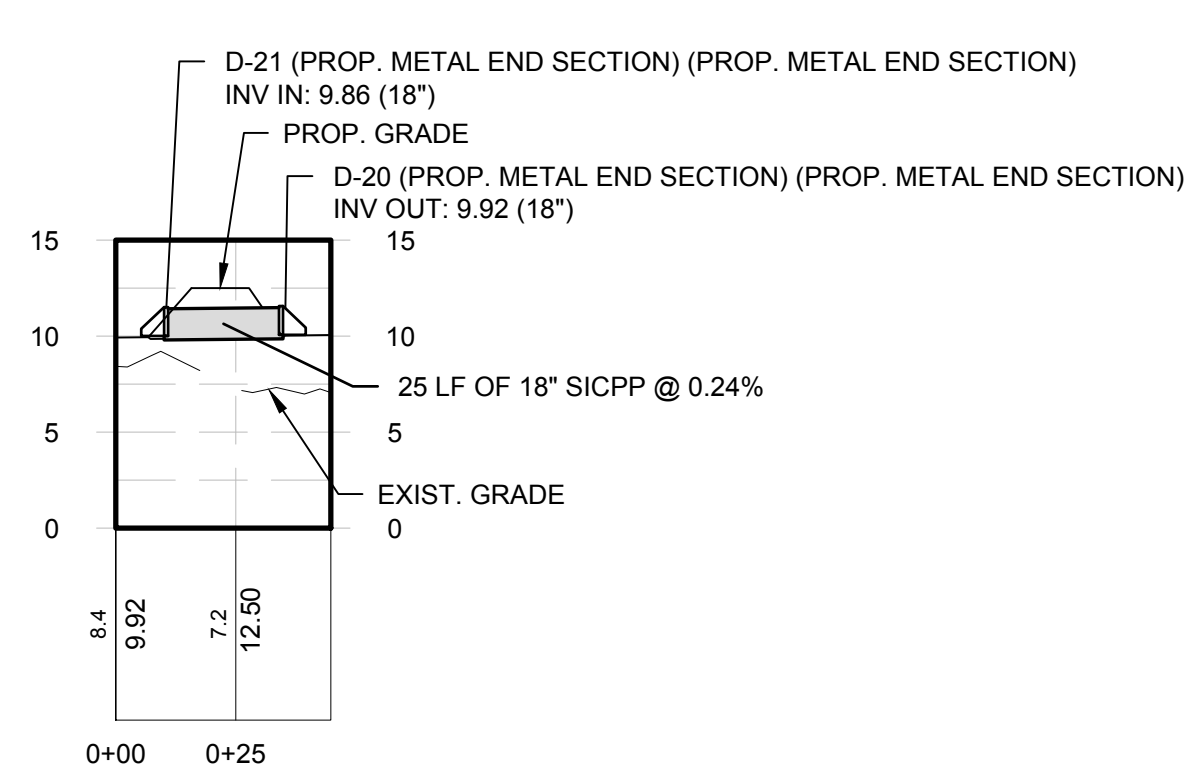
DRAWING NUMBER
GR-01



D-16 TO D-17
 Horizontal Scale: 1" = 40'
 Vertical Scale: 1" = 10'



D-18 TO D-20
 Horizontal Scale: 1" = 40'
 Vertical Scale: 1" = 10'



D-20 TO D-21
 Horizontal Scale: 1" = 40'
 Vertical Scale: 1" = 10'

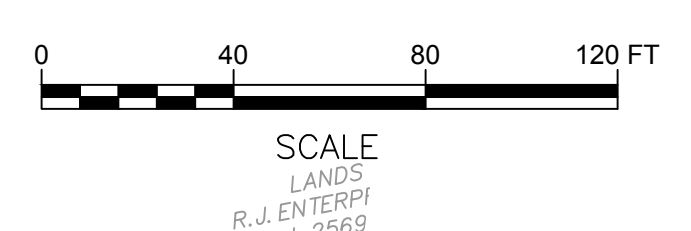
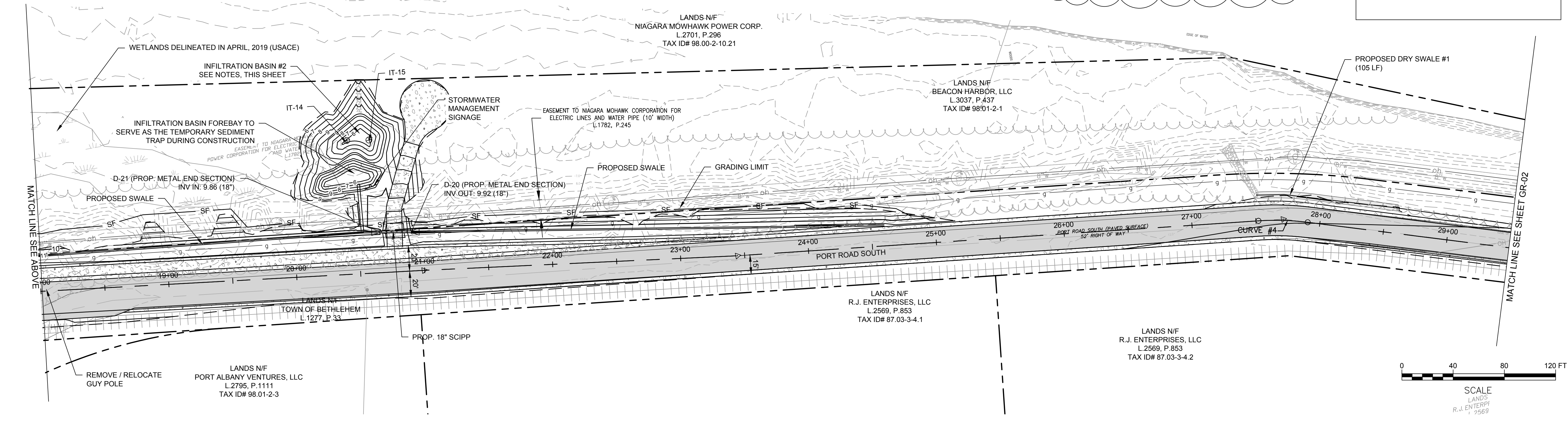
LEGEND

PROPERTY LINE	---	EXISTING OVERHEAD ELECTRIC	OH
PROPOSED BOX BEAM GUIDE RAIL	—●—	EXISTING GAS LINE	G
DITCH CENTERLINE	—+—	EXISTING WATERLINE	W
WETLAND AREA	(Hatched)	PROPOSED PAVEMENT	(Solid Grey)
SECURITY FENCE	—X—	PROPOSED CONCRETE	(Dotted)
SILT FENCE	—SF—	RIP-RAP WATER EMBANKMENT STABILIZATION	(Stippled)
CATCH BASIN	□		

NOTES:

- UPSTREAM CONSTRUCTION SHALL BE COMPLETED AND STABILIZED BEFORE CONNECTION TO A DOWNSTREAM INFILTRATION FACILITY. A DENSE AND VIGOROUS VEGETATIVE COVER SHALL BE ESTABLISHED OVER THE CONTRIBUTING PERVIOUS DRAINAGE AREAS BEFORE RUNOFF CAN BE ACCEPTED INTO THE FACILITY.
- PROPOSED INFILTRATION BASINS SHALL BE OWNED, OPERATED AND MAINTAINED BY THE PORT OF ALBANY AND BE ACCESSIBLE BY THE TOWN FOR INSPECTION.
- SEE TABLE ON SHEET GR-04 FOR INFILTRATION TEST INFORMATION.

PLANNING BOARD HTE# 21-00100006





McFarland Johnson
 60 RAILROAD PLACE
 SUITE 402
 SARATOGA SPRINGS, NEW YORK 12866
 P:518-580-9380 F:518-580-9383
 SaratogaROM@mjinc.com

**PROJECT MILESTONE
 FINAL DESIGN PLANS**

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

CLIENT:
 ALBANY PORT DISTRICT COMMISSION
 ALBANY, NEW YORK

PROJECT:
 NORMANSKILL ST. REHAB

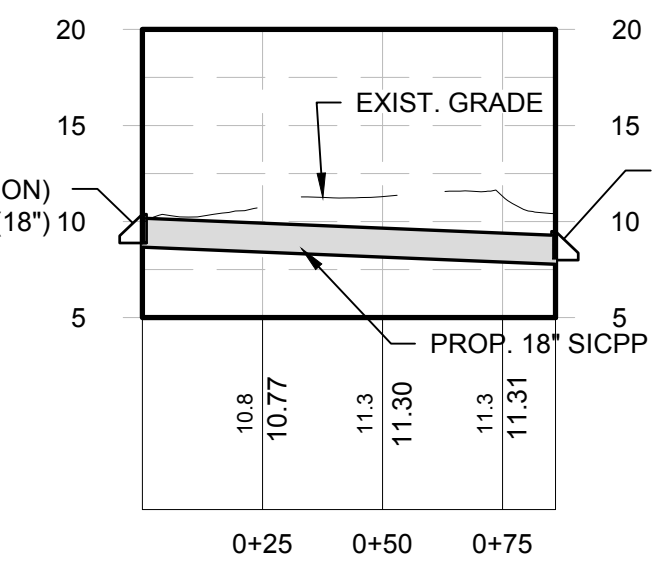
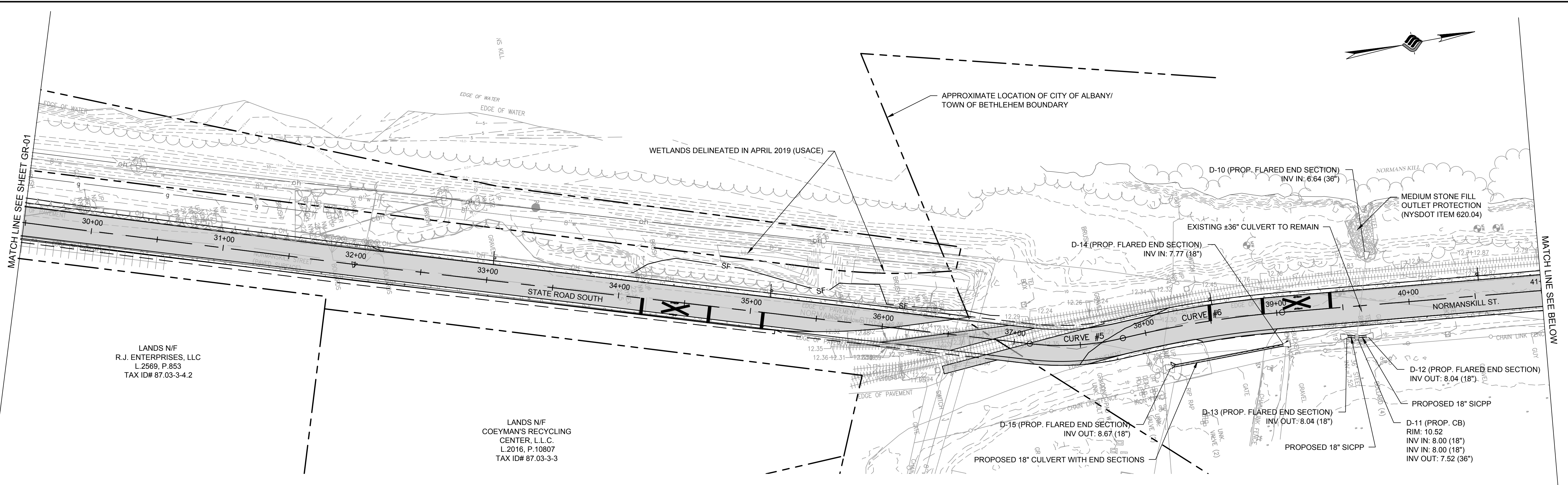
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DESIGNED	NSO
CHECKED	AJF
SCALE	1"=40'
DATE	05-10-2022
PROJECT	18641.00



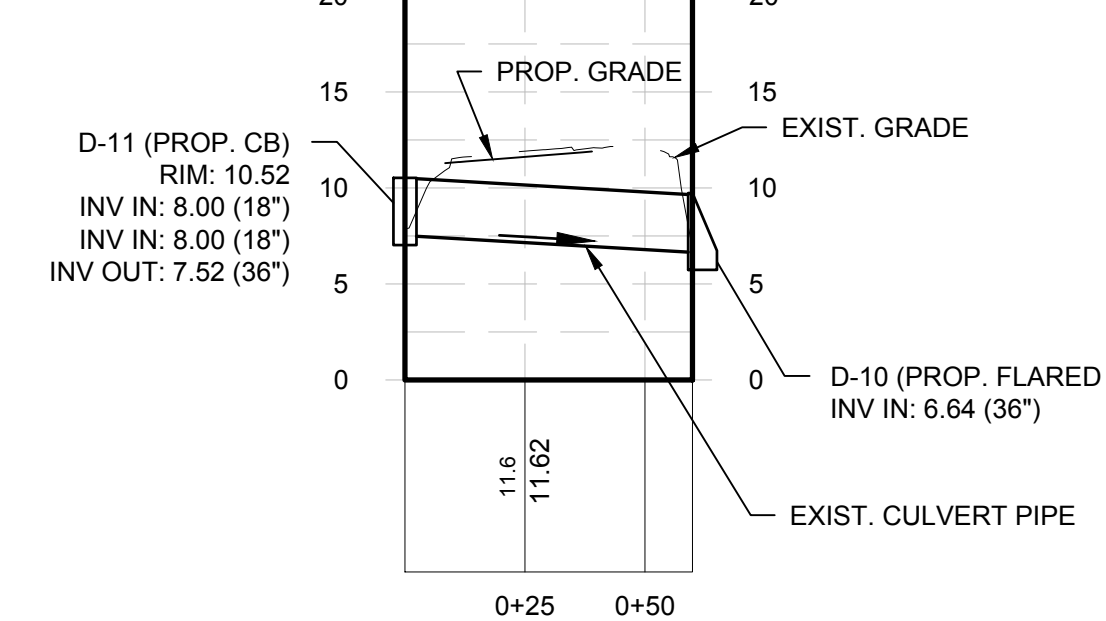
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 GRADING, DRAINAGE,
 EROSION AND
 SEDIMENT CONTROL

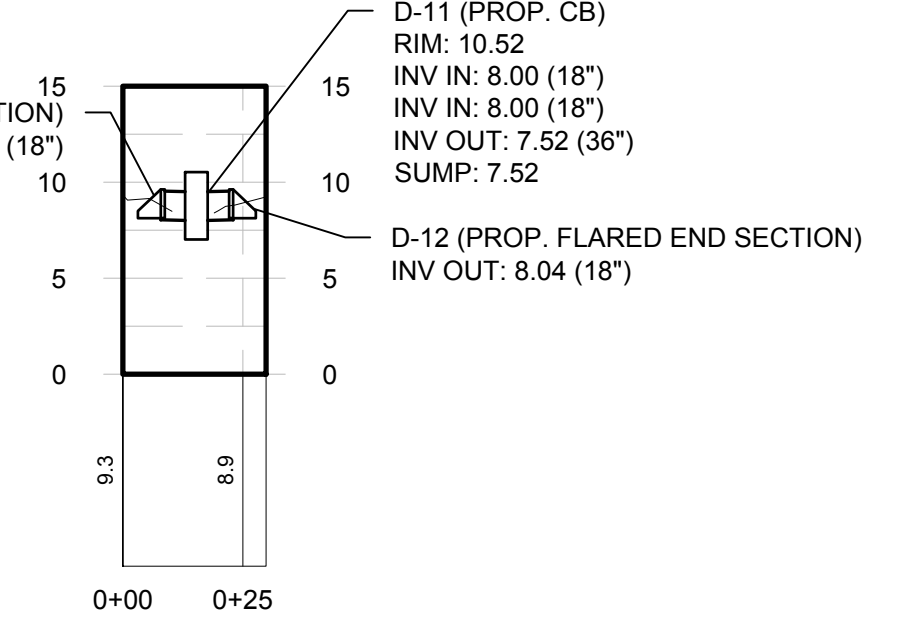
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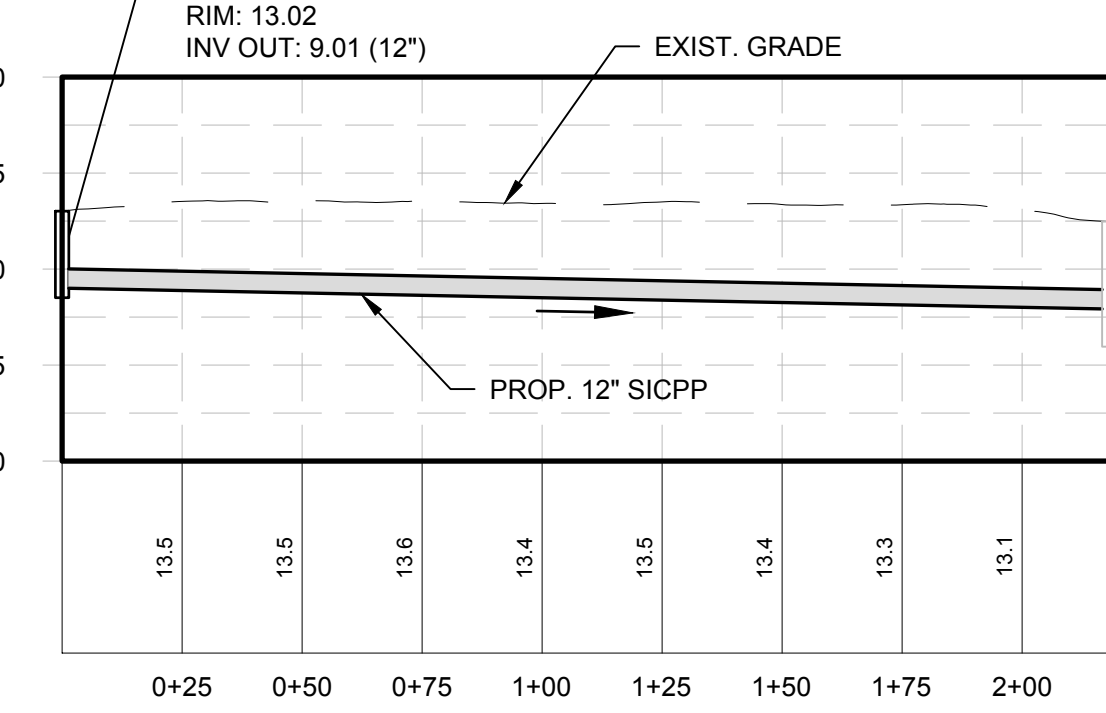
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 Vertical Scale: 1" = 10'



D-11 TO D-10
 Horizontal Scale: 1" = 40'
 Vertical Scale: 1" = 10'



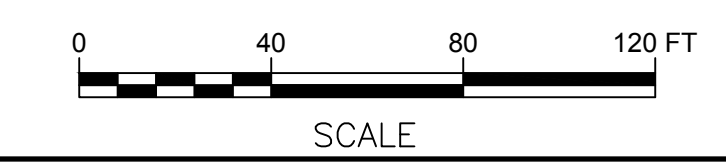
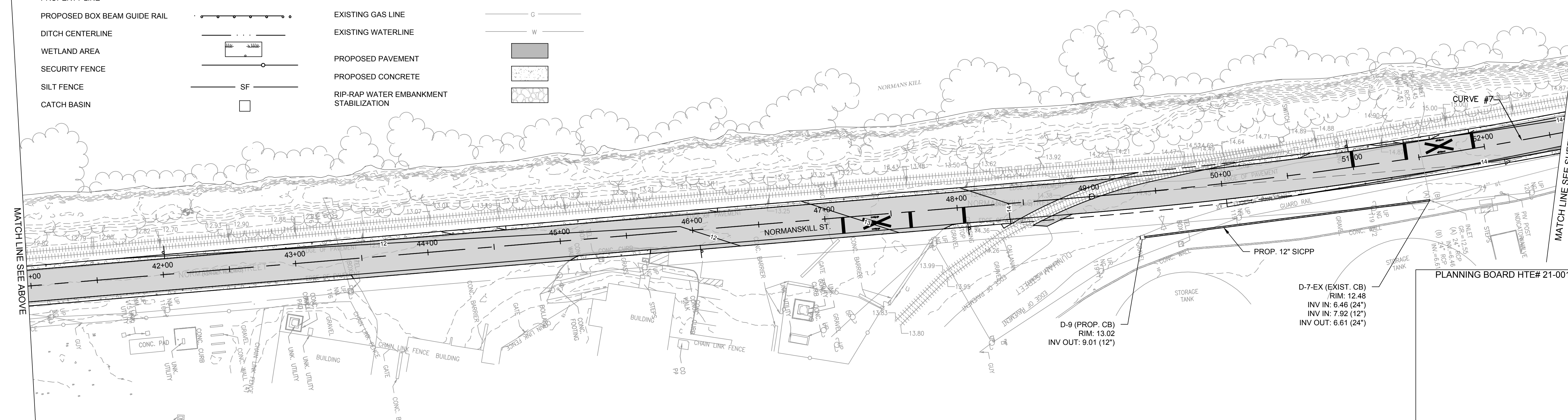
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 Horizontal Scale: 1" = 40'
 Vertical Scale: 1" = 10'



D-9 TO D-7-EX
 Horizontal Scale: 1" = 40'
 Vertical Scale: 1" = 10'

LEGEND

PROPERTY LINE	---	EXISTING OVERHEAD ELECTRIC	OH
PROPOSED BOX BEAM GUIDE RAIL	---	EXISTING GAS LINE	G
DITCH CENTERLINE	---	EXISTING WATERLINE	W
WETLAND AREA	---	PROPOSED PAVEMENT	---
SECURITY FENCE	SF	PROPOSED CONCRETE	---
SILT FENCE	SF	RIP-RAP WATER EMBANKMENT STABILIZATION	---
CATCH BASIN	□		





McFarland Johnson
 60 RAILROAD PLACE
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 SARATOGA SPRINGS, NEW YORK 12866
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PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

CLIENT:
ALBANY PORT DISTRICT COMMISSION
 ALBANY, NEW YORK

PROJECT:
NORMANSKILL ST. REHAB

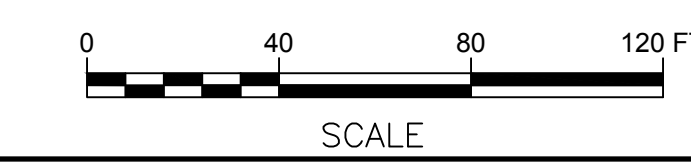
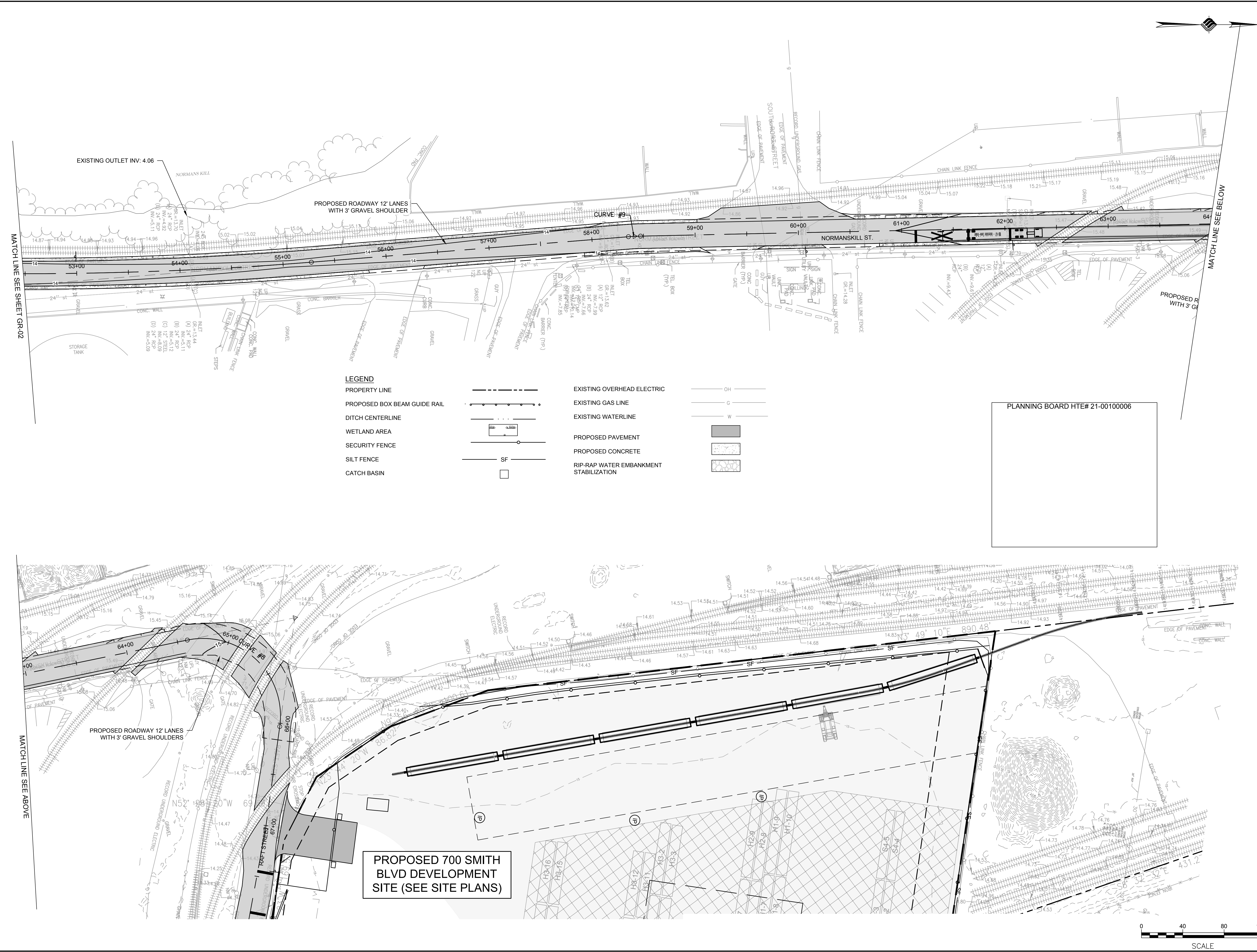
DRAWN	JES
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DRAWING TITLE
GRADING, DRAINAGE, EROSION AND SEDIMENT CONTROL

DRAWING NUMBER
GR-03



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APPENDIX C

DRAINAGE DESIGN REPORT

DRAINAGE DESIGN REPORT

FOR

MARMEN-WELCON TOWER MANUFACTURING PLANT

**TOWN OF BETHLEHEM
ALBANY COUNTY
NEW YORK**

**FINAL SUBMISSION
JUNE 20, 2022**

CREATED FOR:



**ALBANY PORT DISTRICT COMMISSION
106 Smith Boulevard
Albany, NY 12202
518-463-8763
www.portofalbany.us**

CREATED BY:



McFarland Johnson

**60 Railroad Place, Suite 402
Saratoga Springs, NY 12866
518-580-9380
www.mjinc.com**

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 - B. Water Quality Volume (WQv) / Runoff Reduction Volume (RRv)*
 - C. Channel Protection Volume (CPv)*
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- IV. Summary of Findings**
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I. General Information

A. Project Description

This Stormwater Management Report has been developed for a Supplemental Environmental Impact Statement (SEIS) regarding a proposed development at the Port of Albany. The proposed development is an offshore wind (OSW) manufacturing facility that will produce wind turbine tower components. The Project is situated on 81.62 acres of land at the Beacon Island site, located at the confluence of the Normans Kill and Hudson River. The project also includes development within 4.4 acres of the adjoining parcel owned by National Grid, the extension and improvement of Normanskill Street, and widening of Rt. 144. The project owner, Albany Port District Commission (APDC), is proposing to develop the vacant parcels of land (tax parcels 98.00-2-10.23 and 98.01-2-1.0) to expand the existing Port of Albany in the Town of Bethlehem, Albany County, New York.

The proposed project will include development of an OSW tower manufacturing (Marmen-Welcon) facility consisting of five (5) separate buildings totaling up to 625,539+/- square feet of floor space. The following is a breakdown of the function and size of each building:

- Building A Plate Preparation & Welding (299,250 SF)
- Building B Welding Finishing (111,023 SF)
- Building C Blast Metallization Plant (131,968 SF)
- Building D Internal Assembly Finishing (61,550 SF)
- Building E Material Receiving (21,748 SF)

Tower production will occur within four (4) buildings (Buildings A-D) at the main facility on the Port Expansion property located in the Town of Bethlehem. The 5th building (Building E) will be located at 700 Smith Boulevard within the existing Port District in the City of Albany. A proposed gated bridge over the Normans Kill will provide a truck transportation route in and out of the main facility, by connecting Beacon Island and the 14.7-acre offsite parcel at 700 Smith Boulevard. In conjunction with the proposed bridge, Normanskill Street is to be extended from its existing end point to the bridge. The existing pavement will be improved to accommodate the proposed trucking route. River Road (Rt. 144) will be widened to accommodate the employee entrance. Employee parking will be situated on the adjoining land owned by National Grid with access from River Road. A proposed 500 LF wharf and associated dredging along the Hudson River will be used to load and ship completed tower sections. A separate stormwater analysis and SWPPP has been prepared for the 14.7-acre Building E site at 700 Smith Boulevard and the portion of Normanskill Street located in the City of Albany, as the sites are separated by approximately 1-mile and are under separate MS4 jurisdictions.

Historically, the Port Expansion site was composed of small islands and river channels subject to natural shifts due to flows associated with the Hudson River and the former Island Creek, a side channel of the Hudson River. Island Creek historically flowed along the western side of the site

through the current power line corridor and discharged to the Hudson River at the southern end of the site. Based on available mapping, sometime between 1936 and 1961, Island Creek channel was diverted at the north end of the site directly to the Hudson River, whereupon it was referred to solely as Normans Kill, the main tributary to this former channel. The site was subject to historic filling operations to create usable lands and a portion of the site was operated as a coal ash (fly ash) disposal site by Niagara Mohawk from approximately 1952 to 1970. As such, there are large areas of fly ash deposits on the site that must be considered during the design and construction of the site infrastructure and stormwater management facilities. Excavated fly ash material will need to be appropriately handled and properly disposed of as discussed in Section B below. A soil management plan has been developed and will require a cap over the site.

The purpose of this report is to assess the stormwater quality, quantity, and erosion and sediment control for the development of the site. This report has been developed in accordance with the New York State Department of Environmental Conservation (NYSDEC) State Pollution Discharge Elimination System (SPDES) General Permit for Stormwater Discharges from Construction Activity, GP-0-20-001 (Permit) and the NYSDEC Stormwater Management Design Manual (The Manual). The project site is located within the Town of Bethlehem, Albany County, New York, which is an MS4 community, requiring this report and project to receive approval from the Town. A separate stormwater analysis and SWPPP has been prepared for the 14.7-acre Building E site at 700 Smith Boulevard and the portion of Normanskill Street located in the City of Albany, as the sites are separated by approximately 1-mile and are under separate MS4 jurisdictions.

The overall project limits analyzed in this Drainage Report are broken up into three (3) areas, hereafter referred to as (1) "Expansion Site", (2) "Normanskill Street Improvements", (3) "Offsite Improvements". See Existing Conditions Map (Appendix A) for the location of each of these areas. The Expansion Site is the portion of the project area that is located on Beacon Island. The Normanskill Street Improvement portion begins on the north end of the proposed bridge over the Normans Kill and extends north to the border of the Town of Bethlehem and City of Albany. The Offsite Improvements portion refers to the widening of Rt. 144 adjacent to the employee entrance.

B. Soil Classification

According to the Natural Resources Conservation Service (NRCS) web soil survey, there are five (5) mapped soil units identified within the project boundary (see Appendix E). The majority of the soil at the expansion site falls within the hydrologic soil group B/D. The first letter corresponds to drained soil's properties under drained conditions and the second to saturated conditions. Group B soils have moderate infiltration and runoff rates while group D have a low infiltration rate and a high runoff rate. The soils with dual group identifiers have been modeled with the more conservative of the two, in this case a D soils group. Most of the soil adjacent to Normanskill Street Improvements is within soil group A. Group A soils have a high infiltration rate.

The complete list of soils found on the project site is identified in the table below (see Appendix E for NRCS Soils Report).

Table I – Soils Summary

Symbol	Soil Name	Hydrologic Soil Group
HuE	Hudson silt loam, 25 to 45 Percent slopes	C/D
NrD	Nassau very channery silt loam, hilly, very rocky	D
Ug	Udorthents, loamy	A
Ur	Urban land	-
Wo	Wayland soils complex, non-calcareous substratum, 0 to 3 percent slopes, frequently flooded	B/D

Geotechnical studies have been undertaken to evaluate the subsurface conditions of the site. These investigations have been summarized in the following reports:

- *Preliminary Geotechnical Evaluation and Interpretive Report*, CME Associates, Inc., April 5, 2017
- *Supplemental Geotechnical Report*, Dente Group, July 20, 2017

Copies of these reports were included in the TOWN OF BETHLEHEM PLANNING BOARD, DRAFT GENERIC ENVIRONMENTAL IMPACT STATEMENT For ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY EXPANSION PROJECT, Appendix E.

- *Draft Geotechnical Engineering Report*, Terracon, October 15, 2021

A copy of this reports is included in the TOWN OF BETHLEHEM PLANNING BOARD, SUPPLEMENTAL ENVIRONMENTAL IMPACT STATEMENT For ALBANY PORT DISTRICT COMMISSION PORT OF ALBANY EXPANSION PROJECT.

Based on these previous investigations, the subsurface conditions of the Expansion Site portion of the project site are generally characterized by historic fills of various depths overlying, in sequence with depth; river sediments, alluvial sands, glaciolacustrine silt/ clay, glacial till, and shale bedrock. The fill was noted at specific boring locations ranging from 6 to 23 feet below existing grade. The fill material is characterized as a random landfill deposit containing natural and solid waste deposits such as, but not limited to, foundry sand waste, sand, silt, coal ash, gravel, and organic matter. A predominant component of the fill was reported as coal ash.

Shale bedrock was found beneath the glacial till soils at select boring locations. The depth to rock ranged from approximately 61 feet below grade near the northwest portion of the site, to greater than 148 feet at the southeast portion of the site. The rock depths appear shallowest on the north and west sides of the site and increase to the east towards the Hudson River and in a south

direction across the site. Based on the New York State Museum and Science Service's Geologic Map of New York: State Hudson-Mohawk Sheet, and the geotechnical rock core samples, the bedrock appears to be consistent with the Normans kill Shale Formation.

According to the geotechnical reports, shallow groundwater was observed at depths ranging from approximately 1.5 to 13.7 feet below existing grade. However, due to the subsurface conditions, the shallower observations could be representative of perched groundwater zones due to discontinuous impermeable layers. Shallow groundwater fluctuations should be expected to occur at this site depending on several factors such as rainfall, seasonal changes, prevailing climate, ambient weather conditions, and the tidal influences of the Hudson River.

A soil management plan (SMP) has been prepared in accordance with the NYSDEC regulations. The SMP is included in SWPPP. The SMP pertains only to the Expansion Site portion of the project.

II. Hydrology

A. Existing Conditions

The existing drainage area totals 108.4 +/- acres, separated by the Normans Kill. The drainage area is bordered by the Hudson River to the east. At the south boundary there is a Public Service Energy Group (PSEG) power plant, and to the west a parcel owned by National Grid that conveys overhead electric transmission lines as well as an underground gas main. The Port Expansion site consists primarily of brush and trees with a small gravel area as well as abandoned railroad tracks. The Normanskill Street Improvement site consists of an existing road as well as brush and trees to the west. The Offsite Improvements consist of the existing roadway as well as brush and trees to the east and west.

The existing drainage condition is split up into seven (7) drainage areas. Drainage area DR-A drains to analysis point #1A, drainage areas DR-B and DR-F drain to analysis point #1, drainage areas DR-D and DR-E drain to analysis point #2. Drainage area DR-G drains to analysis point #3. Drainage area DR-C drains to a self-contained depression for storage. See Appendix A for the Existing Conditions Drainage Map.

Runoff from DR-A travels via sheet and shallow concentrated flow directly to a wetland located in the northwest corner of the site (Wetland 1). During large storm events the wetland overflows into an existing 40" pipe with direct outlet to the Normans Kill. Analysis of the existing capacity of the outlet pipe is provided in section IV below. Runoff from areas DR-B, DR-D, DR-E, and DR-F travel via sheet and concentrated flow to low areas with eventual outfall directly to the Normans Kill and Hudson River. An approximately 30-acre internal portion of the site (DR-C) was determined to be self-contained within the site capable of storing and infiltrating the 100-year storm event. Runoff from area DR-G sheet flows to the west side of River Road and travels to a low spot adjacent to the roadway where it is stored and eventually infiltrated.

A wetland delineation was conducted in April 2019 by McFarland Johnson for the FGEIS. The results of the delineation indicated that there are 8 freshwater wetlands located within the project limits. These wetlands are hereafter referred to as Wetlands 1, 3, 4, 5, 6, 7, 8, and 9. Wetlands within the original study area totaled approximately 2.33 acres.

A Supplemental Wetland Delineation was performed by MJ in April 2021 of the 18.22 acres on the National Grid Parcel. One contiguous wetland, comprising of approximately 7.13 acres, was delineated within the 18.22-acre area. The delineated wetland represents an extension of the 2019 wetland delineation and previously identified as Wetland 1. Wetland 1 drains in a northerly direction into a 40-inch corrugated metal pipe (CMP) which discharges directly to the Normans Kill.

The existing site falls within the Normans Kill watershed of the Middle Hudson Sub-Basin for the Lower Hudson River Basin (HUC10: 0202000602, Water Index No H-221-4) which is listed as a Class C water. Neither the Normans Kill nor the Hudson River are listed in the Manual's Appendix C as a watershed where enhanced phosphorus removal standards are required. Additionally, neither are listed in the Manual's Appendix E as a watershed impaired by pollutants related to construction activity.

B. Proposed Conditions

The proposed Port Expansion Site development includes 603,791 +/- square feet of OSW manufacturing facility space spread out over four (4) separate buildings. Ancillary impervious areas include parking for automobiles and trucks, a roadway, bridge, and a maritime wharf. The remainder of the site will be used for tower storage and be made up of dense graded aggregate. There will also be small pervious areas of grass and unaltered brush and trees.

The Normanskill Street Improvements are along a 0.52 mile stretch of roadway within the Town of Bethlehem. A new portion of Normanskill Street is to be constructed from the proposed vehicle bridge north to the existing roadway. This extension is approximately 925 feet long and will be dense graded aggregate. The existing portion of Normanskill Street will be widened on the west side of the roadway. The remaining portion of the existing roadway will be re-paved and not disturbed, as subbase will remain. A top course mill and fill of 1.11 acres is proposed. The improvements also include the required corresponding stormwater conveyance and treatment.

The Offsite Improvements consist of widening an approximately 600 LF stretch of Rt. 144 adjacent to the expansion site employee entrance. The roadway is to be widened by 7 +/- ft on the east side. The new impervious area is 0.14 acres. Corresponding grading is also part of the offsite improvements.

The total post-development drainage area will be 108.6 acres. The post-development drainage area is larger than the pre-development area by 0.2 acres due to the proposed bridge over the Normans Kill. The total disturbance for construction of the site will be approximately 72.7 +/-

acres.

The proposed drainage condition is split up into seventeen (17) drainage areas. Drainage Areas DR-8, DR-9, and DR-10 drain to analysis point #1A. Drainage Areas DR-5, DR-6, DR-7, DR-12, DR-13, DR-14, DR-15, and DR-16 drain directly to analysis point #1. Drainage areas DR-1, DR-2, DR-3, DR-4, and DR-11 drain to analysis point #2. Drainage area DR-17 drains to analysis point #3. Each analysis point remains the same in the pre- and post-development condition for comparison. See Appendix B for the Proposed Conditions Drainage Map.

On the Expansion Site, runoff from the proposed impervious areas will travel via sheet and shallow concentrated flow to one of seven (7) closed drainage networks. Drainage networks 1-7 will be conveyed through a NYSDEC approved stormwater filtering system and/or an off-line infiltration chamber system which will provide water quality volume treatment and runoff reduction prior to being discharged into the Normans Kill or Hudson River.

Runoff from DR-8 and DR-9 will be conveyed via vegetated swales to Micropool Extended Detention Ponds (Type P-1 per the Manual). The ponds will provide water quality volume treatment. The portion of the water held above the wet pool will be slowly discharged to the surrounding area over a 24-hour period. The ponds will also hold larger storm events up to the 10-year storm. During the 10-year storm and larger, emergency spillways outlet to the surrounding vegetated area, eventually flowing to Wetland #1.

Drainage Areas DR-10, DR-11, and DR-12 maintain their existing drainage patterns.

Drainage areas DR-13 and DR-14 correspond to sections of new Normanskill Street roadway. In each area, stormwater is collected via roadside swales and directed into a sedimentation basin which overflows into Infiltration Basin #1. The basins are designed to infiltrate the WQv as well as smaller storm events. During large storm events water will overflow to the Normans Kill.

Drainage area DR-15 corresponds to a section of Normanskill Street that is being expanded to the west. Stormwater is collected via a roadside swale with a dry swale at the end. In large storm events, water will flow through the dry swale to an overflow trench to be discharged to the surrounding vegetated area, eventually flowing into the Normans Kill. Drainage Area DR-16 will not be disturbed in the development of this project and will continue to drain into the Normans Kill.

Drainage area DR-17 will collect runoff on Rt. 144 via a roadside swale with a dry swale at the end. In large storm events, water will flow through the dry swale to an overflow trench to be discharged to the surrounding area. The surround area is self-contained and eventually infiltrates stormwater runoff.

The overall drainage plan incorporates multiple separate systems with outlets to the Normans Kill and/or Hudson River to avoid a more concentrated larger outlet for the site. See Appendix B

for proposed conditions plans and watershed mapping.

III. Stormwater Management & SPDES Requirements

The Proposed Development Project will have land disturbance of more than 1-acre, a full SPDES permit will be required, and a Stormwater Pollution Prevention Plan (SWPPP) will be developed in accordance with the Permit regulations and MS4 requirements as part of the Town of Bethlehem site plan approval process. A 5-acre waiver will also be requested in order to disturb more than 5 acres at one time.

Due to the presence of fly ash on the Expansion Site, in addition to a NYSDEC SPDES, a Site Management Plan (SMP) has been prepared in accordance with 6 NYCRR Part 375 and DER Technical Guidance for Site Investigation and Remediation and submitted to the NYSDEC, Division of Environmental Remediation and the NYSDOH. The SMP includes: a Health and Safety Plan (HASP), to inform and protect the contractor and their work force; a Community Air Monitoring Plan (CAMP), to monitor and protect the surrounding communities; and an Excavation Work Plan (EWP), to direct the activities of the contractor during construction. The EWP includes a detailed description of the work to be performed, the anticipated environmental conditions, and engineering controls to mitigate the movement of fly ash. The SMP has been included in the SEIS and SWPPP.

The SWPPP will be prepared in coordination with the Manual and meet the following criteria as the principal objectives contained in an approved SWPPP:

- Reduction or elimination of erosion and sediment loading to waterbodies during construction activities. Controls will be designed in accordance with the NYSDEC's New York State Standards and Specifications for Erosion and Sediment Control.
- Mitigate the impact of stormwater runoff on the water quality of the receiving waters.
- Maintenance of stormwater controls during and after completion of construction.

These objectives will be accomplished by incorporating design criteria outlined within the Technical Guidelines provided by The Manual and summarized below.

A. Methodology

To analyze the hydrologic impacts of the proposed development, a storm water management model was developed in accordance with the Manual. HydroCAD™, by HydroCAD Software Solutions LLC was used to model both the existing and proposed conditions: soil data from the NRCS Web Soil Survey was entered into the software; land coverage areas were estimated using aerial photography and site visits; watershed areas were developed using the surveyed topography; time of concentrations were estimated using USDA, Urban Hydrology for Small Watersheds, TR-55 (TR-55) methodology; and finally runoff and routing calculations were performed using the SCS Unit Hydrograph method.

The following rainfall depths were utilized in the analysis of the 1, 10, and 100-year storm events:

Table II – Hydrologic Analysis Data

Storm Event	Rainfall Depth (in.)
1-year	2.20
10-year	3.63
100-year	6.11

Rainfall depths were determined using the Northeast Regional Climate Center (NRCC) data for Albany County. The rainfall intensity utilized is the Type II-24 hour storm. This data is pre-programmed in the HydroCAD software.

Green Infrastructure practices were designed in accordance with the Manual using the NYSDEC Runoff Reduction Worksheets available through the NYSDEC’s Construction Stormwater Toolbox, available on their website.

The following general steps are followed when conducting a stormwater design:

1. **Site Planning:** The existing natural resource areas and drainage patterns including wetlands, waterways, floodplains, and soils are identified. Conservation of natural resources are maximized given the proposed site.
2. **Pre and Post-Development Conditions Analysis:** The pre and post-development stormwater runoff conditions for the 1, 10, and 100-year storm events are determined using HydroCAD (detailed HydroCAD reports for this project can be found in Appendices A and B).
3. **Water Quality:** The Water Quality Volume and Runoff Reduction Volume are calculated using Chapter 4 of the Manual and Green Infrastructure Worksheets (provided in Appendix C).
4. **Water Quantity:** Peak runoff and stormwater retention/detention are evaluated using the Manual.

B. Water Quality Volume (WQv) / Runoff Reduction Volume (RRv)

Section 4.2 of the Manual states that Water Quality Volume (WQv) is intended to improve the water quality by capturing and treating runoff from small, frequent storm events that contain higher pollutant levels created through the increase of impervious surfaces. Impervious surfaces accumulate pollutants that quickly wash off and rapidly enter downstream waters as well as prevent natural groundwater recharge.

The WQv required for the proposed site is based upon the 90% rainfall event number, percent of impervious cover, and the total site area. Calculations were done using the Green Infrastructure worksheets and can be found in Appendix C. The total WQv required is 273,874 cubic feet.

Runoff Reduction Volume (RRv) is the reduction of the total WQv by application of green infrastructure techniques and stormwater management practices to replicate pre-development

hydrology more closely. The intent of RRV is to recognize the water quality benefits of certain site design practices to address flow as a pollutant of concern.

According to Section 4.3 of the Manual, RRV may be calculated based on three methods:

1. Reduction of the practice contributing area in WQv
2. Reduction of runoff volume by storage capacity of the practice
3. Reduction using standard SMPs with runoff reduction capacity

The minimum RRV required by the proposed site is based on the total area of new impervious cover and the Hydrologic Soil Group (HSG) Specific Reduction Factor (S). The specific reduction factor is based on the HSGs present at the existing site. Calculations were done using the NYSDEC Green Infrastructure worksheets and can be found in Appendix C. The minimum RRV was determined to be 57,313 cubic feet.

Due to the level of contamination present in the existing soils across the Expansion Site, stormwater infiltration practices were located only in areas along the Hudson River and Normans Kill where contamination is not expected to be present. However, the Normanskill Street extension project area does not contain contaminated soils, so all treatment practices selected utilize infiltration and therefore include RRV. Infiltration testing has been performed at all proposed infiltration practices. Test results are included as Appendix F.

The following stormwater treatment practices were designed to meet the WQv and RRV requirements of the Manual:

Stormwater Ponds

Two stormwater quality ponds (Pond #1 and Pond #2) have been designed as Micropool Extended Detention Ponds (P-1) in accordance with the Manual. Ponds #1 and #2 treat stormwater runoff from drainage areas DR-8 and DR-9 respectively. Runoff from these areas sheet flow to a vegetated swale and outlet into the forebay of the pond. As required by the manual, the permanent pool volume is a minimum 20% of the WQv. Any stormwater held above the permanent pool elevation will be slowly discharged from the pond over a period of 24 hours. In larger storm events, the ponds will provide a “first flush” treatment for up to a 10-year storm event with stabilized emergency spillways to direct flow from larger event greater than a 10-year event to the surrounding area. Due to the topography of the surrounding undisturbed area, water will flow toward Wetland #1. A pre- and post-development analysis of the inflow to Wetland #1 (Analysis Point #1A) has been included in Section IV below. The post-development runoff going to Wetland #1 does not exceed the pre-development condition. Detailed design of the stormwater ponds can be found on page GR-14 of the Expansion Site plan set.

Manufactured Stormwater Filtering Units

Six stormwater filtering systems have been designed to treat runoff from drainage areas DR-1, DR-2, DR-3, DR-4, DR-6, and DR-7. Runoff from these areas sheet flow to its respective closed drainage system and is treated through a filtering manhole unit(s) before the outfall. Details of

the proposed systems are located on sheet GR-15 of the Expansion Site plan set. All systems meet the minimum criteria as defined in Chapter 4 of the Manual and are certified by Washington State Department of Ecology (TAPE) the Maryland Department of the Environment. The systems provide 89% TSS removal and 40% TP removal, which exceed the performance requirements defined in section 3.3.2 of the Manual. Usage of the manufactured stormwater systems is documented in section 9 of the SWPPP. The design and sizing calculations for the manufactured stormwater filtering units is provided in the GI Worksheets (Appendix C).

Infiltration Chamber Systems

Three infiltration chamber systems have been designed to provide runoff reduction volume. For drainage areas DR-1 and DR-4 the infiltration chambers work in conjunction with Stormwater Filtering Units in order to treat the entire water quality volume. For drainage area DR-5 the infiltration chamber system provides sufficient volume to provide runoff reduction as well as treat the entire water quality volume. After flowing through the stormwater filtering units, runoff flows into the infiltration chambers and is stored until infiltrated into the ground. During large storm events, a diversion manhole allows runoff to bypass the infiltration chambers and flow to the Hudson River or Normans Kill. The design and sizing calculations for the chambers is provided in the GI Worksheets under the Infiltration Basin tab (Appendix C). Specifications for the chamber systems utilized are provided in Appendix D.

Infiltration Basins

Two infiltration basins (Basin #1 and Basin #2) have been designed in accordance with the manual. Basin #1 and #2 treat stormwater runoff from drainage areas DR-13 and DR-14 respectively. Runoff from these areas sheet flow to an open roadside swale which outlets into the forebay of the pond. Both ponds have been designed to infiltrate the WQv as required by each catchment area. Because both ponds outlet directly to the Normans Kill, detention of large storm events is not required (see section III.C through III.E below). The basins do not have additional capacity for the Channel Protection Volume (CPv), Overbank Flood Control (Qp), or Extreme Flood Control (Qf). In large storm events, the basin will provide a “first flush” treatment with stabilized emergency spillways to direct flow to the Normans Kill. All stormwater within the basin will be infiltrated within 48 hours of a rain event. Design of the infiltration basins is provided in the GI Worksheets (Appendix C).

Dry Swale

Two dry swales have been designed to treat the new impervious area within DR-15 and DR-17 respectively. Runoff from each area will sheet flow to a roadside swale with the end segment constructed as a dry swale. In large storm events, water not infiltrated into the swale will overflow to a stabilized outlet which drains to the surrounding area. Dry swale #2 has been designed without infiltration, and therefore will only take credit for WQv. Design of the dry swales is provided in the GI Worksheets (Appendix C).

Conservation of Natural Areas

Drainage Area DR-11 will be deed restricted to ensure the perpetual protection of the proposed area to remain vegetated along the Hudson River. Therefore, this area qualifies under the “Conservation of Natural Areas” volume reduction practice.

The RRv provided in the designed practices are summarized in Table III below:

Table III – Practices Providing Runoff Reduction

Drainage Area	Stormwater Practice	RRv (cf)
DR-1	Infiltration Chamber	21,248
DR-4	Infiltration Chamber	18,464
DR-5	Infiltration Chamber	18,426
DR-11	Conservation of Natural Areas	868
DR-13	Infiltration Basin #1	1,995
DR-14	Infiltration Basin #2	2,245
DR-15	Dry Swale #1	87
Total RRv		63,333

The WQv provided for each drainage area is summarized in Table IV below:

Table IV – Practices Providing Water Quality Volume

Drainage Area	Stormwater Practice	WQv (cf)
DR-1	Filter Type 2	18,005
	Infiltration Chamber	2,802
DR-2	Filter Type 1	21,971
DR-3	Filter Type 1	43,939
DR-4	Filter Type 3	14,989
	Infiltration Chamber	2,052
DR-5	Infiltration Chamber	2,047
DR-6	Filter Type 1	48,060
DR-7	Filter Type 2	34,826
DR-8	Stormwater Pond #1	8,437
DR-9	Stormwater Pond #2	13,361
DR-14	Infiltration Basin #2	141
DR-15	Dry Swale #1	129
DR-17	Dry Swale #2	636
Total WQv		211,395

C. Channel Protection Volume (CPv)

Stream Channel Protection Volume Requirements (CPv) are designed to protect stream channels from erosion. The Manual was used to determine the water quantity requirements of CPv; specifically, providing 24-hour extended detention for the 1-year storm event or discharging directly to tidal waters.

According to Section 4.4 of the Manual, the Stream Channel Protection Volume (CPV) requirement does not apply when the site discharges to a tidal waterbody.

The CPv requirement does not apply in certain conditions, including the following:

- Reduction of the entire CPv volume is achieved at a site through green infrastructure or infiltration systems.
- The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, 24-hour extended detention of the 1-year storm event is not required for all drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and analyzed as Analysis Point #1A. The existing 40" outlet pipe from the existing wetland 1 was also analyzed to confirm that adequate capacity was present for the proposed drainage conditions prior to being discharged to the Normans Kill. See Section IV.

The change in hydrology for the 1-year storm event from existing to proposed is shown in the HydroCAD Report printouts provided in Appendix A and B and summarized in Table VI.

D. Overbank Flood Control (Qp)

The primary purpose of the overbank flood control sizing criterion is to prevent an increase in the frequency and magnitude of out-of-bank flooding generated by urban development. The Manual was used to determine the water quantity requirements of Qp; specifically, providing sufficient retention volume to discharge all runoff from the proposed 10-year storm event at a rate equal to or less than the existing peak 10-year runoff rate or discharging directly to tidal waters.

According to Section 4.5 of the Manual, the Overbank Flood Control Criteria (Qp) requirement does not apply when the site discharges to a tidal waterbody.

The overbank flood control requirement (Qp) does not apply in certain conditions, including:

- The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams. Refer to Section 4.3 of the Manual for instructions.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, retention the 10-year storm event is not required for all drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and analyzed as Analysis Point #1A. The existing 40" outlet pipe from the existing wetland 1 was also analyzed to confirm that adequate capacity was present for the proposed drainage conditions prior to being discharged to the Normans Kill. See Section IV.

The change in hydrology for the 10-year storm event from existing to proposed is shown in the HydroCAD Report printouts provided in Appendix A and B and summarized in Table VI.

E. Extreme Flood Control (Qf)

The intent of the extreme flood criteria is to prevent the increased risk of flood damage from large storm events, maintain the boundaries of the predevelopment 100-year floodplain, and protect the physical integrity of stormwater management practices. The Manual was used to determine the water quantity requirements of Qf; specifically, providing sufficient retention volume to discharge all runoff from the proposed 100-year storm event at a rate equal to or less than the existing peak 100-year runoff rate or discharging directly to tidal waters.

According to Section 4.6 of the Manual, the Extreme Flood Control Criteria (Qf) requirement does not apply when the site discharges to a tidal waterbody.

The 100-year storm control requirement can be waived if:

- The site discharges directly tidal waters or fifth order (fifth downstream) or larger streams. Refer to Section 4.3 of the Manual for instructions.

The Hudson River and Normans Kill are classified as tidal waters at the project site. Therefore, retention the 100-year storm event is not required for all drainage areas that outlet directly to the Hudson River or Normans Kill.

Drainage areas DR-8 and DR-9 convey large storm events to Wetland #1, and therefore require water quantity controls. A pre-and post-development analysis of the inflow to Wetland #1 was performed and analyzed as Analysis Point #1A. The existing 40" outlet pipe from the existing wetland 1 was also analyzed to confirm that adequate capacity was present for the proposed drainage conditions prior to being discharged to the Normans Kill. See Section IV.

The change in hydrology for the 100-year storm event from existing to proposed is shown in the HydroCAD Report printouts provided in Appendix A and B and summarized in Table VI.

IV. Summary of Findings

A. Summary of Results

Table V lists the required and provided RRv and WQv for the project. As shown, the project meets both the total water quality volume and runoff reduction volume required by the Manual.

Table V – Stormwater Management Practice Summary

Drainage Area	Stormwater Practice	RRv (cf)	WQv (cf)	Total (RRv + WQv)
DR-1	Filter Type 2	-	18,005	42,055
	Infiltration Chamber	21,248	2,802	
DR-2	Filter Type 1	-	21,971	21,971
DR-3	Filter Type 1	-	43,939	43,939
DR-4	Filter Type 3	-	14,989	35,505
	Infiltration Chamber	18,464	2,052	
DR-5	Infiltration Chamber	18,426	2,047	20,473
DR-6	Filter Type 1	-	48,060	48,060
DR-7	Filter Type 2	-	34,826	34,826
DR-8	Stormwater Pond #1	-	8,437	8,437
DR-9	Stormwater Pond #2	-	13,361	13,361
DR-11	Conservation of Natural Areas	868	-	868
DR-13	Infiltration Basin #1	1,995	-	1,995
DR-14	Infiltration Basin #2	2,245	141	2,386
DR-15	Dry Swale #1	87	129	216
DR-17	Dry Swale #2	-	636	636
Totals	-	63,333	211,395	274,728
Required	-	57,313	-	273,874

Table VI below depicts the peak discharge in the existing and proposed conditions for the 1-year, 10-year and 100-year design storms. The peak discharge for all storm events draining to Analysis Point #1A is decreased in the post-development condition. The peak discharge for all storm events for the remaining analysis points exceed the existing value; however, as described in Sections III, C through E above, this requirement does not apply to analysis points 1 (Hudson River) and 2 (Normans Kill).

Table VI – Peak Discharge Storm Analysis

Analysis Point	Storm Event	Existing (cfs)	Proposed (cfs)
1A	1-year	27.32	4.77
	10-year	73.24	12.46
	100-year	163.60	30.97
1	1-year	3.25	58.54
	10-year	14.96	124.96
	100-year	43.20	205.59
2	1-year	7.17	82.79
	10-year	20.65	166.00
	100-year	48.06	290.19
3	1-year	0.60	1.20
	10-year	1.84	2.62
	100-year	4.39	5.25

Analysis Point #1A analyzes the peak discharge at Wetland #1. In large storm events, stormwater quality ponds #1 and #2 will overflow to an emergency spillway that outlets to the area surrounding Wetland #1. In the post-development condition, Analysis Point #1A has a peak discharge less than the pre-development condition during all storm events, therefore the required water quantity controls are met.

In the post-development condition, Analysis Point #1 has a total drainage area of 0.12 square miles (75.28 acres). This point drains to the Normans Kill with a drainage area of 162 square miles (103,680 acres). The project area makes up approximately 0.07% of the total drainage area of the Normans Kill. With an overall project time of concentration of around 10 minutes, the proposed project will have a negligible impact on the total Normans Kill hydrology as the site-produced runoff will be conveyed prior to the Normans Kill peak and will not impact the overall flood conditions of the Normans Kill.

In the post-development condition, Analysis Point #2 has a total drainage area of 0.04 square miles (23.6 acres). This point drains to the Hudson River with a drainage area of 8,090 square miles (5,177,600 acres). The project area makes up approximately 0.0005% of the total drainage area of the Hudson. With an overall project time of concentration of around 10 minutes, the proposed project will have a negligible impact on the total Hudson River hydrology, as the site-produced runoff will be conveyed prior to the Hudson River peak and will not impact the overall flood conditions of the Hudson River.

In the post-development condition, Analysis Point #3 discharge rates are higher than the pre-development condition. However, analysis point #3 drains to the surrounding area which stores runoff to be gradually infiltrated. Runoff from this analysis point does not flow to a stream or wetland.

The existing 40" outlet pipe from Wetland #1 was also analyzed for capacity. The analysis is summarized in table VII below.

Table VII – Outlet Pipe Capacity Comparison

Storm Event	Existing (cfs)	Proposed (cfs)	Capacity (cfs)
1-year	3.19	1.61	70.83
10-year	14.53	5.17	70.83
100-year	41.52	18.15	70.83

B. Deviation from NYS Stormwater Management Design Manual

The proposed stormwater management design deviates from The Manual by utilizing manufactured stormwater filtering systems for new development.

The need for alternative stormwater management practices is rooted in the extremely limited space available as well as the current site conditions. The proposed Offshore Wind Manufacturing Facility requires 85 acres of usable manufacturing and storage space along the Hudson River. It also requires close proximity to an existing port. Such requirements narrow the available project locations to a select few plots of unoccupied land in the entire state and this site was selected through a solicitation process by the state for off-shore wind development. This site was chosen given it is located adjacent to the existing Port of Albany and is directly on the Hudson River. However, the usable portion of the site adjacent to the Hudson River, is only 66-acres. Therefore, the entirety of the site is needed for the OSW manufacturing process, with an ancillary receiving site located at 700 Smith Boulevard.

The Expansion Site extends also onto the adjacent National Grid property from which APDC is leasing approximately 4.4 acres. However, National Grid has prohibited the installation of permanent stormwater practices within their property.

In addition to space limitations, the existing soils conditions prevent infiltration from being utilized as a stormwater management practice over most of the site. The existing soils are classified as Hydrologic Group D and B/D which provide little to no infiltration and are underlaid by fly ash. Infiltration practices were utilized in the areas where greater than 0.5 in/hr infiltration rates were achieved.

To adequately satisfy the WQv requirements of the Manual, manufactured systems are needed. The Contech Jellyfish units designed meet both the performance and sizing requirements of Chapter 4 of the Manual. The units are also certified by Washington State Department of Ecology (TAPE) and the Maryland Department of the Environment, adequate sources accepted by the NYSDEC. Specifications for the proposed units are provided in Appendix D.

C. Conclusion

Based upon the analysis provided in this report, the proposed development can meet the sizing and performance requirements as defined in Chapter 4 of the Manual. During construction, Erosion and Sediment Control activities will be designed and enforced in accordance with the NYSDEC New York State Standards and Specifications for Erosion and Sediment Control. Stormwater management practices can provide the required RRv and WQv for the proposed conditions. The elements of the Manual and the SPDES Permit that relate to stormwater quantity controls, specifically CPv (1-year), Qp (10-year), and Qf (100-year), are not applicable for portions of the site that discharge directly to a tidal water. For the remaining areas, the peak discharge for the 1-year, 10-year, and 100-year storm events are reduced in the post-development condition. A downstream analysis was completed for the existing Wetland #1 (Analysis Point #1A) and its outlet pipe to confirm adequate capacity prior to discharging into the tidal waters of the Normans Kill. All elements of the closed drainage system have been designed to be non-erosive during a 2-year storm event and capable of conveying a 10-year storm event. Analysis of all closed drainage pipe networks is included in Appendix C. After construction, a maintenance and operation report program and agreement will be made between the site operator and MS4 (Town of Bethlehem) to ensure all stormwater management practices are maintained over the life of the site's operations.

Appendix A

Existing Conditions Drainage Map and HydroCAD Report



McFarland Johnson
 60 RAILROAD PLACE
 SUITE 402
 SARATOGA SPRINGS, NEW YORK 12866
 P: 518-580-9380 F: 518-580-9383
 SaratogaROM@mjinc.com

PROJECT MILESTONE
NFC

NO.	DATE	DESCRIPTION

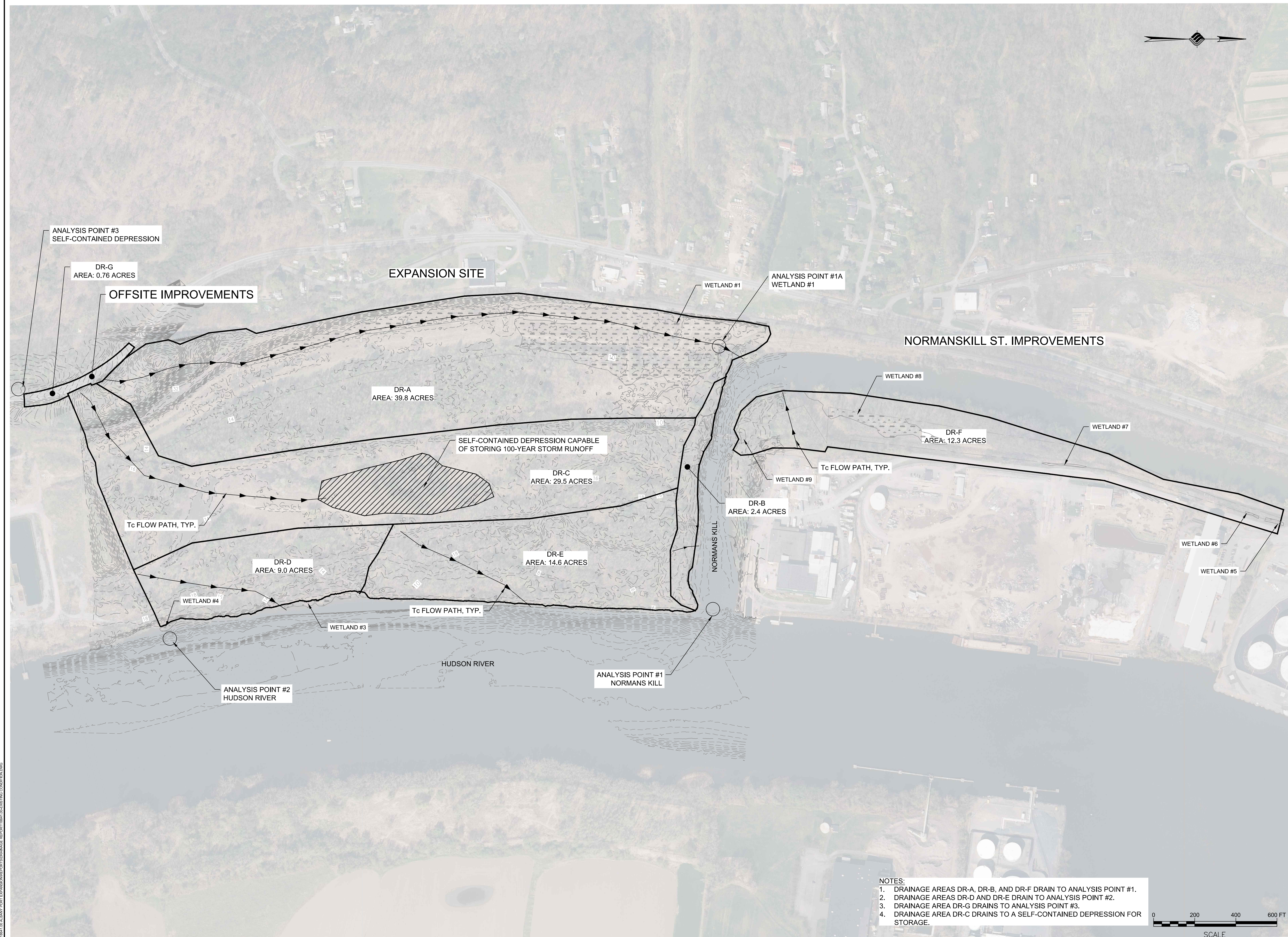
CLIENT: **ALBANY PORT DISTRICT COMMISSION**
 ALBANY, NEW YORK
 PROJECT: **PORT OF ALBANY SITE INFRASTRUCTURE IMPROVEMENTS**

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DESIGNED	NSO
CHECKED	AJF
SCALE	1" = 200'
DATE	JANUARY 2022
PROJECT	18641.00

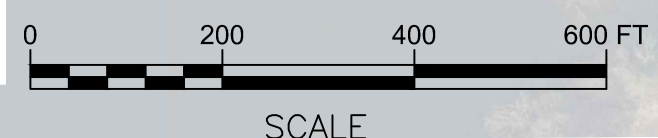
IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECT DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR, TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION.

DRAWING TITLE
PRE-DEVELOPMENT SITE DRAINAGE AREAS

DRAWING NUMBER
DR-EX
 01 OF 01

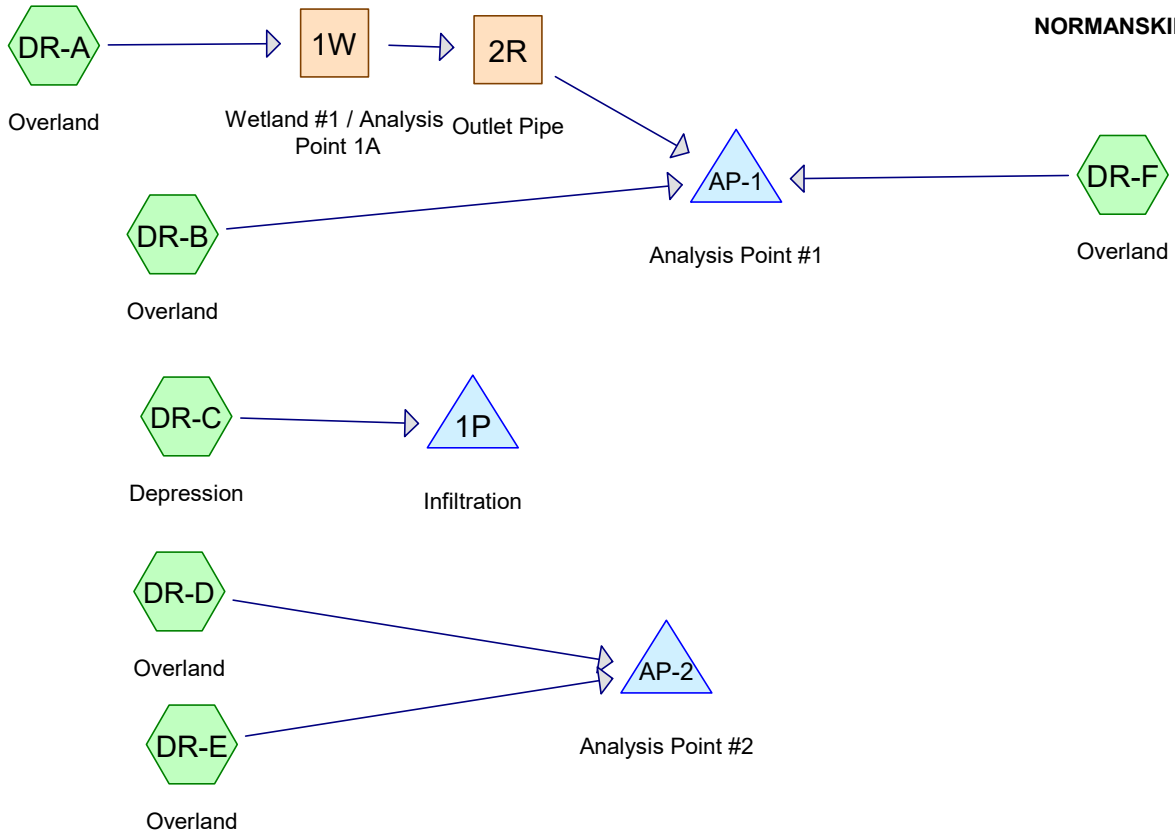


- NOTES:**
- DRAINAGE AREAS DR-A, DR-B, AND DR-F DRAIN TO ANALYSIS POINT #1.
 - DRAINAGE AREAS DR-D AND DR-E DRAIN TO ANALYSIS POINT #2.
 - DRAINAGE AREA DR-G DRAINS TO ANALYSIS POINT #3.
 - DRAINAGE AREA DR-C DRAINS TO A SELF-CONTAINED DEPRESSION FOR STORAGE.



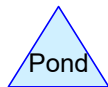
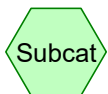
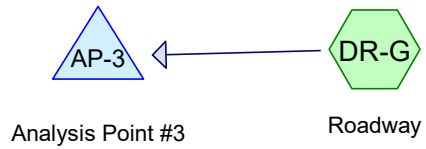
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EXPANSION SITE



NORMANSKILL ST.

OFFSITE IMPROVEMENTS



18641.00-Existing Condition

Prepared by McFarland Johnson

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Page 2

Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.300	39	>75% Grass cover, Good, HSG A (DR-G)
3.970	77	Brush, Fair, HSG D (DR-C)
1.100	98	Existing Railroad (DR-A)
2.500	96	Gravel surface, HSG D (DR-C)
1.100	98	Pavement (DR-F)
0.460	98	Roadway (DR-G)
87.730	79	Woods, Fair, HSG D (DR-A, DR-B, DR-C, DR-D, DR-E)
11.200	43	Woods/grass comb., Fair, HSG A (DR-F)
108.360	76	TOTAL AREA

18641.00-Existing Condition

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Type II 24-hr 1-Year Rainfall=2.20"

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Page 3

Summary for Subcatchment DR-A: Overland

Runoff = 27.32 cfs @ 12.16 hrs, Volume= 2.040 af, Depth> 0.62"

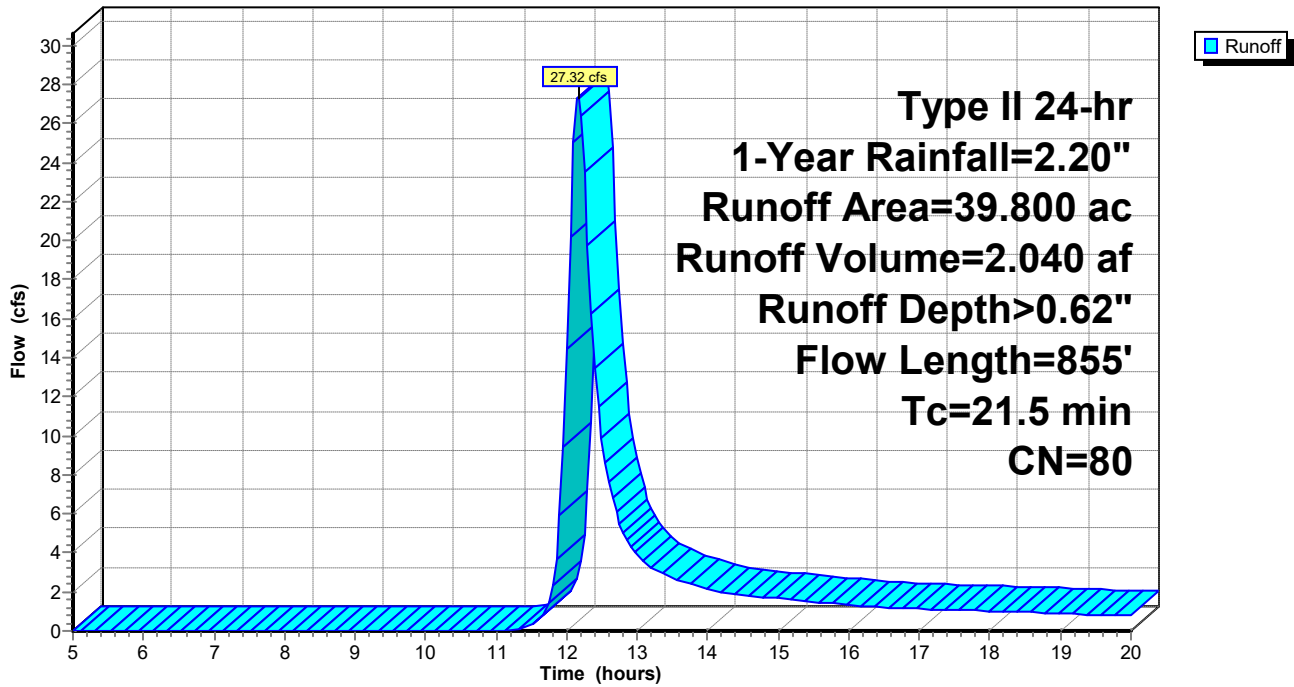
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
38.700	79	Woods, Fair, HSG D
* 1.100	98	Existing Railroad
39.800	80	Weighted Average
38.700		97.24% Pervious Area
1.100		2.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.5	150	0.1500	0.17		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
4.8	575	0.1600	2.00		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
2.2	130	0.0400	1.00		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
21.5	855	Total			

Subcatchment DR-A: Overland

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Subcatchment DR-B: Overland

Runoff = 2.64 cfs @ 11.98 hrs, Volume= 0.115 af, Depth> 0.58"

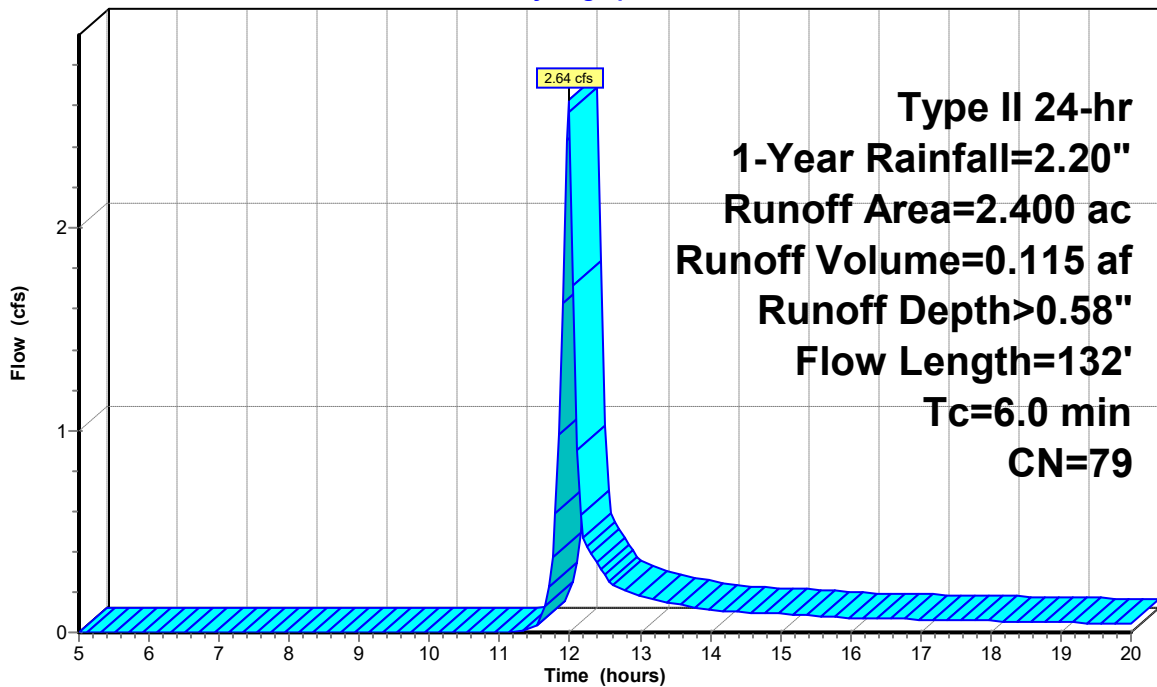
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
2.400	79	Woods, Fair, HSG D
2.400		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	132		0.37		Direct Entry, Sheet Flow

Subcatchment DR-B: Overland

Hydrograph



**Type II 24-hr
1-Year Rainfall=2.20"
Runoff Area=2.400 ac
Runoff Volume=0.115 af
Runoff Depth>0.58"
Flow Length=132'
Tc=6.0 min
CN=79**

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Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Subcatchment DR-C: Depression

Runoff = 34.89 cfs @ 11.98 hrs, Volume= 1.523 af, Depth> 0.62"

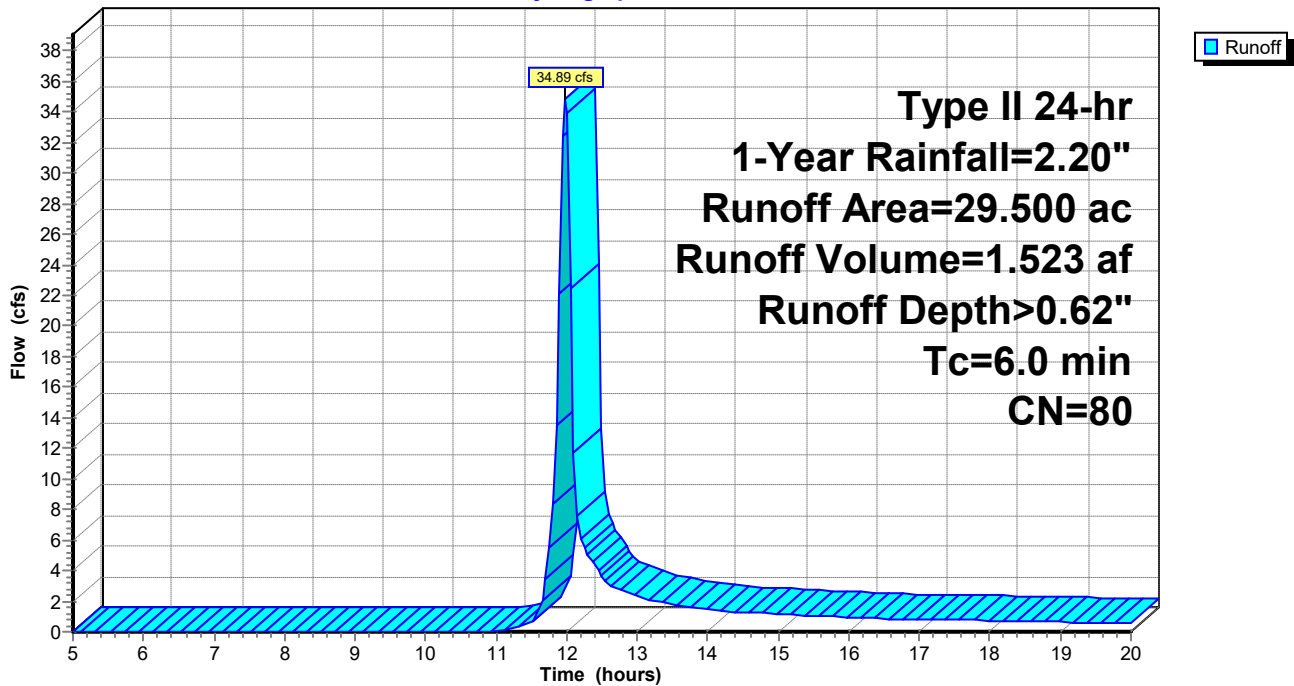
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
3.970	77	Brush, Fair, HSG D
2.500	96	Gravel surface, HSG D
23.030	79	Woods, Fair, HSG D
29.500	80	Weighted Average
29.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-C: Depression

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Subcatchment DR-D: Overland

Runoff = 2.18 cfs @ 12.96 hrs, Volume= 0.416 af, Depth> 0.55"

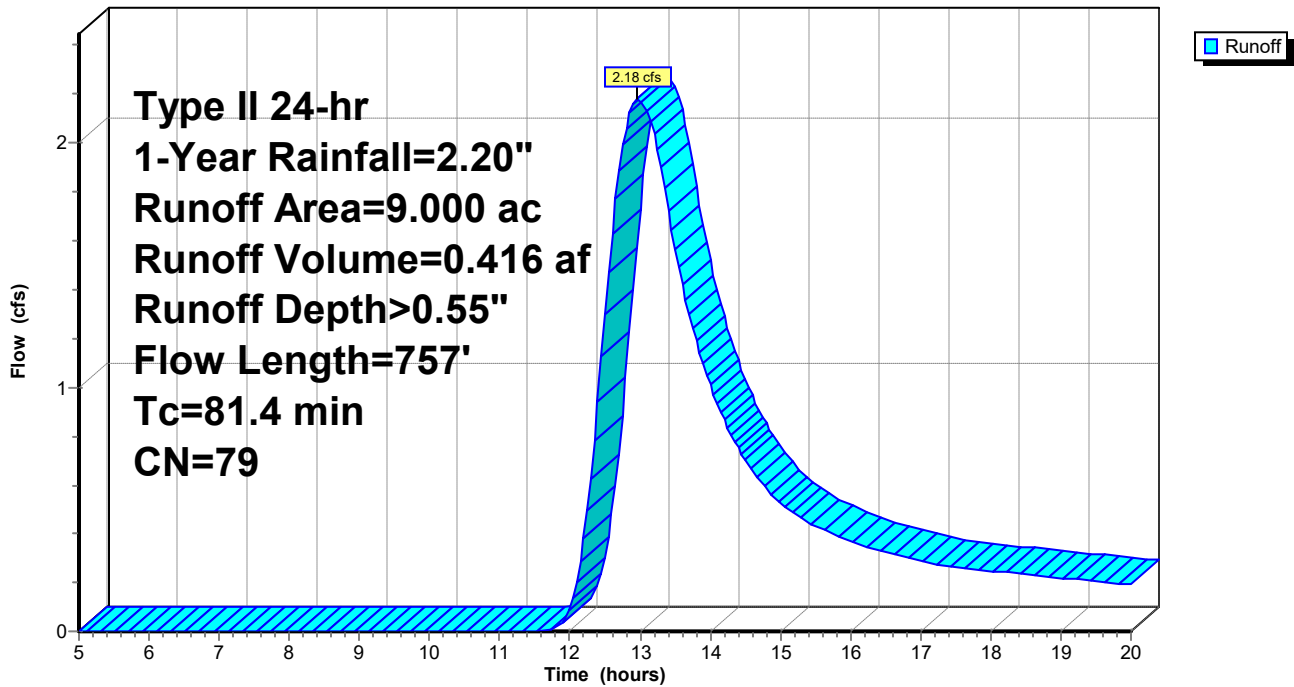
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
9.000	79	Woods, Fair, HSG D
9.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
56.6	150	0.0050	0.04		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
23.9	507	0.0050	0.35		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
0.9	100	0.1300	1.80		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
81.4	757	Total			

Subcatchment DR-D: Overland

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Subcatchment DR-E: Overland

Runoff = 6.22 cfs @ 12.38 hrs, Volume= 0.691 af, Depth> 0.57"

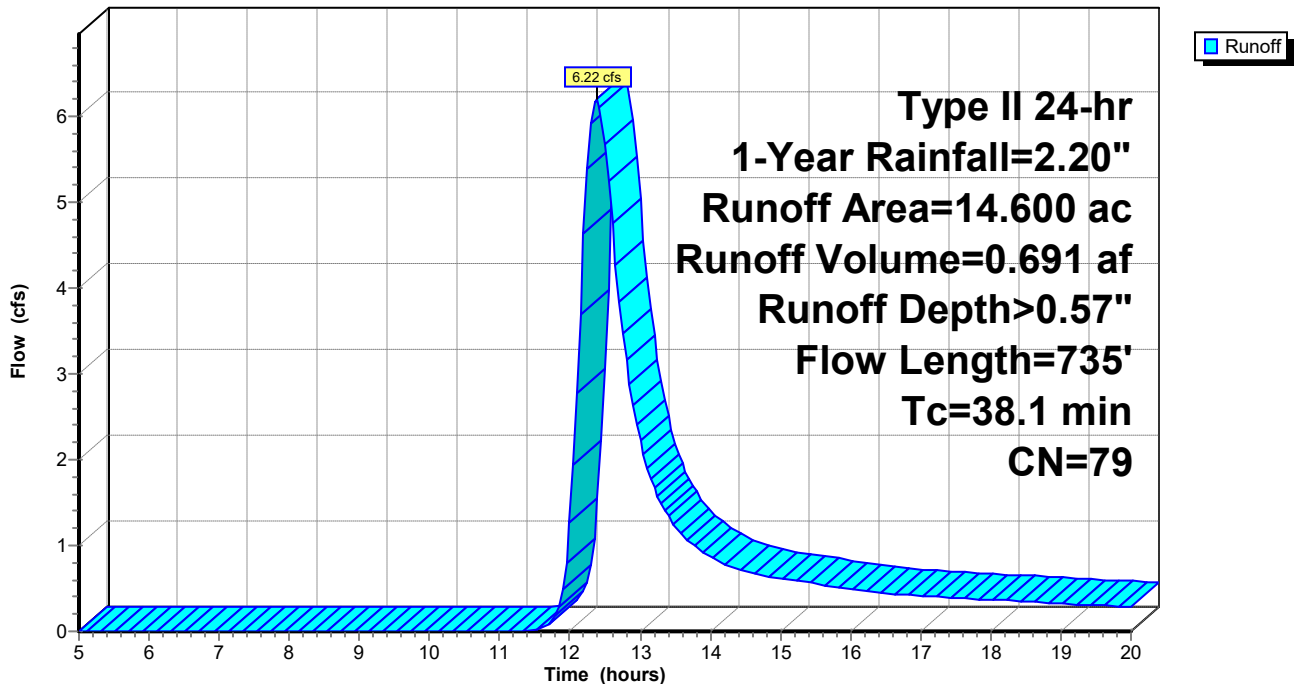
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
14.600	79	Woods, Fair, HSG D
14.600		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
27.6	150	0.0300	0.09		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
9.8	510	0.0300	0.87		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
0.7	75	0.1200	1.73		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
38.1	735	Total			

Subcatchment DR-E: Overland

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Subcatchment DR-F: Overland

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

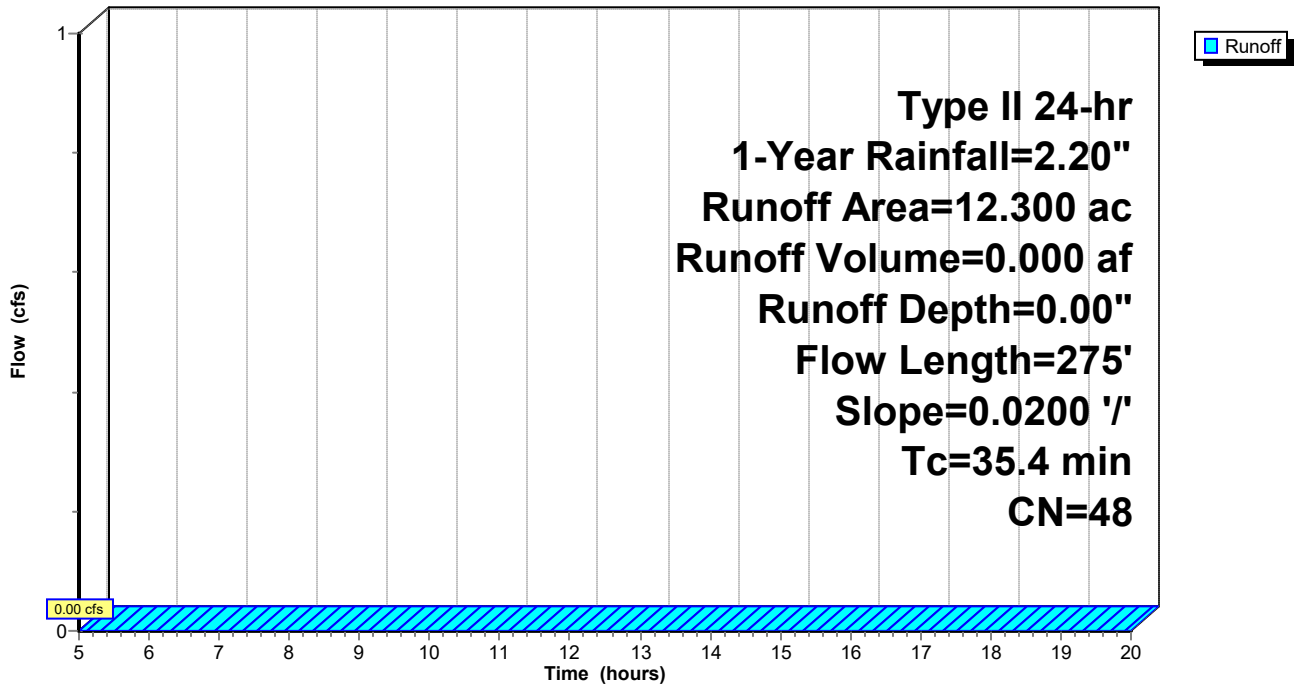
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 1.100	98	Pavement
11.200	43	Woods/grass comb., Fair, HSG A
12.300	48	Weighted Average
11.200		91.06% Pervious Area
1.100		8.94% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
32.5	150	0.0200	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.67"
2.9	125	0.0200	0.71		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
35.4	275	Total			

Subcatchment DR-F: Overland

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Subcatchment DR-G: Roadway

Runoff = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af, Depth> 0.43"

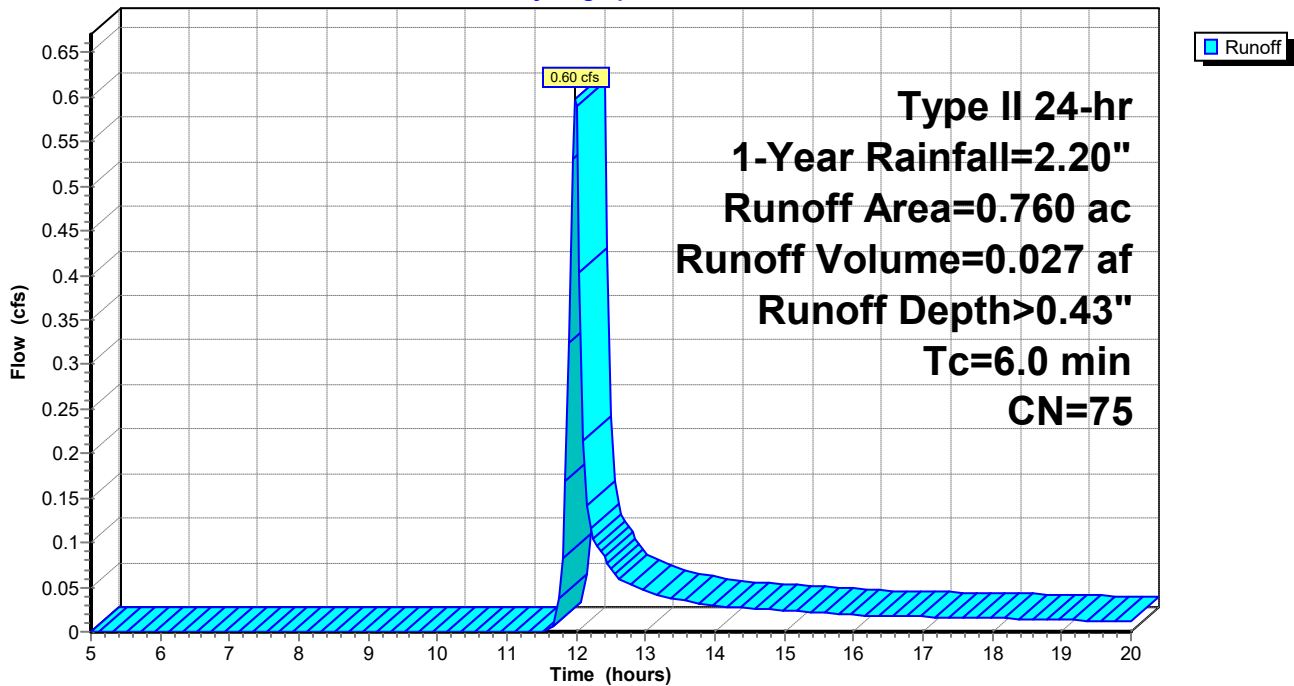
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 0.460	98	Roadway
0.300	39	>75% Grass cover, Good, HSG A
0.760	75	Weighted Average
0.300		39.47% Pervious Area
0.460		60.53% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-G: Roadway

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 0.62" for 1-Year event
 Inflow = 27.32 cfs @ 12.16 hrs, Volume= 2.040 af
 Outflow = 3.19 cfs @ 17.12 hrs, Volume= 0.898 af, Atten= 88%, Lag= 297.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.07 fps, Min. Travel Time= 232.8 min
 Avg. Velocity = 0.05 fps, Avg. Travel Time= 304.0 min

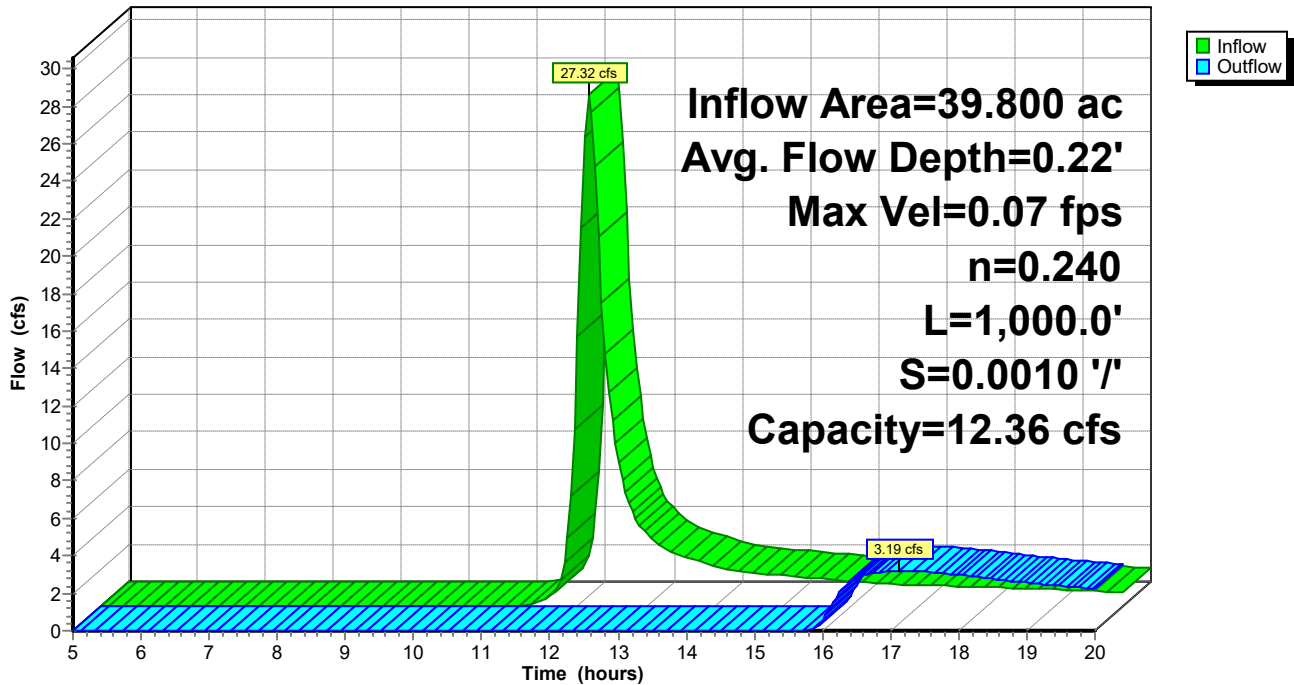
Peak Storage= 44,519 cf @ 13.24 hrs
 Average Depth at Peak Storage= 0.22' , Surface Width= 201.33'
 Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240 Sheet flow over Dense Grass
 Side Slope Z-value= 3.0 '/' Top Width= 203.00'
 Length= 1,000.0' Slope= 0.0010 '/'
 Inlet Invert= 6.00', Outlet Invert= 5.00'



Reach 1W: Wetland #1 / Analysis Point 1A

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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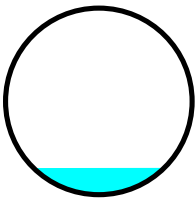
Summary for Reach 2R: Outlet Pipe

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 0.27" for 1-Year event
Inflow = 3.19 cfs @ 17.12 hrs, Volume= 0.898 af
Outflow = 3.19 cfs @ 17.13 hrs, Volume= 0.896 af, Atten= 0%, Lag= 0.5 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Max. Velocity= 4.10 fps, Min. Travel Time= 0.3 min
Avg. Velocity = 3.35 fps, Avg. Travel Time= 0.3 min

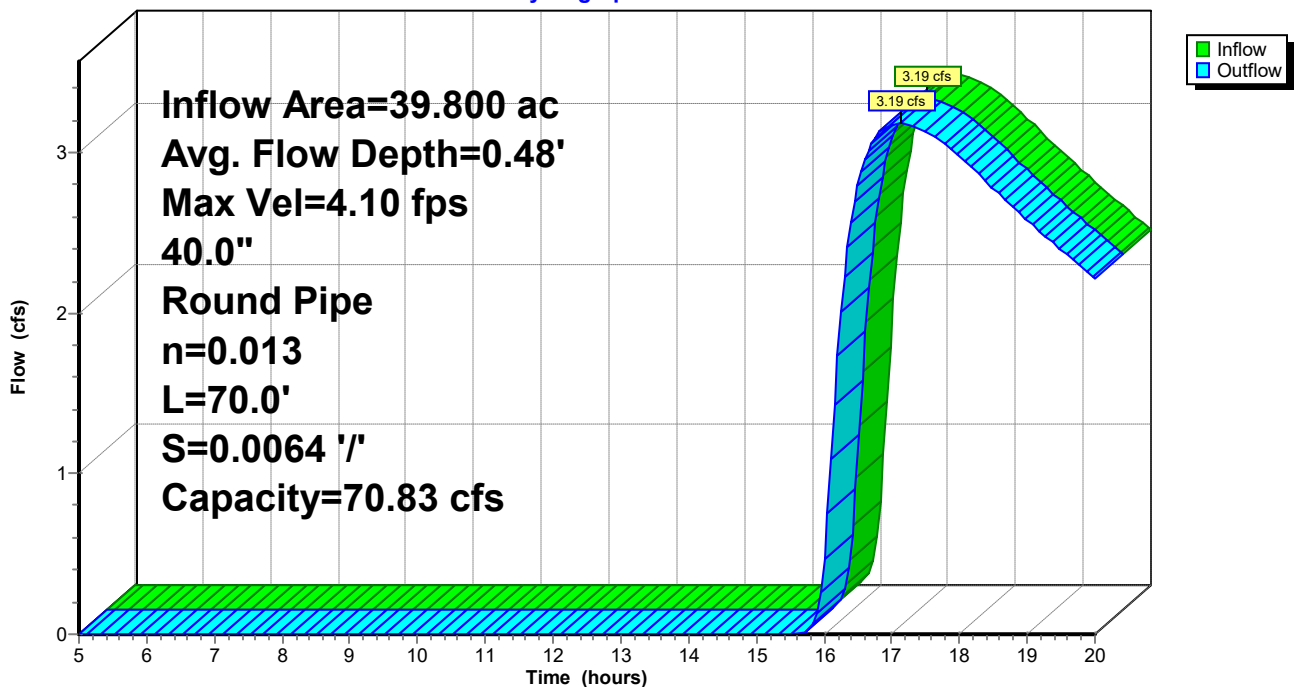
Peak Storage= 54 cf @ 17.12 hrs
Average Depth at Peak Storage= 0.48' , Surface Width= 2.34'
Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe
n= 0.013 Corrugated PE, smooth interior
Length= 70.0' Slope= 0.0064 '/'
Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 2R: Outlet Pipe

Hydrograph



18641.00-Existing Condition

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Type II 24-hr 1-Year Rainfall=2.20"

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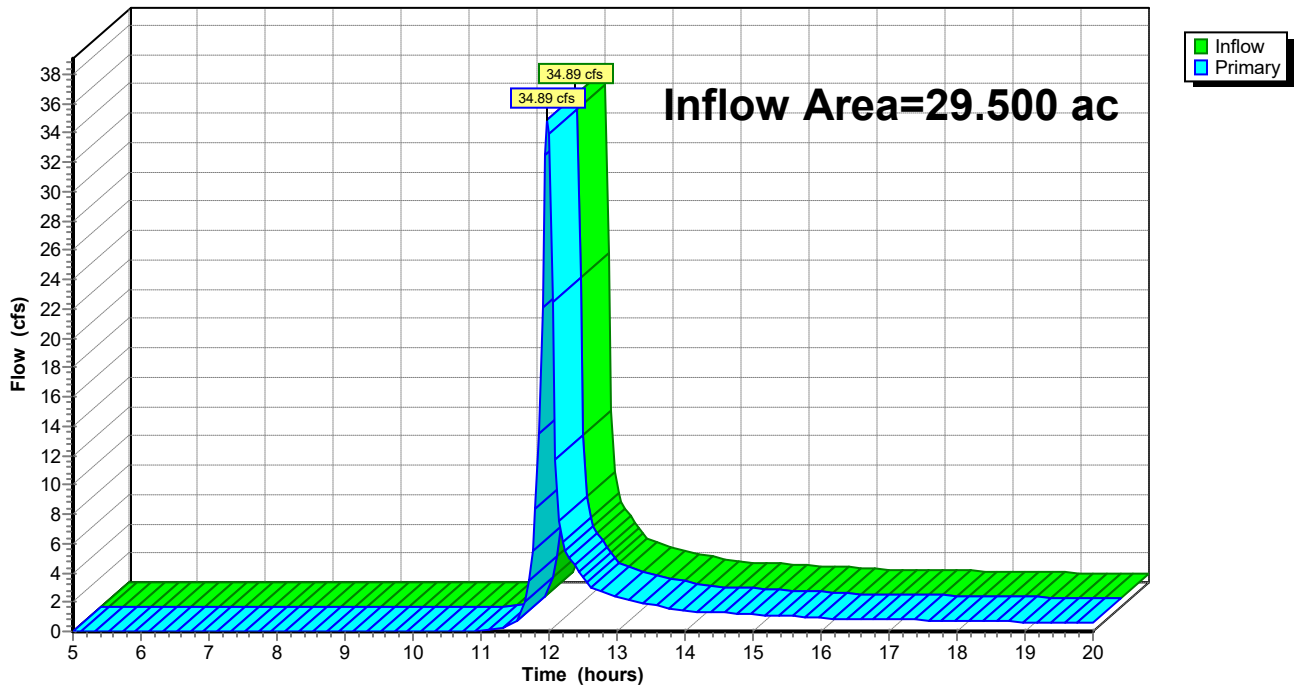
Summary for Pond 1P: Infiltration

Inflow Area = 29.500 ac, 0.00% Impervious, Inflow Depth > 0.62" for 1-Year event
Inflow = 34.89 cfs @ 11.98 hrs, Volume= 1.523 af
Primary = 34.89 cfs @ 11.98 hrs, Volume= 1.523 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond 1P: Infiltration

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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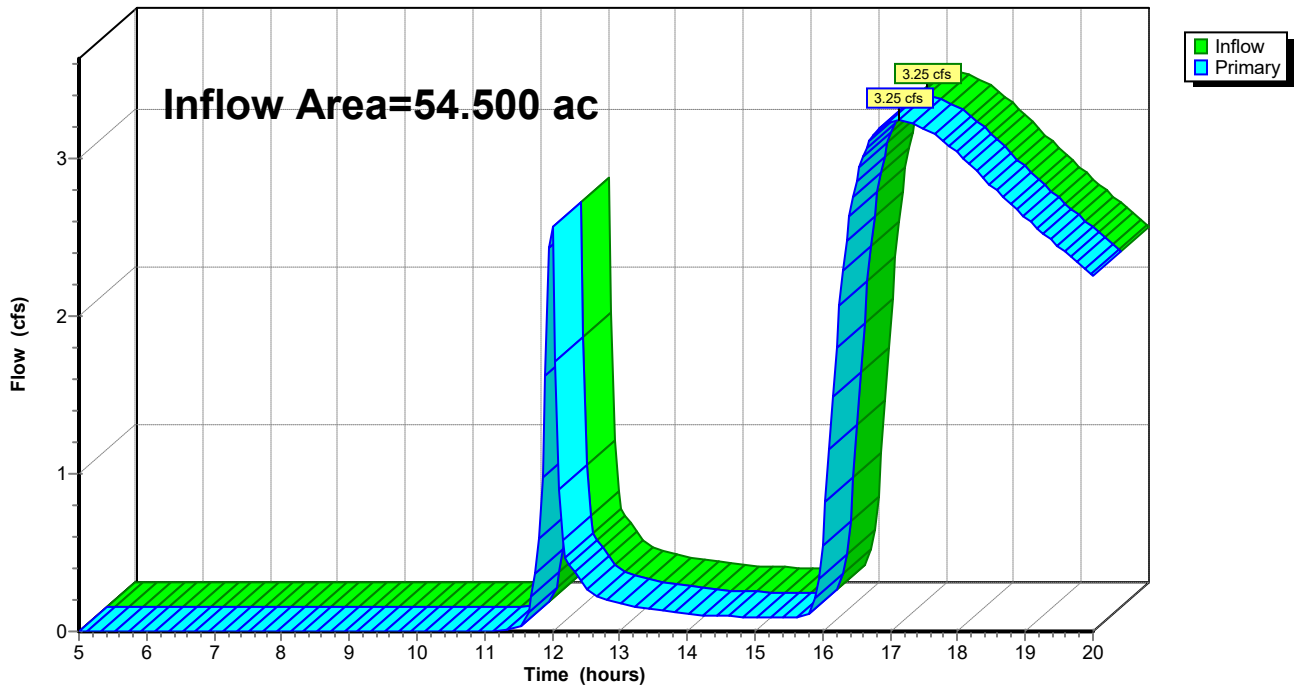
Summary for Pond AP-1: Analysis Point #1

Inflow Area = 54.500 ac, 4.04% Impervious, Inflow Depth > 0.22" for 1-Year event
Inflow = 3.25 cfs @ 17.12 hrs, Volume= 1.012 af
Primary = 3.25 cfs @ 17.12 hrs, Volume= 1.012 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1

Hydrograph



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Type II 24-hr 1-Year Rainfall=2.20"

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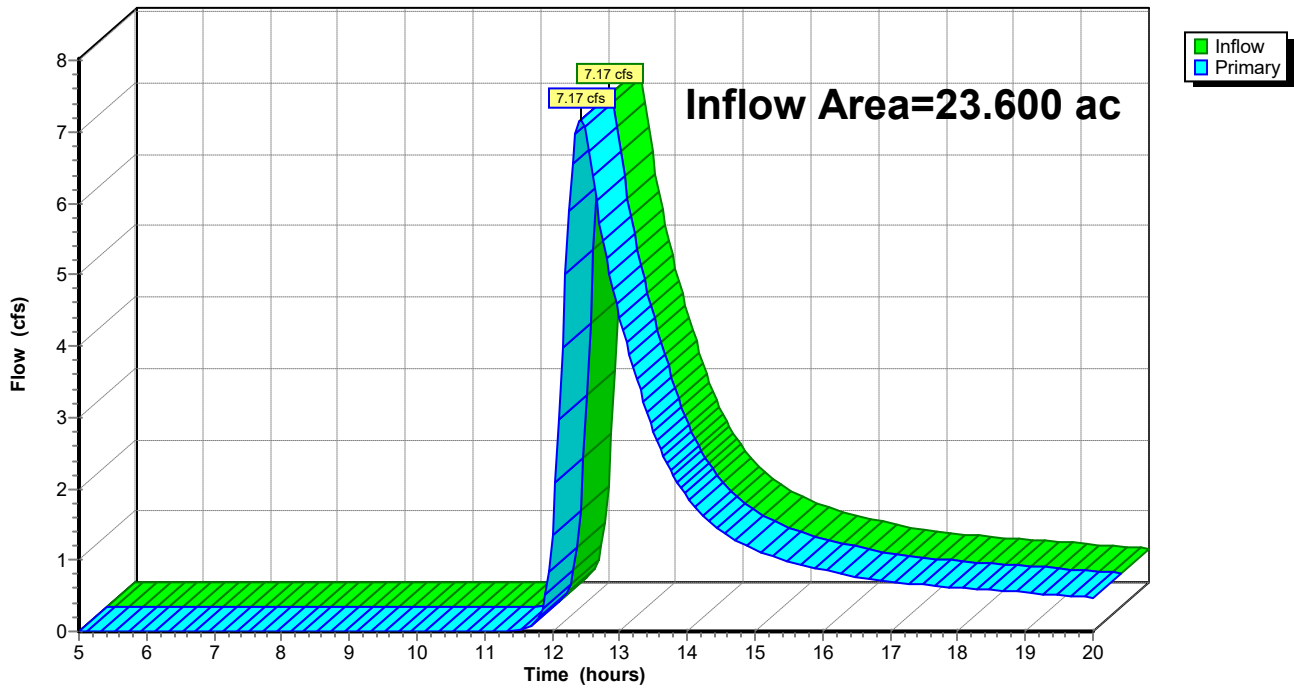
Summary for Pond AP-2: Analysis Point #2

Inflow Area = 23.600 ac, 0.00% Impervious, Inflow Depth > 0.56" for 1-Year event
Inflow = 7.17 cfs @ 12.42 hrs, Volume= 1.107 af
Primary = 7.17 cfs @ 12.42 hrs, Volume= 1.107 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2

Hydrograph



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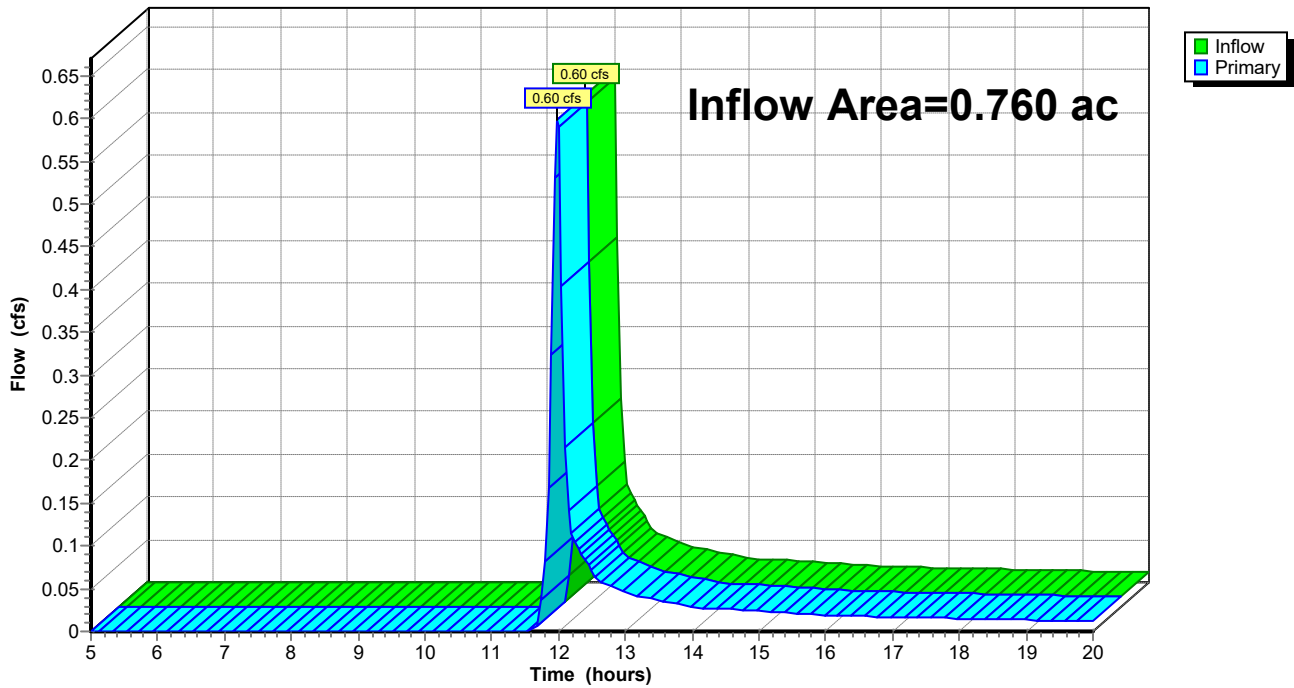
Summary for Pond AP-3: Analysis Point #3

Inflow Area = 0.760 ac, 60.53% Impervious, Inflow Depth > 0.43" for 1-Year event
Inflow = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af
Primary = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DR-A: Overland

Runoff = 73.24 cfs @ 12.15 hrs, Volume= 5.272 af, Depth> 1.59"

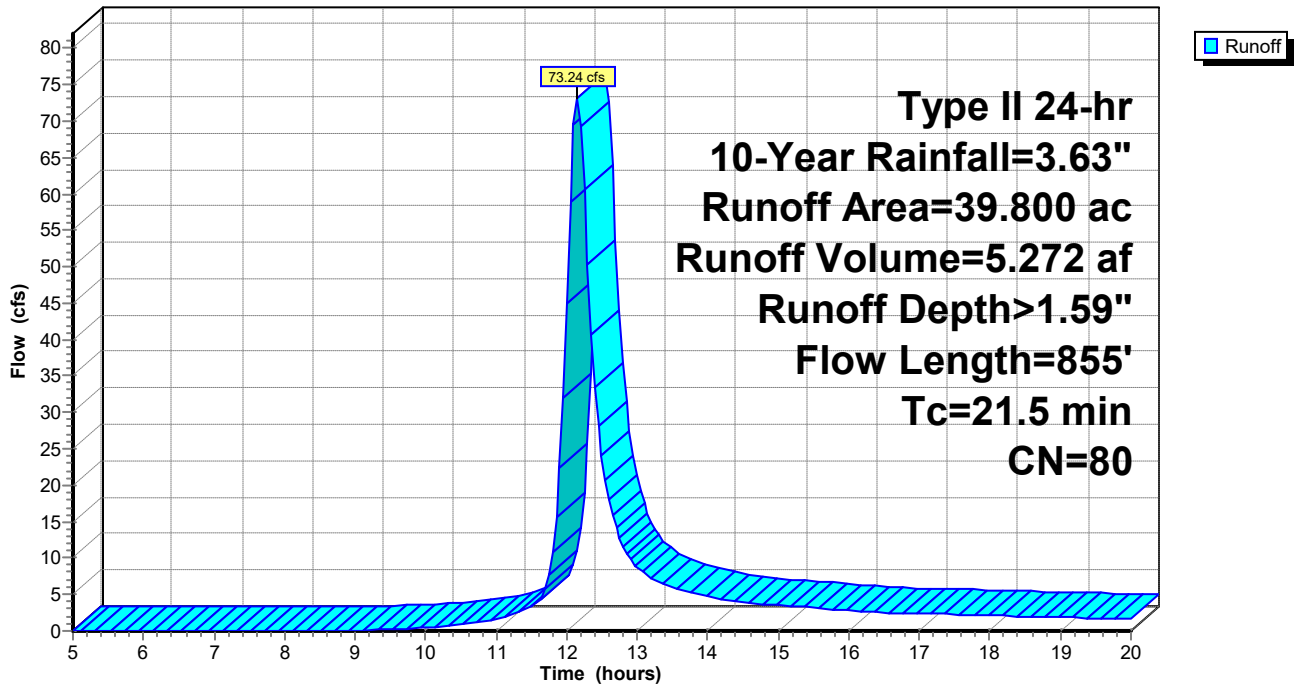
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
38.700	79	Woods, Fair, HSG D
* 1.100	98	Existing Railroad
39.800	80	Weighted Average
38.700		97.24% Pervious Area
1.100		2.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.5	150	0.1500	0.17		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
4.8	575	0.1600	2.00		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
2.2	130	0.0400	1.00		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
21.5	855	Total			

Subcatchment DR-A: Overland

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DR-B: Overland

Runoff = 6.90 cfs @ 11.97 hrs, Volume= 0.306 af, Depth> 1.53"

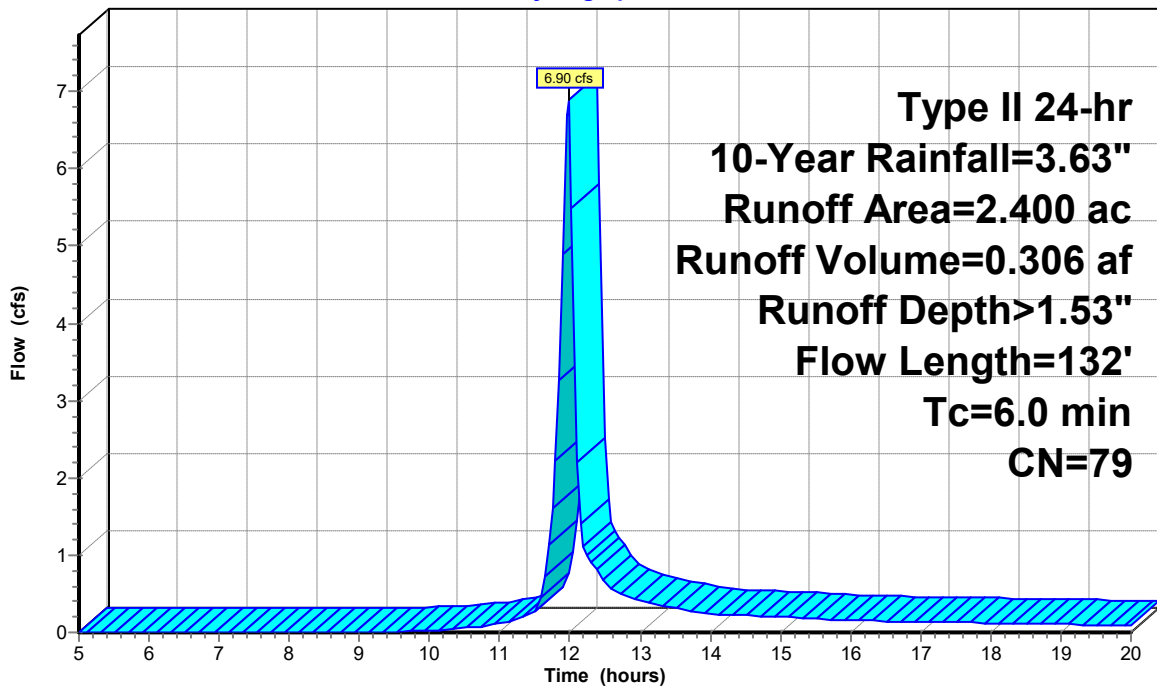
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
2.400	79	Woods, Fair, HSG D
2.400		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	132		0.37		Direct Entry, Sheet Flow

Subcatchment DR-B: Overland

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DR-C: Depression

Runoff = 88.48 cfs @ 11.97 hrs, Volume= 3.930 af, Depth> 1.60"

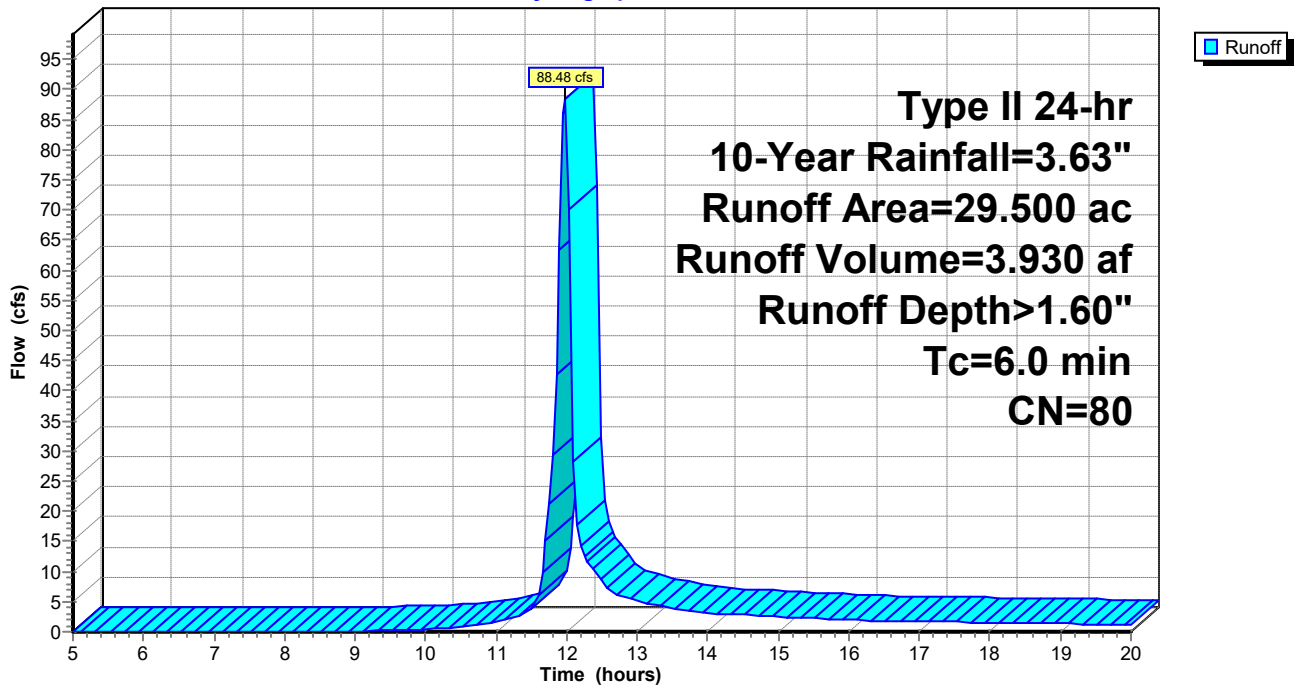
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
3.970	77	Brush, Fair, HSG D
2.500	96	Gravel surface, HSG D
23.030	79	Woods, Fair, HSG D
29.500	80	Weighted Average
29.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-C: Depression

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DR-D: Overland

Runoff = 6.25 cfs @ 12.93 hrs, Volume= 1.110 af, Depth> 1.48"

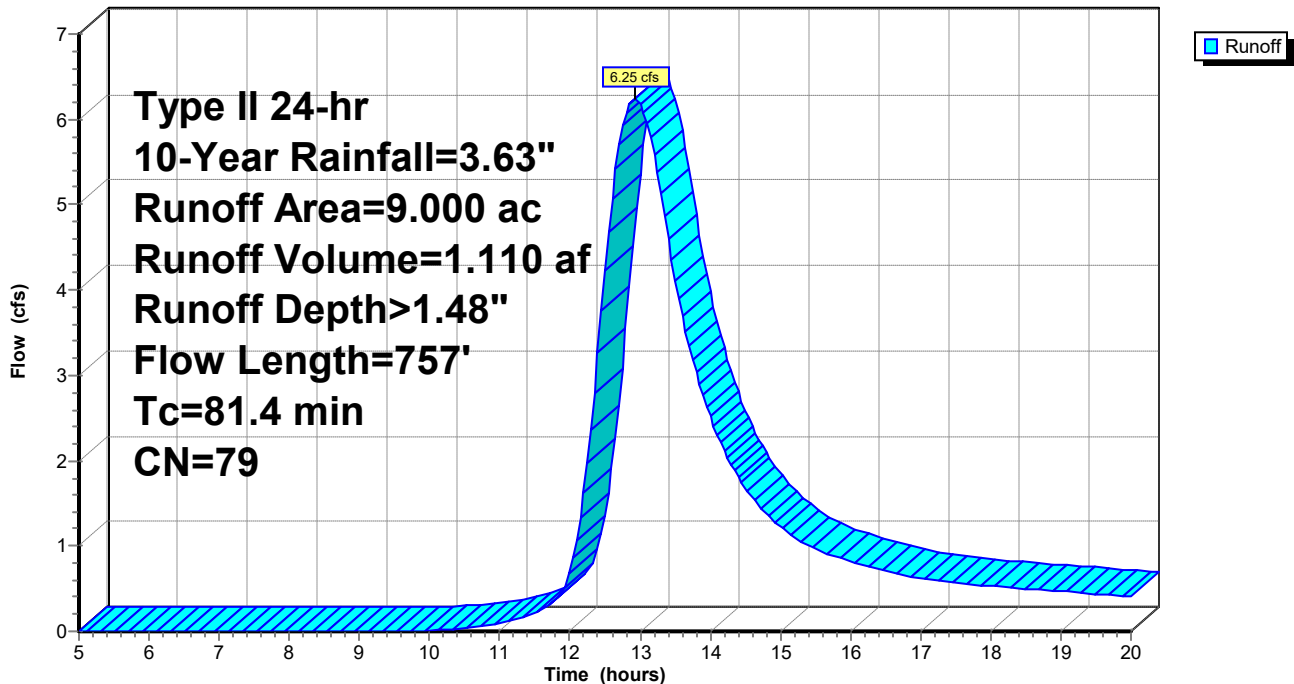
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
9.000	79	Woods, Fair, HSG D
9.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
56.6	150	0.0050	0.04		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
23.9	507	0.0050	0.35		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
0.9	100	0.1300	1.80		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
81.4	757	Total			

Subcatchment DR-D: Overland

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DR-E: Overland

Runoff = 17.64 cfs @ 12.35 hrs, Volume= 1.837 af, Depth> 1.51"

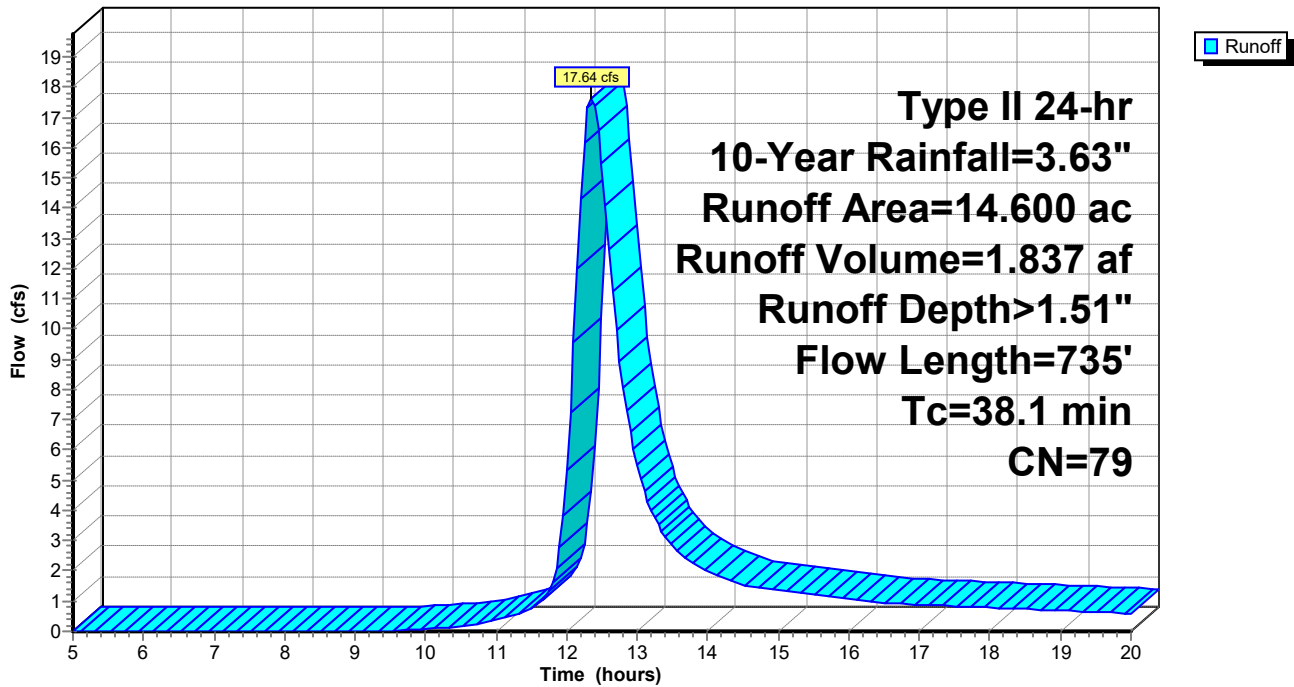
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
14.600	79	Woods, Fair, HSG D
14.600		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
27.6	150	0.0300	0.09		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
9.8	510	0.0300	0.87		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
0.7	75	0.1200	1.73		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
38.1	735	Total			

Subcatchment DR-E: Overland

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DR-F: Overland

Runoff = 0.38 cfs @ 12.75 hrs, Volume= 0.135 af, Depth> 0.13"

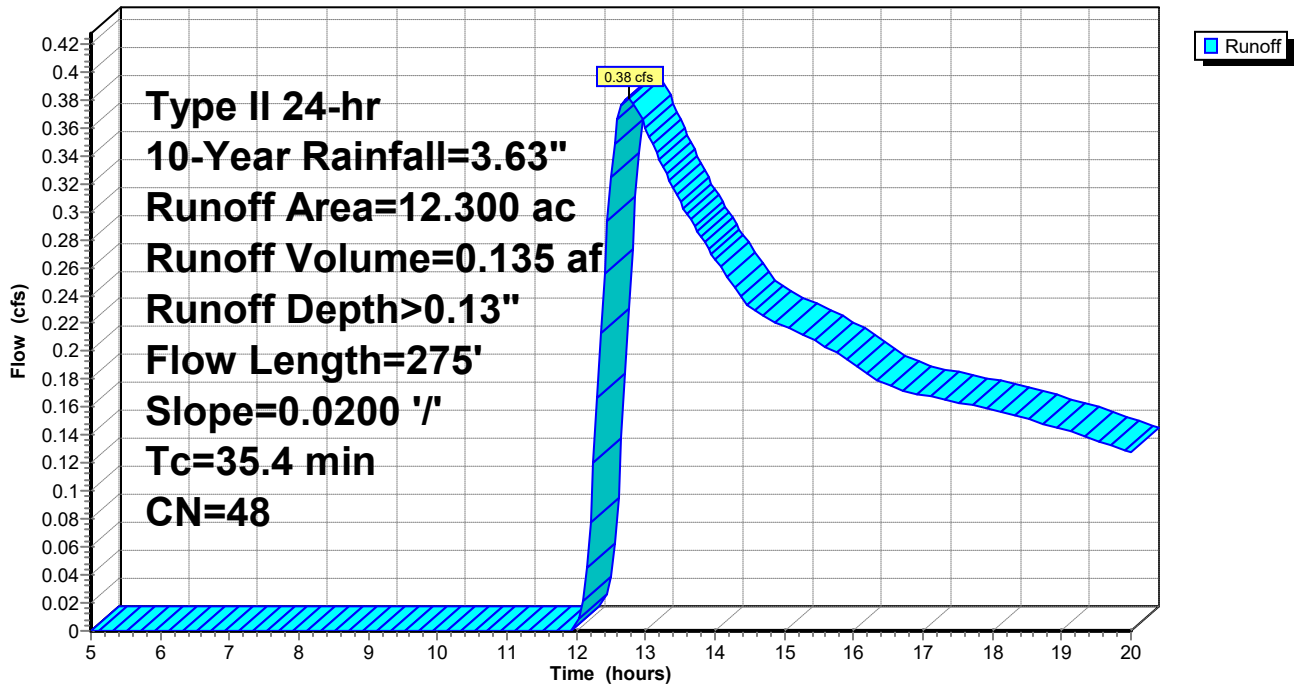
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 1.100	98	Pavement
11.200	43	Woods/grass comb., Fair, HSG A
12.300	48	Weighted Average
11.200		91.06% Pervious Area
1.100		8.94% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
32.5	150	0.0200	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.67"
2.9	125	0.0200	0.71		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
35.4	275	Total			

Subcatchment DR-F: Overland

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DR-G: Roadway

Runoff = 1.84 cfs @ 11.98 hrs, Volume= 0.080 af, Depth> 1.27"

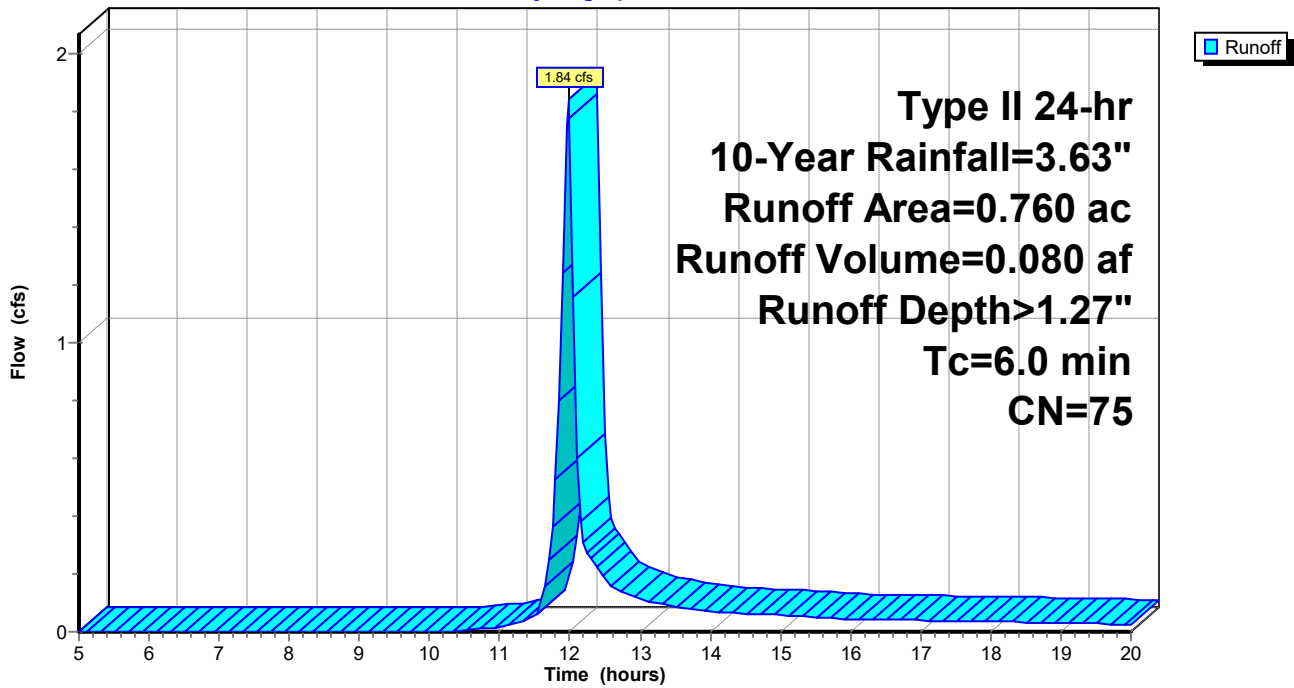
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 0.460	98	Roadway
0.300	39	>75% Grass cover, Good, HSG A
0.760	75	Weighted Average
0.300		39.47% Pervious Area
0.460		60.53% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-G: Roadway

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 1.59" for 10-Year event
Inflow = 73.24 cfs @ 12.15 hrs, Volume= 5.272 af
Outflow = 14.53 cfs @ 14.82 hrs, Volume= 3.841 af, Atten= 80%, Lag= 160.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Max. Velocity= 0.13 fps, Min. Travel Time= 127.8 min
Avg. Velocity = 0.07 fps, Avg. Travel Time= 239.5 min

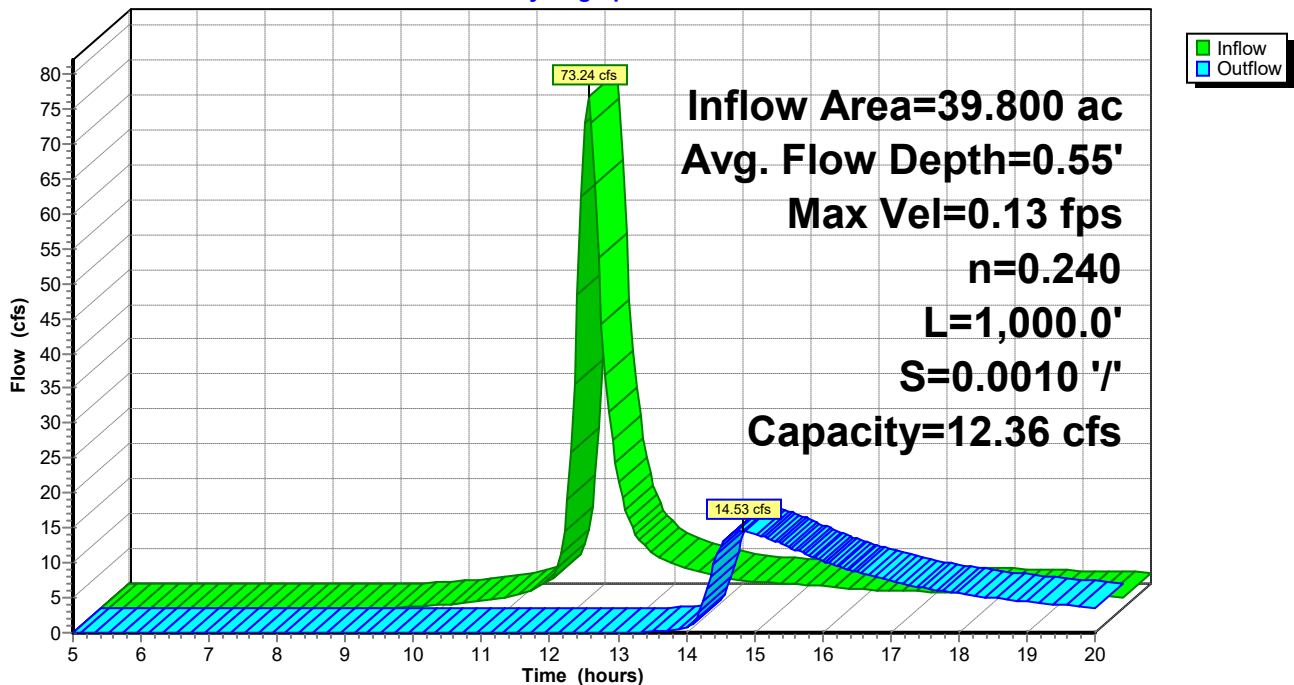
Peak Storage= 111,494 cf @ 12.69 hrs
Average Depth at Peak Storage= 0.55' , Surface Width= 203.32'
Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240 Sheet flow over Dense Grass
Side Slope Z-value= 3.0 '/' Top Width= 203.00'
Length= 1,000.0' Slope= 0.0010 '/'
Inlet Invert= 6.00', Outlet Invert= 5.00'



Reach 1W: Wetland #1 / Analysis Point 1A

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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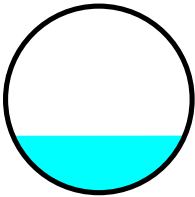
Summary for Reach 2R: Outlet Pipe

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 1.16" for 10-Year event
Inflow = 14.53 cfs @ 14.82 hrs, Volume= 3.841 af
Outflow = 14.53 cfs @ 14.83 hrs, Volume= 3.838 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Max. Velocity= 6.38 fps, Min. Travel Time= 0.2 min
Avg. Velocity = 3.89 fps, Avg. Travel Time= 0.3 min

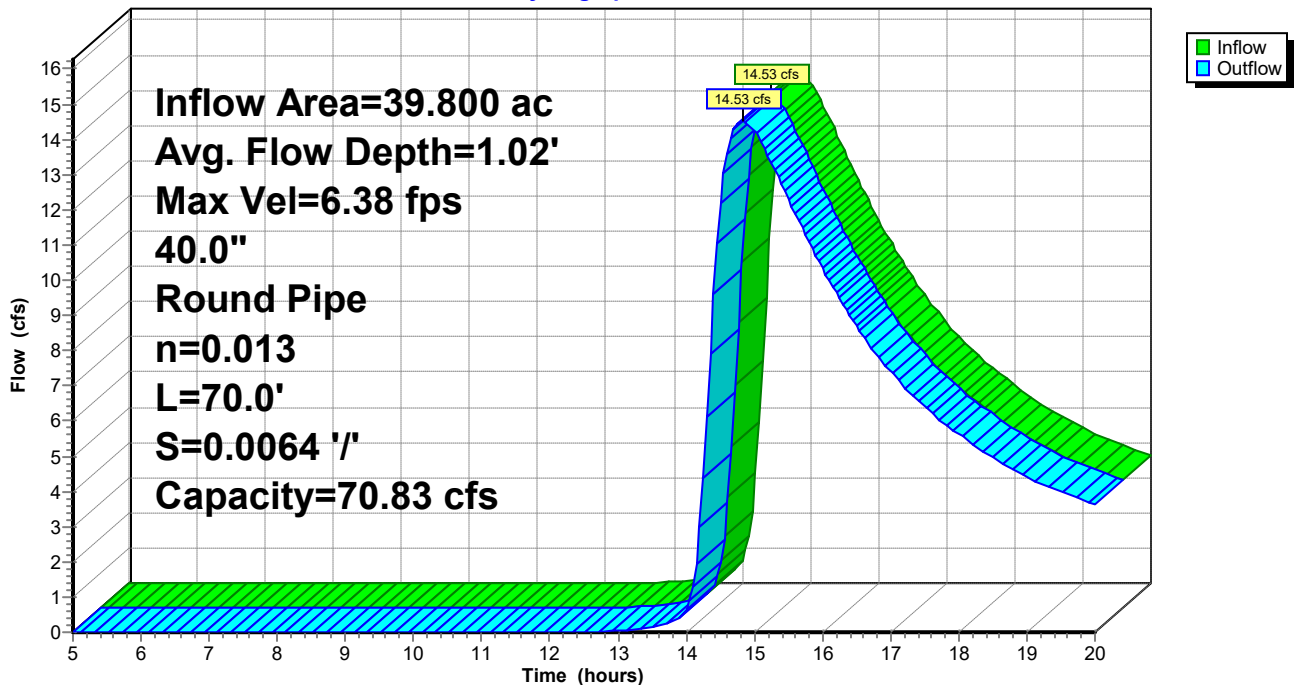
Peak Storage= 159 cf @ 14.82 hrs
Average Depth at Peak Storage= 1.02' , Surface Width= 3.08'
Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe
n= 0.013 Corrugated PE, smooth interior
Length= 70.0' Slope= 0.0064 '/'
Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 2R: Outlet Pipe

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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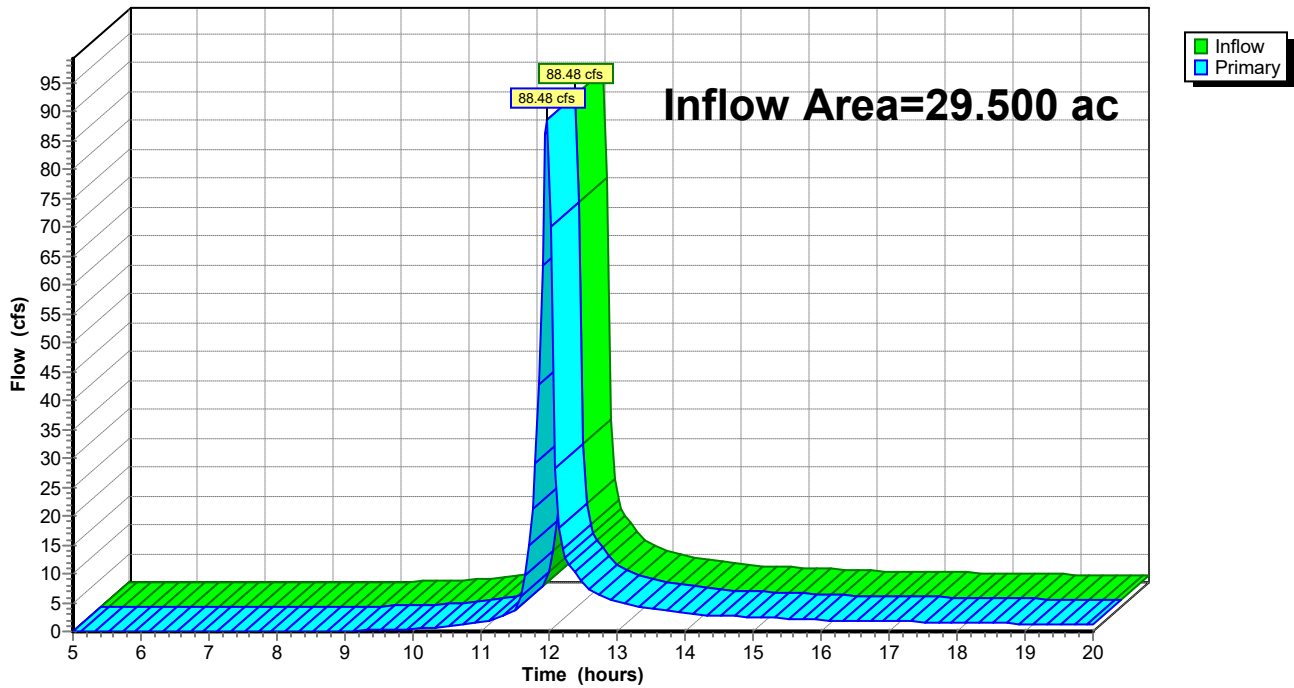
Summary for Pond 1P: Infiltration

Inflow Area = 29.500 ac, 0.00% Impervious, Inflow Depth > 1.60" for 10-Year event
Inflow = 88.48 cfs @ 11.97 hrs, Volume= 3.930 af
Primary = 88.48 cfs @ 11.97 hrs, Volume= 3.930 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond 1P: Infiltration

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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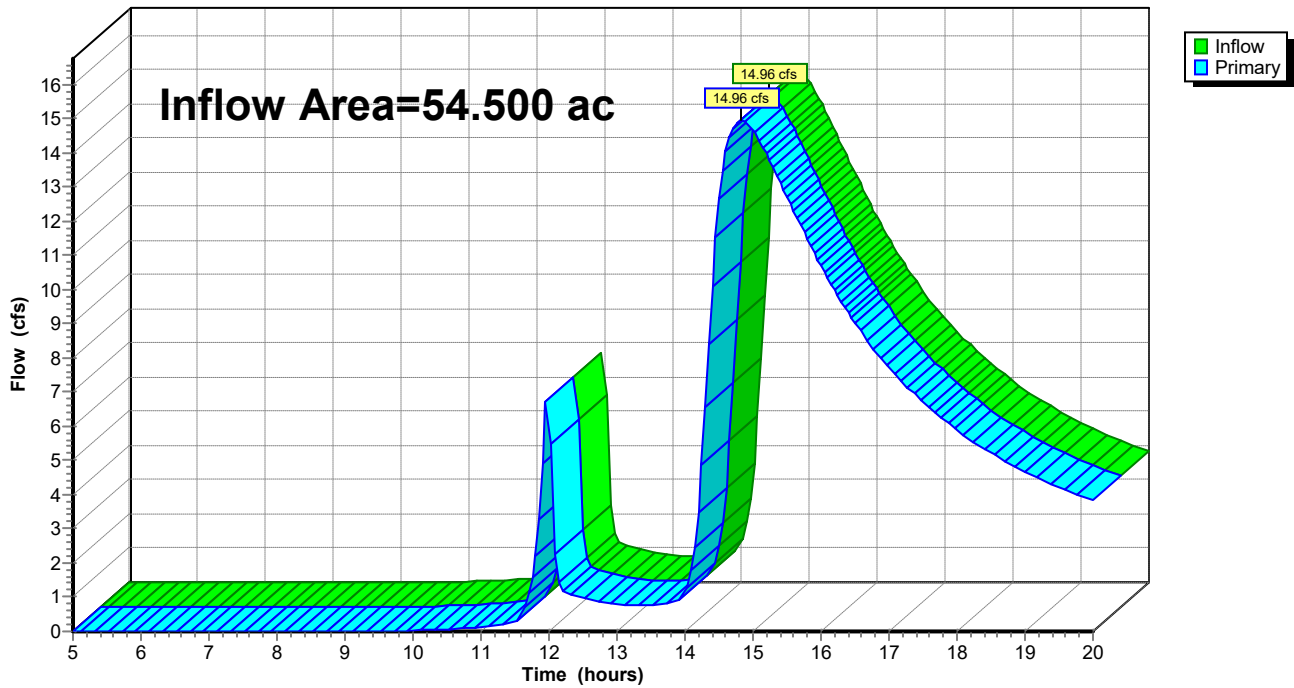
Summary for Pond AP-1: Analysis Point #1

Inflow Area = 54.500 ac, 4.04% Impervious, Inflow Depth > 0.94" for 10-Year event
Inflow = 14.96 cfs @ 14.82 hrs, Volume= 4.279 af
Primary = 14.96 cfs @ 14.82 hrs, Volume= 4.279 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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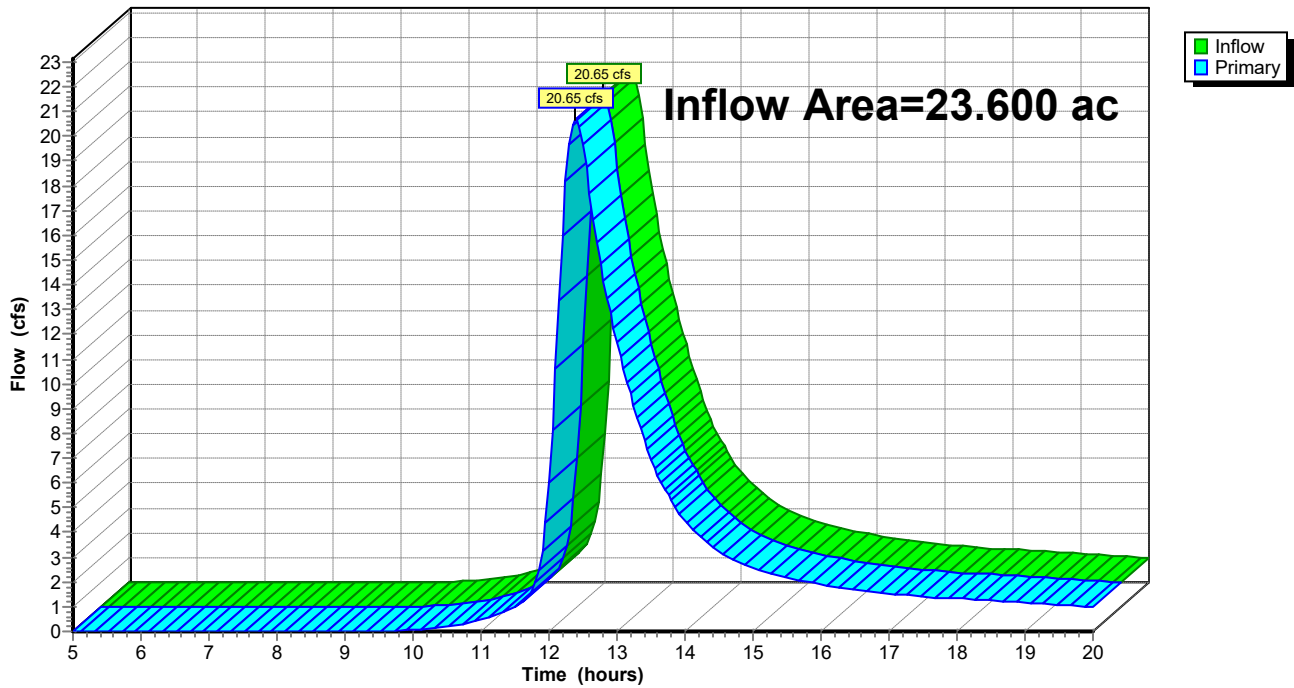
Summary for Pond AP-2: Analysis Point #2

Inflow Area = 23.600 ac, 0.00% Impervious, Inflow Depth > 1.50" for 10-Year event
Inflow = 20.65 cfs @ 12.40 hrs, Volume= 2.947 af
Primary = 20.65 cfs @ 12.40 hrs, Volume= 2.947 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2

Hydrograph



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Type II 24-hr 10-Year Rainfall=3.63"

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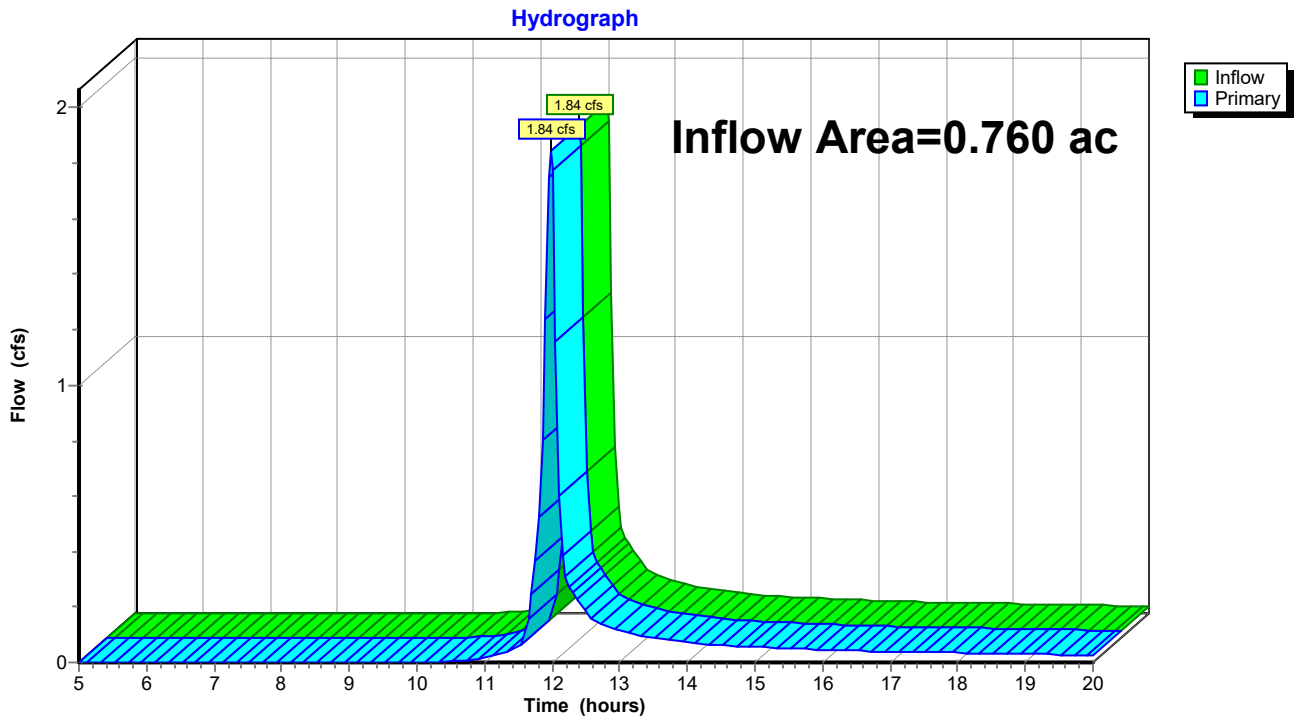
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Summary for Pond AP-3: Analysis Point #3

Inflow Area = 0.760 ac, 60.53% Impervious, Inflow Depth > 1.27" for 10-Year event
Inflow = 1.84 cfs @ 11.98 hrs, Volume= 0.080 af
Primary = 1.84 cfs @ 11.98 hrs, Volume= 0.080 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3



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Type II 24-hr 100-Year Rainfall=6.11"

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Summary for Subcatchment DR-A: Overland

Runoff = 163.60 cfs @ 12.14 hrs, Volume= 11.919 af, Depth> 3.59"

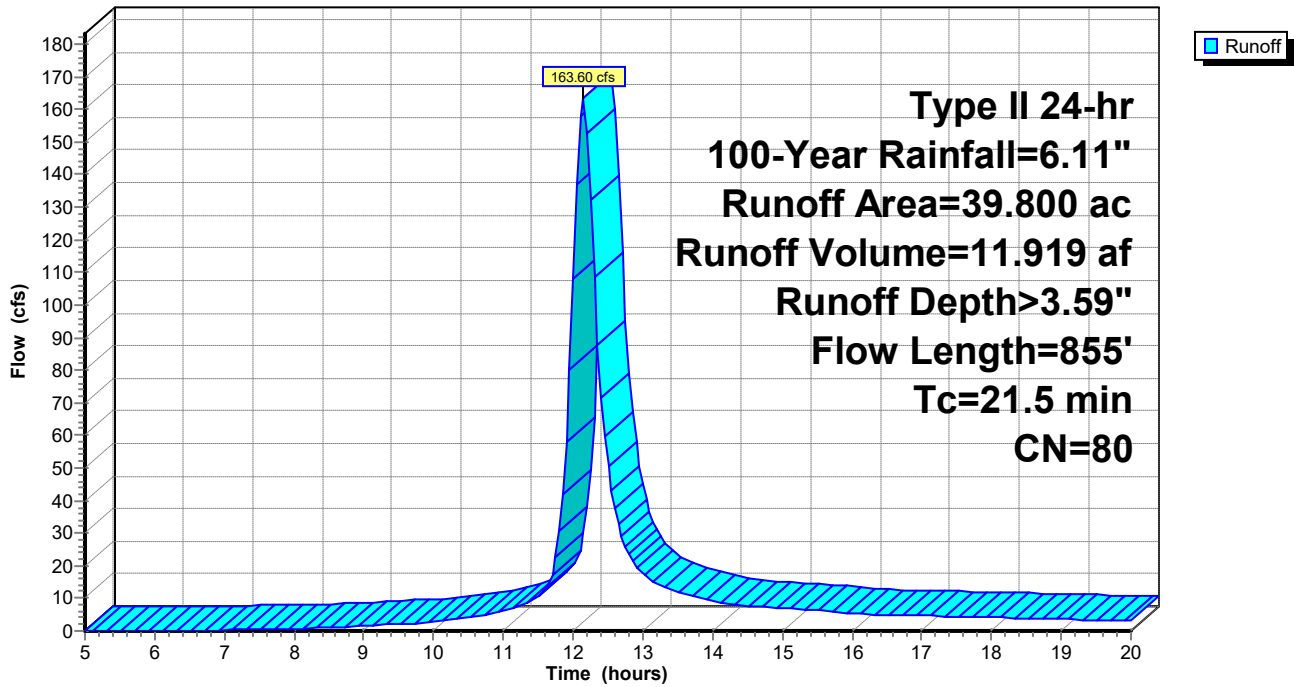
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
38.700	79	Woods, Fair, HSG D
* 1.100	98	Existing Railroad
39.800	80	Weighted Average
38.700		97.24% Pervious Area
1.100		2.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.5	150	0.1500	0.17		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
4.8	575	0.1600	2.00		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
2.2	130	0.0400	1.00		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
21.5	855	Total			

Subcatchment DR-A: Overland

Hydrograph



18641.00-Existing Condition

Type II 24-hr 100-Year Rainfall=6.11"

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Summary for Subcatchment DR-B: Overland

Runoff = 15.35 cfs @ 11.97 hrs, Volume= 0.702 af, Depth> 3.51"

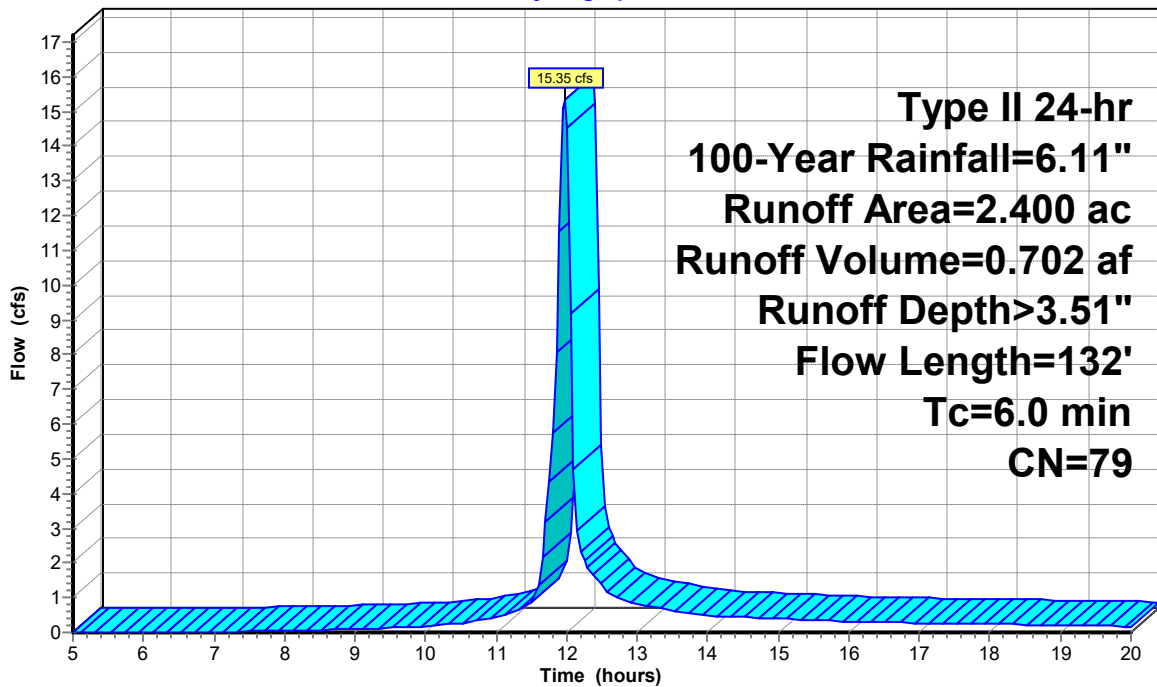
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
2.400	79	Woods, Fair, HSG D
2.400		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	132		0.37		Direct Entry, Sheet Flow

Subcatchment DR-B: Overland

Hydrograph



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Type II 24-hr 100-Year Rainfall=6.11"

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Summary for Subcatchment DR-C: Depression

Runoff = 193.14 cfs @ 11.97 hrs, Volume= 8.878 af, Depth> 3.61"

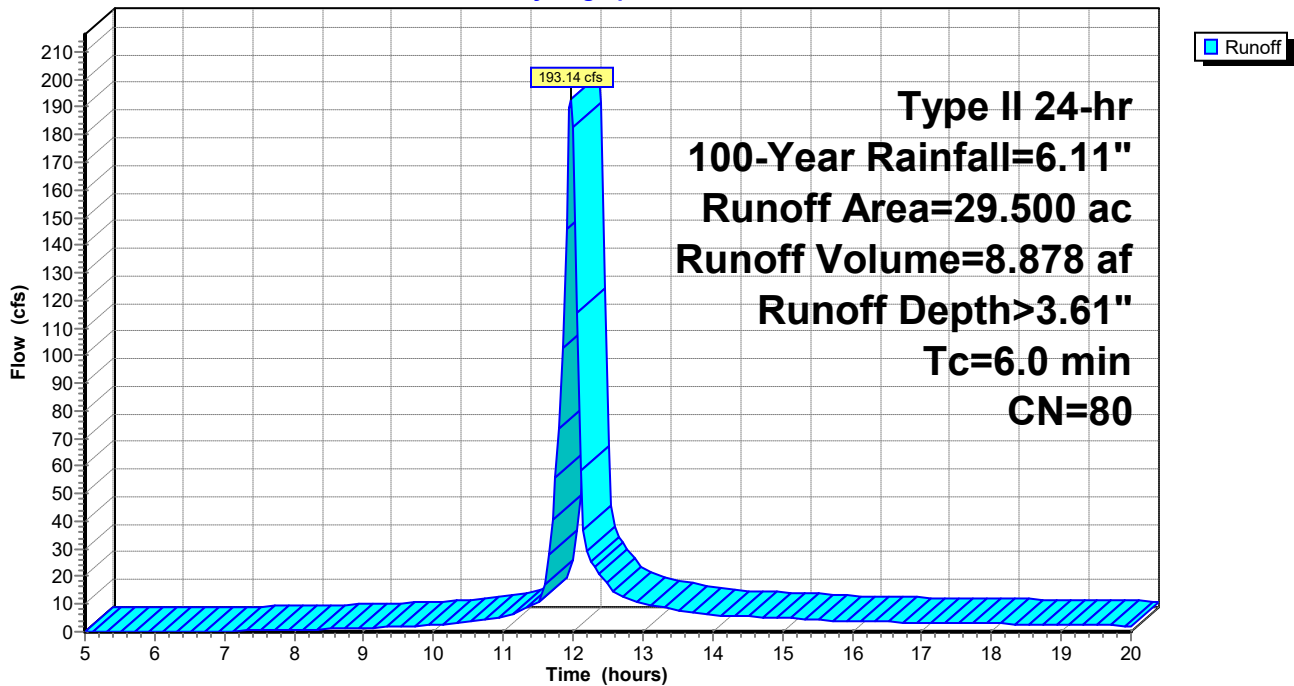
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
3.970	77	Brush, Fair, HSG D
2.500	96	Gravel surface, HSG D
23.030	79	Woods, Fair, HSG D
29.500	80	Weighted Average
29.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-C: Depression

Hydrograph



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Type II 24-hr 100-Year Rainfall=6.11"

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Summary for Subcatchment DR-D: Overland

Runoff = 14.49 cfs @ 12.90 hrs, Volume= 2.563 af, Depth> 3.42"

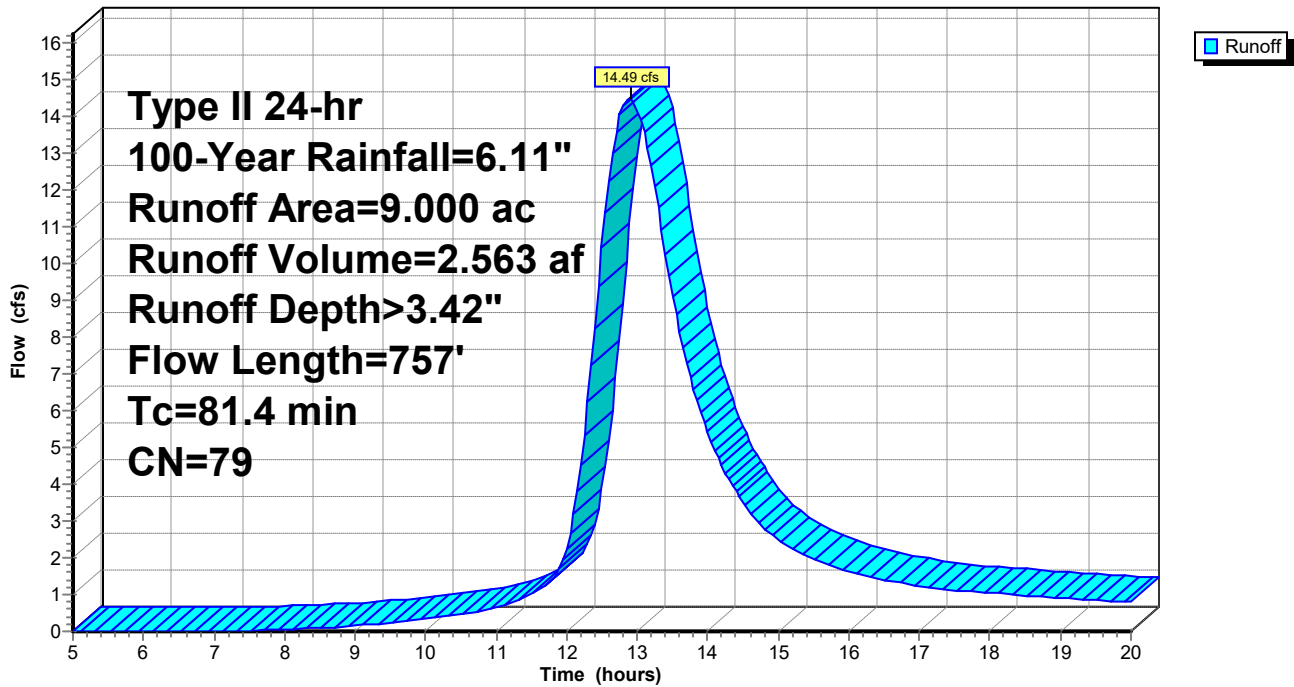
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
9.000	79	Woods, Fair, HSG D
9.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
56.6	150	0.0050	0.04		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
23.9	507	0.0050	0.35		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
0.9	100	0.1300	1.80		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
81.4	757	Total			

Subcatchment DR-D: Overland

Hydrograph



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Type II 24-hr 100-Year Rainfall=6.11"

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Summary for Subcatchment DR-E: Overland

Runoff = 40.67 cfs @ 12.34 hrs, Volume= 4.227 af, Depth> 3.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

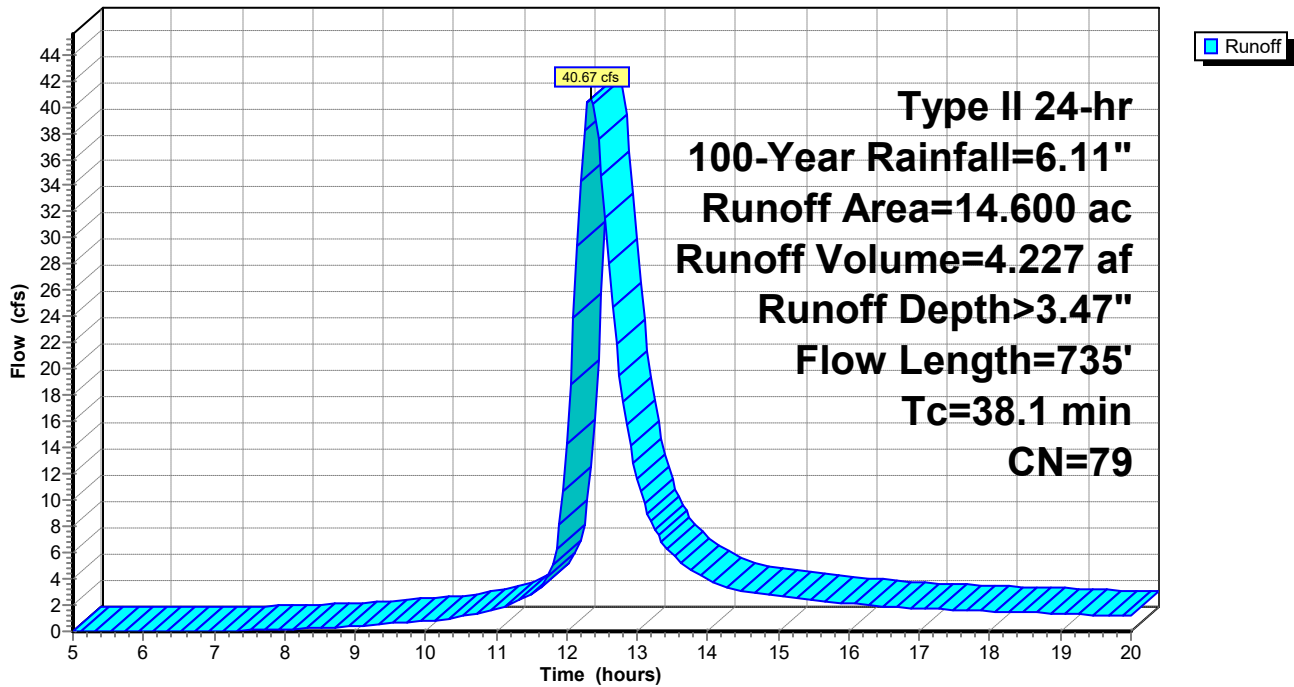
Area (ac)	CN	Description
14.600	79	Woods, Fair, HSG D
14.600		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
27.6	150	0.0300	0.09		Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 2.67"
9.8	510	0.0300	0.87		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps
0.7	75	0.1200	1.73		Shallow Concentrated Flow, Shallow Concentrated Woodland Kv= 5.0 fps

38.1 735 Total

Subcatchment DR-E: Overland

Hydrograph



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Type II 24-hr 100-Year Rainfall=6.11"

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Summary for Subcatchment DR-F: Overland

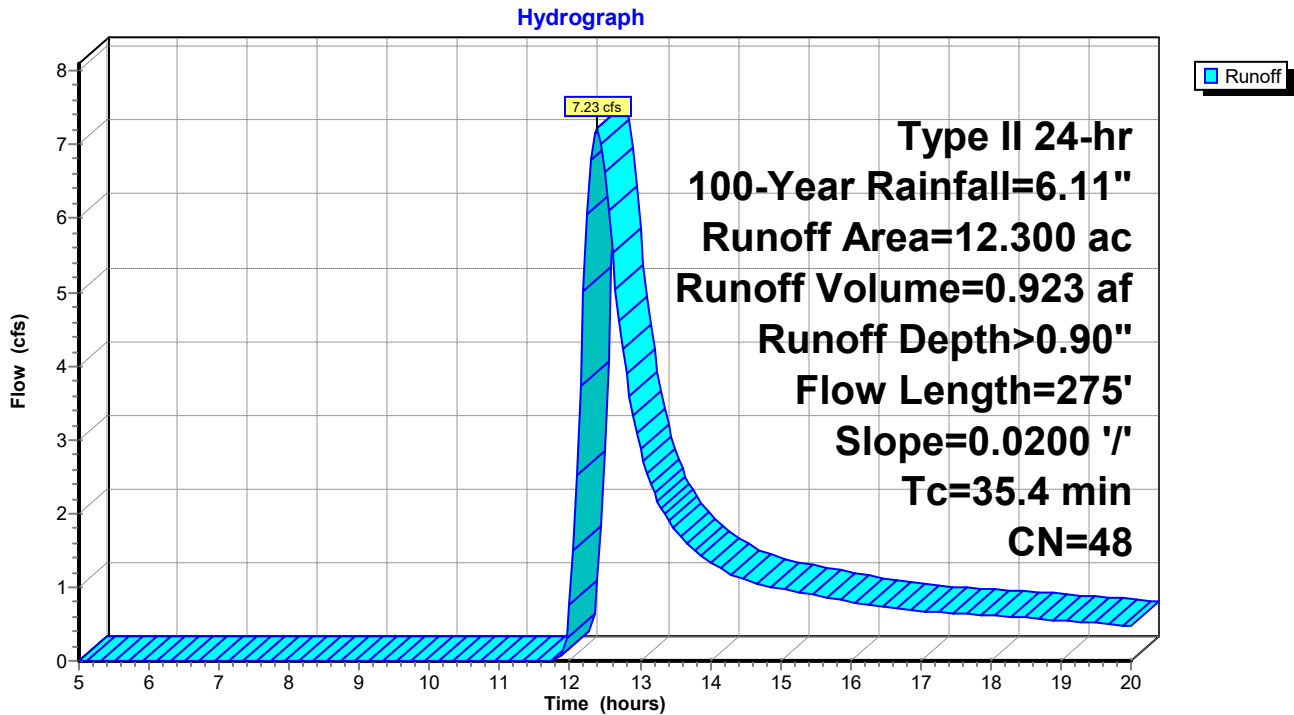
Runoff = 7.23 cfs @ 12.39 hrs, Volume= 0.923 af, Depth> 0.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 1.100	98	Pavement
11.200	43	Woods/grass comb., Fair, HSG A
12.300	48	Weighted Average
11.200		91.06% Pervious Area
1.100		8.94% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
32.5	150	0.0200	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.67"
2.9	125	0.0200	0.71		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
35.4	275	Total			

Subcatchment DR-F: Overland



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Summary for Subcatchment DR-G: Roadway

Runoff = 4.39 cfs @ 11.97 hrs, Volume= 0.198 af, Depth> 3.12"

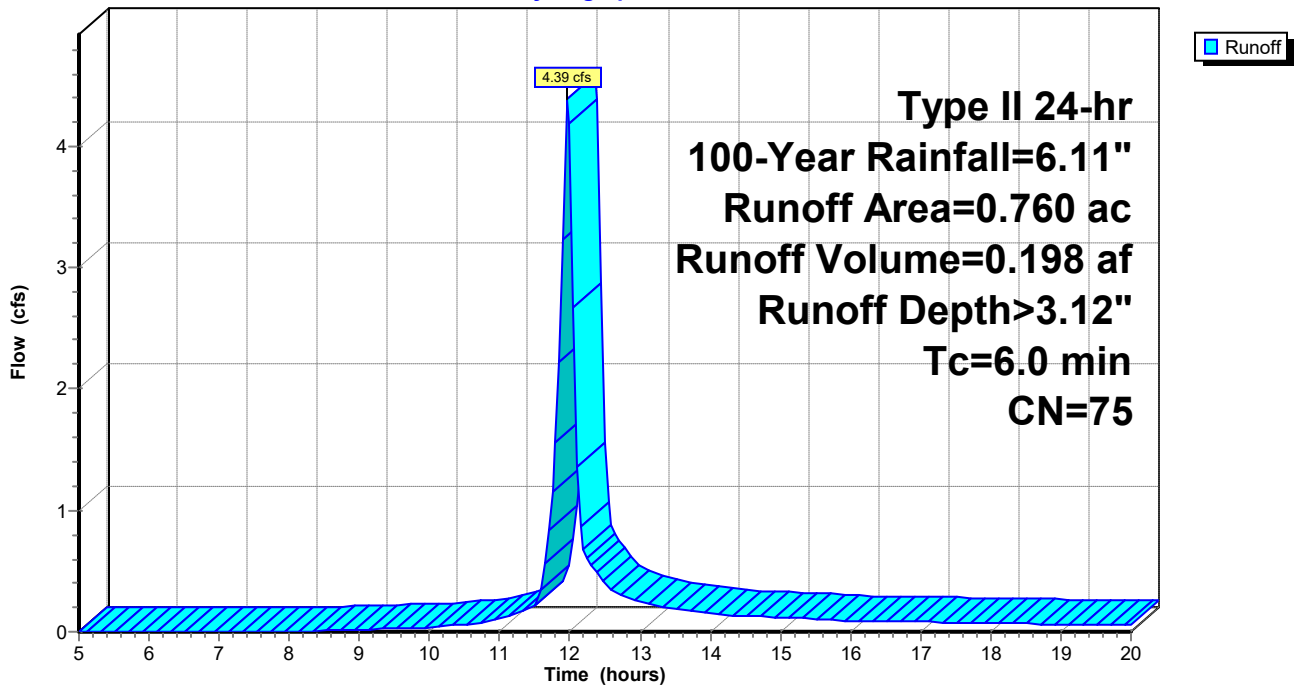
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 0.460	98	Roadway
0.300	39	>75% Grass cover, Good, HSG A
0.760	75	Weighted Average
0.300		39.47% Pervious Area
0.460		60.53% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-G: Roadway

Hydrograph



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Type II 24-hr 100-Year Rainfall=6.11"

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Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 3.59" for 100-Year event
Inflow = 163.60 cfs @ 12.14 hrs, Volume= 11.919 af
Outflow = 41.52 cfs @ 14.21 hrs, Volume= 9.967 af, Atten= 75%, Lag= 123.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Max. Velocity= 0.17 fps, Min. Travel Time= 98.2 min
Avg. Velocity = 0.08 fps, Avg. Travel Time= 203.6 min

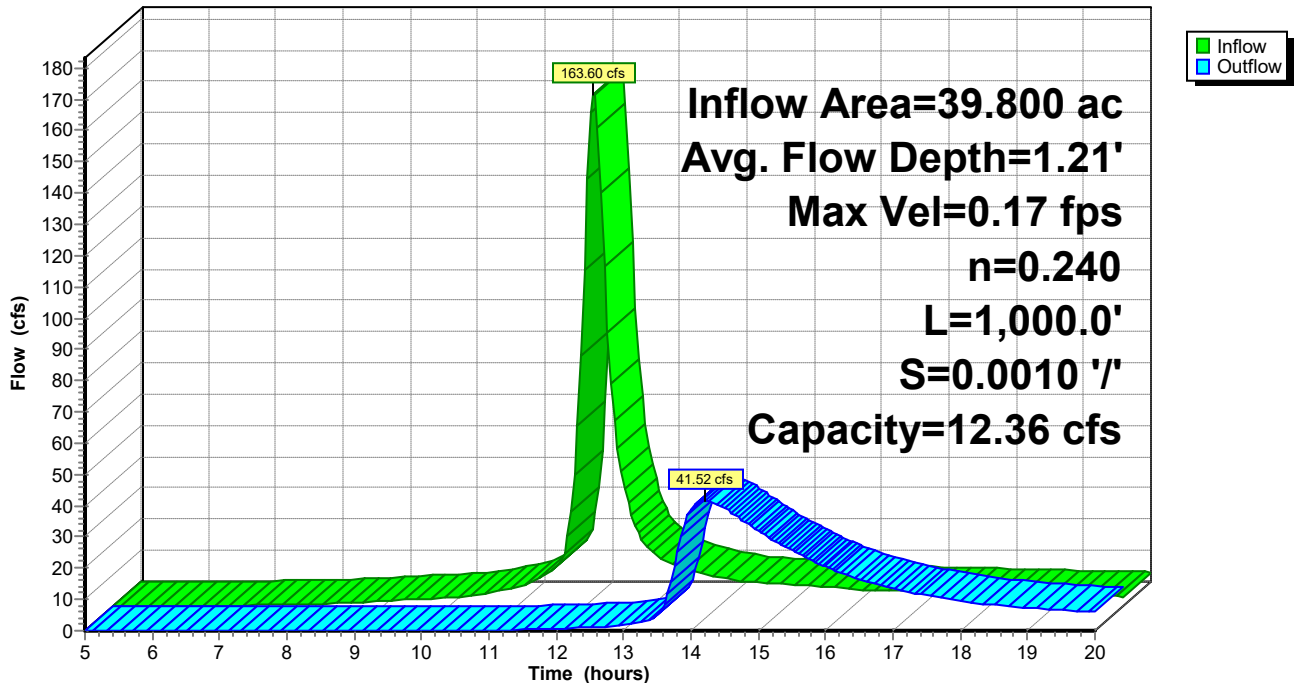
Peak Storage= 244,871 cf @ 12.57 hrs
Average Depth at Peak Storage= 1.21' , Surface Width= 207.26'
Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240 Sheet flow over Dense Grass
Side Slope Z-value= 3.0 '/' Top Width= 203.00'
Length= 1,000.0' Slope= 0.0010 '/'
Inlet Invert= 6.00', Outlet Invert= 5.00'



Reach 1W: Wetland #1 / Analysis Point 1A

Hydrograph



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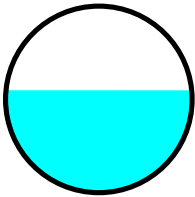
Summary for Reach 2R: Outlet Pipe

Inflow Area = 39.800 ac, 2.76% Impervious, Inflow Depth > 3.01" for 100-Year event
Inflow = 41.52 cfs @ 14.21 hrs, Volume= 9.967 af
Outflow = 41.52 cfs @ 14.21 hrs, Volume= 9.964 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Max. Velocity= 8.44 fps, Min. Travel Time= 0.1 min
Avg. Velocity = 4.38 fps, Avg. Travel Time= 0.3 min

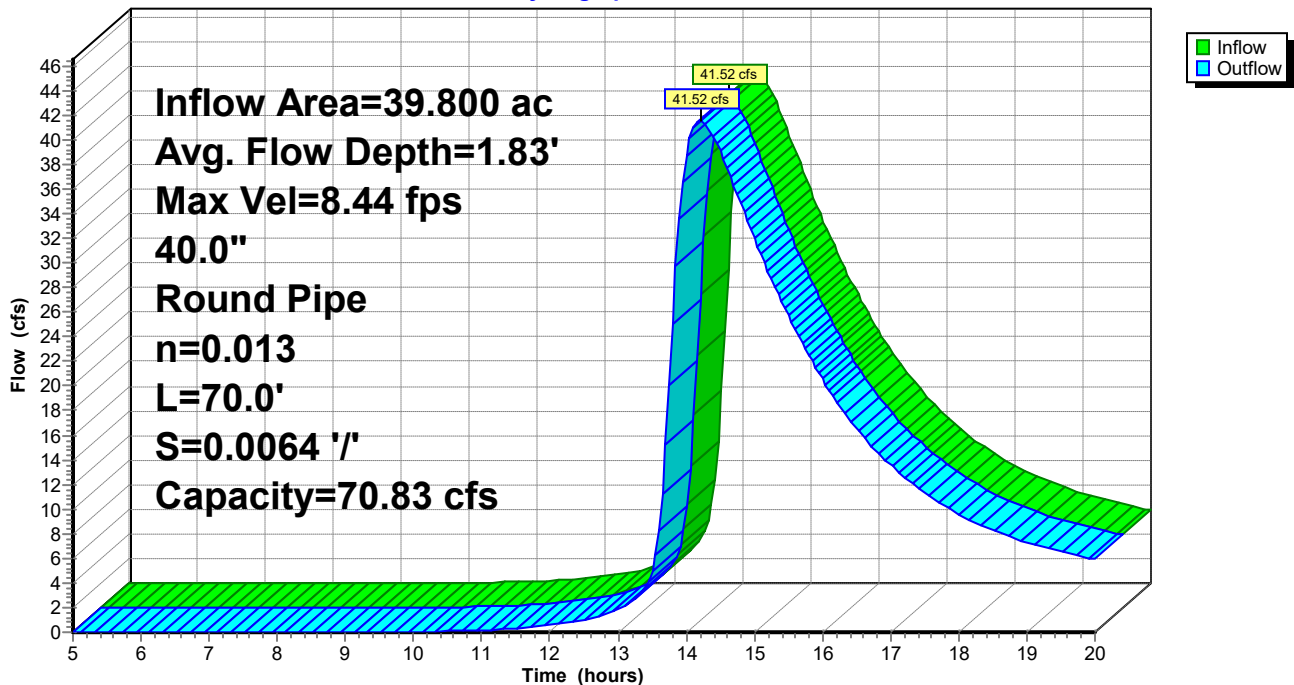
Peak Storage= 345 cf @ 14.21 hrs
Average Depth at Peak Storage= 1.83' , Surface Width= 3.32'
Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe
n= 0.013 Corrugated PE, smooth interior
Length= 70.0' Slope= 0.0064 '/'
Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 2R: Outlet Pipe

Hydrograph



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Type II 24-hr 100-Year Rainfall=6.11"

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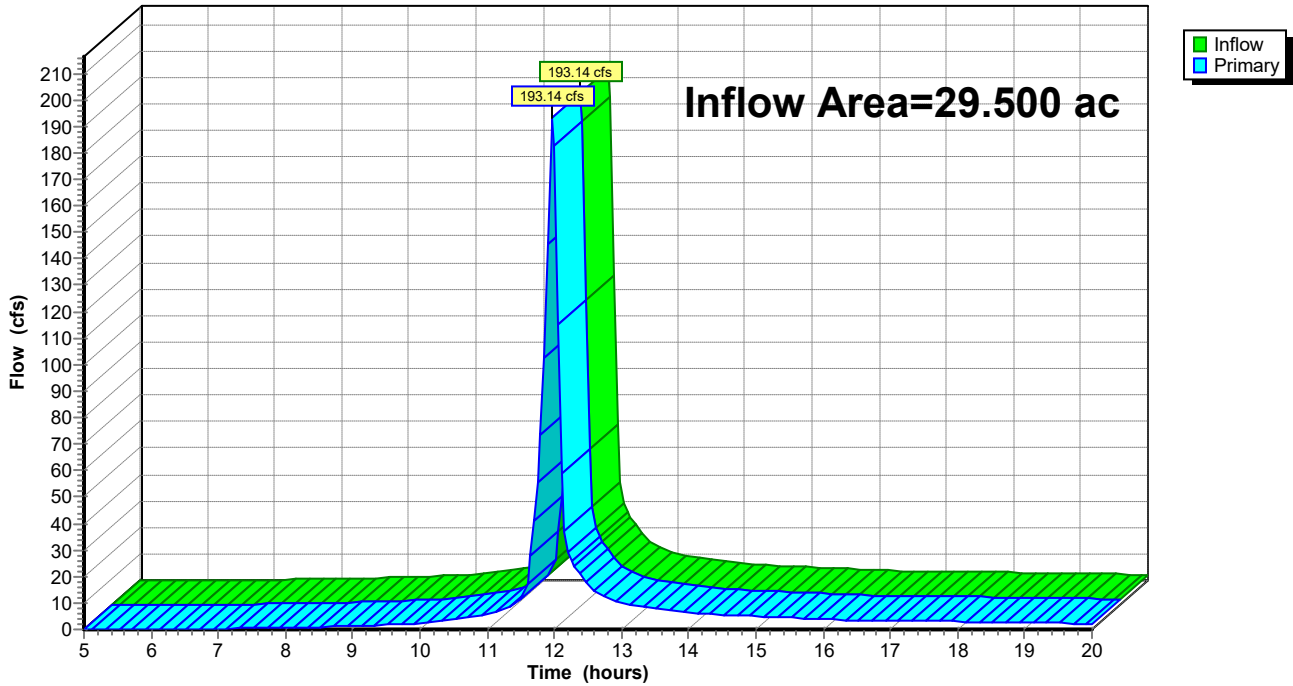
Summary for Pond 1P: Infiltration

Inflow Area = 29.500 ac, 0.00% Impervious, Inflow Depth > 3.61" for 100-Year event
Inflow = 193.14 cfs @ 11.97 hrs, Volume= 8.878 af
Primary = 193.14 cfs @ 11.97 hrs, Volume= 8.878 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond 1P: Infiltration

Hydrograph



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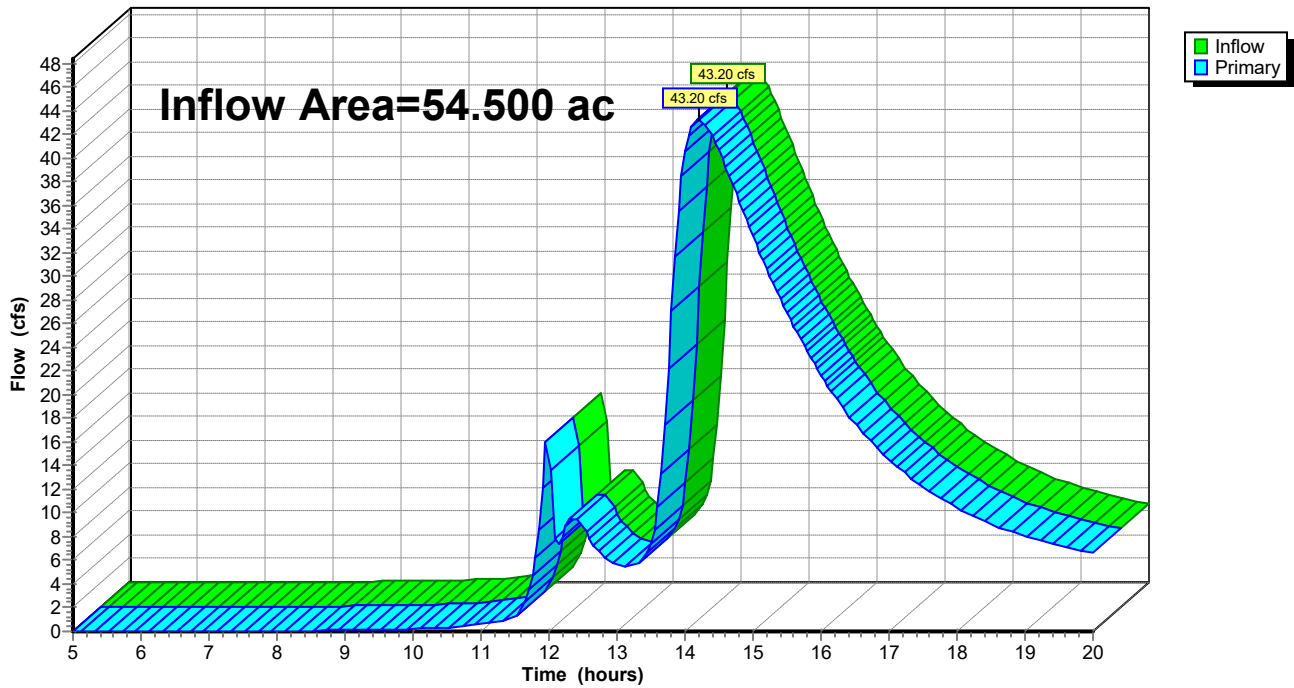
Summary for Pond AP-1: Analysis Point #1

Inflow Area = 54.500 ac, 4.04% Impervious, Inflow Depth > 2.55" for 100-Year event
Inflow = 43.20 cfs @ 14.20 hrs, Volume= 11.589 af
Primary = 43.20 cfs @ 14.20 hrs, Volume= 11.589 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1

Hydrograph



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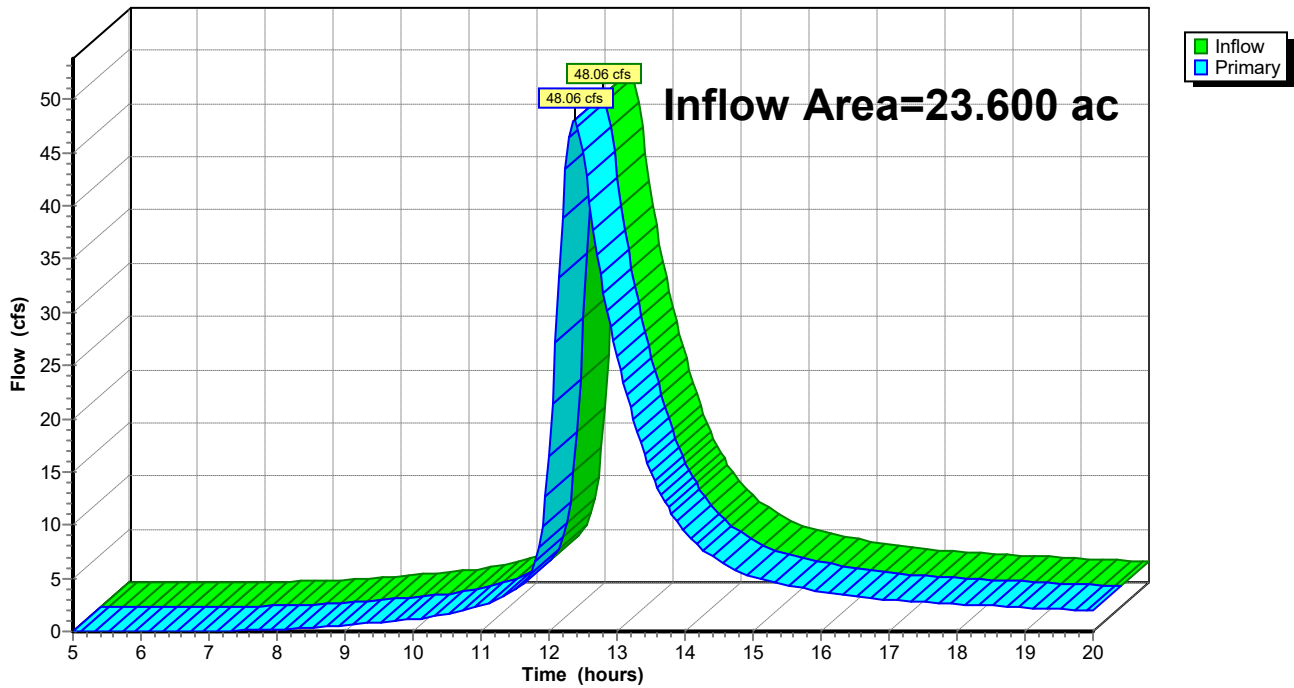
Summary for Pond AP-2: Analysis Point #2

Inflow Area = 23.600 ac, 0.00% Impervious, Inflow Depth > 3.45" for 100-Year event
Inflow = 48.06 cfs @ 12.38 hrs, Volume= 6.789 af
Primary = 48.06 cfs @ 12.38 hrs, Volume= 6.789 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2

Hydrograph



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Type II 24-hr 100-Year Rainfall=6.11"

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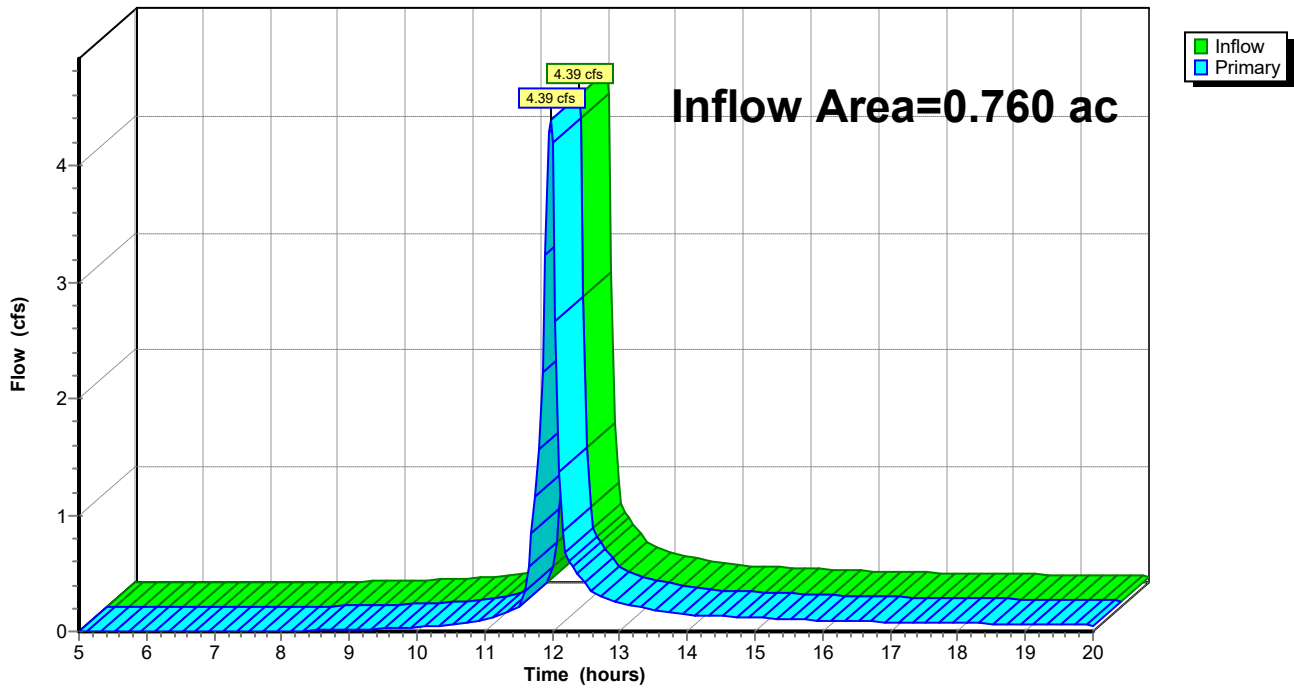
Summary for Pond AP-3: Analysis Point #3

Inflow Area = 0.760 ac, 60.53% Impervious, Inflow Depth > 3.12" for 100-Year event
Inflow = 4.39 cfs @ 11.97 hrs, Volume= 0.198 af
Primary = 4.39 cfs @ 11.97 hrs, Volume= 0.198 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3

Hydrograph



Appendix B

Proposed Conditions Drainage Map and HydroCAD Report



McFarland Johnson
 60 RAILROAD PLACE
 SUITE 402
 SARATOGA SPRINGS, NEW YORK 12866
 P:518-580-9380 F:518-580-9383
 SaratogaROM@mjinc.com

PROJECT MILESTONE
NFC

NO.	DATE	DESCRIPTION
1	05/20/22	TOWN COMMENTS

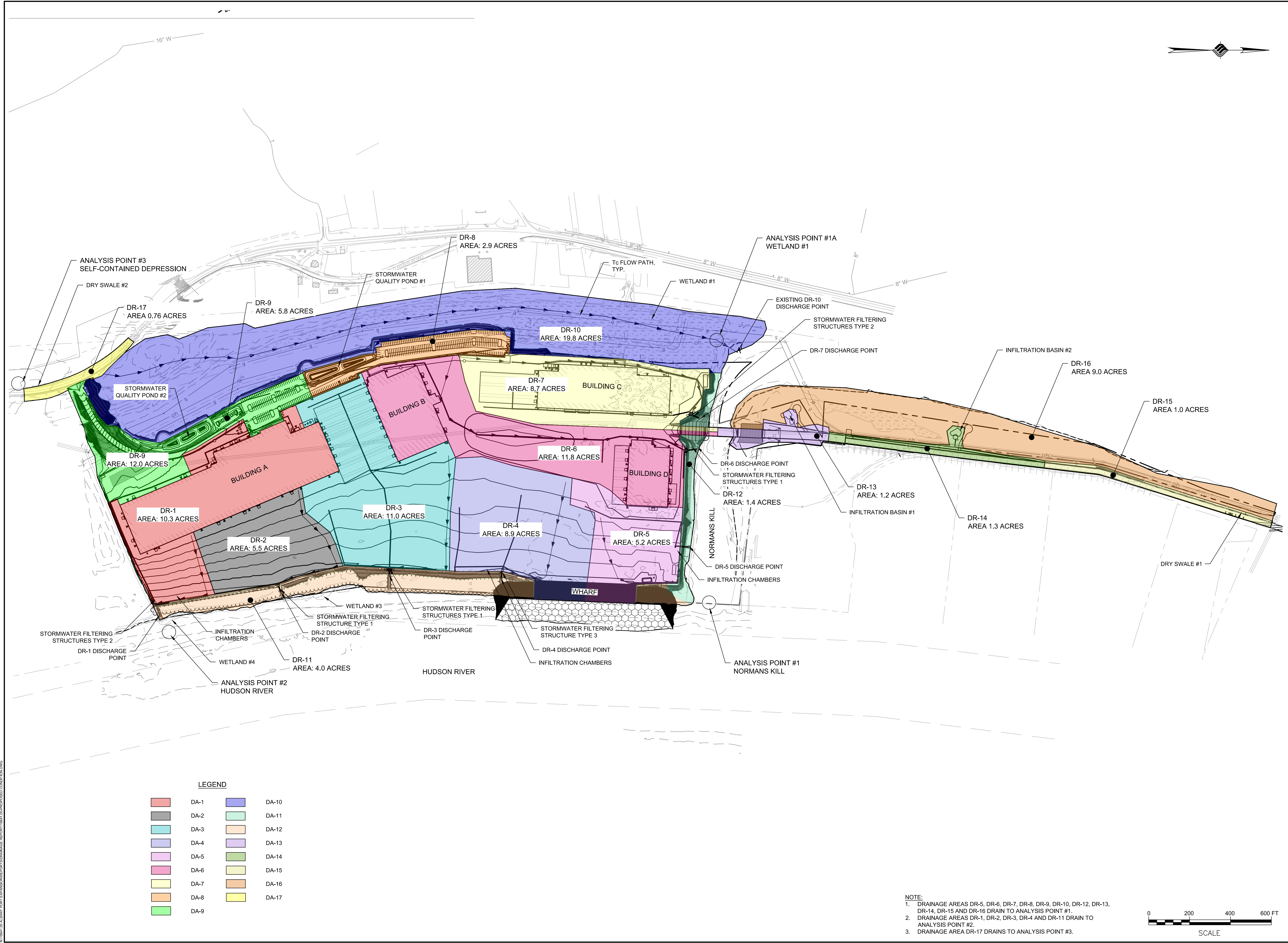
CLIENT:
ALBANY PORT DISTRICT COMMISSION
 TOWN OF BETHLEHEM, NEW YORK
 PROJECT:
PORT OF ALBANY SITE INFRASTRUCTURE IMPROVEMENTS

DRAWN	NSO
DESIGNED	NSO
CHECKED	AJF
SCALE	1" = 200'
DATE	MAY 2022
PROJECT	18641.00

IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECT DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR, TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION.

DRAWING TITLE
POST-DEVELOPMENT SITE DRAINAGE AREAS

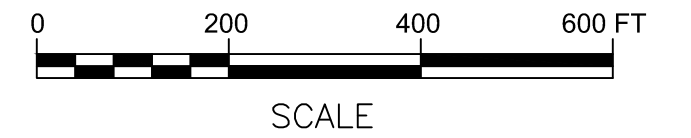
DRAWING NUMBER
DR-PR
 01 OF 01



LEGEND

DA-1	DA-10
DA-2	DA-11
DA-3	DA-12
DA-4	DA-13
DA-5	DA-14
DA-6	DA-15
DA-7	DA-16
DA-8	DA-17
DA-9	

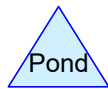
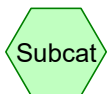
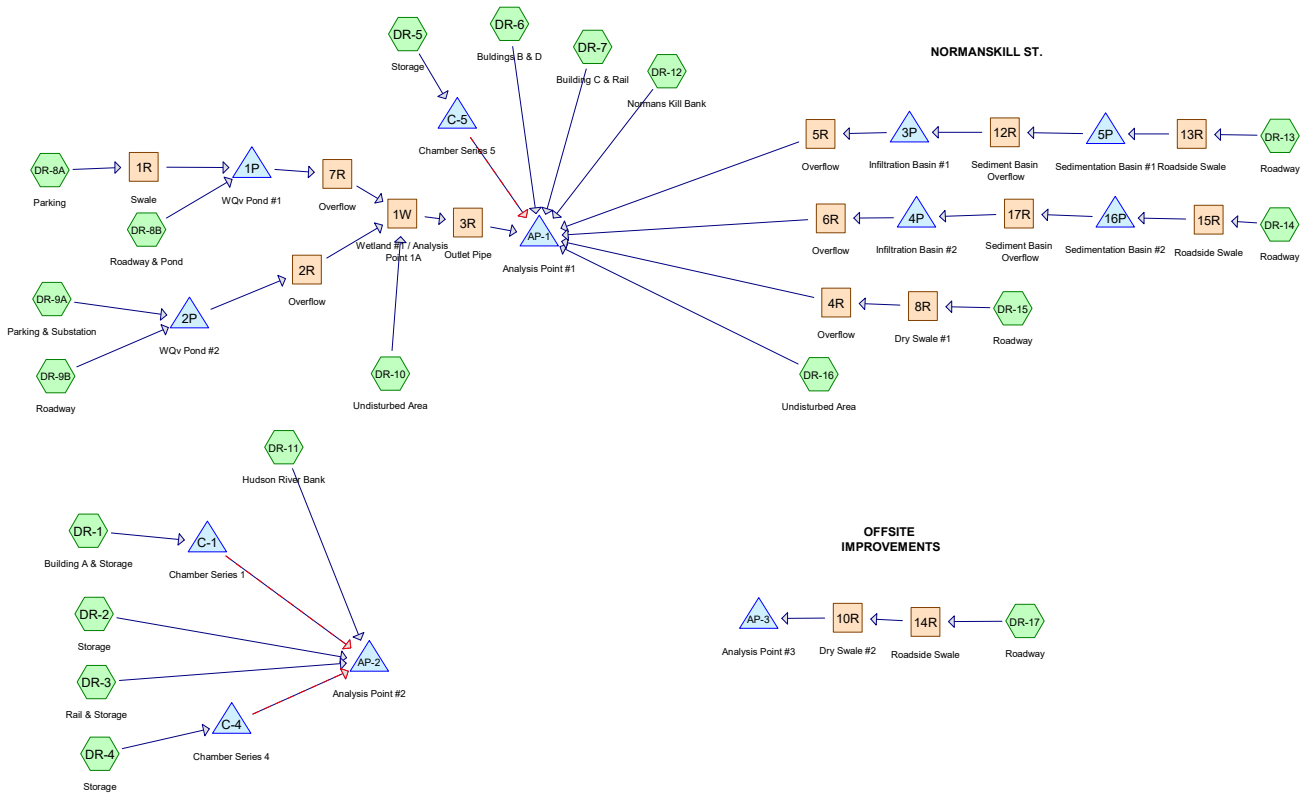
NOTE:
 1. DRAINAGE AREAS DR-5, DR-6, DR-7, DR-8, DR-9, DR-10, DR-12, DR-13, DR-14, DR-15 AND DR-16 DRAIN TO ANALYSIS POINT #1.
 2. DRAINAGE AREAS DR-1, DR-2, DR-3, DR-4 AND DR-11 DRAIN TO ANALYSIS POINT #2.
 3. DRAINAGE AREA DR-17 DRAINS TO ANALYSIS POINT #3.



N:\18641_00\ALBANY PORT DISTRICT COMMISSION\REPORTS\DRAINAGE IMPROVEMENTS\18641.DWG

EXPANSION SITE

NORMANSKILL ST.



Routing Diagram for 18641.00-Proposed Condition Chambers_CULVERTS_AJF
 Prepared by McFarland Johnson, Printed 6/8/2022
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18641.00-Proposed Condition_Chambers_CULVERTS_AJF

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Page 2

Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	1-Year	Type II 24-hr		Default	24.00	1	2.20	2
2	10-Year	Type II 24-hr		Default	24.00	1	3.63	2
3	100-Year	Type II 24-hr		Default	24.00	1	6.11	2

18641.00-Proposed Condition_Chambers_CULVERTS_AJF

Prepared by McFarland Johnson

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
1.510	39	>75% Grass cover, Good, HSG A (DR-13, DR-14, DR-15, DR-17)
5.500	80	>75% Grass cover, Good, HSG D (DR-1, DR-2, DR-3, DR-4, DR-5, DR-6, DR-7, DR-8A, DR-8B, DR-9A, DR-9B)
6.870	98	Building A (DR-1)
2.549	98	Building B (DR-6)
3.030	98	Building C (DR-7)
1.413	98	Building D (DR-6)
16.900	95	Compacted Gravel (DR-3, DR-4)
0.200	92	Compacted Gravel (DR-9A)
26.618	95	Dense Graded Aggregate (DR-1, DR-2, DR-5, DR-6, DR-7, DR-9B)
0.970	96	Gravel surface, HSG D (DR-12)
1.100	98	Mill & Fill of Old Pavement (DR-14, DR-15)
0.600	98	New Pavement (DR-14, DR-15)
1.600	98	Parking (DR-8A)
1.200	98	Parking and Road (DR-9A)
0.450	98	Pavement (DR-13)
3.270	98	Rail (DR-3, DR-7)
0.140	98	Road Widening (DR-17)
1.240	98	Roadway (DR-17, DR-8B, DR-9B)
0.170	98	Substation (DR-9A)
24.230	79	Woods, Fair, HSG D (DR-10, DR-11, DR-12)
9.000	43	Woods/grass comb., Fair, HSG A (DR-16)
108.560	86	TOTAL AREA

Summary for Subcatchment DR-1: Building A & Storage

Runoff = 29.34 cfs @ 11.98 hrs, Volume= 1.592 af, Depth> 1.85"

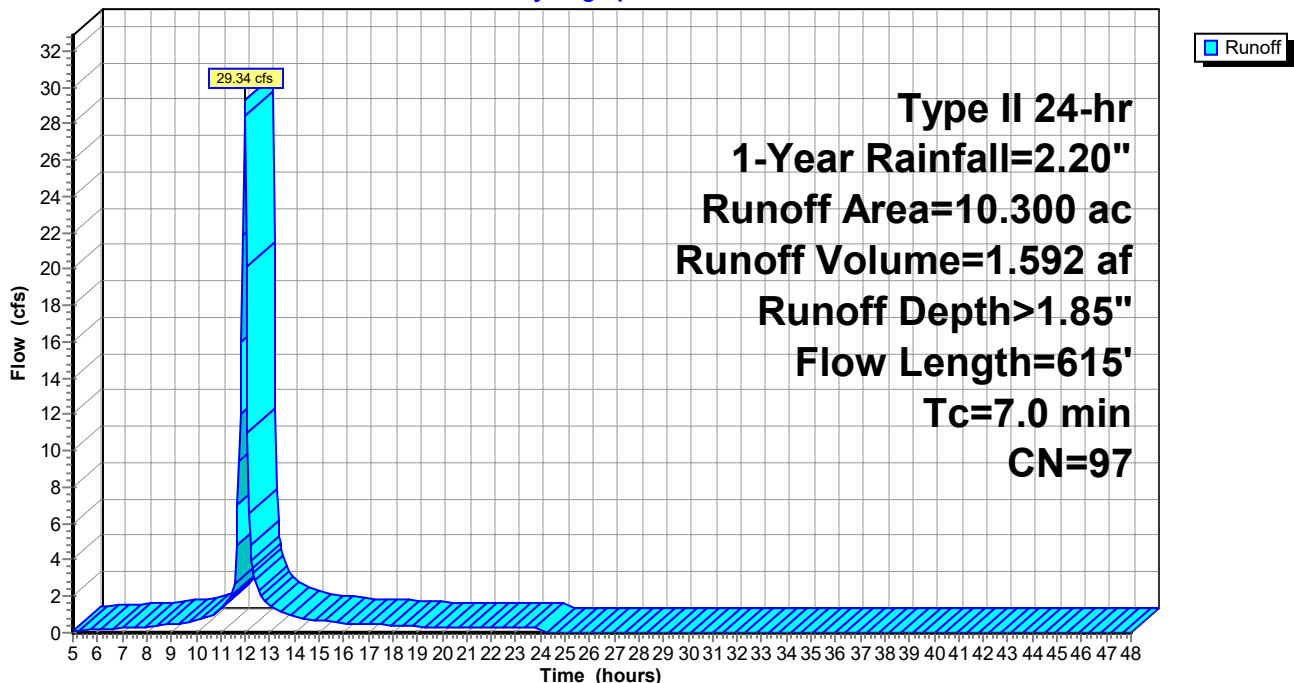
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 6.870	98	Building A
0.100	80	>75% Grass cover, Good, HSG D
* 3.330	95	Dense Graded Aggregate
10.300	97	Weighted Average
3.430		33.30% Pervious Area
6.870		66.70% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
3.1	300	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	215	0.0050	5.91	29.00	Pipe Channel, 30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63' n= 0.013
7.0	615	Total			

Subcatchment DR-1: Building A & Storage

Hydrograph



Summary for Subcatchment DR-10: Undisturbed Area

Runoff = 4.00 cfs @ 13.29 hrs, Volume= 1.061 af, Depth= 0.64"

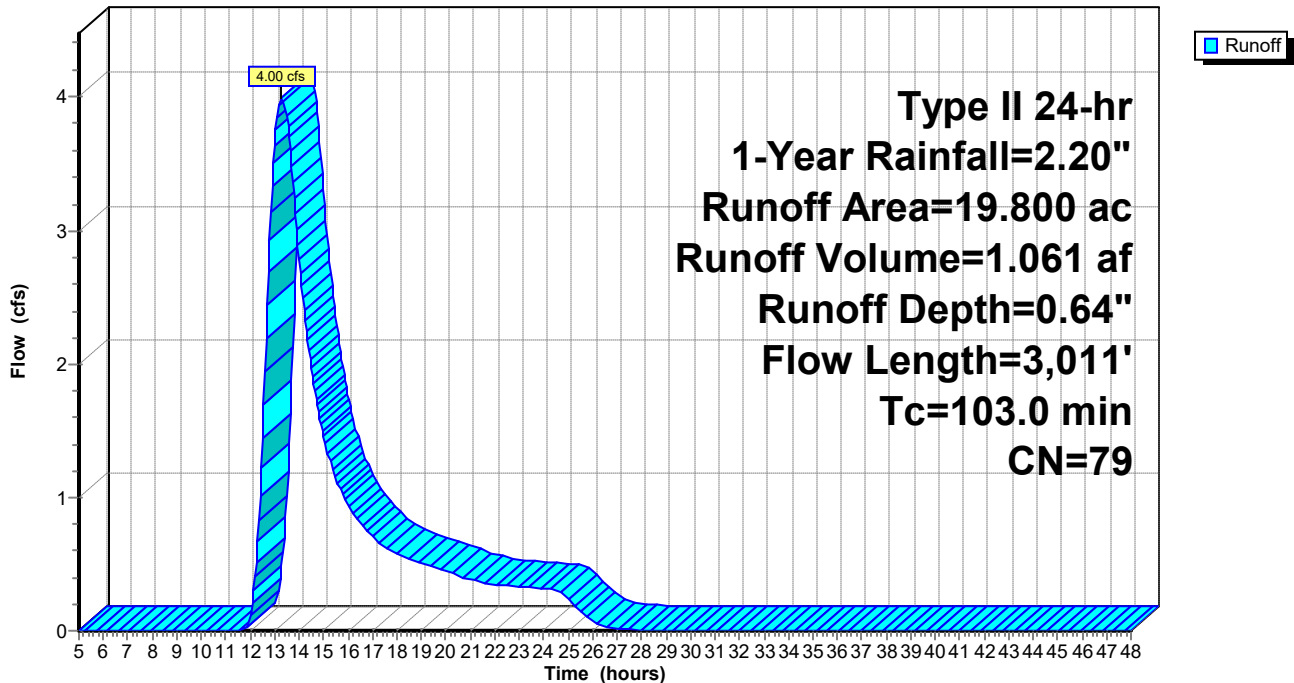
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
19.800	79	Woods, Fair, HSG D
19.800		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
19.7	150	0.0800	0.13		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"
3.0	200	0.0500	1.12		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
1.6	250	0.2600	2.55		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
78.7	2,361	0.0100	0.50		Shallow Concentrated Flow, Wetland Flow Woodland Kv= 5.0 fps
0.0	50	0.0500	22.86	161.57	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.012 Corrugated PP, smooth interior
103.0	3,011	Total			

Subcatchment DR-10: Undisturbed Area

Hydrograph



Summary for Subcatchment DR-11: Hudson River Bank

Runoff = 3.01 cfs @ 12.10 hrs, Volume= 0.214 af, Depth= 0.64"

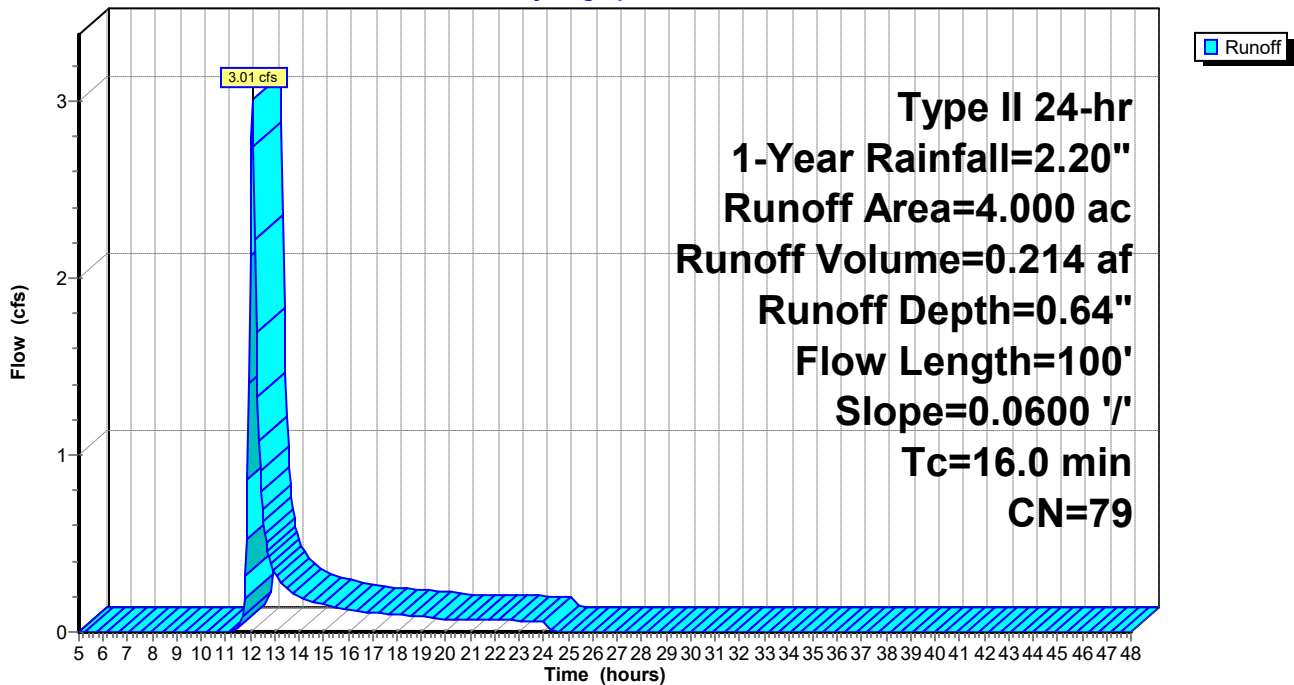
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
4.000	79	Woods, Fair, HSG D
4.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.0	100	0.0600	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-11: Hudson River Bank

Hydrograph



Summary for Subcatchment DR-12: Normans Kill Bank

Runoff = 3.18 cfs @ 11.97 hrs, Volume= 0.156 af, Depth= 1.34"

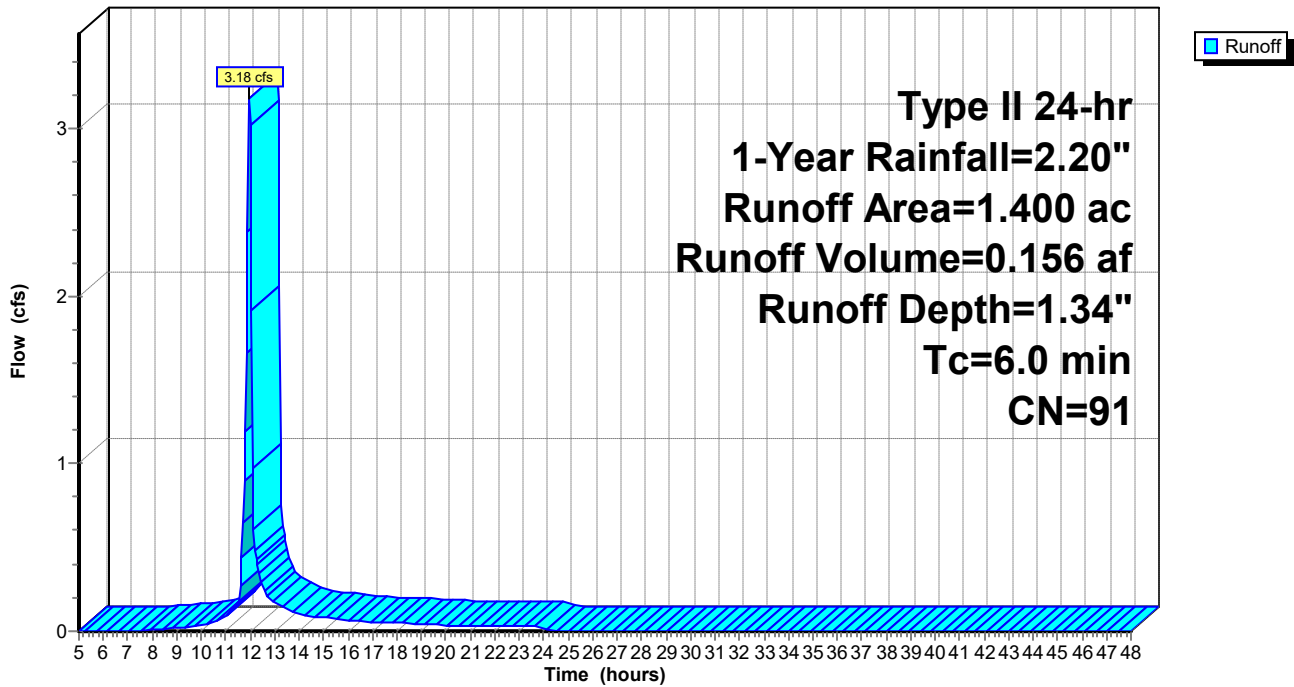
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
0.430	79	Woods, Fair, HSG D
0.970	96	Gravel surface, HSG D
1.400	91	Weighted Average
1.400		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-12: Normans Kill Bank

Hydrograph



Summary for Subcatchment DR-13: Roadway

Runoff = 0.05 cfs @ 12.05 hrs, Volume= 0.012 af, Depth= 0.12"

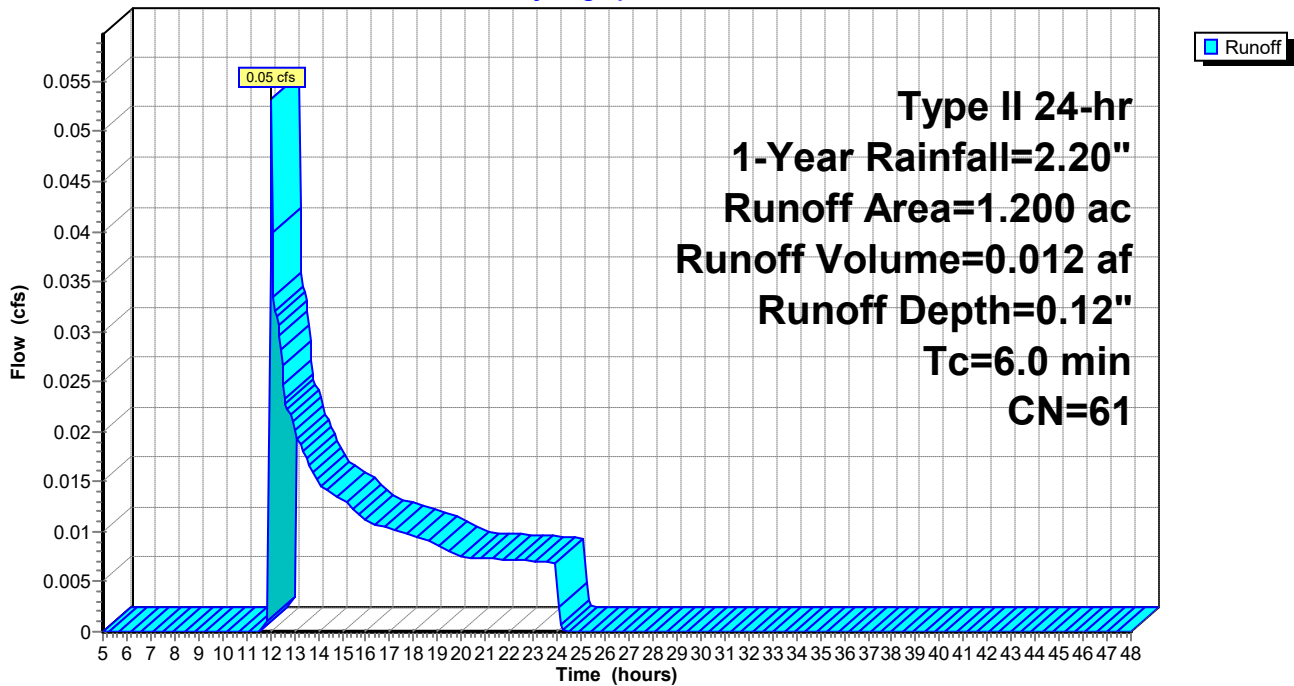
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 0.450	98	Pavement
0.750	39	>75% Grass cover, Good, HSG A
1.200	61	Weighted Average
0.750		62.50% Pervious Area
0.450		37.50% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-13: Roadway

Hydrograph



Summary for Subcatchment DR-14: Roadway

Runoff = 0.84 cfs @ 11.99 hrs, Volume= 0.045 af, Depth= 0.41"

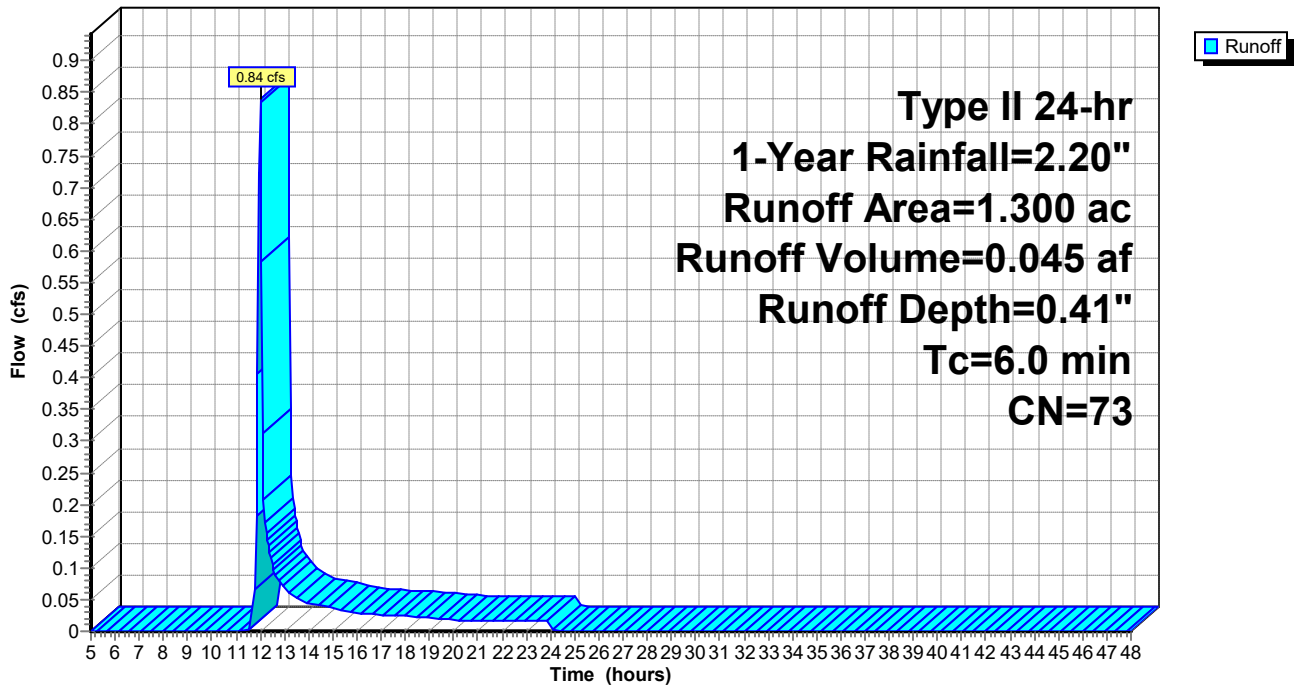
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 0.550	98	New Pavement
0.550	39	>75% Grass cover, Good, HSG A
* 0.200	98	Mill & Fill of Old Pavement
1.300	73	Weighted Average
0.550		42.31% Pervious Area
0.750		57.69% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-14: Roadway

Hydrograph



Summary for Subcatchment DR-15: Roadway

Runoff = 2.72 cfs @ 11.96 hrs, Volume= 0.139 af, Depth> 1.67"

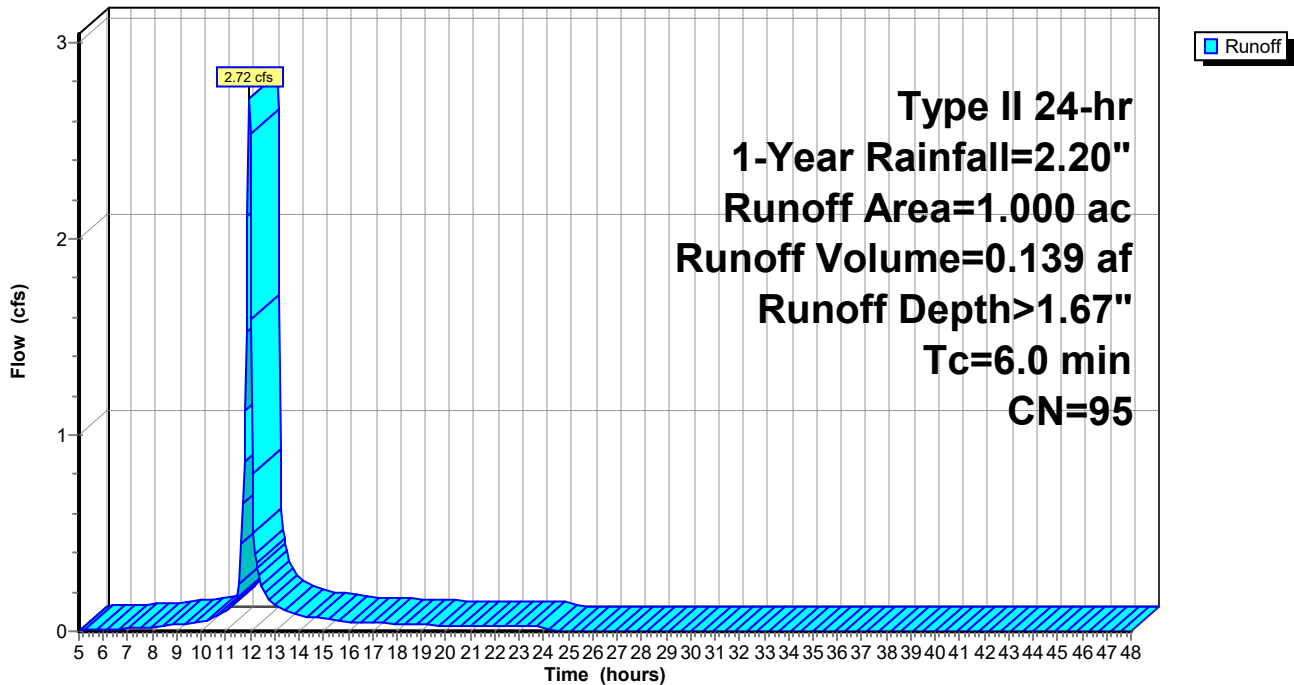
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 0.050	98	New Pavement
0.050	39	>75% Grass cover, Good, HSG A
* 0.900	98	Mill & Fill of Old Pavement
1.000	95	Weighted Average
0.050		5.00% Pervious Area
0.950		95.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-15: Roadway

Hydrograph



Summary for Subcatchment DR-16: Undisturbed Area

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

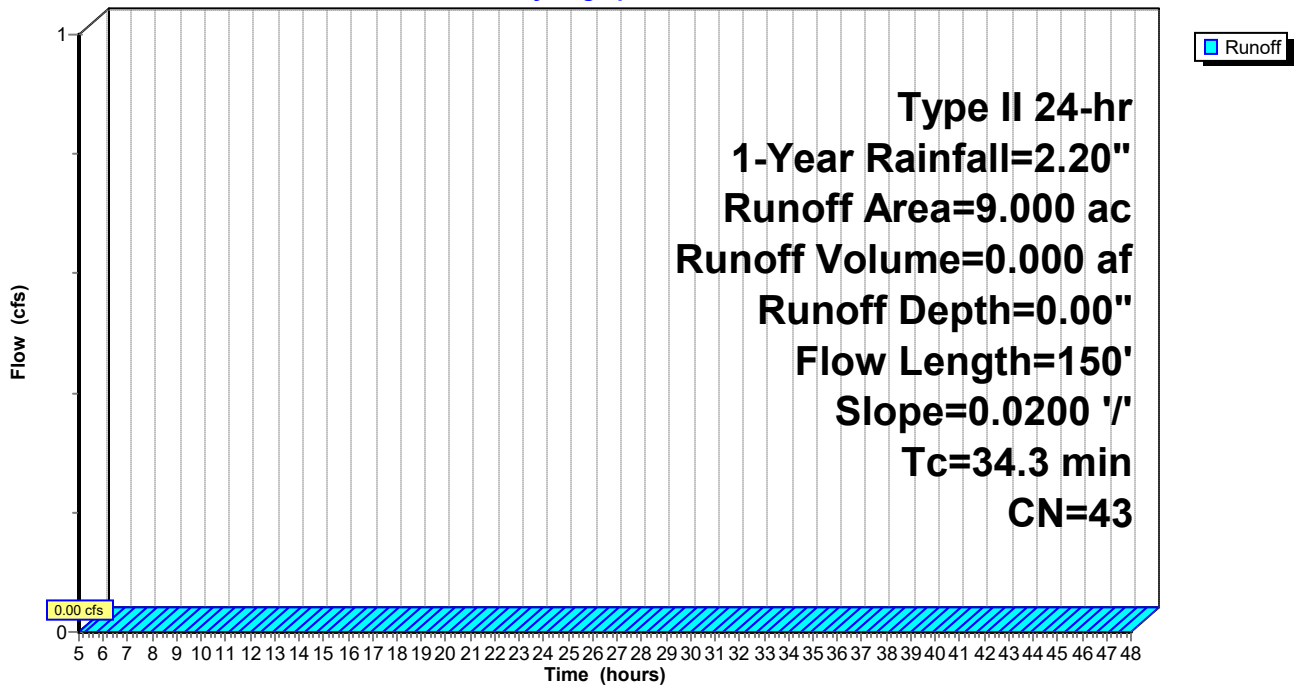
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
9.000	43	Woods/grass comb., Fair, HSG A
9.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
34.3	150	0.0200	0.07		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-16: Undisturbed Area

Hydrograph



Summary for Subcatchment DR-17: Roadway

Runoff = 1.32 cfs @ 11.97 hrs, Volume= 0.064 af, Depth= 1.00"

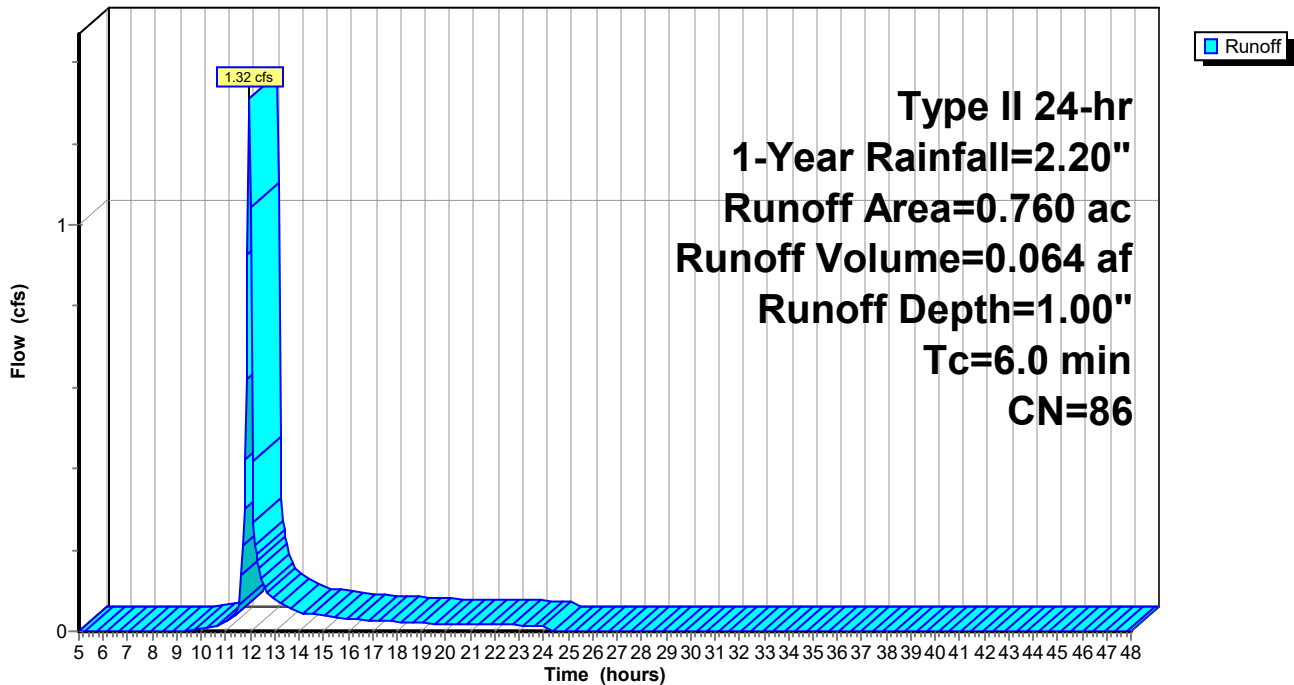
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 0.140	98	Road Widening
* 0.460	98	Roadway
0.160	39	>75% Grass cover, Good, HSG A
0.760	86	Weighted Average
0.160		21.05% Pervious Area
0.600		78.95% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-17: Roadway

Hydrograph



Summary for Subcatchment DR-2: Storage

Runoff = 13.32 cfs @ 12.00 hrs, Volume= 0.726 af, Depth> 1.58"

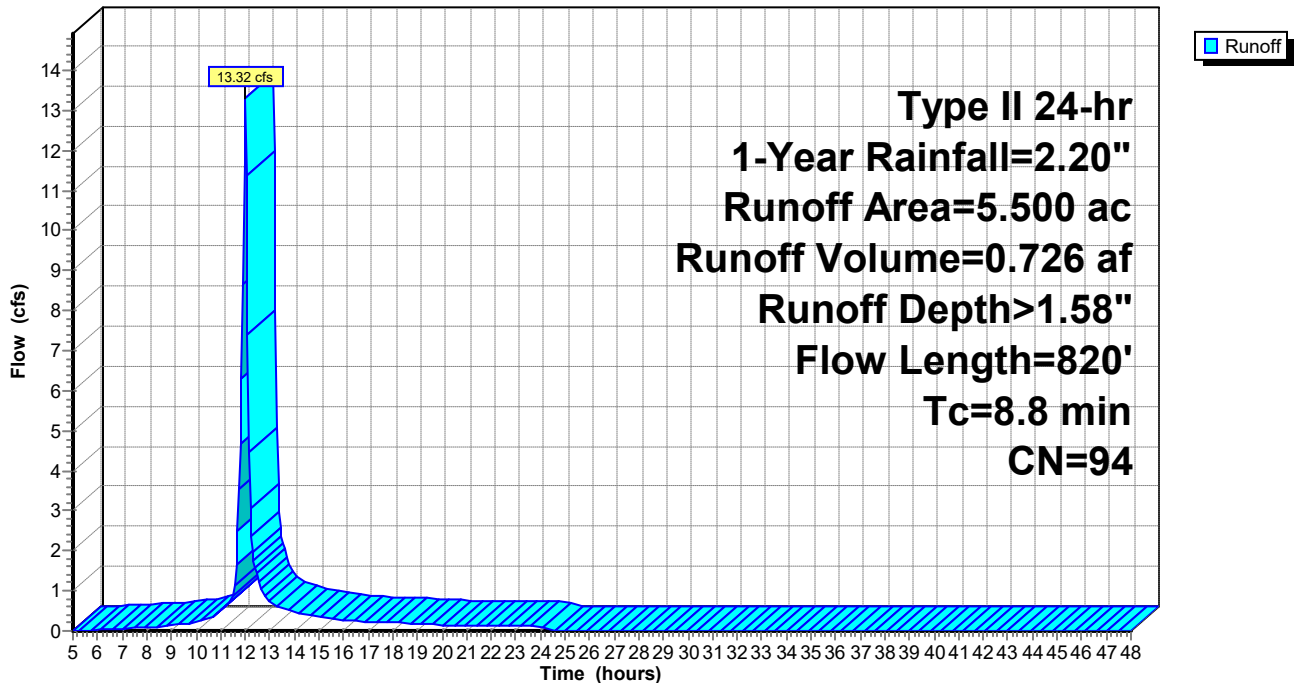
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 5.300	95	Dense Graded Aggregate
0.200	80	>75% Grass cover, Good, HSG D
5.500	94	Weighted Average
5.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
4.9	470	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	250	0.0050	6.67	47.16	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.013
8.8	820	Total			

Subcatchment DR-2: Storage

Hydrograph



Summary for Subcatchment DR-3: Rail & Storage

Runoff = 27.00 cfs @ 12.01 hrs, Volume= 1.533 af, Depth> 1.67"

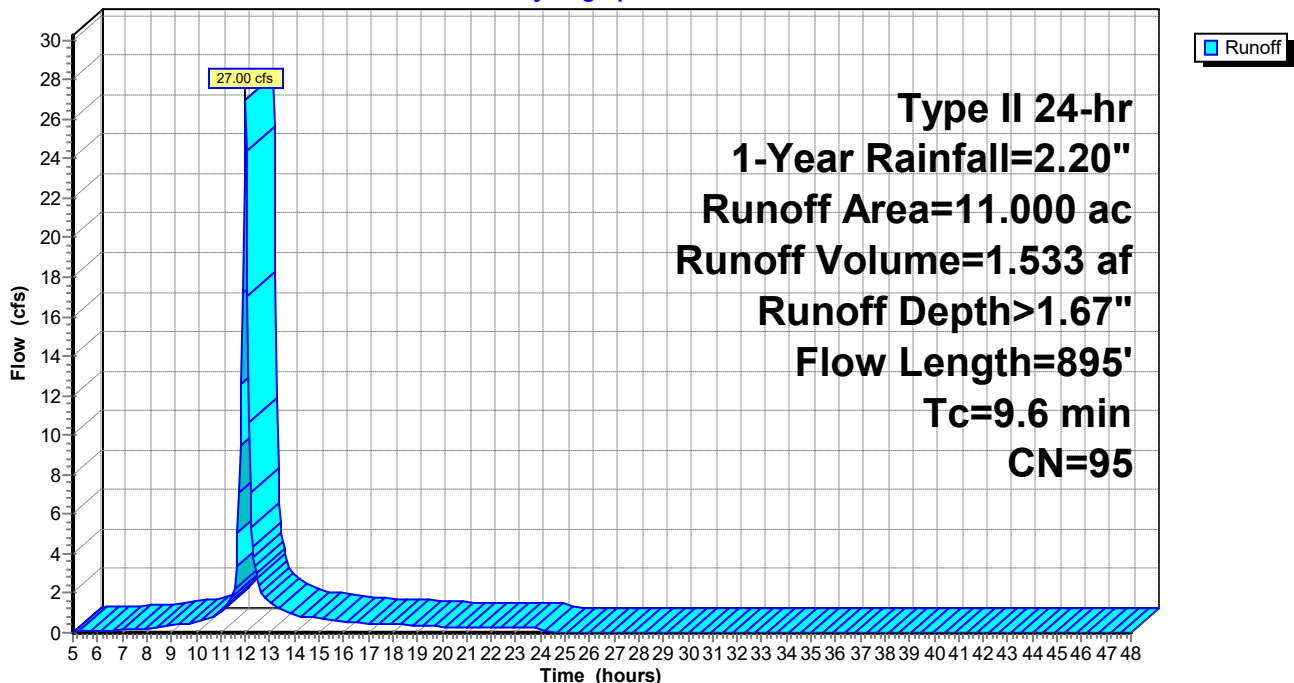
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 8.300	95	Compacted Gravel
0.400	80	>75% Grass cover, Good, HSG D
* 2.300	98	Rail
11.000	95	Weighted Average
8.700		79.09% Pervious Area
2.300		20.91% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
5.4	525	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.9	270	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
9.6	895	Total			

Subcatchment DR-3: Rail & Storage

Hydrograph



Summary for Subcatchment DR-4: Storage

Runoff = 22.13 cfs @ 11.99 hrs, Volume= 1.175 af, Depth> 1.58"

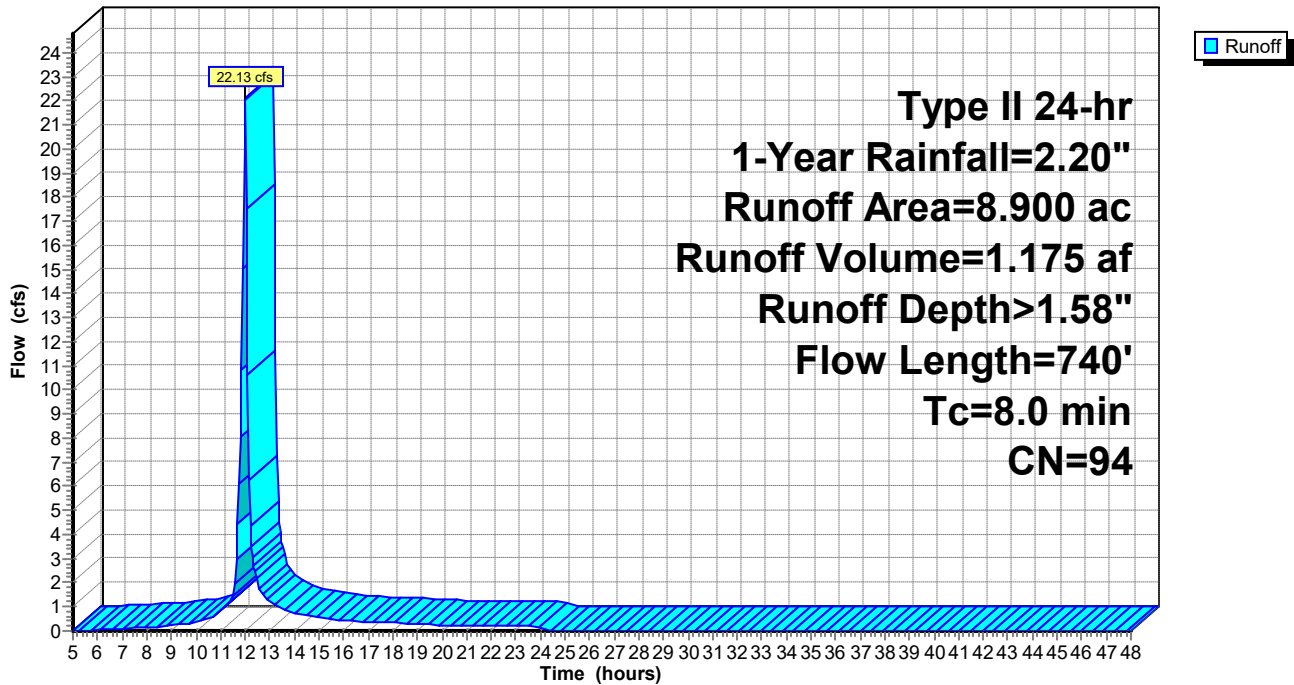
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 8.600	95	Compacted Gravel
0.300	80	>75% Grass cover, Good, HSG D
8.900	94	Weighted Average
8.900		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
4.1	400	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	240	0.0050	6.67	47.16	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.013 Corrugated PE, smooth interior
8.0	740	Total			

Subcatchment DR-4: Storage

Hydrograph



Summary for Subcatchment DR-5: Storage

Runoff = 13.09 cfs @ 11.99 hrs, Volume= 0.687 af, Depth> 1.58"

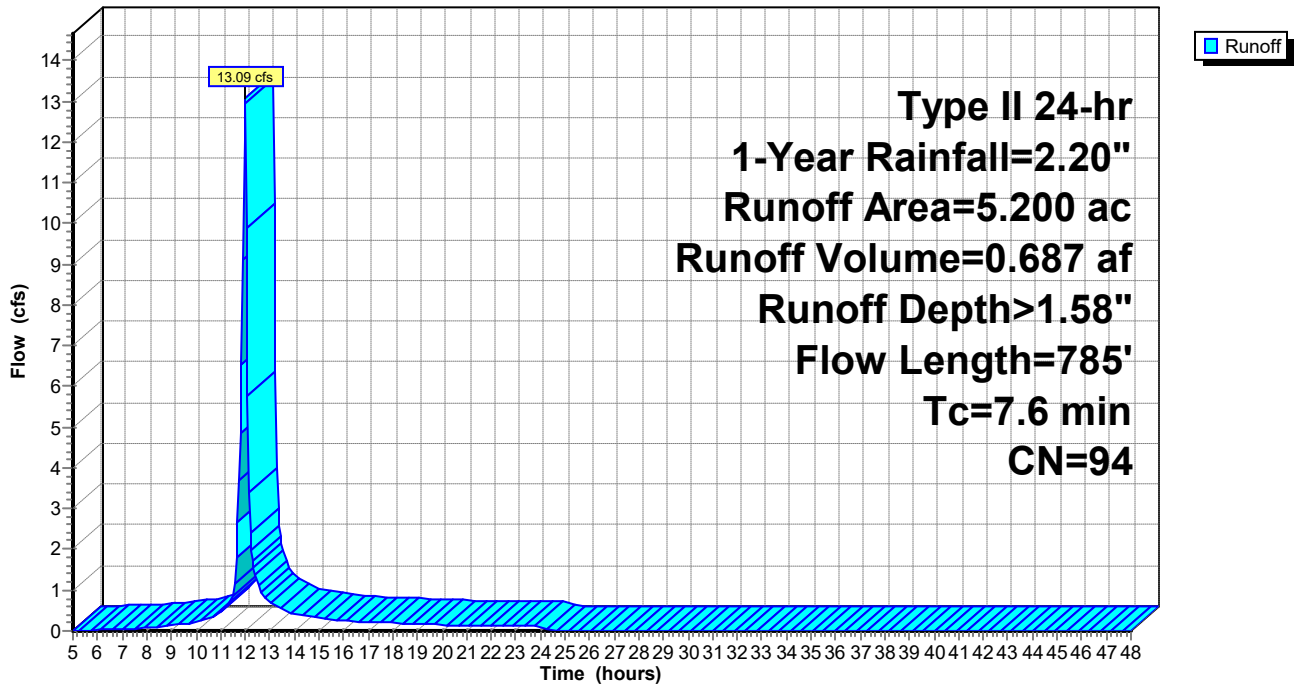
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 4.900	95	Dense Graded Aggregate
0.300	80	>75% Grass cover, Good, HSG D
5.200	94	Weighted Average
5.200		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
3.0	285	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.3	400	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
7.6	785	Total			

Subcatchment DR-5: Storage

Hydrograph



Summary for Subcatchment DR-6: Buldings B & D

Runoff = 30.91 cfs @ 12.00 hrs, Volume= 1.734 af, Depth> 1.76"

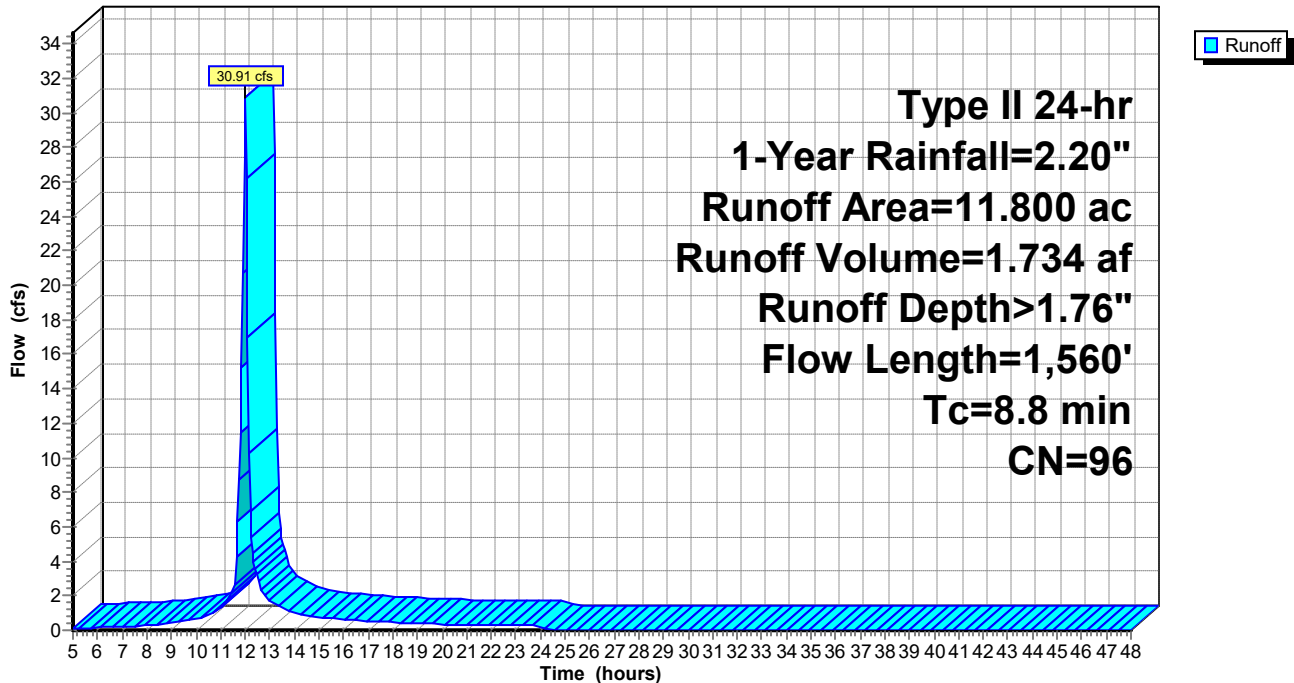
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 2.549	98	Building B
* 1.413	98	Building D
0.200	80	>75% Grass cover, Good, HSG D
* 7.638	95	Dense Graded Aggregate
11.800	96	Weighted Average
7.838		66.42% Pervious Area
3.962		33.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
1.0	100	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.5	1,360	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
8.8	1,560	Total			

Subcatchment DR-6: Buldings B & D

Hydrograph



Summary for Subcatchment DR-7: Building C & Rail

Runoff = 22.09 cfs @ 12.01 hrs, Volume= 1.278 af, Depth> 1.76"

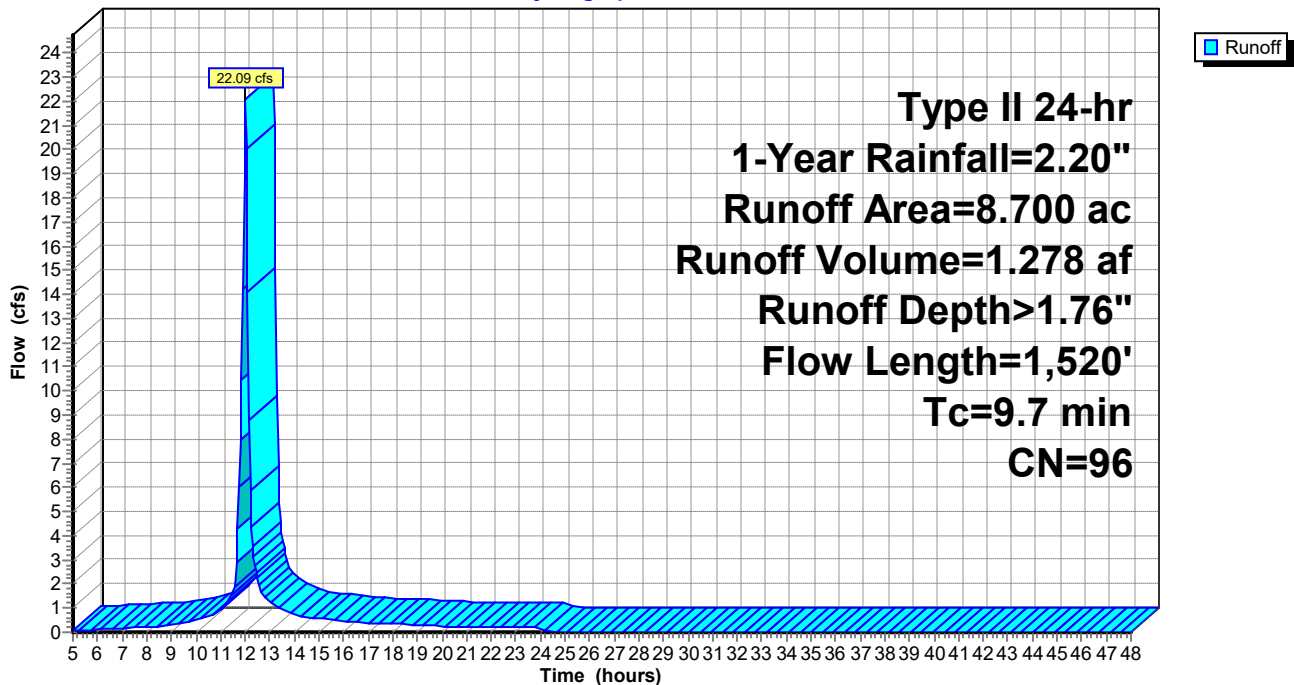
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 3.030	98	Building C
* 0.970	98	Rail
* 4.400	95	Dense Graded Aggregate
0.300	80	>75% Grass cover, Good, HSG D
8.700	96	Weighted Average
4.700		54.02% Pervious Area
4.000		45.98% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
2.6	250	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
3.8	1,170	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
9.7	1,520	Total			

Subcatchment DR-7: Building C & Rail

Hydrograph



Summary for Subcatchment DR-8A: Parking

Runoff = 5.17 cfs @ 11.96 hrs, Volume= 0.265 af, Depth> 1.67"

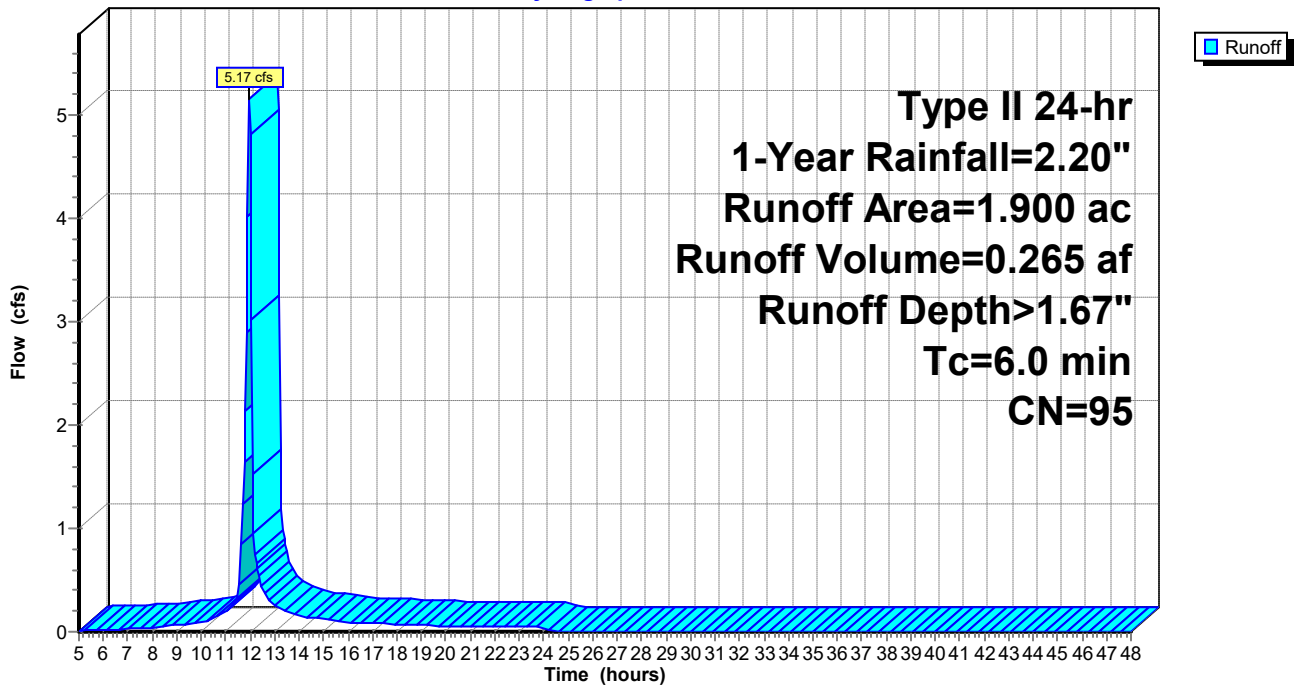
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 1.600	98	Parking
0.300	80	>75% Grass cover, Good, HSG D
1.900	95	Weighted Average
0.300		15.79% Pervious Area
1.600		84.21% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-8A: Parking

Hydrograph



Summary for Subcatchment DR-8B: Roadway & Pond

Runoff = 1.65 cfs @ 11.98 hrs, Volume= 0.079 af, Depth= 0.94"

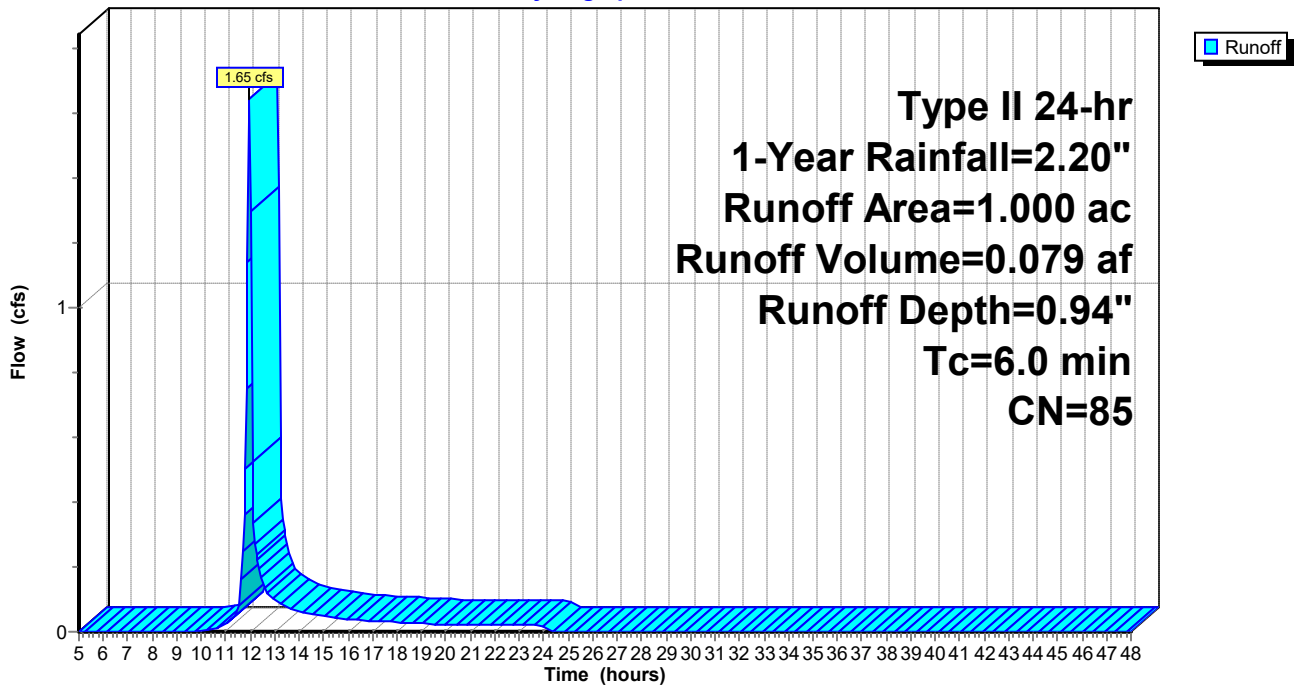
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 0.300	98	Roadway
0.700	80	>75% Grass cover, Good, HSG D
1.000	85	Weighted Average
0.700		70.00% Pervious Area
0.300		30.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-8B: Roadway & Pond

Hydrograph



Summary for Subcatchment DR-9A: Parking & Substation

Runoff = 3.97 cfs @ 12.04 hrs, Volume= 0.251 af, Depth> 1.67"

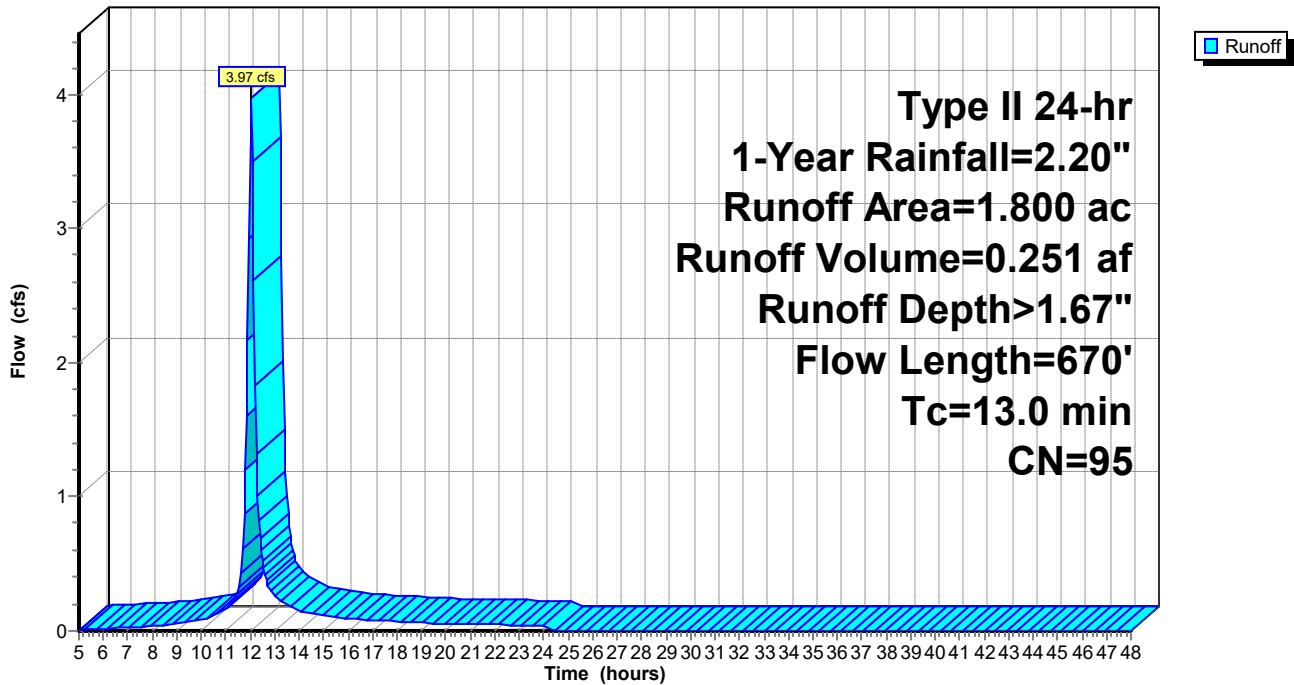
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
0.230	80	>75% Grass cover, Good, HSG D
* 0.200	92	Compacted Gravel
* 1.200	98	Parking and Road
* 0.170	98	Substation
1.800	95	Weighted Average
0.430		23.89% Pervious Area
1.370		76.11% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0200	1.19		Sheet Flow, Parking Lot Runoff Smooth surfaces n= 0.011 P2= 2.40"
11.6	570	0.0030	0.82		Shallow Concentrated Flow, Grass Lined Ditch to Pond Grassed Waterway Kv= 15.0 fps
13.0	670	Total			

Subcatchment DR-9A: Parking & Substation

Hydrograph



Summary for Subcatchment DR-9B: Roadway

Runoff = 7.13 cfs @ 11.96 hrs, Volume= 0.334 af, Depth= 1.00"

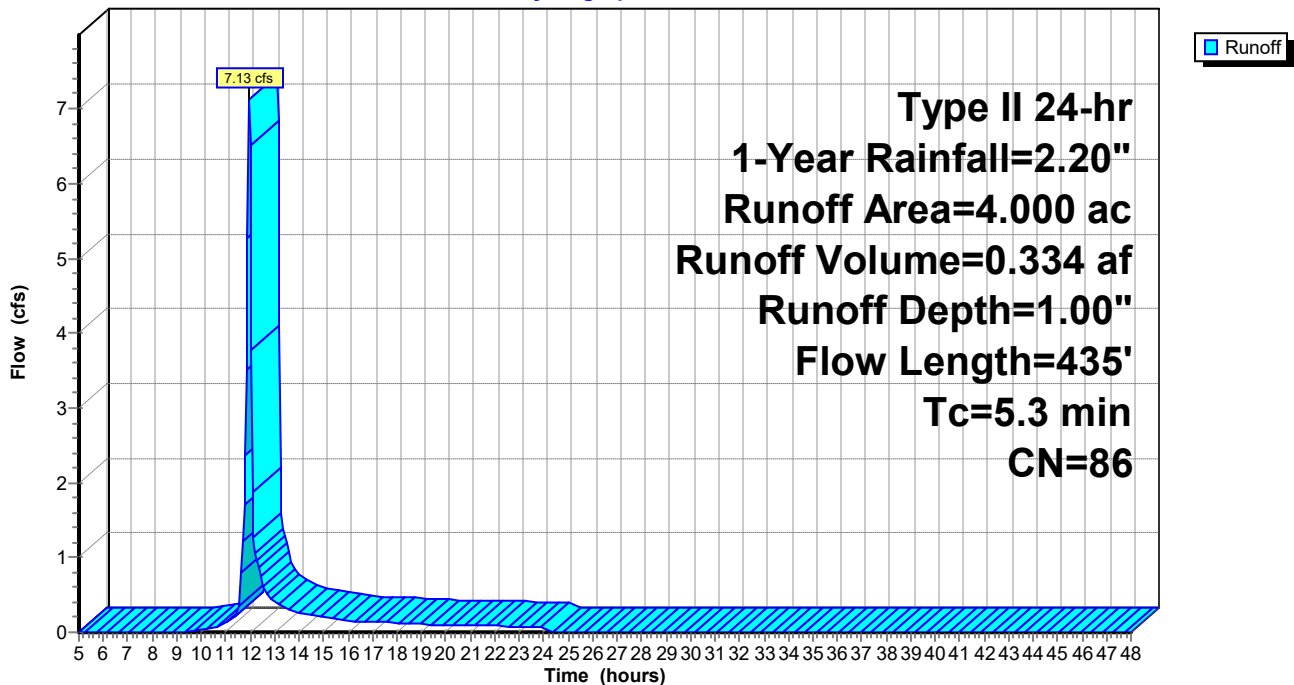
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 1-Year Rainfall=2.20"

Area (ac)	CN	Description
* 1.050	95	Dense Graded Aggregate
* 0.480	98	Roadway
2.470	80	>75% Grass cover, Good, HSG D
4.000	86	Weighted Average
3.520		88.00% Pervious Area
0.480		12.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.0250	0.46		Sheet Flow, Dense Graded Aggregate Yard n= 0.040 P2= 2.40"
1.3	230	0.0100	3.07	9.20	Channel Flow, Grass lined ditch Area= 3.0 sf Perim= 4.0' r= 0.75' n= 0.040 Earth, cobble bottom, clean sides
0.4	105	0.0050	4.20	7.43	Pipe Channel, driveway culvert 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013 Corrugated PE, smooth interior
5.3	435	Total			

Subcatchment DR-9B: Roadway

Hydrograph



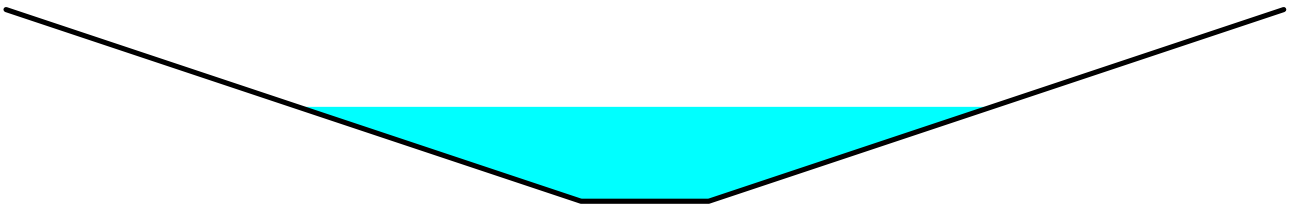
Summary for Reach 1R: Swale

Inflow Area = 1.900 ac, 84.21% Impervious, Inflow Depth > 1.67" for 1-Year event
 Inflow = 5.17 cfs @ 11.96 hrs, Volume= 0.265 af
 Outflow = 4.10 cfs @ 12.13 hrs, Volume= 0.265 af, Atten= 21%, Lag= 9.9 min

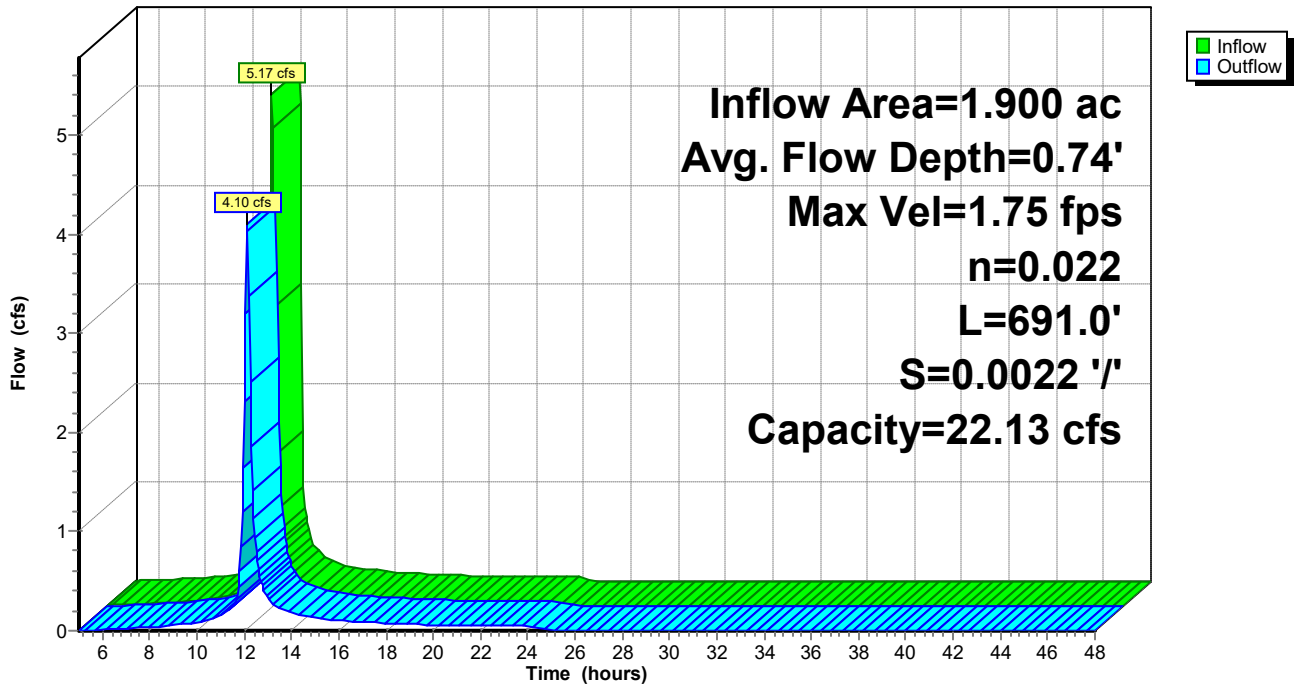
Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 1.75 fps, Min. Travel Time= 6.6 min
 Avg. Velocity = 0.50 fps, Avg. Travel Time= 22.9 min

Peak Storage= 1,638 cf @ 12.02 hrs
 Average Depth at Peak Storage= 0.74' , Surface Width= 5.43'
 Bank-Full Depth= 1.50' Flow Area= 8.3 sf, Capacity= 22.13 cfs

1.00' x 1.50' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 '/' Top Width= 10.00'
 Length= 691.0' Slope= 0.0022 '/'
 Inlet Invert= 15.50', Outlet Invert= 14.00'



Reach 1R: Swale
 Hydrograph



Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 0.83" for 1-Year event
 Inflow = 4.77 cfs @ 13.30 hrs, Volume= 1.982 af
 Outflow = 1.61 cfs @ 21.37 hrs, Volume= 1.851 af, Atten= 66%, Lag= 484.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.05 fps, Min. Travel Time= 305.5 min
 Avg. Velocity = 0.03 fps, Avg. Travel Time= 568.8 min

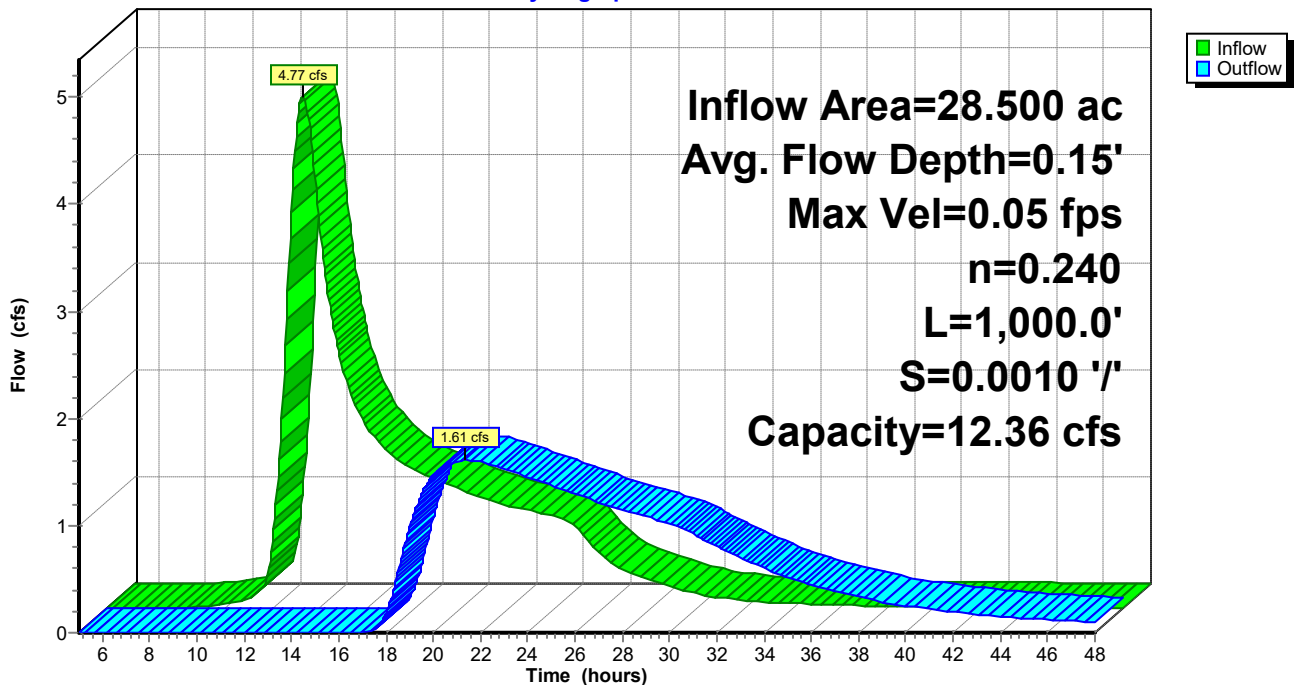
Peak Storage= 29,542 cf @ 16.28 hrs
 Average Depth at Peak Storage= 0.15' , Surface Width= 200.88'
 Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240
 Side Slope Z-value= 3.0 '/' Top Width= 203.00'
 Length= 1,000.0' Slope= 0.0010 '/'
 Inlet Invert= 6.00', Outlet Invert= 5.00'



Reach 1W: Wetland #1 / Analysis Point 1A

Hydrograph



Summary for Reach 2R: Overflow

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 1.20" for 1-Year event
 Inflow = 0.48 cfs @ 13.64 hrs, Volume= 0.581 af
 Outflow = 0.48 cfs @ 13.65 hrs, Volume= 0.581 af, Atten= 0%, Lag= 0.8 min

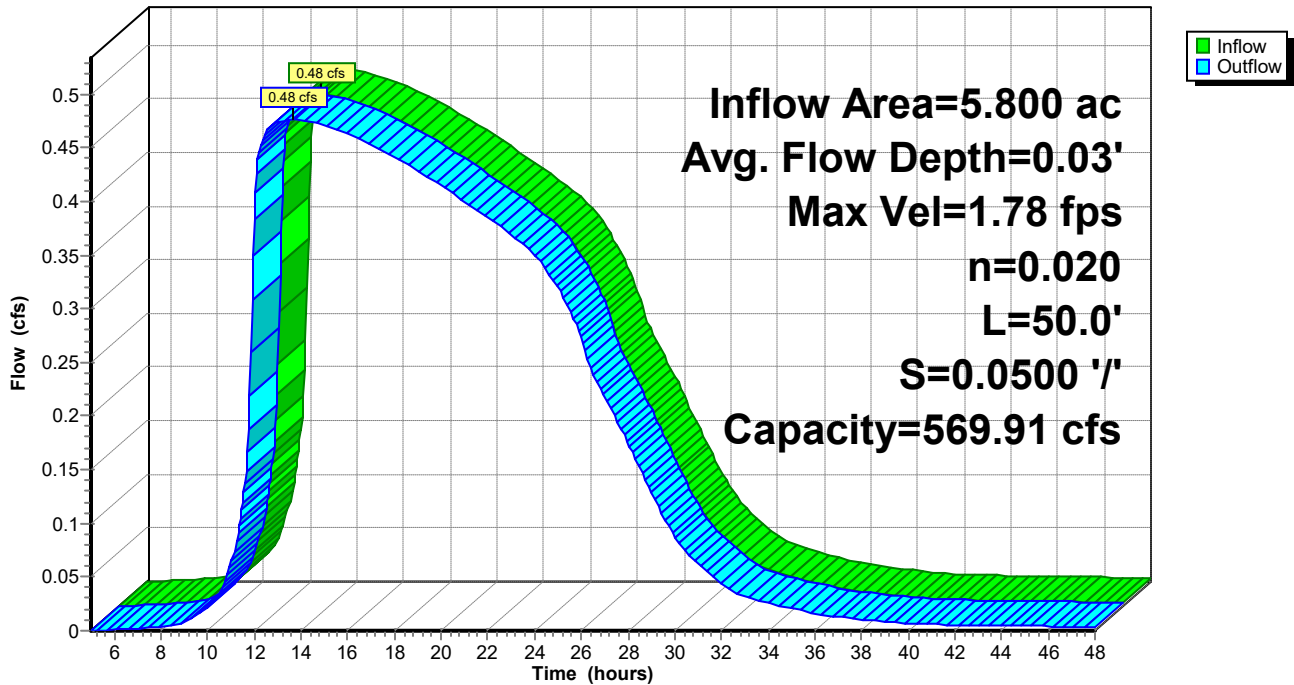
Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 1.78 fps, Min. Travel Time= 0.5 min
 Avg. Velocity = 1.38 fps, Avg. Travel Time= 0.6 min

Peak Storage= 13 cf @ 13.64 hrs
 Average Depth at Peak Storage= 0.03' , Surface Width= 8.20'
 Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 569.91 cfs

8.00' x 2.00' deep channel, n= 0.020 Corrugated PE, corrugated interior
 Side Slope Z-value= 3.0 ' / ' Top Width= 20.00'
 Length= 50.0' Slope= 0.0500 ' / '
 Inlet Invert= 16.50', Outlet Invert= 14.00'



Reach 2R: Overflow
 Hydrograph



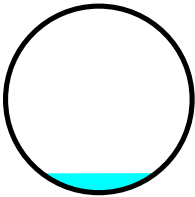
Summary for Reach 3R: Outlet Pipe

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 0.78" for 1-Year event
 Inflow = 1.61 cfs @ 21.37 hrs, Volume= 1.851 af
 Outflow = 1.61 cfs @ 21.38 hrs, Volume= 1.851 af, Atten= 0%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 3.34 fps, Min. Travel Time= 0.3 min
 Avg. Velocity = 2.22 fps, Avg. Travel Time= 0.5 min

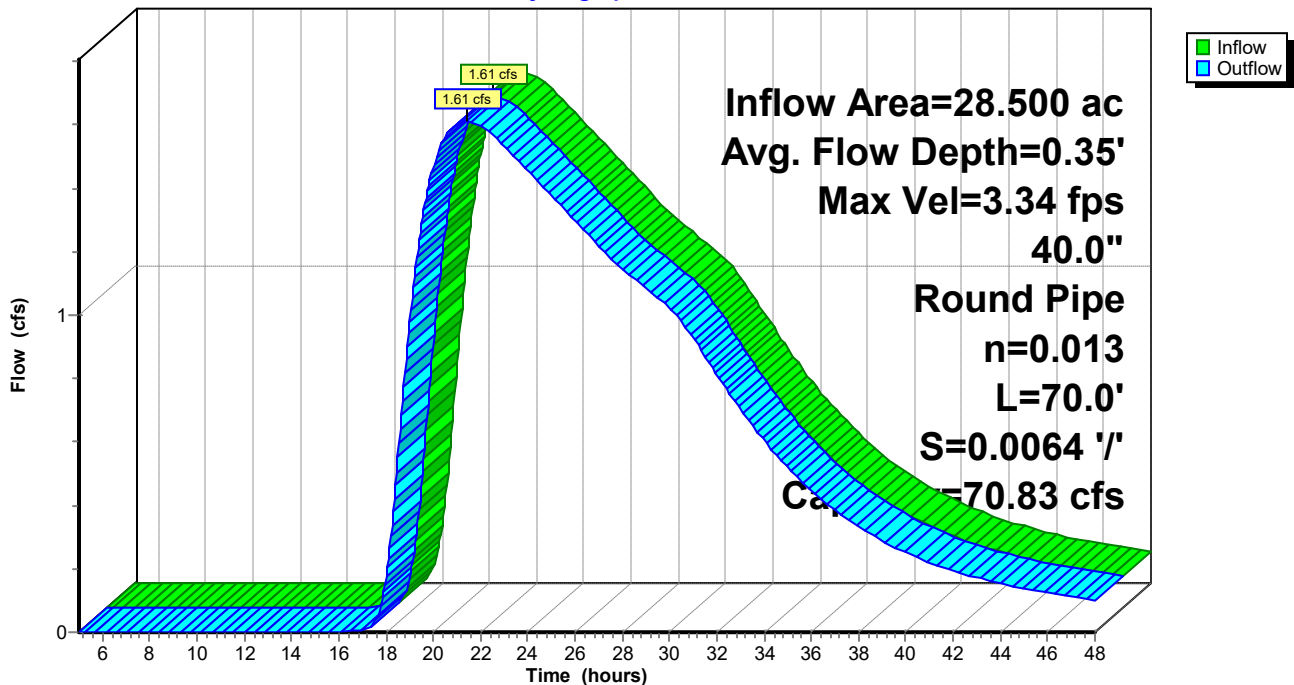
Peak Storage= 34 cf @ 21.38 hrs
 Average Depth at Peak Storage= 0.35' , Surface Width= 2.04'
 Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe
 n= 0.013 Corrugated PE, smooth interior
 Length= 70.0' Slope= 0.0064 '/'
 Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 3R: Outlet Pipe

Hydrograph



Summary for Reach 4R: Overflow

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 1.67" for 1-Year event
 Inflow = 2.65 cfs @ 11.99 hrs, Volume= 0.139 af
 Outflow = 2.56 cfs @ 12.00 hrs, Volume= 0.139 af, Atten= 3%, Lag= 1.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.29 fps, Min. Travel Time= 0.7 min
 Avg. Velocity = 0.58 fps, Avg. Travel Time= 2.9 min

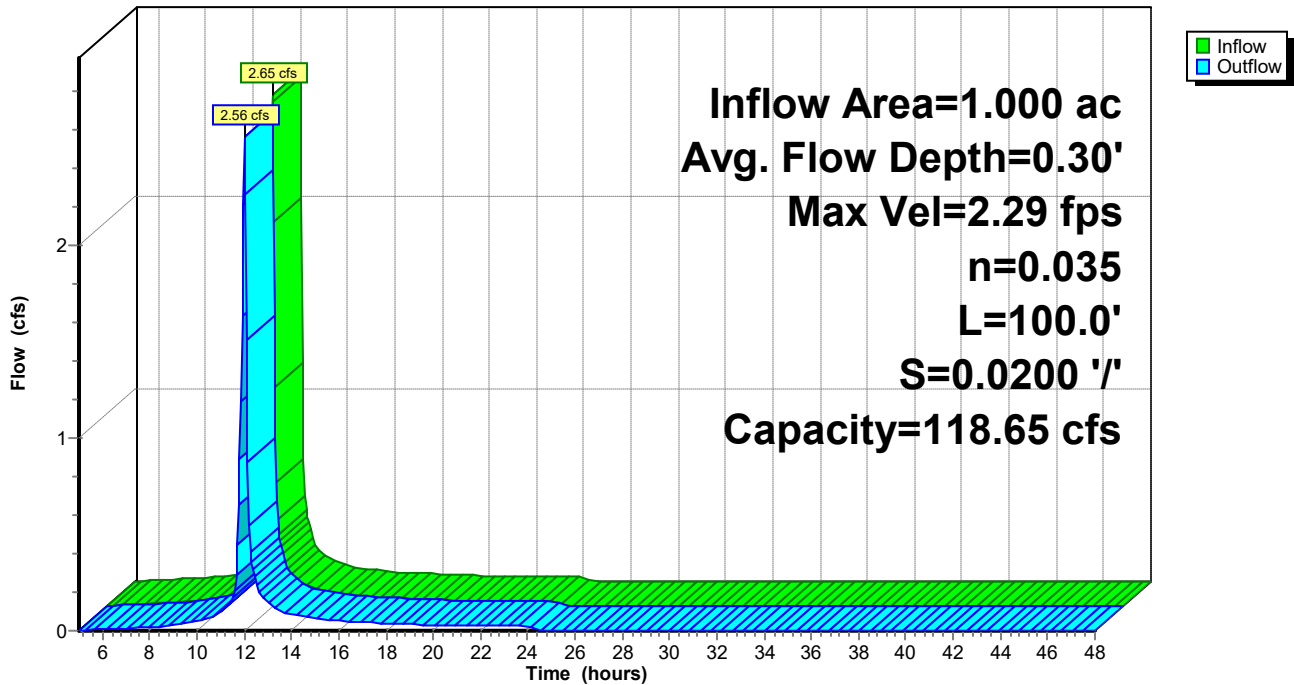
Peak Storage= 115 cf @ 11.99 hrs
 Average Depth at Peak Storage= 0.30' , Surface Width= 4.77'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 118.65 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'
 Length= 100.0' Slope= 0.0200 '/'
 Inlet Invert= 12.00', Outlet Invert= 10.00'



Reach 4R: Overflow

Hydrograph



Summary for Reach 5R: Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.00" for 1-Year event
 Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af
 Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min
 Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

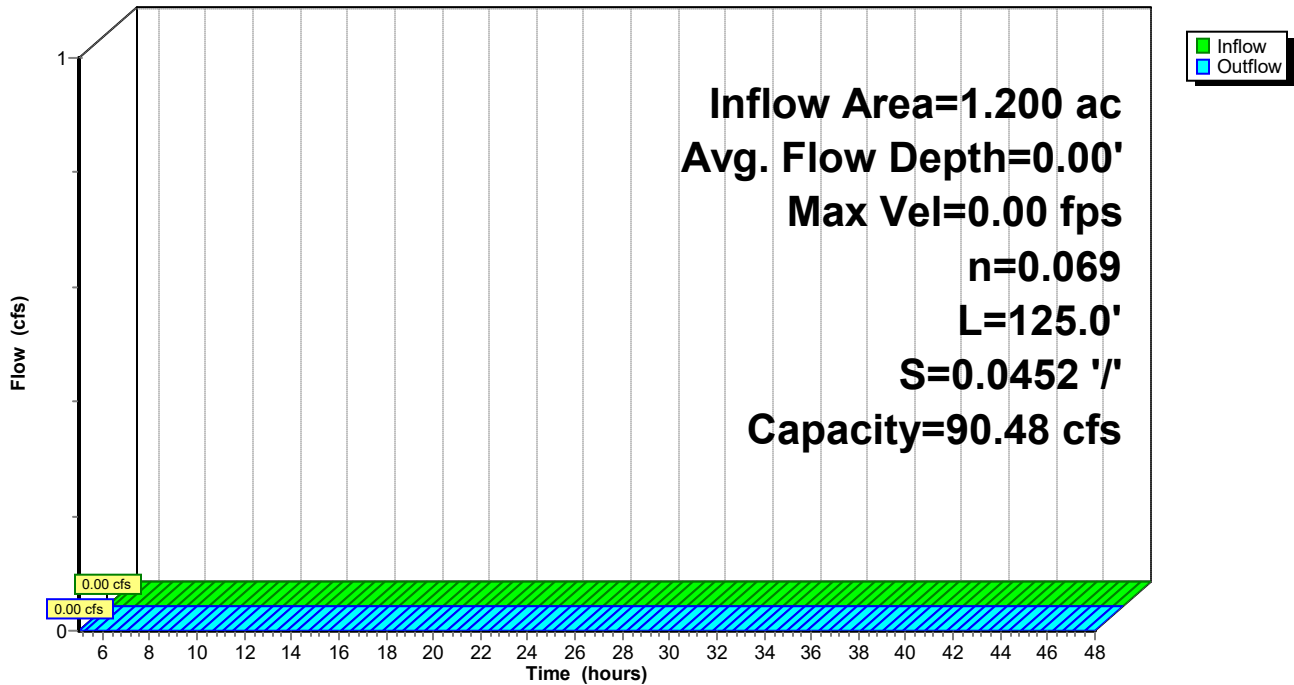
Peak Storage= 0 cf @ 5.00 hrs
 Average Depth at Peak Storage= 0.00'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 90.48 cfs

3.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'
 Length= 125.0' Slope= 0.0452 '/'
 Inlet Invert= 11.65', Outlet Invert= 6.00'



Reach 5R: Overflow

Hydrograph



Summary for Reach 6R: Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.00" for 1-Year event
 Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af
 Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min
 Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

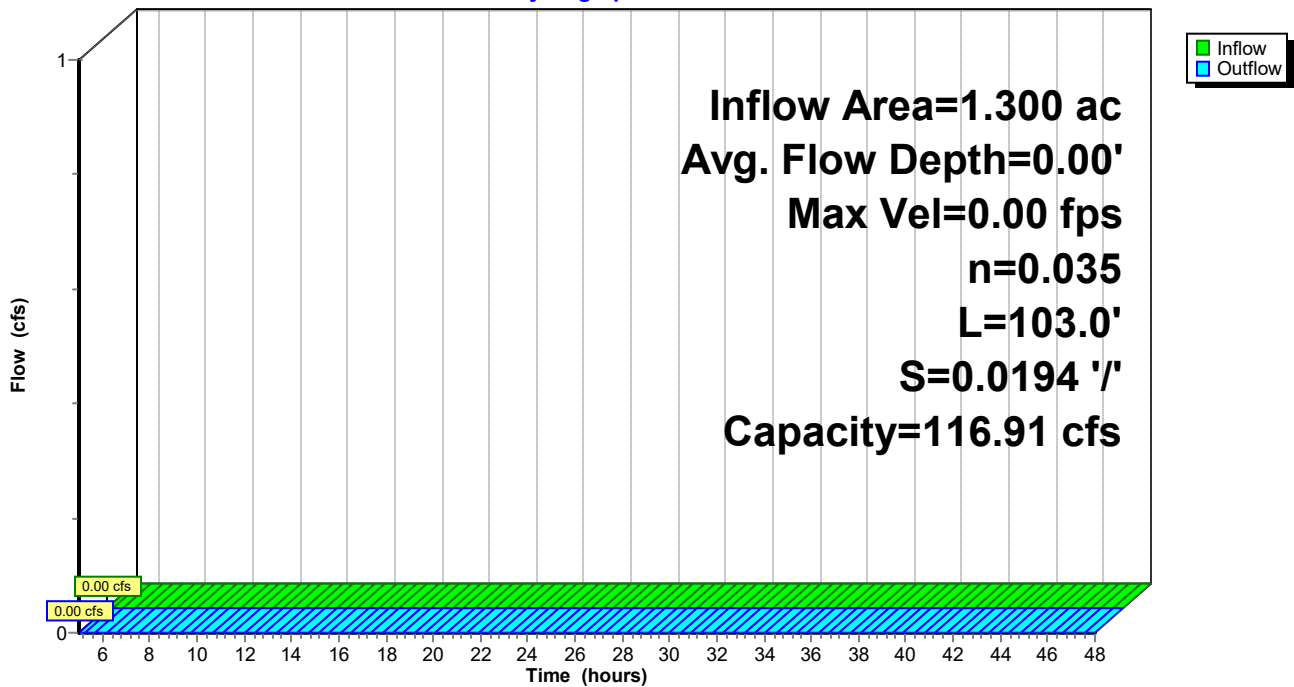
Peak Storage= 0 cf @ 5.00 hrs
 Average Depth at Peak Storage= 0.00'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 116.91 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'
 Length= 103.0' Slope= 0.0194 '/'
 Inlet Invert= 8.50', Outlet Invert= 6.50'



Reach 6R: Overflow

Hydrograph



Summary for Reach 7R: Overflow

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth > 1.40" for 1-Year event
 Inflow = 0.30 cfs @ 13.53 hrs, Volume= 0.339 af
 Outflow = 0.30 cfs @ 13.61 hrs, Volume= 0.339 af, Atten= 0%, Lag= 4.9 min

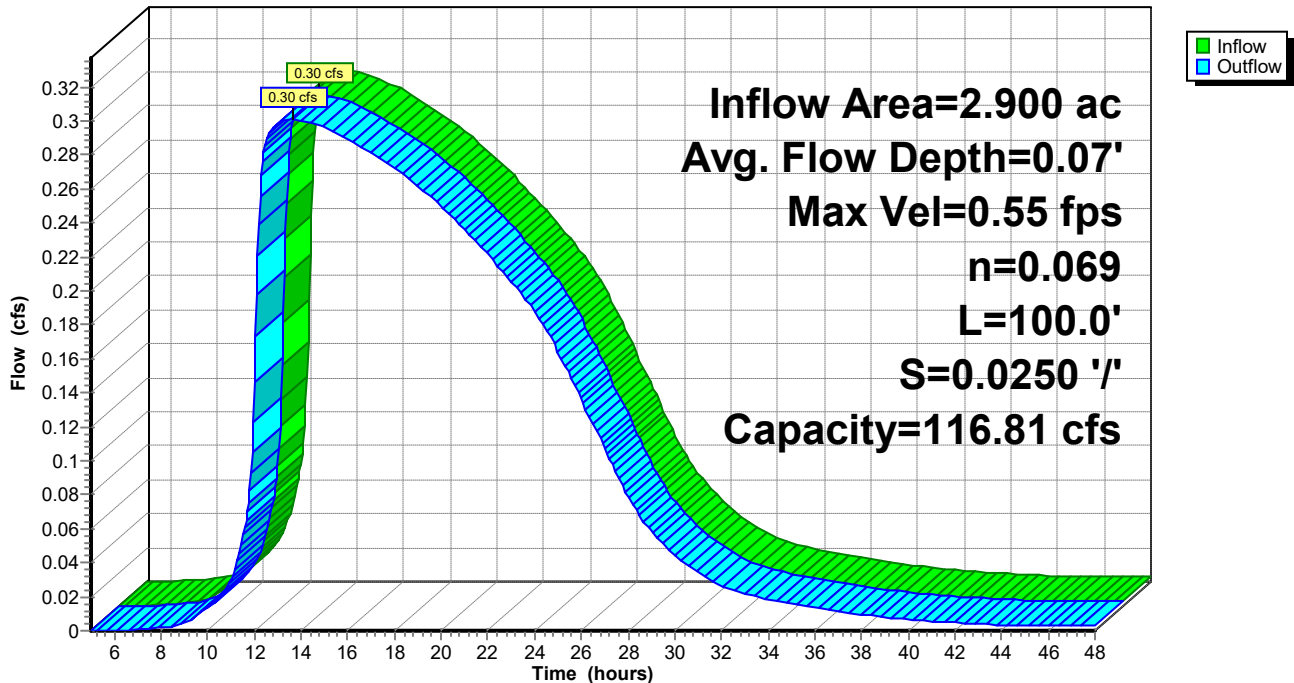
Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.55 fps, Min. Travel Time= 3.0 min
 Avg. Velocity = 0.34 fps, Avg. Travel Time= 4.8 min

Peak Storage= 54 cf @ 13.56 hrs
 Average Depth at Peak Storage= 0.07' , Surface Width= 8.40'
 Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 116.81 cfs

8.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 20.00'
 Length= 100.0' Slope= 0.0250 '/'
 Inlet Invert= 14.50', Outlet Invert= 12.00'



Reach 7R: Overflow
 Hydrograph



Summary for Reach 8R: Dry Swale #1

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 1.67" for 1-Year event
 Inflow = 2.72 cfs @ 11.96 hrs, Volume= 0.139 af
 Outflow = 2.65 cfs @ 11.99 hrs, Volume= 0.139 af, Atten= 3%, Lag= 1.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.47 fps, Min. Travel Time= 0.7 min
 Avg. Velocity = 0.61 fps, Avg. Travel Time= 2.9 min

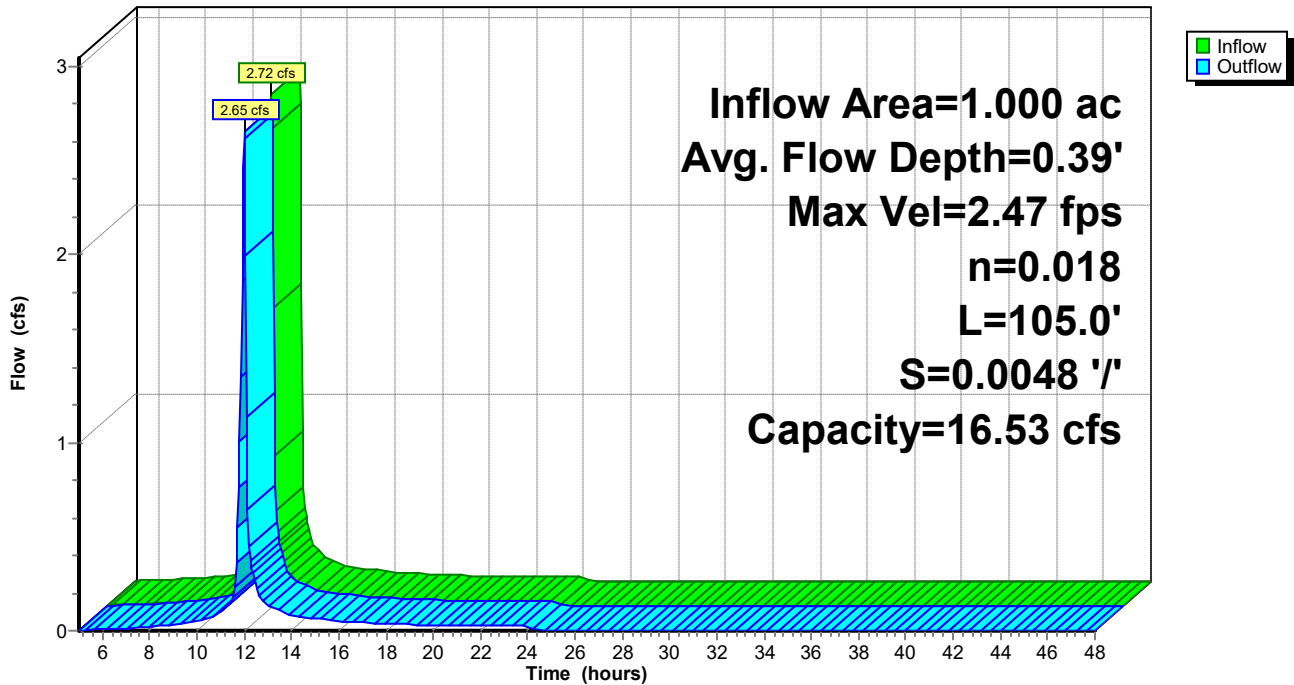
Peak Storage= 114 cf @ 11.98 hrs
 Average Depth at Peak Storage= 0.39' , Surface Width= 3.57'
 Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 16.53 cfs

2.00' x 1.00' deep channel, n= 0.018 Earth, clean & straight
 Side Slope Z-value= 2.0 ' / ' Top Width= 6.00'
 Length= 105.0' Slope= 0.0048 ' / '
 Inlet Invert= 10.00', Outlet Invert= 9.50'



Reach 8R: Dry Swale #1

Hydrograph



Summary for Reach 10R: Dry Swale #2

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 1.00" for 1-Year event
 Inflow = 1.22 cfs @ 12.03 hrs, Volume= 0.064 af
 Outflow = 1.20 cfs @ 12.04 hrs, Volume= 0.064 af, Atten= 2%, Lag= 0.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 3.19 fps, Min. Travel Time= 0.6 min
 Avg. Velocity = 1.01 fps, Avg. Travel Time= 1.9 min

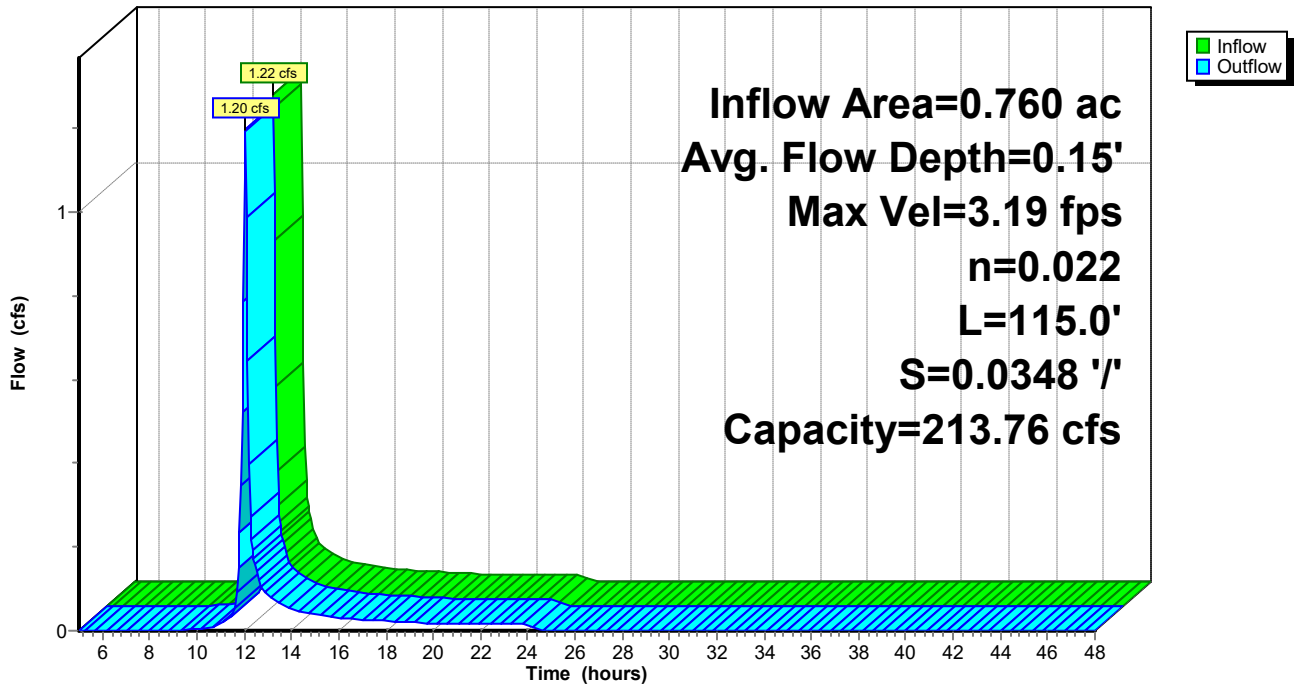
Peak Storage= 44 cf @ 12.03 hrs
 Average Depth at Peak Storage= 0.15' , Surface Width= 2.93'
 Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 213.76 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 14.00'
 Length= 115.0' Slope= 0.0348 ' / '
 Inlet Invert= 37.00', Outlet Invert= 33.00'



Reach 10R: Dry Swale #2

Hydrograph



Summary for Reach 12R: Sediment Basin Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.00" for 1-Year event
 Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af
 Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min
 Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

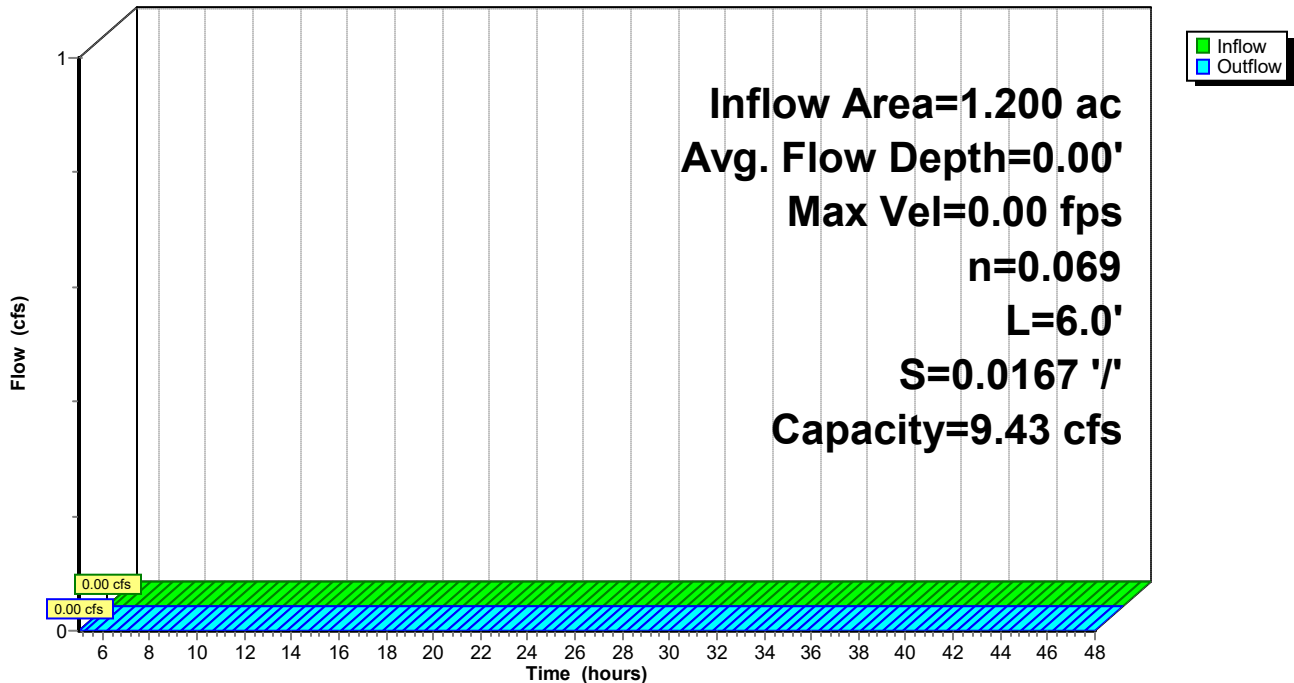
Peak Storage= 0 cf @ 5.00 hrs
 Average Depth at Peak Storage= 0.00'
 Bank-Full Depth= 0.50' Flow Area= 6.0 sf, Capacity= 9.43 cfs

10.00' x 0.50' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 4.0 '/' Top Width= 14.00'
 Length= 6.0' Slope= 0.0167 '/'
 Inlet Invert= 12.00', Outlet Invert= 11.90'



Reach 12R: Sediment Basin Overflow

Hydrograph



Summary for Reach 13R: Roadside Swale

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.12" for 1-Year event
 Inflow = 0.05 cfs @ 12.05 hrs, Volume= 0.012 af
 Outflow = 0.04 cfs @ 12.26 hrs, Volume= 0.012 af, Atten= 34%, Lag= 12.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.76 fps, Min. Travel Time= 6.4 min
 Avg. Velocity = 0.48 fps, Avg. Travel Time= 10.0 min

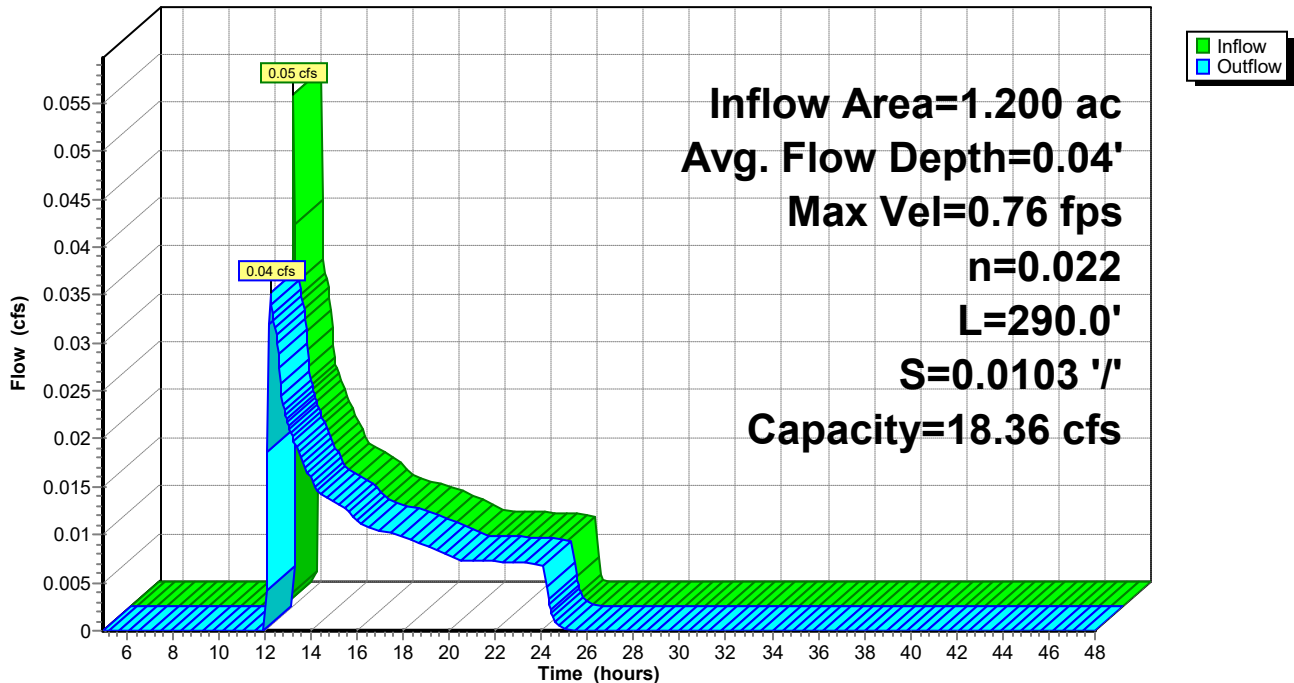
Peak Storage= 13 cf @ 12.15 hrs
 Average Depth at Peak Storage= 0.04' , Surface Width= 1.25'
 Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.36 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 7.00'
 Length= 290.0' Slope= 0.0103 ' / '
 Inlet Invert= 15.00', Outlet Invert= 12.00'



Reach 13R: Roadside Swale

Hydrograph



Summary for Reach 14R: Roadside Swale

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 1.00" for 1-Year event
 Inflow = 1.32 cfs @ 11.97 hrs, Volume= 0.064 af
 Outflow = 1.22 cfs @ 12.03 hrs, Volume= 0.064 af, Atten= 7%, Lag= 3.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 3.99 fps, Min. Travel Time= 1.9 min
 Avg. Velocity = 1.33 fps, Avg. Travel Time= 5.7 min

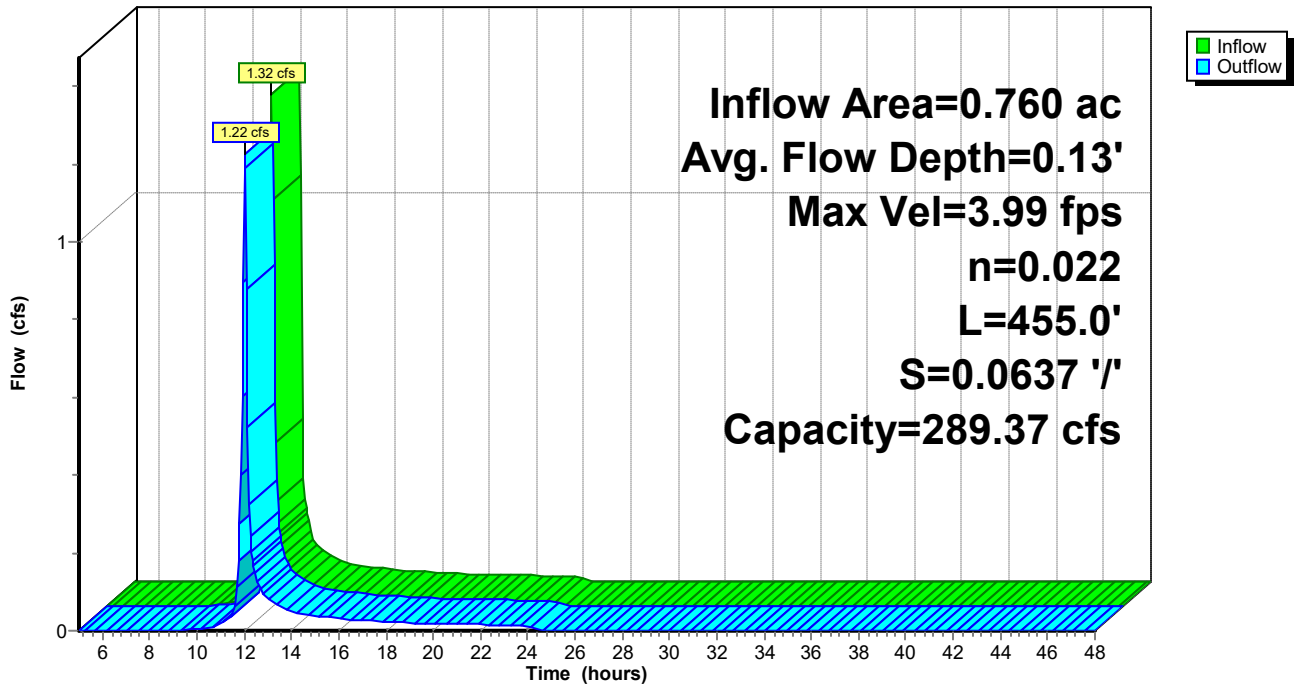
Peak Storage= 146 cf @ 11.99 hrs
 Average Depth at Peak Storage= 0.13' , Surface Width= 2.80'
 Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 289.37 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 '/' Top Width= 14.00'
 Length= 455.0' Slope= 0.0637 '/'
 Inlet Invert= 66.00', Outlet Invert= 37.00'



Reach 14R: Roadside Swale

Hydrograph



Summary for Reach 15R: Roadside Swale

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.41" for 1-Year event
 Inflow = 0.84 cfs @ 11.99 hrs, Volume= 0.045 af
 Outflow = 0.46 cfs @ 12.27 hrs, Volume= 0.045 af, Atten= 46%, Lag= 16.5 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.64 fps, Min. Travel Time= 11.2 min
 Avg. Velocity = 0.21 fps, Avg. Travel Time= 34.0 min

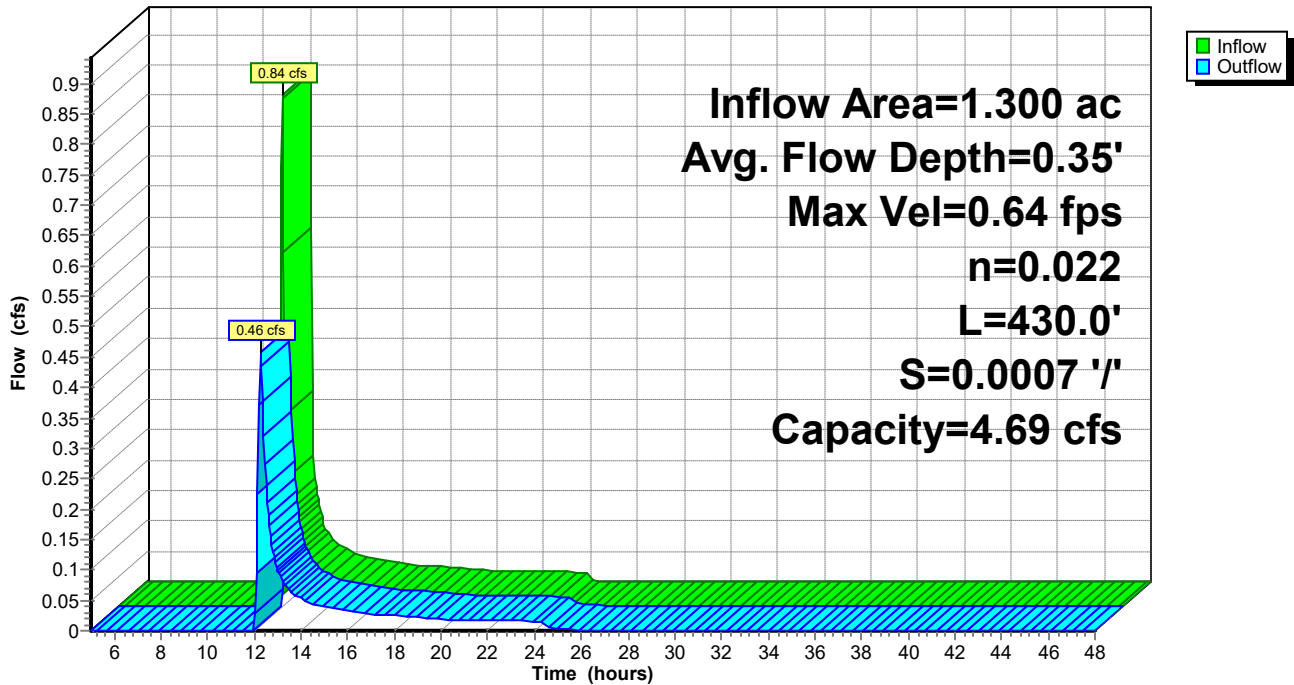
Peak Storage= 310 cf @ 12.07 hrs
 Average Depth at Peak Storage= 0.35' , Surface Width= 3.11'
 Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 4.69 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 7.00'
 Length= 430.0' Slope= 0.0007 ' / '
 Inlet Invert= 10.00', Outlet Invert= 9.71'



Reach 15R: Roadside Swale

Hydrograph



Summary for Reach 17R: Sediment Basin Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.05" for 1-Year event
 Inflow = 0.02 cfs @ 20.86 hrs, Volume= 0.006 af
 Outflow = 0.02 cfs @ 20.88 hrs, Volume= 0.006 af, Atten= 0%, Lag= 1.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.13 fps, Min. Travel Time= 0.8 min
 Avg. Velocity = 0.11 fps, Avg. Travel Time= 0.9 min

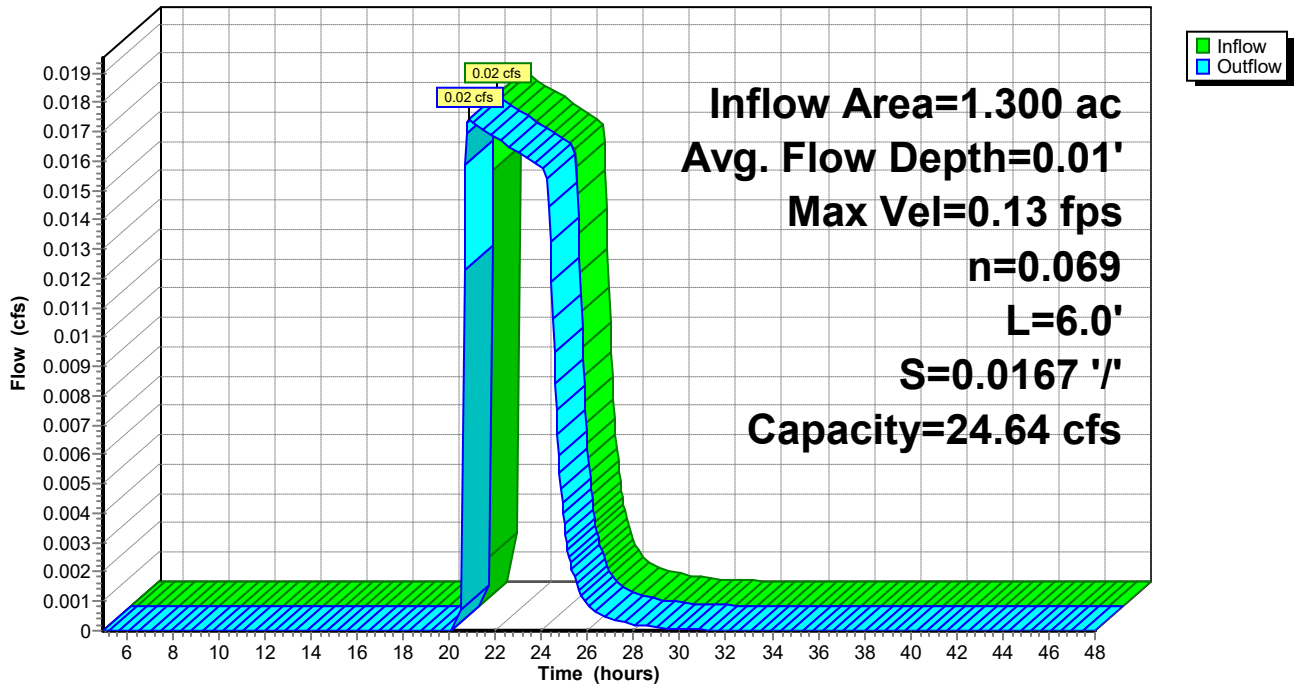
Peak Storage= 1 cf @ 20.86 hrs
 Average Depth at Peak Storage= 0.01' , Surface Width= 15.07'
 Bank-Full Depth= 0.70' Flow Area= 12.5 sf, Capacity= 24.64 cfs

15.00' x 0.70' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 4.0 ' / ' Top Width= 20.60'
 Length= 6.0' Slope= 0.0167 ' / '
 Inlet Invert= 9.00', Outlet Invert= 8.90'



Reach 17R: Sediment Basin Overflow

Hydrograph



Summary for Pond 1P: WQv Pond #1

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth = 1.42" for 1-Year event
 Inflow = 4.50 cfs @ 12.11 hrs, Volume= 0.344 af
 Outflow = 0.30 cfs @ 13.53 hrs, Volume= 0.339 af, Atten= 93%, Lag= 85.1 min
 Primary = 0.30 cfs @ 13.53 hrs, Volume= 0.339 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Starting Elev= 14.00' Surf.Area= 9,229 sf Storage= 19,003 cf
 Peak Elev= 14.99' @ 13.53 hrs Surf.Area= 17,494 sf Storage= 27,569 cf (8,566 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)
 Center-of-Mass det. time= 363.1 min (1,180.3 - 817.1)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,795 cf	Forebay (Prismatic) Listed below (Recalc)
#2	9.00'	57,882 cf	Permanent Pool (Prismatic) Listed below (Recalc)
		62,677 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	232	0	0
11.00	569	401	401
12.00	1,018	794	1,194
13.00	1,467	1,243	2,437
14.00	3,249	2,358	4,795

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
9.00	1,145	0	0
10.00	1,751	1,448	1,448
11.00	2,339	2,045	3,493
12.00	2,959	2,649	6,142
13.00	3,597	3,278	9,420
14.00	5,980	4,789	14,209
14.50	7,240	3,305	17,514
15.00	14,392	5,408	22,922
16.00	17,455	15,924	38,845
17.00	20,619	19,037	57,882

Device	Routing	Invert	Outlet Devices
#1	Primary	13.50'	12.0" Round Culvert L= 50.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 13.50' / 13.23' S= 0.0054 ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	16.00'	24.0" x 24.0" Horiz. Outlet Structure Top Grate C= 0.600 in 24.0" x 24.0" Grate (100% open area) Limited to weir flow at low heads
#3	Device 1	14.00'	4.0" Round Reverse Slope Pipe L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 9.00' / 14.00' S= -0.1250 ' Cc= 0.900

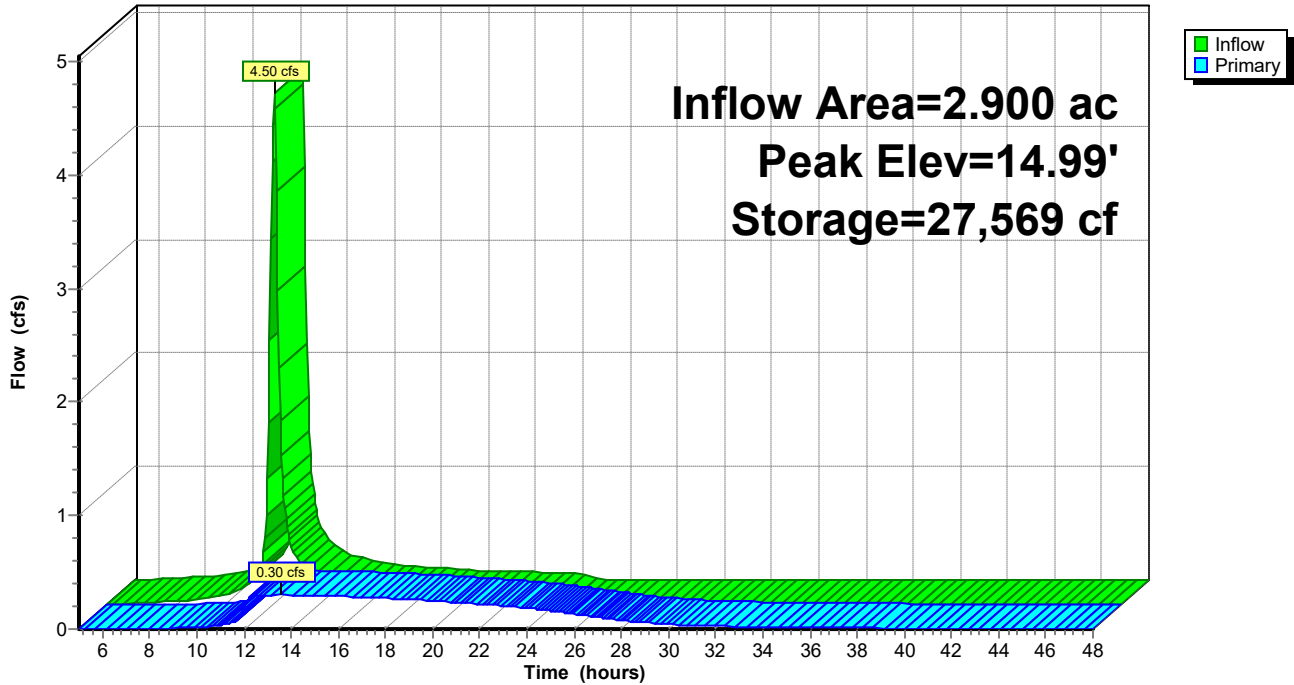
#4 Primary 16.25' n= 0.010 PVC, smooth interior, Flow Area= 0.09 sf
6.0' long x 1.0' breadth Broad-Crested Rectangular Weir
 Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
 2.50 3.00
 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
 3.30 3.31 3.32

Primary OutFlow Max=0.30 cfs @ 13.53 hrs HW=14.99' (Free Discharge)

- 1=Culvert (Passes 0.30 cfs of 3.14 cfs potential flow)
- 2=Outlet Structure Top Grate (Controls 0.00 cfs)
- 3=Reverse Slope Pipe (Inlet Controls 0.30 cfs @ 3.45 fps)
- 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: WQv Pond #1

Hydrograph



Summary for Pond 2P: WQv Pond #2

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 1.21" for 1-Year event
 Inflow = 10.43 cfs @ 11.98 hrs, Volume= 0.585 af
 Outflow = 0.48 cfs @ 13.64 hrs, Volume= 0.581 af, Atten= 95%, Lag= 99.4 min
 Primary = 0.48 cfs @ 13.64 hrs, Volume= 0.581 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Starting Elev= 14.00' Surf.Area= 5,917 sf Storage= 9,000 cf
 Peak Elev= 15.45' @ 13.64 hrs Surf.Area= 20,156 sf Storage= 23,392 cf (14,393 cf above start)

Plug-Flow detention time= 671.8 min calculated for 0.374 af (64% of inflow)
 Center-of-Mass det. time= 373.8 min (1,193.1 - 819.3)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,020 cf	Forebay #1 (Prismatic) Listed below (Recalc)
#2	10.00'	2,575 cf	Forebay #2 (Prismatic) Listed below (Recalc)
#3	10.00'	58,093 cf	Permanent Pool (Prismatic) Listed below (Recalc)
		64,688 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	141	0	0
11.00	330	236	236
12.00	562	446	682
13.00	866	714	1,396
14.00	2,023	1,445	2,840
14.50	2,696	1,180	4,020

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	82	0	0
11.00	202	142	142
12.00	351	277	419
13.00	535	443	862
14.00	1,323	929	1,791
14.50	1,815	785	2,575

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	375	0	0
11.00	653	514	514
12.00	957	805	1,319
13.00	1,286	1,122	2,441
14.00	2,571	1,929	4,369
14.50	3,307	1,470	5,839
15.00	13,814	4,280	10,119
16.00	17,852	15,833	25,952
17.00	22,659	20,256	46,207
17.50	24,884	11,886	58,093

18641.00-Proposed Condition_Chambers_CULVERTS_ Type II 24-hr 1-Year Rainfall=2.20"

Prepared by McFarland Johnson

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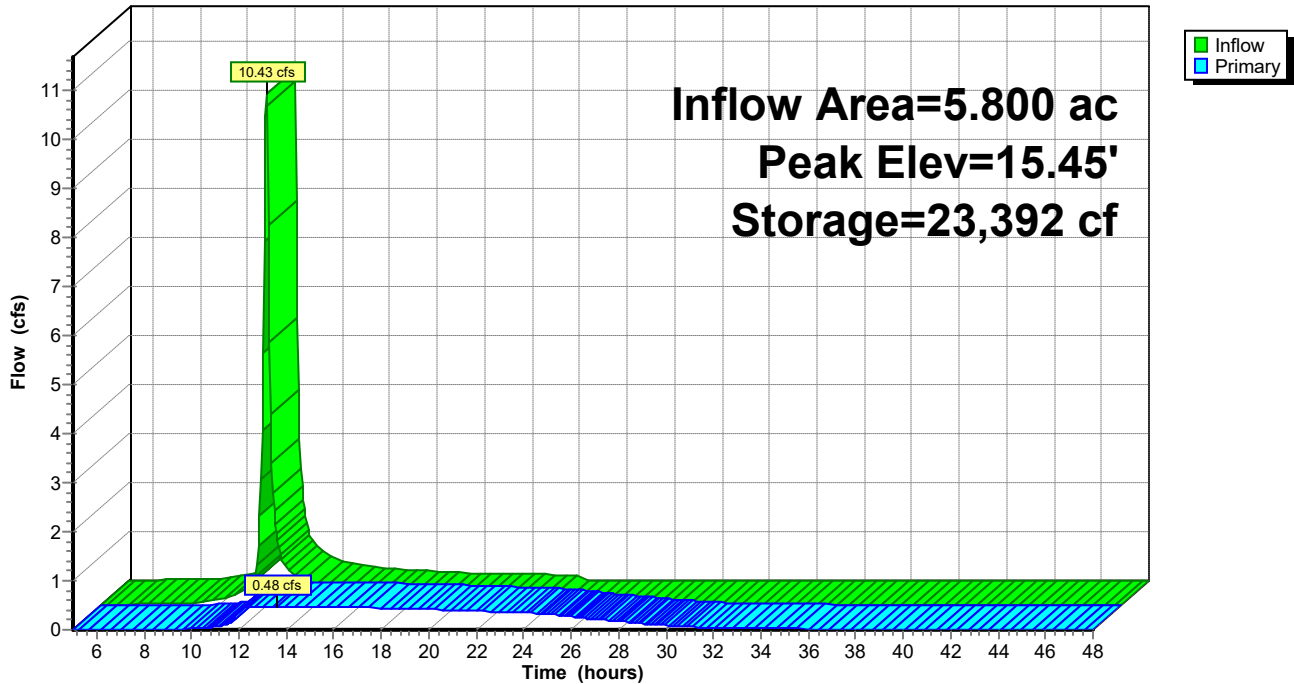
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Device	Routing	Invert	Outlet Devices
#1	Device 3	16.50'	24.0" x 24.0" Horiz. Orifice/Grate C= 0.600 in 24.0" x 24.0" Grate (100% open area) Limited to weir flow at low heads
#2	Device 3	14.00'	4.0" Vert. Reverse Slope Pipe C= 0.600 Limited to weir flow at low heads
#3	Primary	14.00'	12.0" Round Outlet Structure Discard Pipe L= 46.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 14.00' / 13.77' S= 0.0050 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#4	Primary	16.60'	10.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.48 cfs @ 13.64 hrs HW=15.45' (Free Discharge)
 3=Outlet Structure Discard Pipe (Passes 0.48 cfs of 3.04 cfs potential flow)
 1=Orifice/Grate (Controls 0.00 cfs)
 2=Reverse Slope Pipe (Orifice Controls 0.48 cfs @ 5.46 fps)
 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 2P: WQv Pond #2

Hydrograph



Summary for Pond 3P: Infiltration Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.00" for 1-Year event
 Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af
 Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min
 Discarded = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 8.10' @ 5.00 hrs Surf.Area= 109 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)
 Center-of-Mass det. time= (not calculated: no inflow)

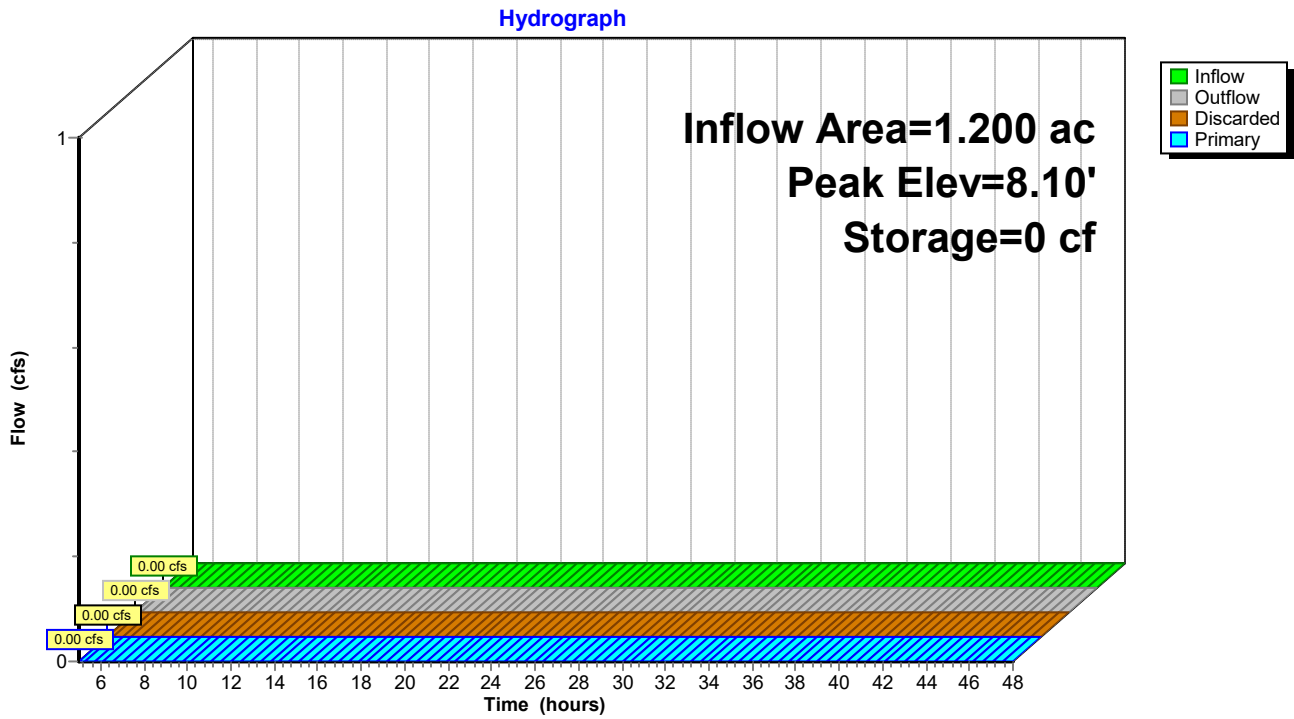
Volume	Invert	Avail.Storage	Storage Description			
#1	8.10'	2,492 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
8.10	109	56.0	0	0	109	
12.00	1,415	149.0	2,492	2,492	1,678	

Device	Routing	Invert	Outlet Devices
#1	Primary	11.65'	Channel/Reach using Reach 5R: Overflow
#2	Discarded	8.10'	0.500 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 4.00'

Discarded OutFlow Max=0.00 cfs @ 5.00 hrs HW=8.10' (Free Discharge)
 ↑**2=Exfiltration** (Passes 0.00 cfs of 0.00 cfs potential flow)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=8.10' (Free Discharge)
 ↑**1=Channel/Reach** (Controls 0.00 cfs)

Pond 3P: Infiltration Basin #1



Summary for Pond 4P: Infiltration Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.05" for 1-Year event
 Inflow = 0.02 cfs @ 20.88 hrs, Volume= 0.006 af
 Outflow = 0.02 cfs @ 20.97 hrs, Volume= 0.006 af, Atten= 0%, Lag= 5.4 min
 Discarded = 0.02 cfs @ 20.97 hrs, Volume= 0.006 af
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 5.82' @ 20.97 hrs Surf.Area= 114 sf Storage= 3 cf

Plug-Flow detention time= 2.7 min calculated for 0.006 af (100% of inflow)
 Center-of-Mass det. time= 2.7 min (1,369.3 - 1,366.6)

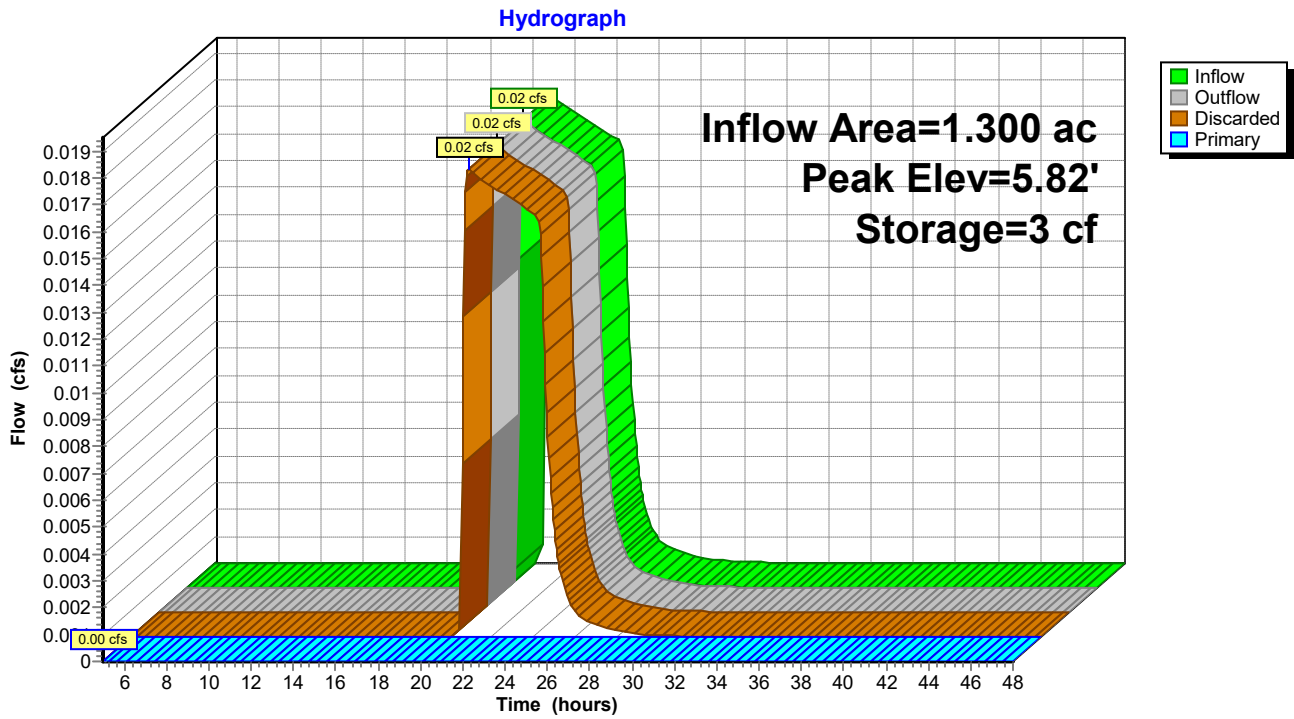
Volume	Invert	Avail.Storage	Storage Description		
#1	5.80'	2,495 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
5.80	110	56.0	0	0	110
9.70	1,415	150.0	2,495	2,495	1,702

Device	Routing	Invert	Outlet Devices
#1	Primary	8.50'	Channel/Reach using Reach 6R: Overflow
#2	Discarded	5.80'	12.000 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 3.00'

Discarded OutFlow Max=0.03 cfs @ 20.97 hrs HW=5.82' (Free Discharge)
 ↑**2=Exfiltration** (Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=5.80' (Free Discharge)
 ↑**1=Channel/Reach** (Controls 0.00 cfs)

Pond 4P: Infiltration Basin #2



Summary for Pond 5P: Sedimentation Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.12" for 1-Year event
 Inflow = 0.04 cfs @ 12.26 hrs, Volume= 0.012 af
 Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 11.50' @ 31.80 hrs Surf.Area= 427 sf Storage= 505 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

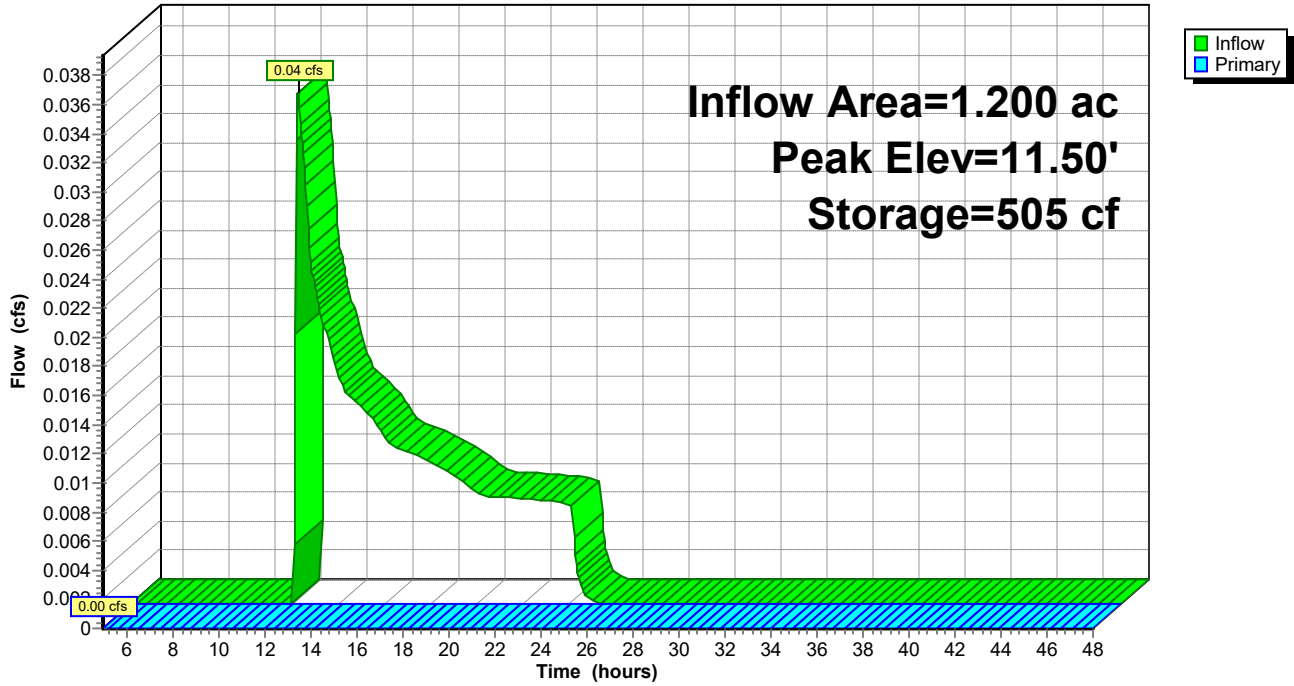
Volume	Invert	Avail.Storage	Storage Description			
#1	9.00'	1,058 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
9.00	41	25.8	0	0	41	
10.00	150	46.7	90	90	167	
11.00	320	66.6	230	320	355	
12.00	550	86.4	430	749	608	
12.50	687	96.2	309	1,058	758	

Device	Routing	Invert	Outlet Devices	
#1	Primary	12.00'	Channel/Reach using Reach 12R: Sediment Basin Overflow	

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=9.00' (Free Discharge)
 ↑1=Channel/Reach (Controls 0.00 cfs)

Pond 5P: Sedimentation Basin #1

Hydrograph



Summary for Pond 16P: Sedimentation Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.41" for 1-Year event
 Inflow = 0.46 cfs @ 12.27 hrs, Volume= 0.045 af
 Outflow = 0.02 cfs @ 20.86 hrs, Volume= 0.006 af, Atten= 96%, Lag= 515.7 min
 Primary = 0.02 cfs @ 20.86 hrs, Volume= 0.006 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 9.00' @ 20.86 hrs Surf.Area= 893 sf Storage= 1,703 cf

Plug-Flow detention time= 632.6 min calculated for 0.006 af (13% of inflow)
 Center-of-Mass det. time= 440.5 min (1,365.0 - 924.5)

Volume	Invert	Avail.Storage	Storage Description		
#1	5.80'	2,389 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
5.80	224	80.0	0	0	224
6.00	257	83.0	48	48	266
7.00	438	98.0	344	392	500
8.00	650	113.0	541	932	773
9.00	892	128.0	768	1,700	1,085
9.70	1,079	139.0	689	2,389	1,337

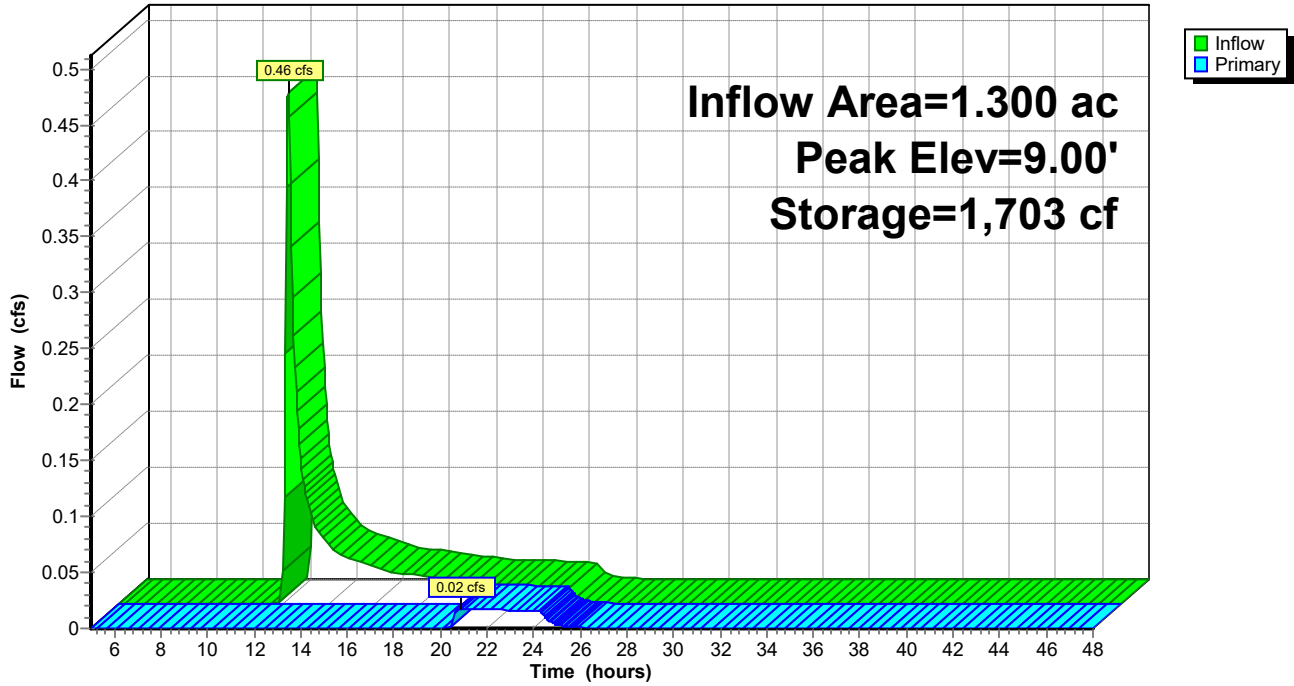
Device	Routing	Invert	Outlet Devices
#1	Primary	9.00'	Channel/Reach using Reach 17R: Sediment Basin Overflow

Primary OutFlow Max=0.00 cfs @ 20.86 hrs HW=9.00' (Free Discharge)

↑**1=Channel/Reach** (Channel Controls 0.00 cfs @ 0.07 fps)

Pond 16P: Sedimentation Basin #2

Hydrograph



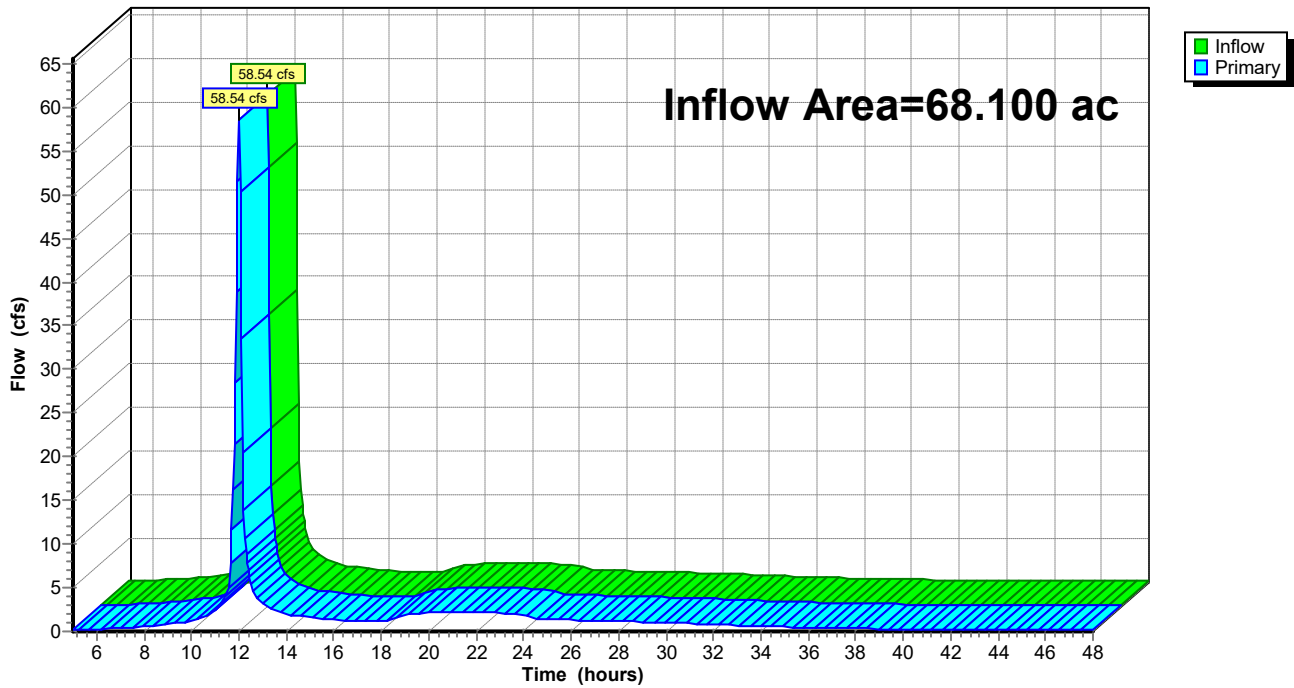
Summary for Pond AP-1: Analysis Point #1

Inflow Area = 68.100 ac, 20.36% Impervious, Inflow Depth > 0.92" for 1-Year event
Inflow = 58.54 cfs @ 12.00 hrs, Volume= 5.220 af
Primary = 58.54 cfs @ 12.00 hrs, Volume= 5.220 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1

Hydrograph



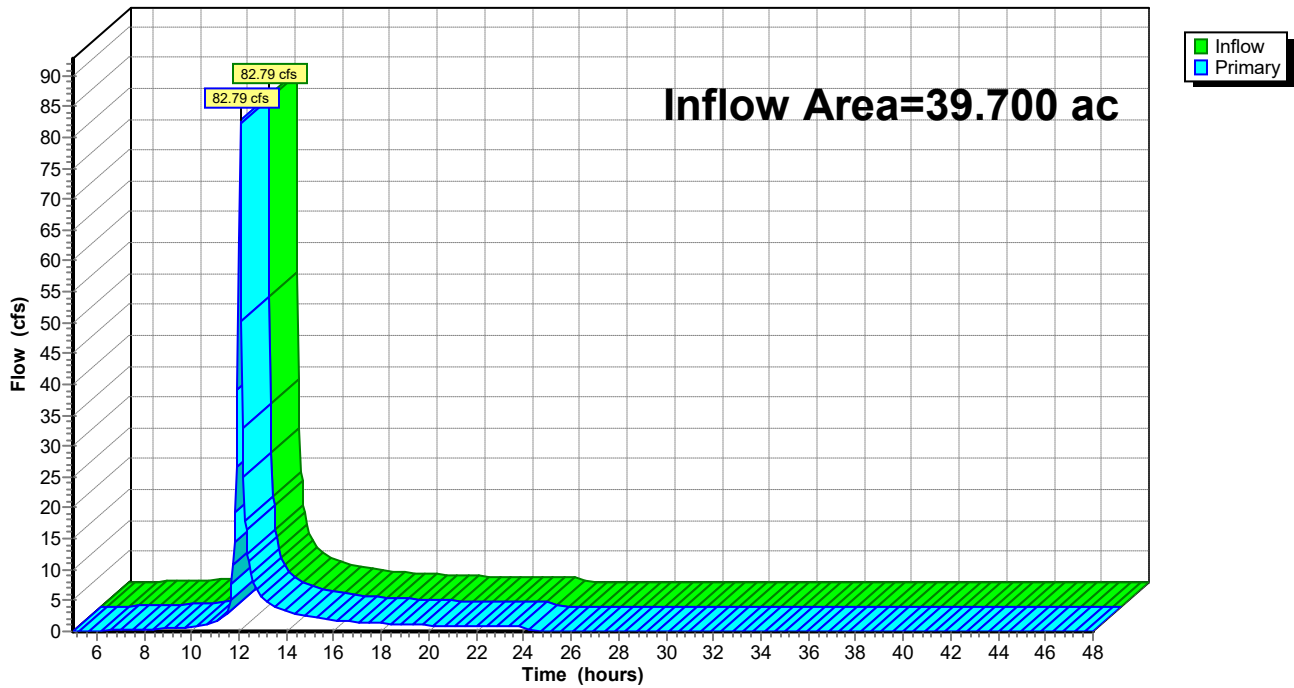
Summary for Pond AP-2: Analysis Point #2

Inflow Area = 39.700 ac, 23.10% Impervious, Inflow Depth > 1.20" for 1-Year event
Inflow = 82.79 cfs @ 12.04 hrs, Volume= 3.954 af
Primary = 82.79 cfs @ 12.04 hrs, Volume= 3.954 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2

Hydrograph



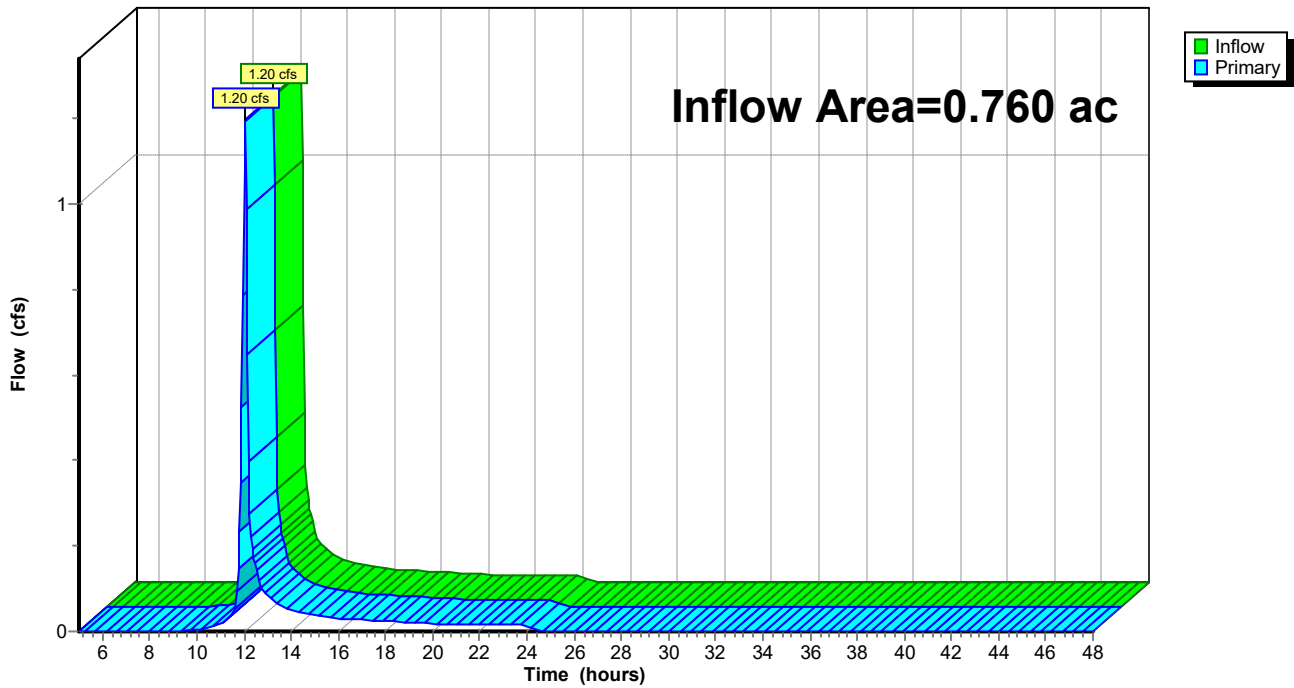
Summary for Pond AP-3: Analysis Point #3

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 1.00" for 1-Year event
Inflow = 1.20 cfs @ 12.04 hrs, Volume= 0.064 af
Primary = 1.20 cfs @ 12.04 hrs, Volume= 0.064 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3

Hydrograph



Summary for Pond C-1: Chamber Series 1

Inflow Area = 10.300 ac, 66.70% Impervious, Inflow Depth > 1.85" for 1-Year event
 Inflow = 29.34 cfs @ 11.98 hrs, Volume= 1.592 af
 Outflow = 27.91 cfs @ 12.04 hrs, Volume= 1.233 af, Atten= 5%, Lag= 3.7 min
 Discarded = 0.10 cfs @ 5.80 hrs, Volume= 0.345 af
 Primary = 27.81 cfs @ 12.04 hrs, Volume= 0.888 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 12.19' @ 12.04 hrs Surf.Area= 8,454 sf Storage= 28,913 cf

Plug-Flow detention time= 361.5 min calculated for 1.232 af (77% of inflow)
 Center-of-Mass det. time= 279.3 min (1,056.9 - 777.6)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	11,722 cf	37.08'W x 227.97'L x 5.50'H Field B 46,496 cf Overall - 17,192 cf Embedded = 29,305 cf x 40.0% Voids
#2B	6.75'	17,192 cf	ADS_StormTech MC-3500 d +Cap x 155 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 155 Chambers in 5 Rows Cap Storage= +14.9 cf x 2 x 5 rows = 149.0 cf
#3	13.25'	6,100 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		35,013 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
13.25	600	0	0
13.75	4,900	1,375	1,375
14.00	8,200	1,638	3,013
14.25	16,500	3,088	6,100

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	10.00'	36.0" Round Culvert L= 55.9' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 10.00' / 7.59' S= 0.0431 ' S= 0.0431 ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	14.24'	50.0' long x 0.7' breadth Concrete Curb Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 Coef. (English) 2.76 2.82 2.93 3.09 3.18 3.22 3.27 3.30 3.32 3.31 3.32

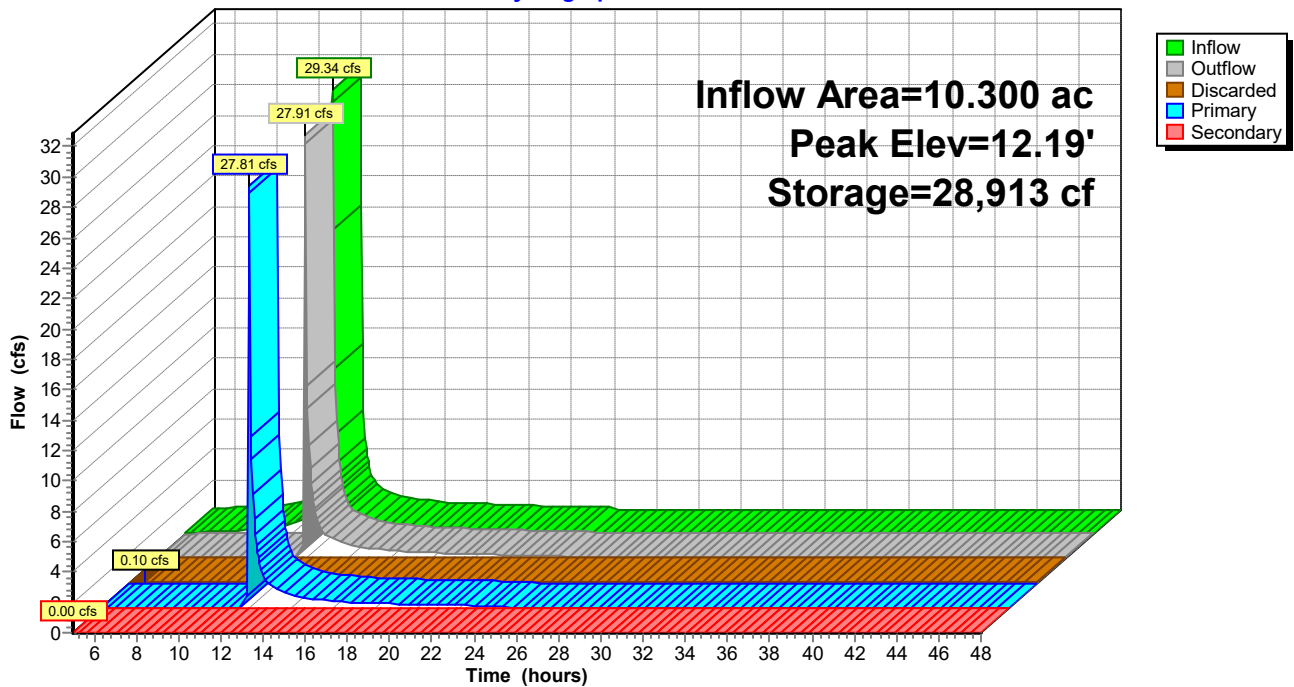
Discarded OutFlow Max=0.10 cfs @ 5.80 hrs HW=6.08' (Free Discharge)
 ↳1=Exfiltration (Exfiltration Controls 0.10 cfs)

Primary OutFlow Max=25.90 cfs @ 12.04 hrs HW=12.09' (Free Discharge)
 ↳2=Culvert (Inlet Controls 25.90 cfs @ 4.92 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge)
 ↳3=Concrete Curb (Controls 0.00 cfs)

Pond C-1: Chamber Series 1

Hydrograph



Summary for Pond C-4: Chamber Series 4

Inflow Area = 8.900 ac, 0.00% Impervious, Inflow Depth > 1.58" for 1-Year event
 Inflow = 22.13 cfs @ 11.99 hrs, Volume= 1.175 af
 Outflow = 17.34 cfs @ 12.06 hrs, Volume= 0.845 af, Atten= 22%, Lag= 4.4 min
 Discarded = 0.07 cfs @ 7.60 hrs, Volume= 0.254 af
 Primary = 17.27 cfs @ 12.06 hrs, Volume= 0.592 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 12.75' @ 12.07 hrs Surf.Area= 6,391 sf Storage= 21,785 cf

Plug-Flow detention time= 397.3 min calculated for 0.844 af (72% of inflow)
 Center-of-Mass det. time= 304.6 min (1,103.4 - 798.9)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	8,911 cf	29.92'W x 213.63'L x 5.50'H Field B 35,151 cf Overall - 12,874 cf Embedded = 22,277 cf x 40.0% Voids
#2B	6.75'	12,874 cf	ADS_StormTech MC-3500 d +Cap x 116 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 116 Chambers in 4 Rows Cap Storage= +14.9 cf x 2 x 4 rows = 119.2 cf
#3	14.10'	8,015 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		29,800 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
14.10	400	0	0
14.60	2,400	700	700
14.80	6,300	870	1,570
15.10	10,000	2,445	4,015
15.50	10,000	4,000	8,015

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	11.00'	36.0" Round Culvert L= 24.3' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 11.00' / 9.42' S= 0.0650 ' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

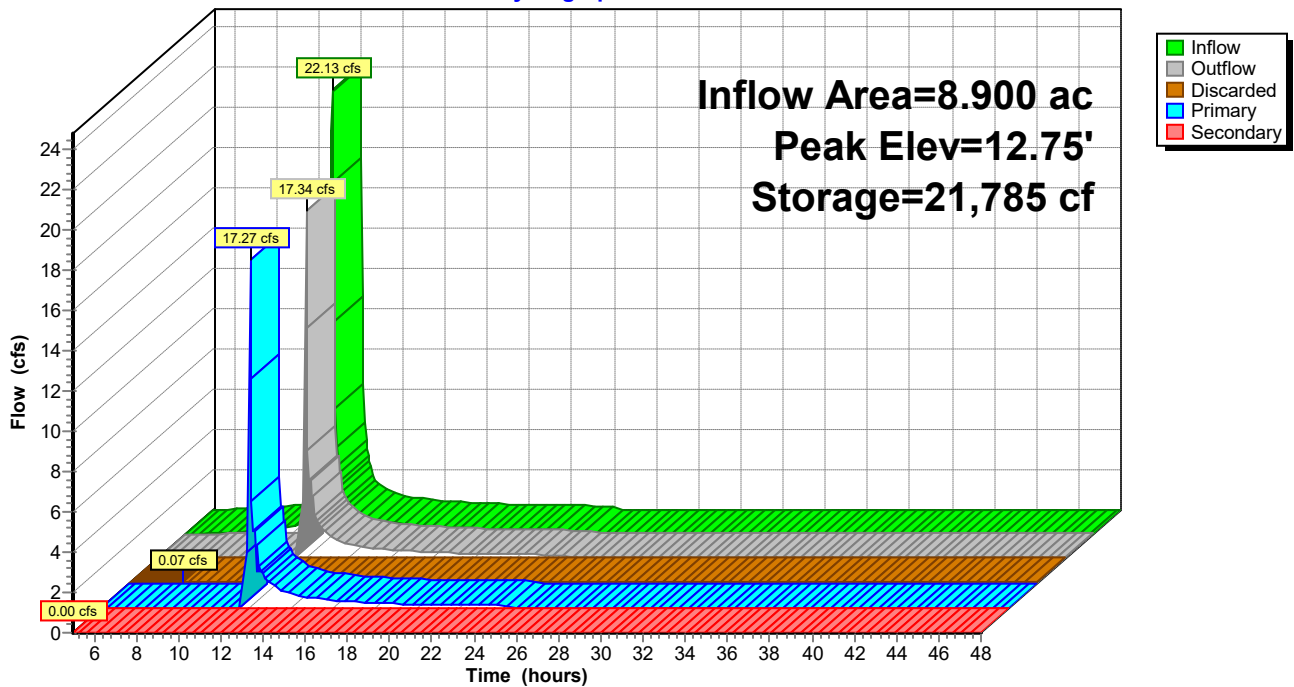
Discarded OutFlow Max=0.07 cfs @ 7.60 hrs HW=6.10' (Free Discharge)
 ↳1=Exfiltration (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=15.10 cfs @ 12.06 hrs HW=12.52' (Free Discharge)
 ↳2=Culvert (Inlet Controls 15.10 cfs @ 4.20 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge)
 ↳3=Wharf (Controls 0.00 cfs)

Pond C-4: Chamber Series 4

Hydrograph



Summary for Pond C-5: Chamber Series 5

Inflow Area = 5.200 ac, 0.00% Impervious, Inflow Depth > 1.58" for 1-Year event
 Inflow = 13.09 cfs @ 11.99 hrs, Volume= 0.687 af
 Outflow = 0.43 cfs @ 14.80 hrs, Volume= 0.434 af, Atten= 97%, Lag= 168.8 min
 Discarded = 0.11 cfs @ 9.00 hrs, Volume= 0.373 af
 Primary = 0.32 cfs @ 14.80 hrs, Volume= 0.062 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 12.84' @ 14.80 hrs Surf.Area= 4,801 sf Storage= 20,773 cf

Plug-Flow detention time= 879.5 min calculated for 0.434 af (63% of inflow)
 Center-of-Mass det. time= 777.3 min (1,575.8 - 798.5)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	7,757 cf	28.50'W x 168.47'L x 6.75'H Field B 32,409 cf Overall - 13,016 cf Embedded = 19,393 cf x 40.0% Voids
#2B	6.75'	13,016 cf	ADS_StormTech MC-4500 b +Cap x 120 Inside #1 Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap 120 Chambers in 3 Rows Cap Storage= +39.5 cf x 2 x 3 rows = 237.0 cf
#3	14.60'	7,420 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		28,193 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
14.60	200	0	0
14.80	1,000	120	120
15.00	10,000	1,100	1,220
15.50	14,800	6,200	7,420

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	1.000 in/hr Exfiltration over Surface area
#2	Primary	12.60'	36.0" Round Culvert L= 62.8' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 12.60' / 12.29' S= 0.0049 ' / Cc= 0.900 n= 0.013 Cast iron, coated, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

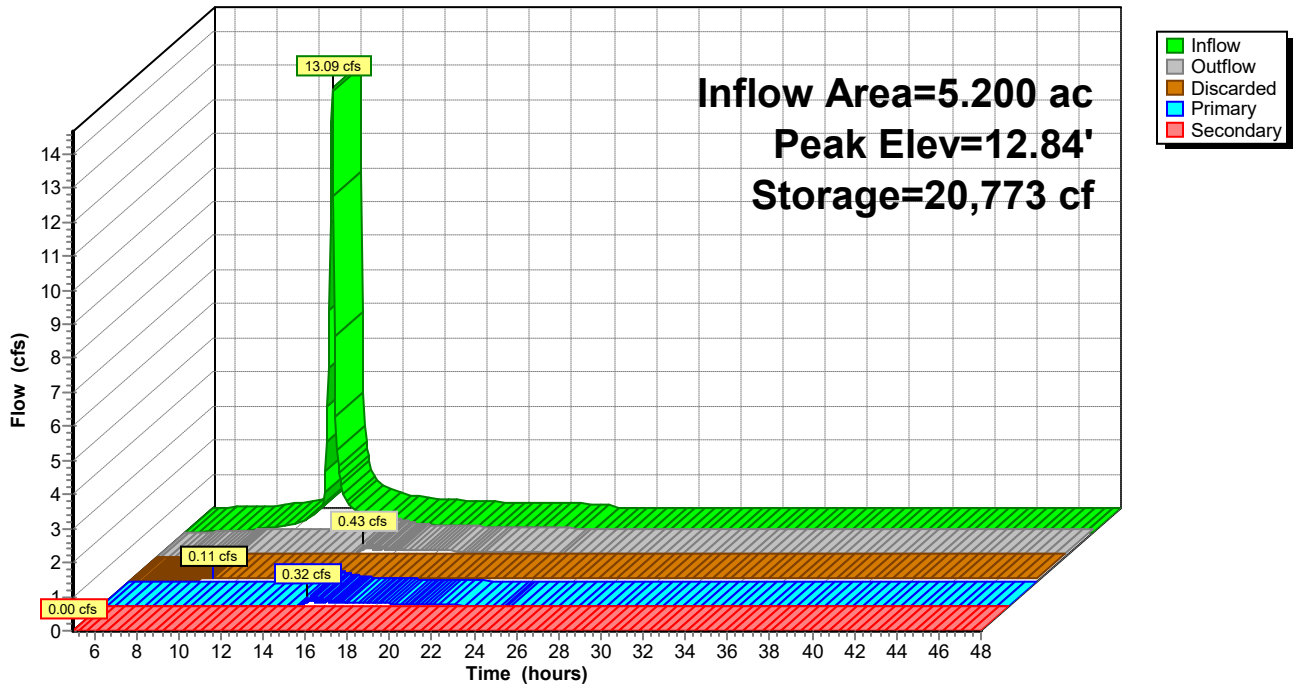
Discarded OutFlow Max=0.11 cfs @ 9.00 hrs HW=6.10' (Free Discharge)
 ↳1=Exfiltration (Exfiltration Controls 0.11 cfs)

Primary OutFlow Max=0.31 cfs @ 14.80 hrs HW=12.84' (Free Discharge)
 ↳2=Culvert (Barrel Controls 0.31 cfs @ 1.84 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge)
 ↳3=Wharf (Controls 0.00 cfs)

Pond C-5: Chamber Series 5

Hydrograph



Summary for Subcatchment DR-1: Building A & Storage

Runoff = 49.84 cfs @ 11.98 hrs, Volume= 2.772 af, Depth> 3.23"

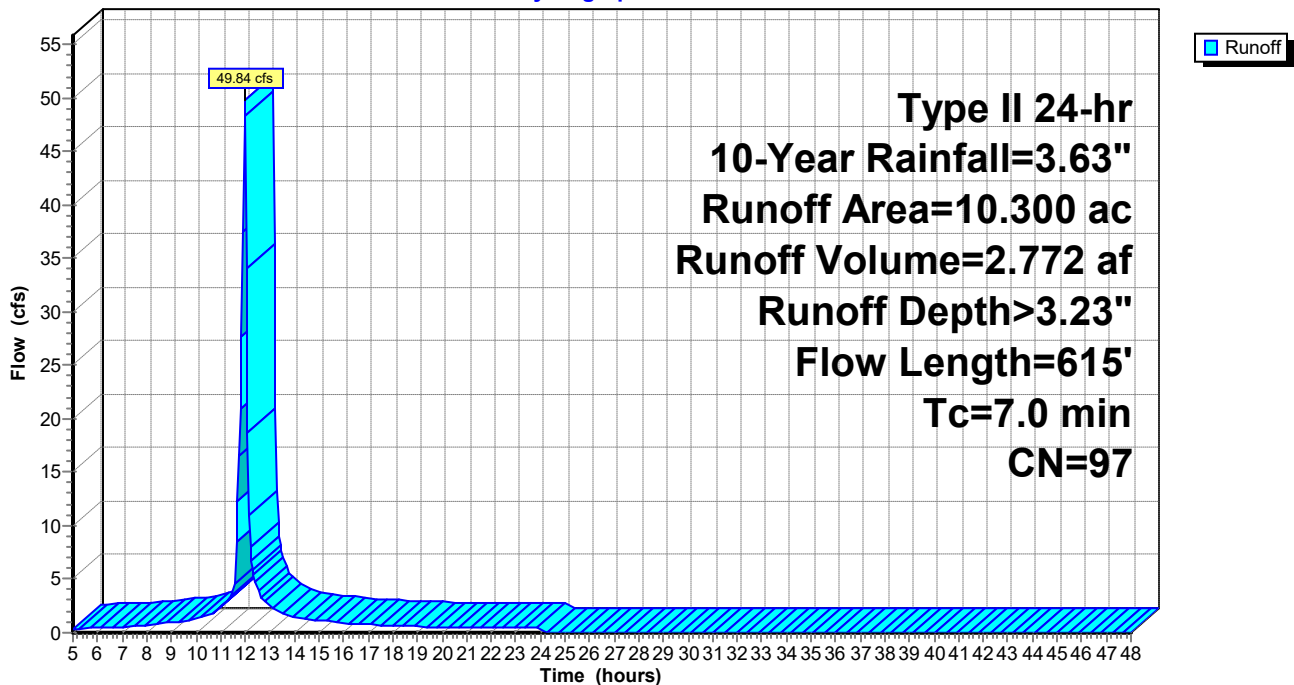
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 6.870	98	Building A
0.100	80	>75% Grass cover, Good, HSG D
* 3.330	95	Dense Graded Aggregate
10.300	97	Weighted Average
3.430		33.30% Pervious Area
6.870		66.70% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
3.1	300	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	215	0.0050	5.91	29.00	Pipe Channel, 30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63' n= 0.013
7.0	615	Total			

Subcatchment DR-1: Building A & Storage

Hydrograph



Summary for Subcatchment DR-10: Undisturbed Area

Runoff = 11.44 cfs @ 13.19 hrs, Volume= 2.752 af, Depth= 1.67"

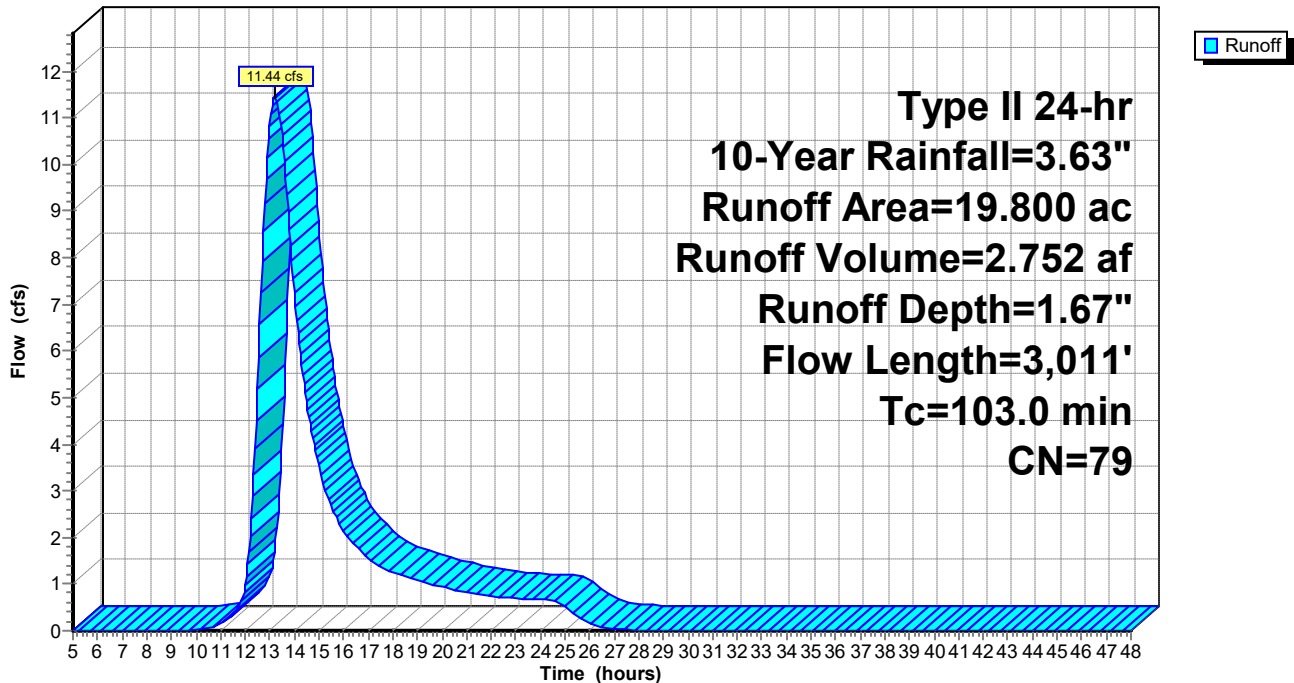
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
19.800	79	Woods, Fair, HSG D
19.800		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
19.7	150	0.0800	0.13		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"
3.0	200	0.0500	1.12		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
1.6	250	0.2600	2.55		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
78.7	2,361	0.0100	0.50		Shallow Concentrated Flow, Wetland Flow Woodland Kv= 5.0 fps
0.0	50	0.0500	22.86	161.57	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.012 Corrugated PP, smooth interior
103.0	3,011	Total			

Subcatchment DR-10: Undisturbed Area

Hydrograph



Summary for Subcatchment DR-11: Hudson River Bank

Runoff = 8.27 cfs @ 12.09 hrs, Volume= 0.556 af, Depth= 1.67"

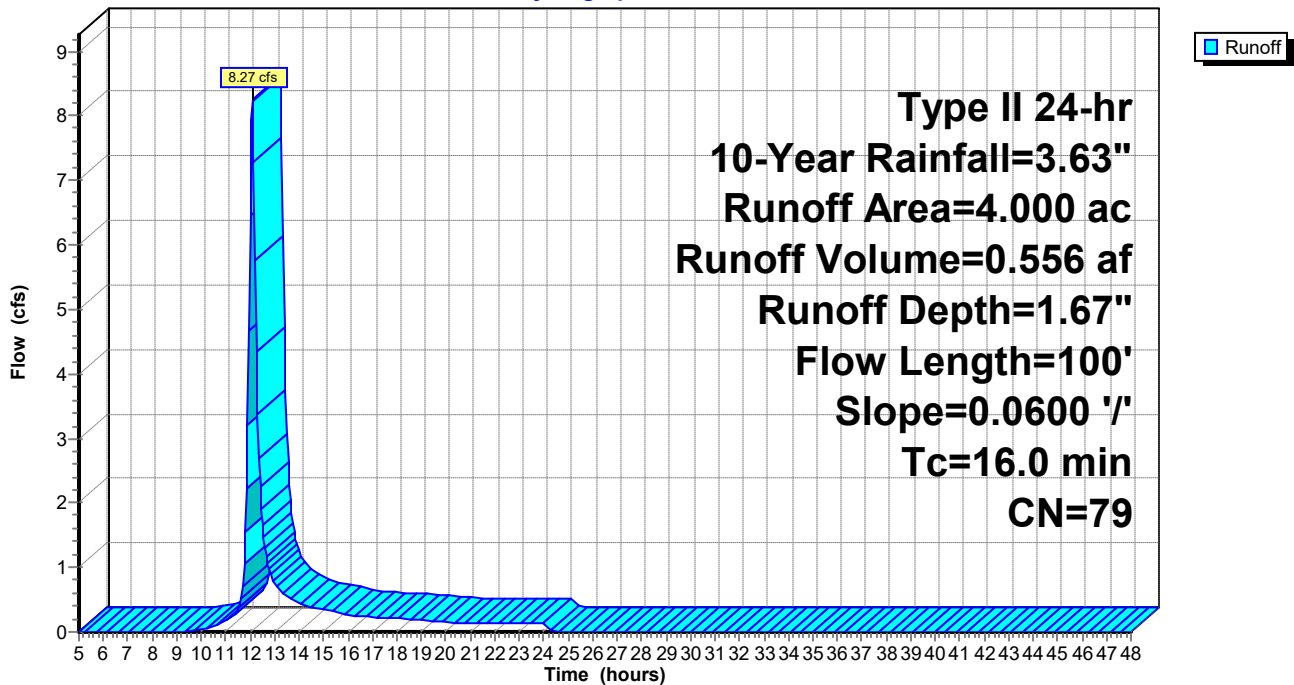
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
4.000	79	Woods, Fair, HSG D
4.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.0	100	0.0600	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-11: Hudson River Bank

Hydrograph



Summary for Subcatchment DR-12: Normans Kill Bank

Runoff = 6.12 cfs @ 11.97 hrs, Volume= 0.311 af, Depth> 2.66"

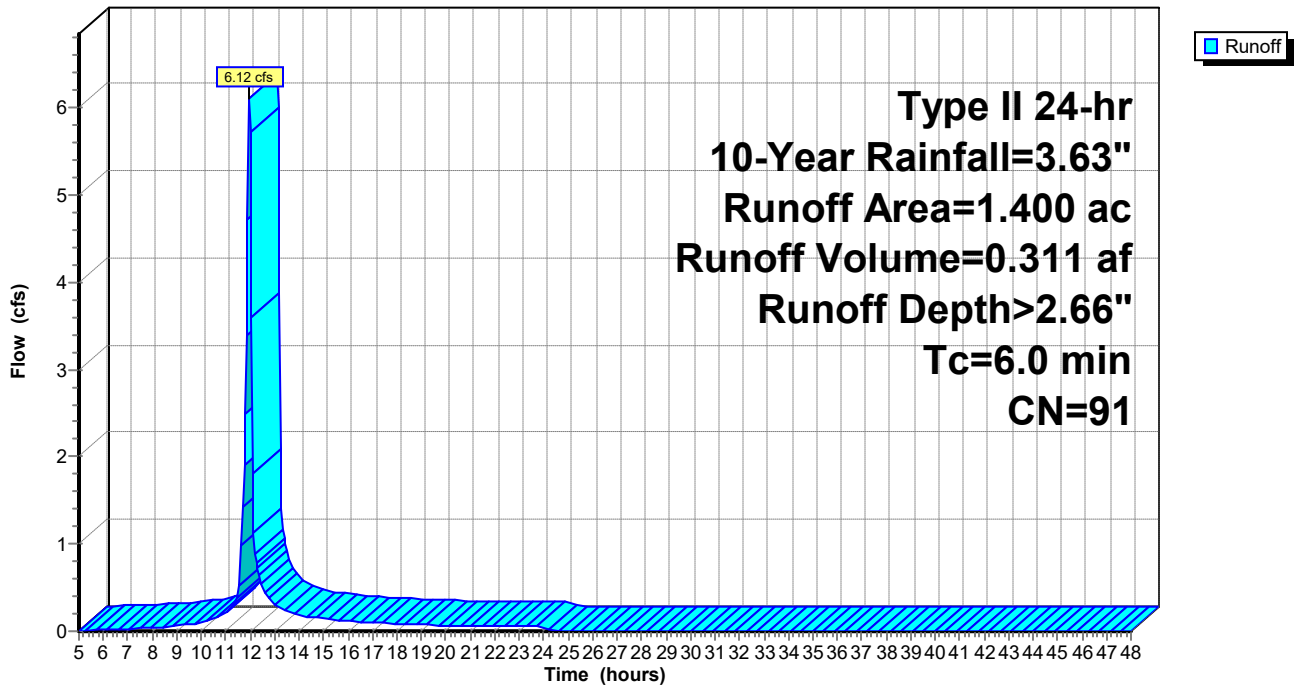
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
0.430	79	Woods, Fair, HSG D
0.970	96	Gravel surface, HSG D
1.400	91	Weighted Average
1.400		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-12: Normans Kill Bank

Hydrograph



Summary for Subcatchment DR-13: Roadway

Runoff = 1.16 cfs @ 11.99 hrs, Volume= 0.063 af, Depth= 0.63"

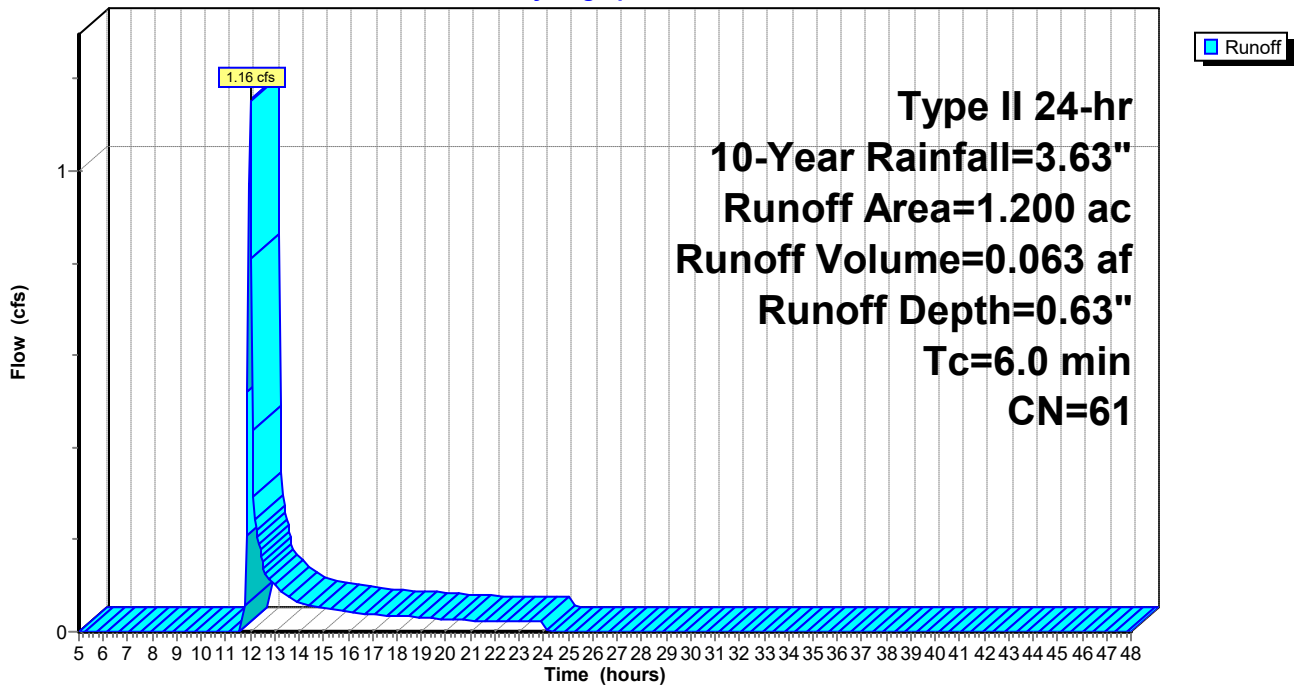
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 0.450	98	Pavement
0.750	39	>75% Grass cover, Good, HSG A
1.200	61	Weighted Average
0.750		62.50% Pervious Area
0.450		37.50% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-13: Roadway

Hydrograph



Summary for Subcatchment DR-14: Roadway

Runoff = 2.86 cfs @ 11.98 hrs, Volume= 0.137 af, Depth= 1.27"

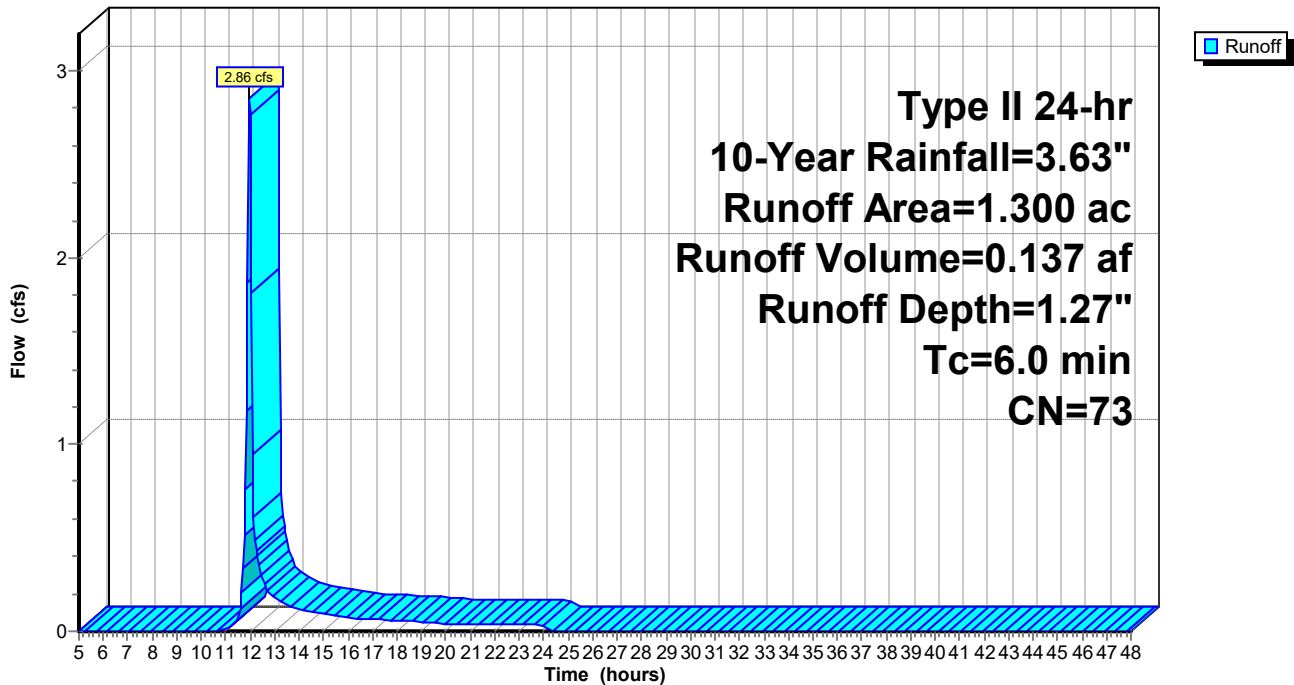
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 0.550	98	New Pavement
0.550	39	>75% Grass cover, Good, HSG A
* 0.200	98	Mill & Fill of Old Pavement
1.300	73	Weighted Average
0.550		42.31% Pervious Area
0.750		57.69% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-14: Roadway

Hydrograph



Summary for Subcatchment DR-15: Roadway

Runoff = 4.79 cfs @ 11.96 hrs, Volume= 0.254 af, Depth> 3.05"

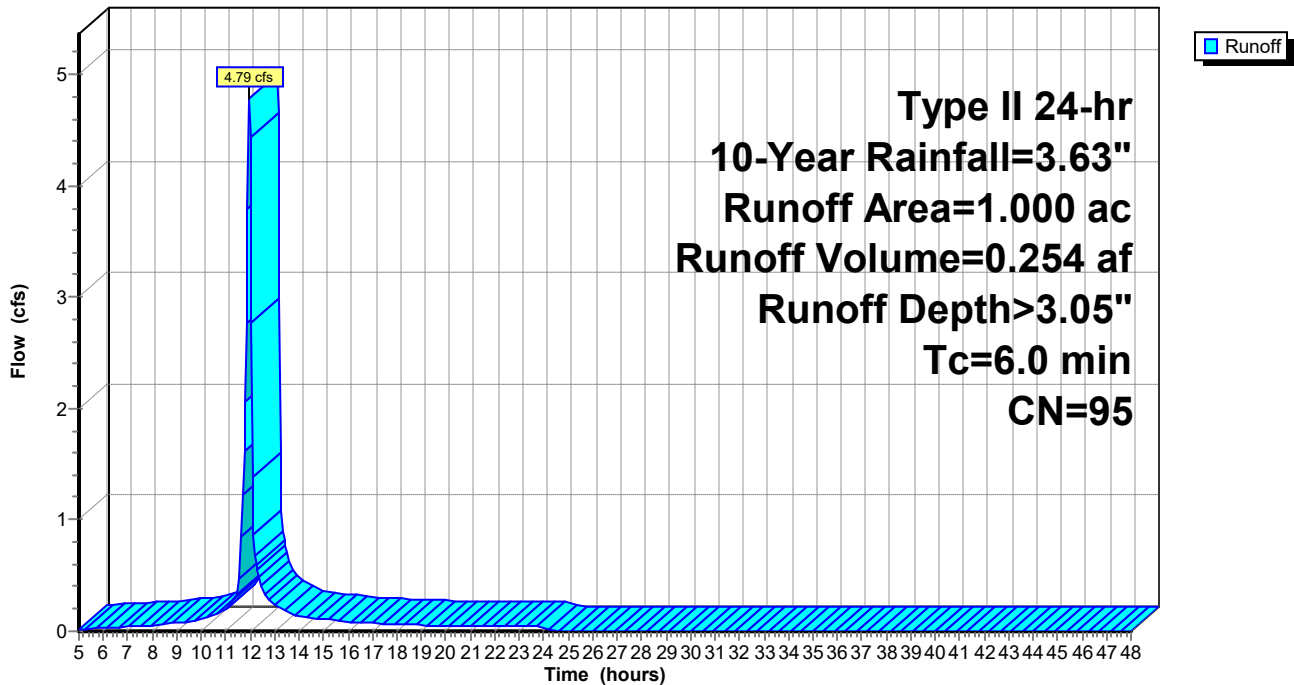
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 0.050	98	New Pavement
0.050	39	>75% Grass cover, Good, HSG A
* 0.900	98	Mill & Fill of Old Pavement
1.000	95	Weighted Average
0.050		5.00% Pervious Area
0.950		95.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-15: Roadway

Hydrograph



Summary for Subcatchment DR-16: Undisturbed Area

Runoff = 0.06 cfs @ 15.50 hrs, Volume= 0.050 af, Depth= 0.07"

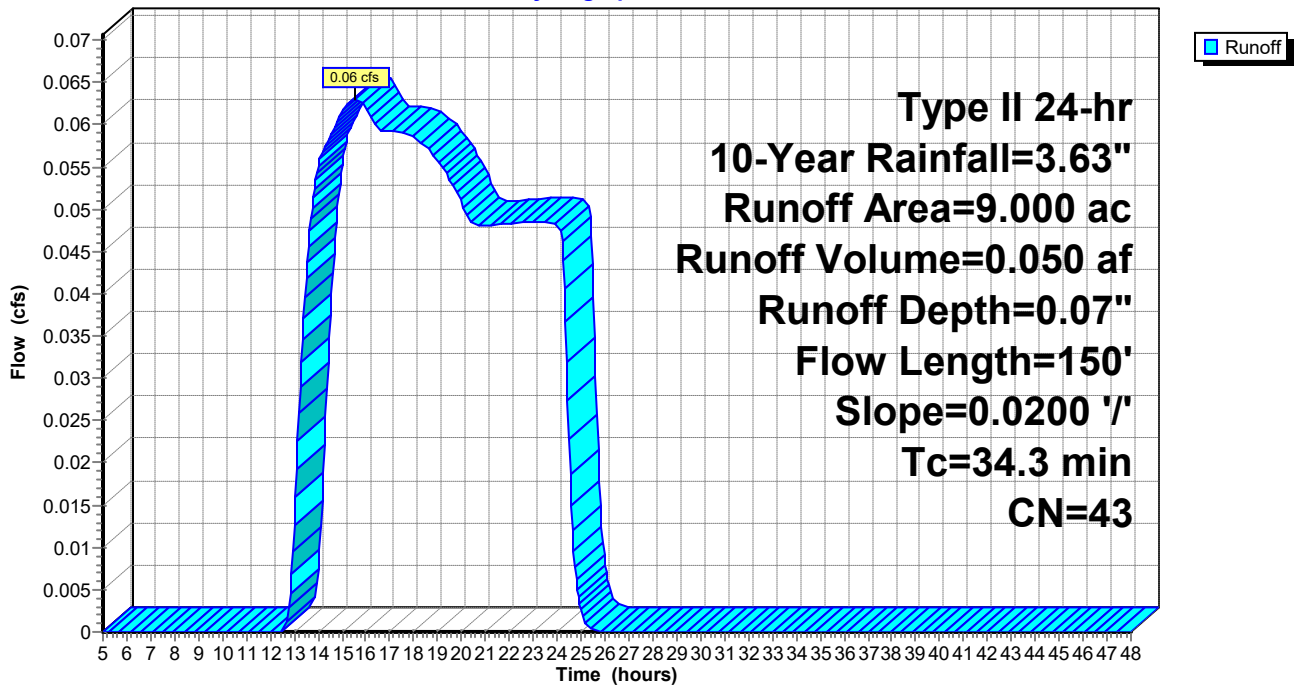
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
9.000	43	Woods/grass comb., Fair, HSG A
9.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
34.3	150	0.0200	0.07		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-16: Undisturbed Area

Hydrograph



Summary for Subcatchment DR-17: Roadway

Runoff = 2.85 cfs @ 11.97 hrs, Volume= 0.140 af, Depth= 2.21"

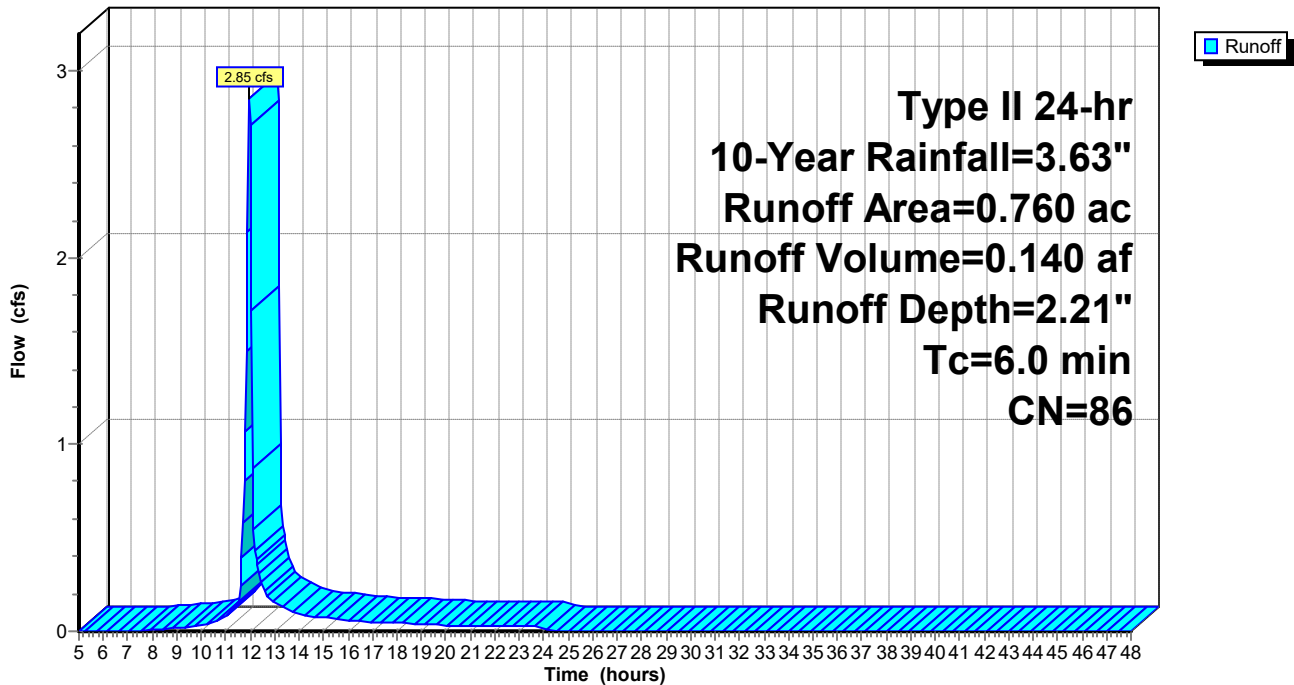
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 0.140	98	Road Widening
* 0.460	98	Roadway
0.160	39	>75% Grass cover, Good, HSG A
0.760	86	Weighted Average
0.160		21.05% Pervious Area
0.600		78.95% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-17: Roadway

Hydrograph



Summary for Subcatchment DR-2: Storage

Runoff = 24.00 cfs @ 12.00 hrs, Volume= 1.352 af, Depth> 2.95"

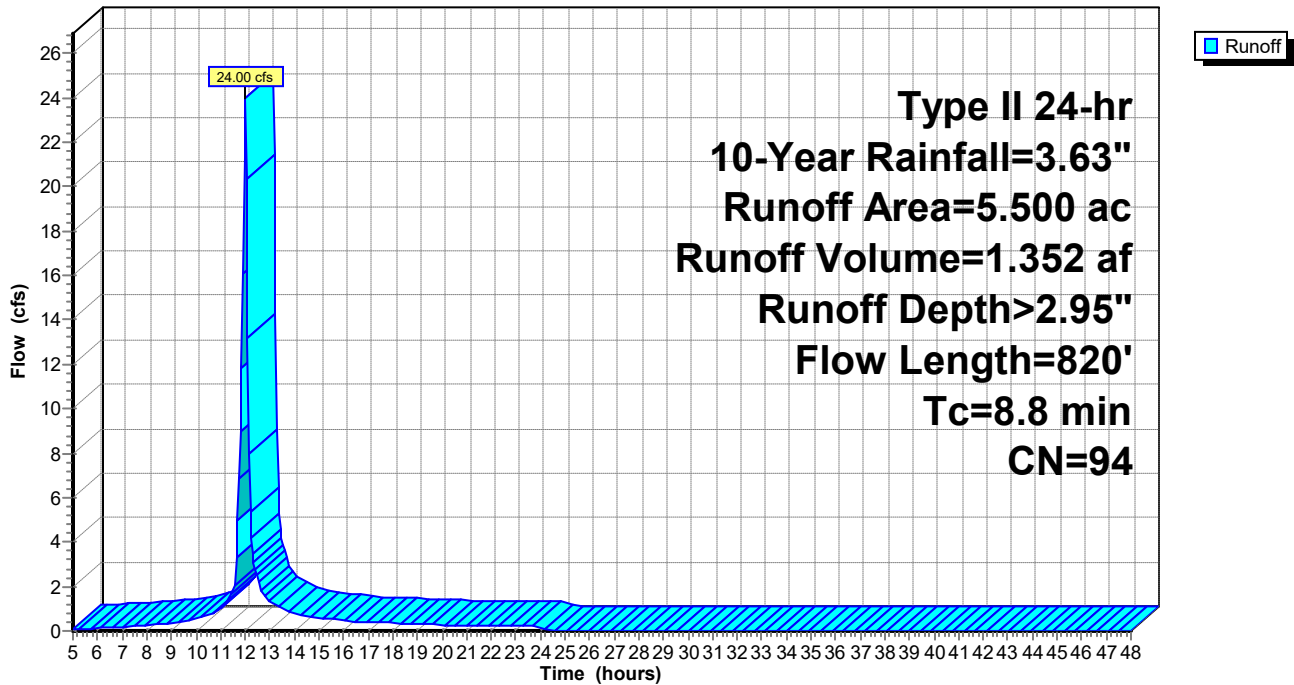
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 5.300	95	Dense Graded Aggregate
0.200	80	>75% Grass cover, Good, HSG D
5.500	94	Weighted Average
5.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
4.9	470	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	250	0.0050	6.67	47.16	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.013
8.8	820	Total			

Subcatchment DR-2: Storage

Hydrograph



Summary for Subcatchment DR-3: Rail & Storage

Runoff = 47.69 cfs @ 12.00 hrs, Volume= 2.793 af, Depth> 3.05"

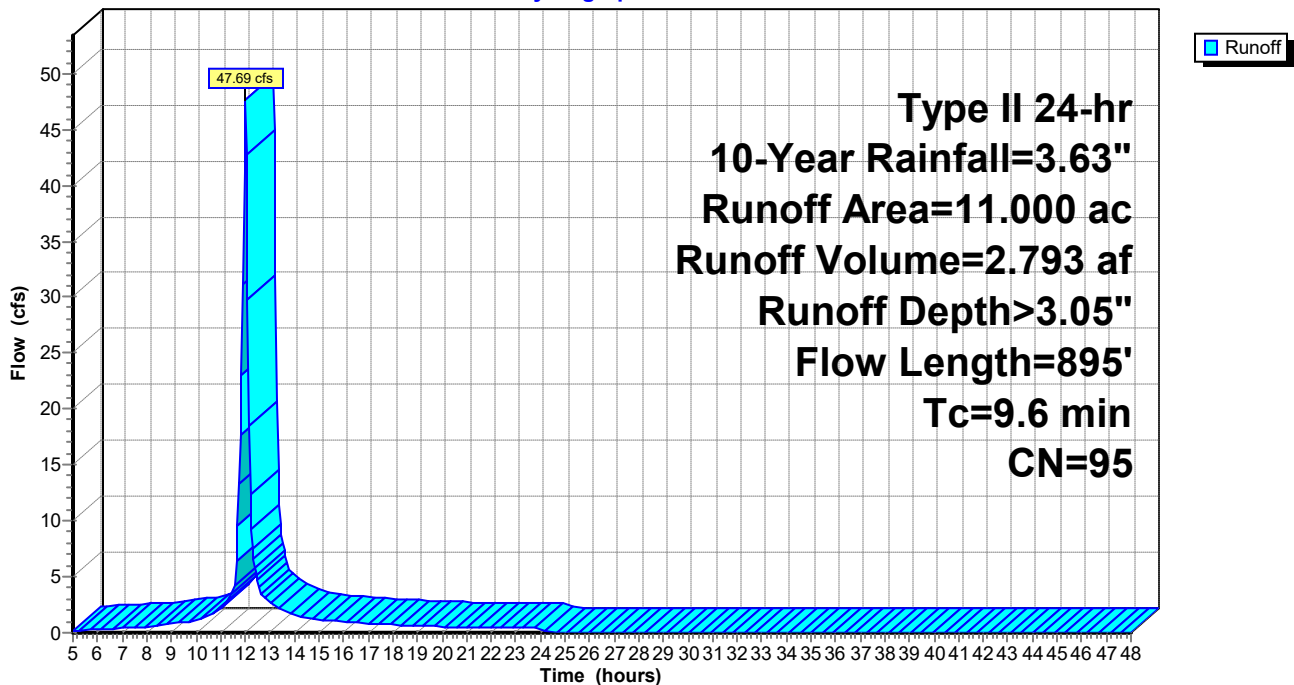
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 8.300	95	Compacted Gravel
0.400	80	>75% Grass cover, Good, HSG D
* 2.300	98	Rail
11.000	95	Weighted Average
8.700		79.09% Pervious Area
2.300		20.91% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
5.4	525	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.9	270	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
9.6	895	Total			

Subcatchment DR-3: Rail & Storage

Hydrograph



Summary for Subcatchment DR-4: Storage

Runoff = 39.82 cfs @ 11.99 hrs, Volume= 2.188 af, Depth> 2.95"

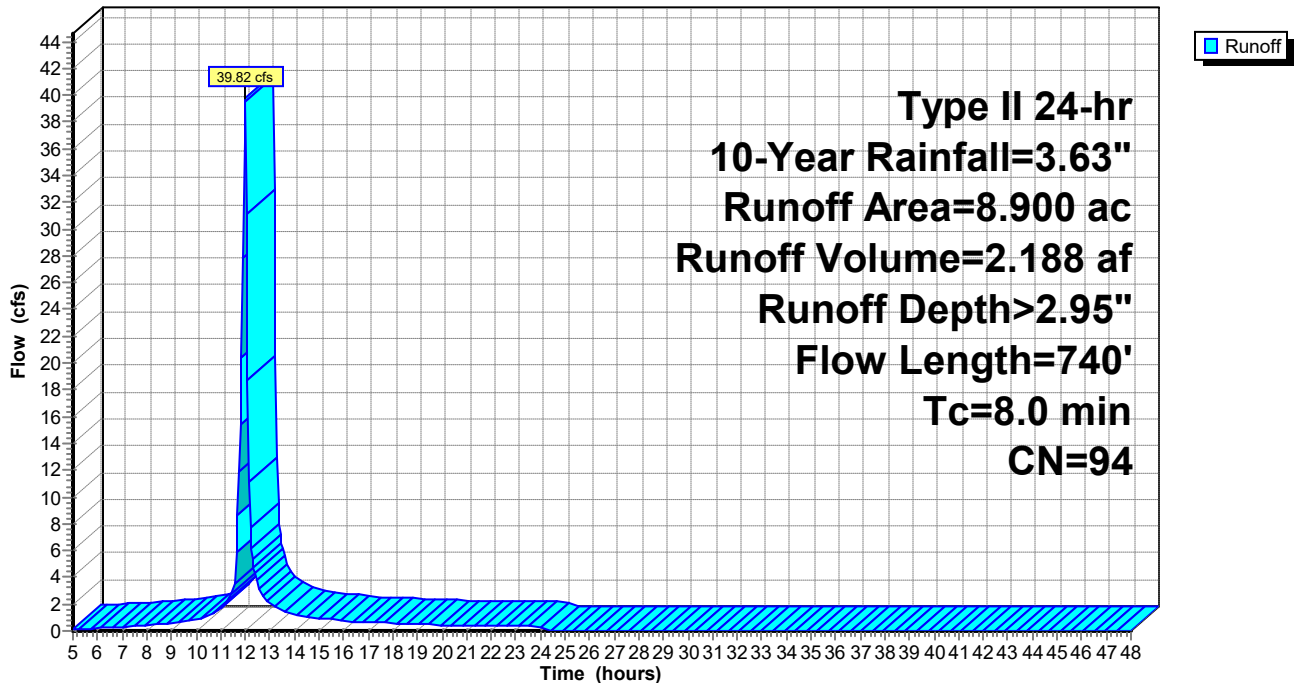
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 8.600	95	Compacted Gravel
0.300	80	>75% Grass cover, Good, HSG D
8.900	94	Weighted Average
8.900		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
4.1	400	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	240	0.0050	6.67	47.16	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.013 Corrugated PE, smooth interior
8.0	740	Total			

Subcatchment DR-4: Storage

Hydrograph



Summary for Subcatchment DR-5: Storage

Runoff = 23.53 cfs @ 11.98 hrs, Volume= 1.279 af, Depth> 2.95"

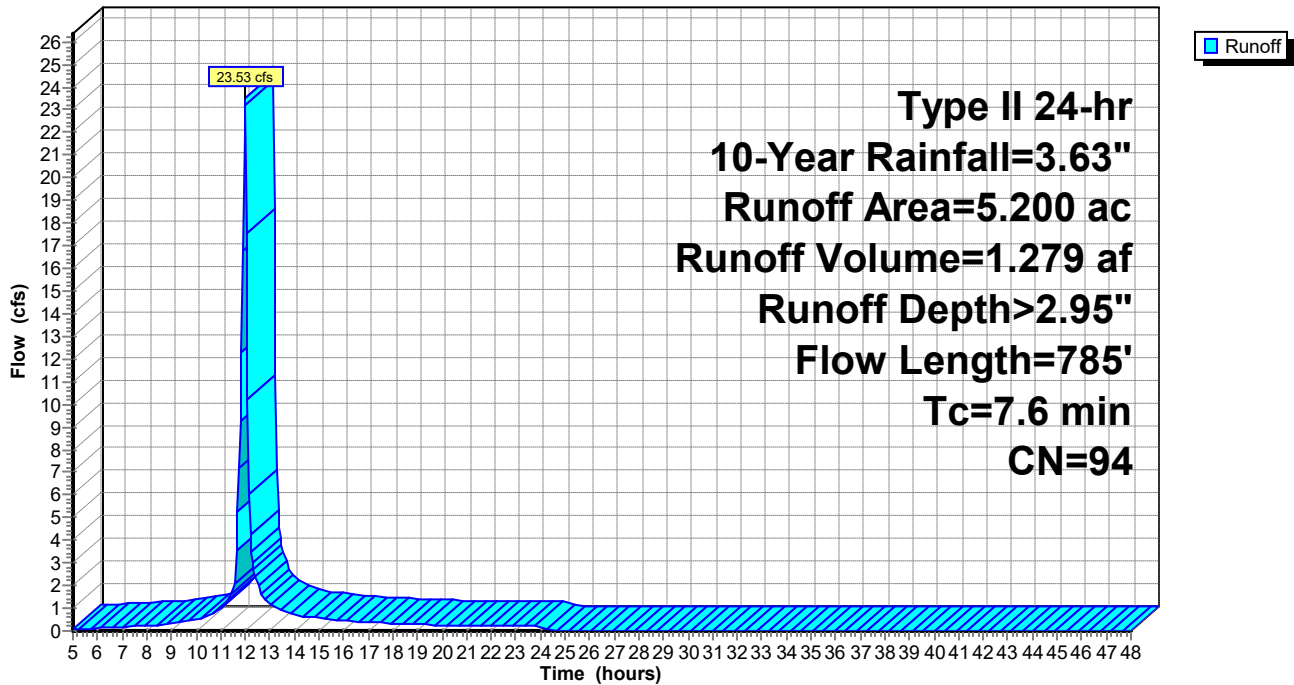
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 4.900	95	Dense Graded Aggregate
0.300	80	>75% Grass cover, Good, HSG D
5.200	94	Weighted Average
5.200		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
3.0	285	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.3	400	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
7.6	785	Total			

Subcatchment DR-5: Storage

Hydrograph



Summary for Subcatchment DR-6: Buldings B & D

Runoff = 53.49 cfs @ 12.00 hrs, Volume= 3.088 af, Depth> 3.14"

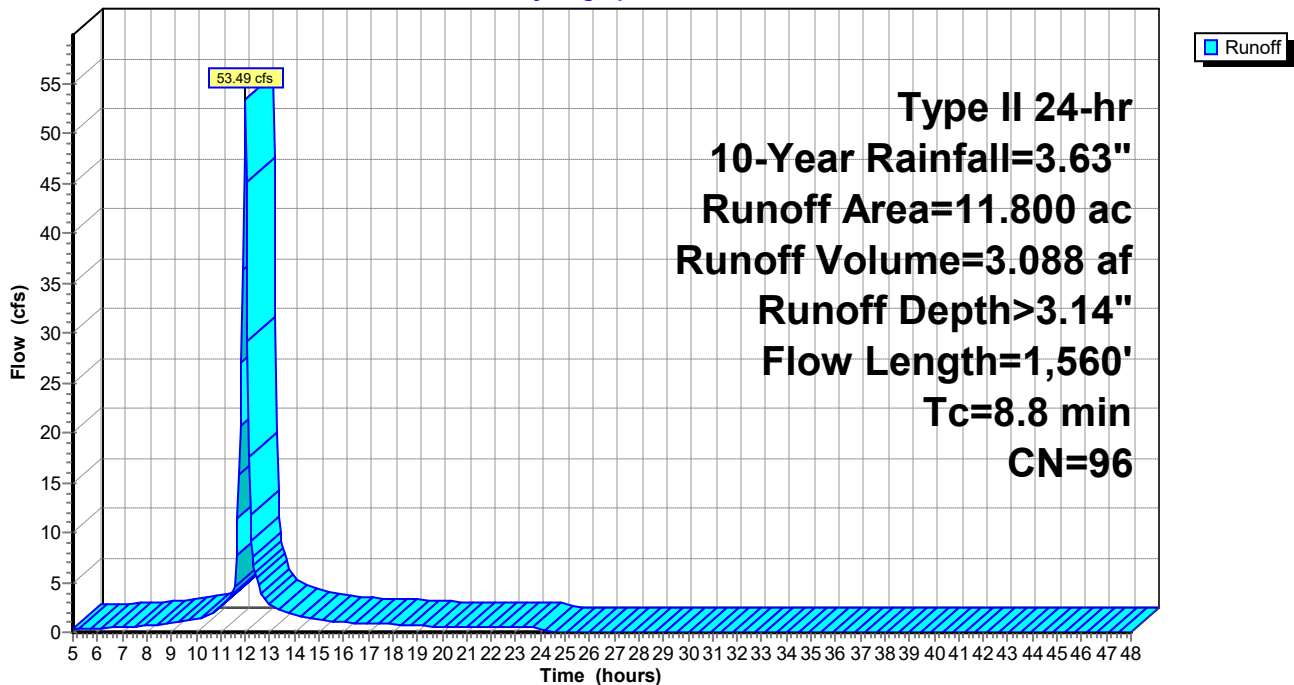
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 2.549	98	Building B
* 1.413	98	Building D
0.200	80	>75% Grass cover, Good, HSG D
* 7.638	95	Dense Graded Aggregate
11.800	96	Weighted Average
7.838		66.42% Pervious Area
3.962		33.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
1.0	100	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.5	1,360	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
8.8	1,560	Total			

Subcatchment DR-6: Buldings B & D

Hydrograph



Summary for Subcatchment DR-7: Building C & Rail

Runoff = 38.26 cfs @ 12.00 hrs, Volume= 2.277 af, Depth> 3.14"

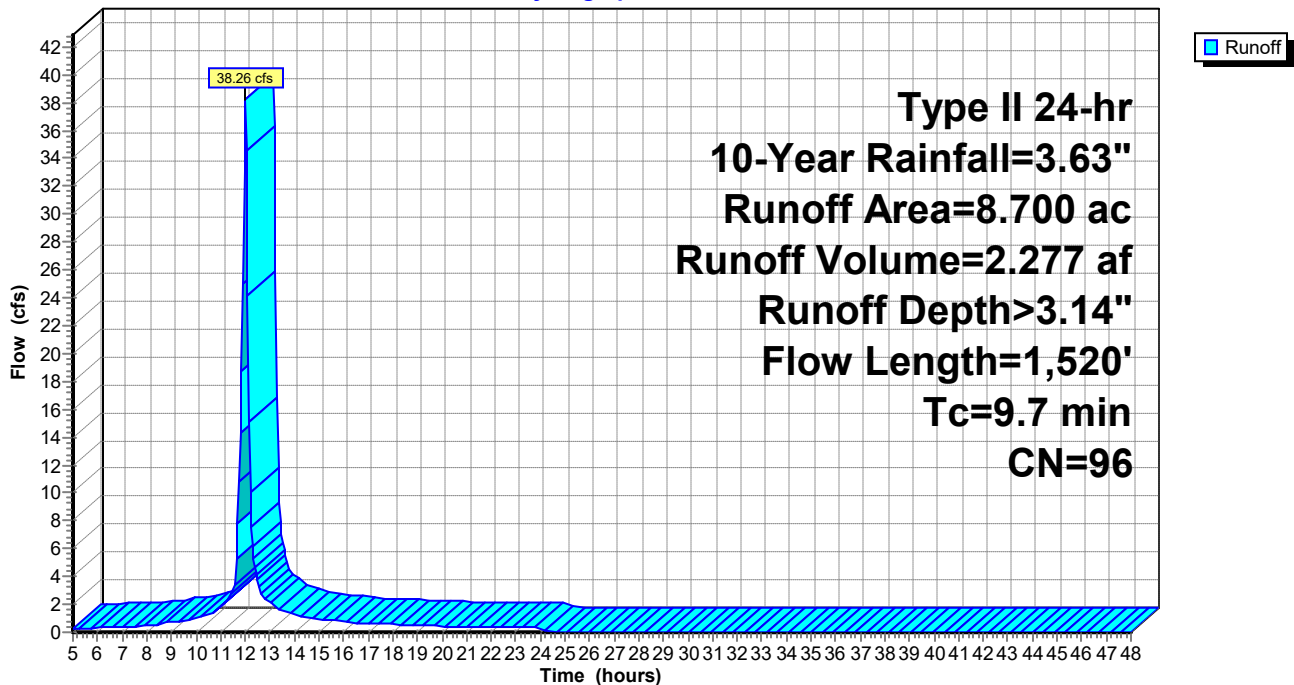
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 3.030	98	Building C
* 0.970	98	Rail
* 4.400	95	Dense Graded Aggregate
0.300	80	>75% Grass cover, Good, HSG D
8.700	96	Weighted Average
4.700		54.02% Pervious Area
4.000		45.98% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
2.6	250	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
3.8	1,170	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
9.7	1,520	Total			

Subcatchment DR-7: Building C & Rail

Hydrograph



Summary for Subcatchment DR-8A: Parking

Runoff = 9.10 cfs @ 11.96 hrs, Volume= 0.482 af, Depth> 3.05"

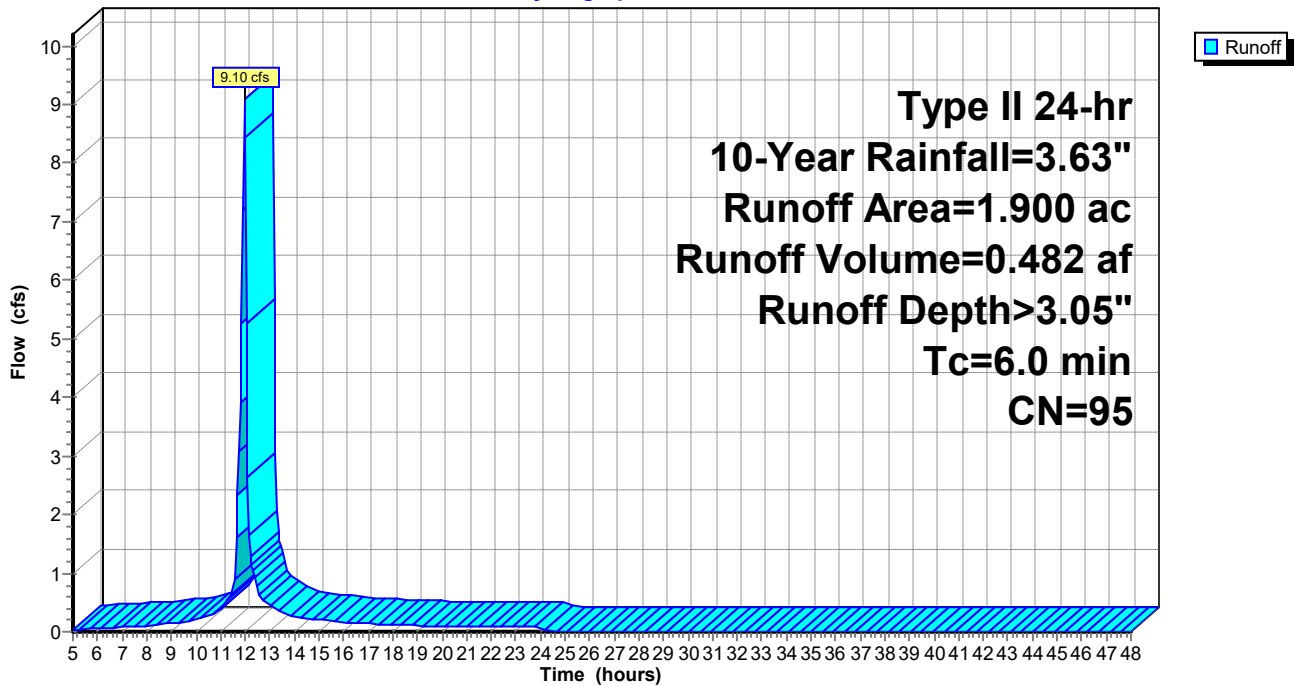
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 1.600	98	Parking
0.300	80	>75% Grass cover, Good, HSG D
1.900	95	Weighted Average
0.300		15.79% Pervious Area
1.600		84.21% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-8A: Parking

Hydrograph



Summary for Subcatchment DR-8B: Roadway & Pond

Runoff = 3.63 cfs @ 11.97 hrs, Volume= 0.178 af, Depth= 2.13"

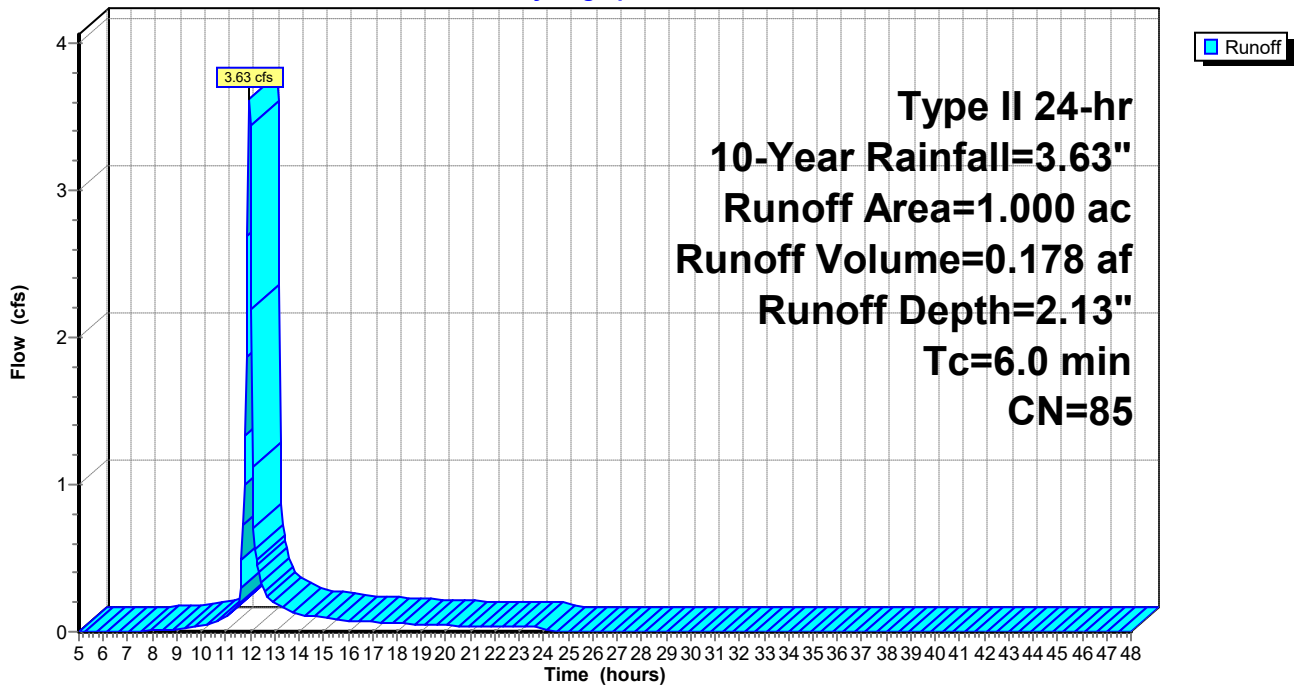
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 0.300	98	Roadway
0.700	80	>75% Grass cover, Good, HSG D
1.000	85	Weighted Average
0.700		70.00% Pervious Area
0.300		30.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-8B: Roadway & Pond

Hydrograph



Summary for Subcatchment DR-9A: Parking & Substation

Runoff = 7.03 cfs @ 12.04 hrs, Volume= 0.457 af, Depth> 3.05"

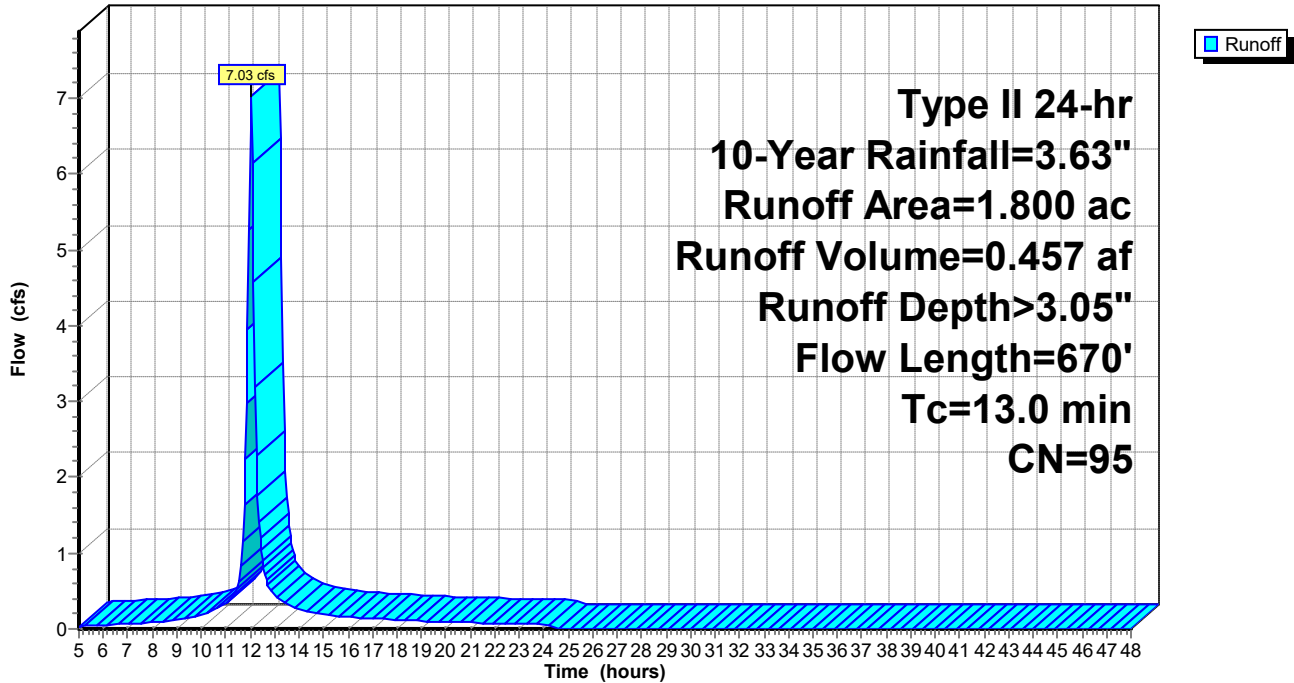
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
0.230	80	>75% Grass cover, Good, HSG D
* 0.200	92	Compacted Gravel
* 1.200	98	Parking and Road
* 0.170	98	Substation
1.800	95	Weighted Average
0.430		23.89% Pervious Area
1.370		76.11% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0200	1.19		Sheet Flow, Parking Lot Runoff Smooth surfaces n= 0.011 P2= 2.40"
11.6	570	0.0030	0.82		Shallow Concentrated Flow, Grass Lined Ditch to Pond Grassed Waterway Kv= 15.0 fps
13.0	670	Total			

Subcatchment DR-9A: Parking & Substation

Hydrograph



Summary for Subcatchment DR-9B: Roadway

Runoff = 15.47 cfs @ 11.96 hrs, Volume= 0.738 af, Depth= 2.21"

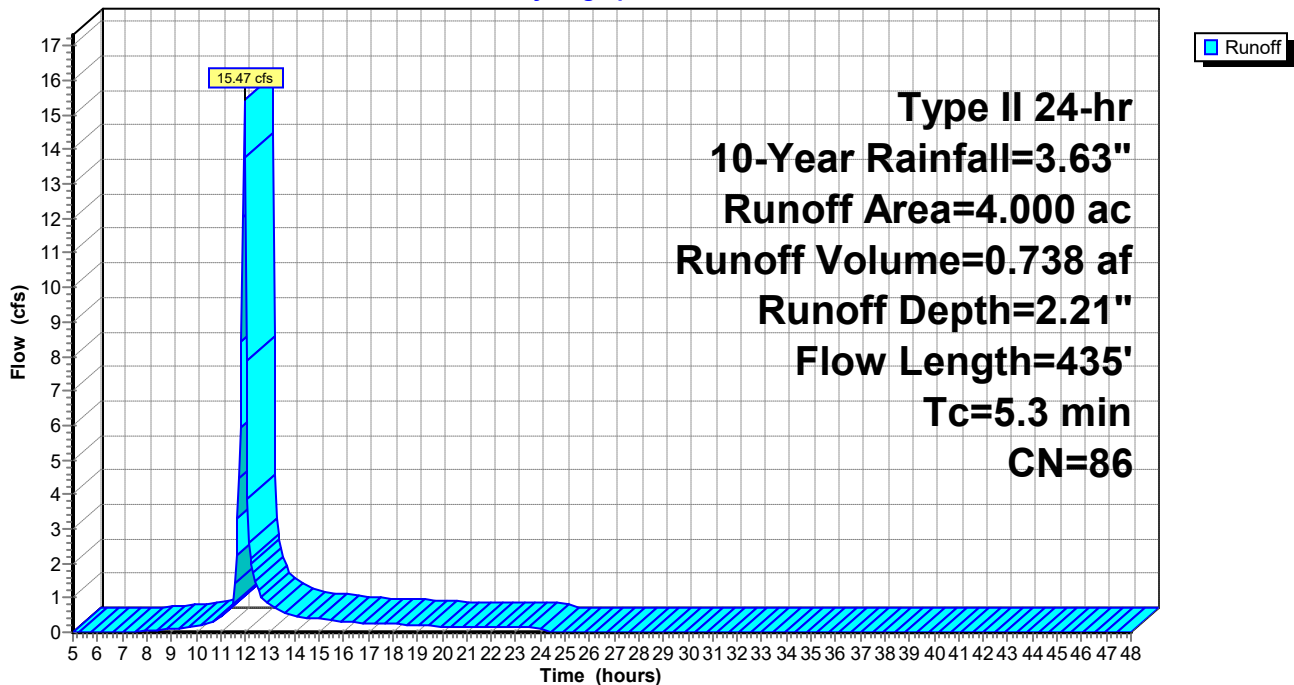
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 1.050	95	Dense Graded Aggregate
* 0.480	98	Roadway
2.470	80	>75% Grass cover, Good, HSG D
4.000	86	Weighted Average
3.520		88.00% Pervious Area
0.480		12.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.0250	0.46		Sheet Flow, Dense Graded Aggregate Yard n= 0.040 P2= 2.40"
1.3	230	0.0100	3.07	9.20	Channel Flow, Grass lined ditch Area= 3.0 sf Perim= 4.0' r= 0.75' n= 0.040 Earth, cobble bottom, clean sides
0.4	105	0.0050	4.20	7.43	Pipe Channel, driveway culvert 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013 Corrugated PE, smooth interior
5.3	435	Total			

Subcatchment DR-9B: Roadway

Hydrograph



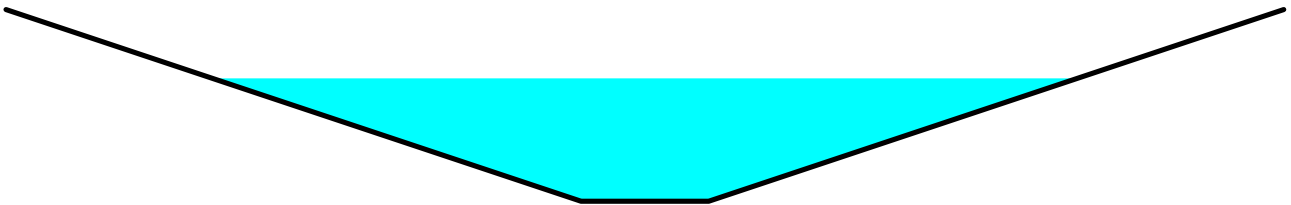
Summary for Reach 1R: Swale

Inflow Area = 1.900 ac, 84.21% Impervious, Inflow Depth > 3.05" for 10-Year event
 Inflow = 9.10 cfs @ 11.96 hrs, Volume= 0.482 af
 Outflow = 7.58 cfs @ 12.11 hrs, Volume= 0.482 af, Atten= 17%, Lag= 8.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.05 fps, Min. Travel Time= 5.6 min
 Avg. Velocity = 0.60 fps, Avg. Travel Time= 19.1 min

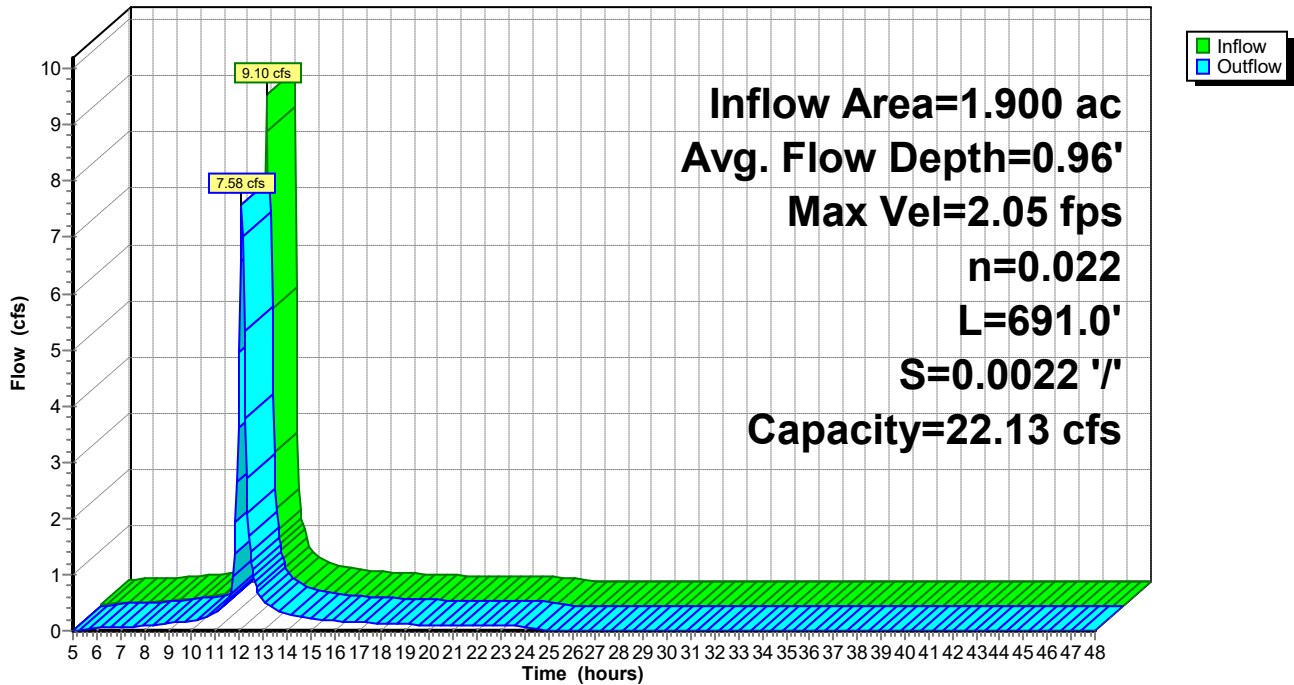
Peak Storage= 2,580 cf @ 12.01 hrs
 Average Depth at Peak Storage= 0.96' , Surface Width= 6.77'
 Bank-Full Depth= 1.50' Flow Area= 8.3 sf, Capacity= 22.13 cfs

1.00' x 1.50' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 10.00'
 Length= 691.0' Slope= 0.0022 ' / '
 Inlet Invert= 15.50', Outlet Invert= 14.00'



Reach 1R: Swale

Hydrograph



Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 1.93" for 10-Year event
 Inflow = 12.46 cfs @ 13.19 hrs, Volume= 4.590 af
 Outflow = 5.17 cfs @ 17.95 hrs, Volume= 4.381 af, Atten= 58%, Lag= 285.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.09 fps, Min. Travel Time= 192.0 min
 Avg. Velocity = 0.04 fps, Avg. Travel Time= 405.5 min

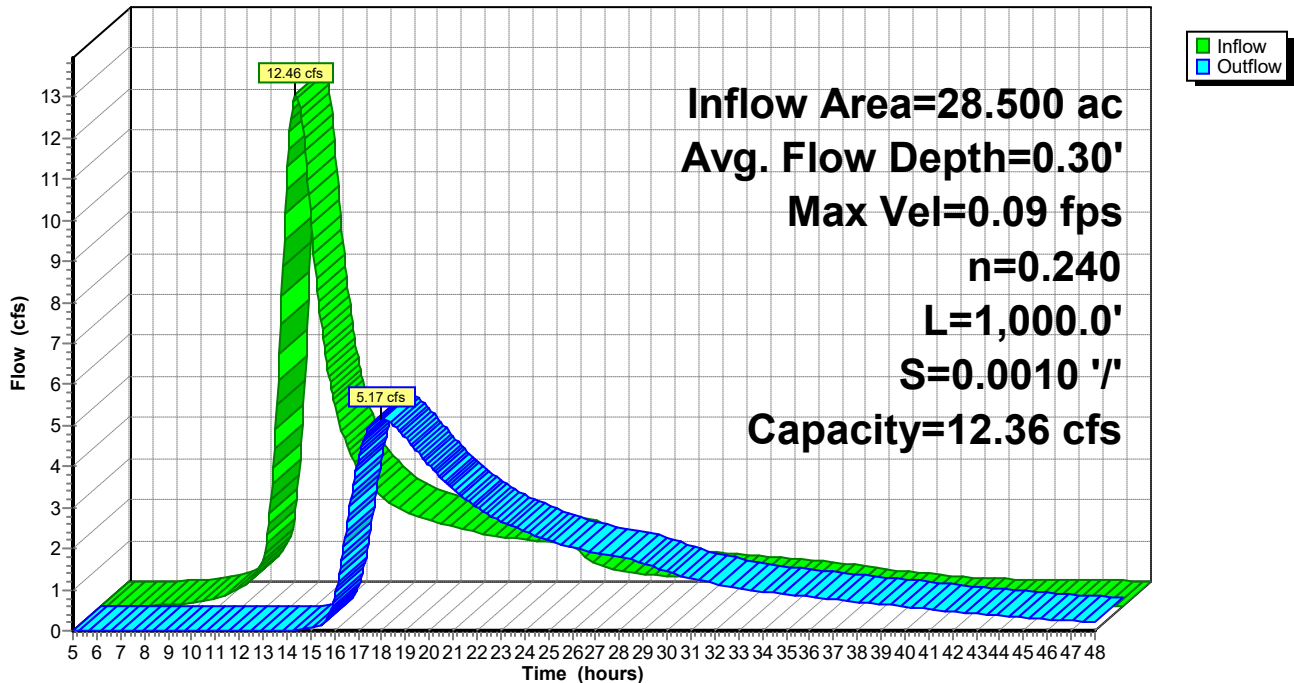
Peak Storage= 59,576 cf @ 14.75 hrs
 Average Depth at Peak Storage= 0.30' , Surface Width= 201.78'
 Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240
 Side Slope Z-value= 3.0 ' / ' Top Width= 203.00'
 Length= 1,000.0' Slope= 0.0010 ' / '
 Inlet Invert= 6.00', Outlet Invert= 5.00'



Reach 1W: Wetland #1 / Analysis Point 1A

Hydrograph



Summary for Reach 2R: Overflow

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 2.45" for 10-Year event
 Inflow = 0.64 cfs @ 14.62 hrs, Volume= 1.187 af
 Outflow = 0.64 cfs @ 14.63 hrs, Volume= 1.186 af, Atten= 0%, Lag= 0.7 min

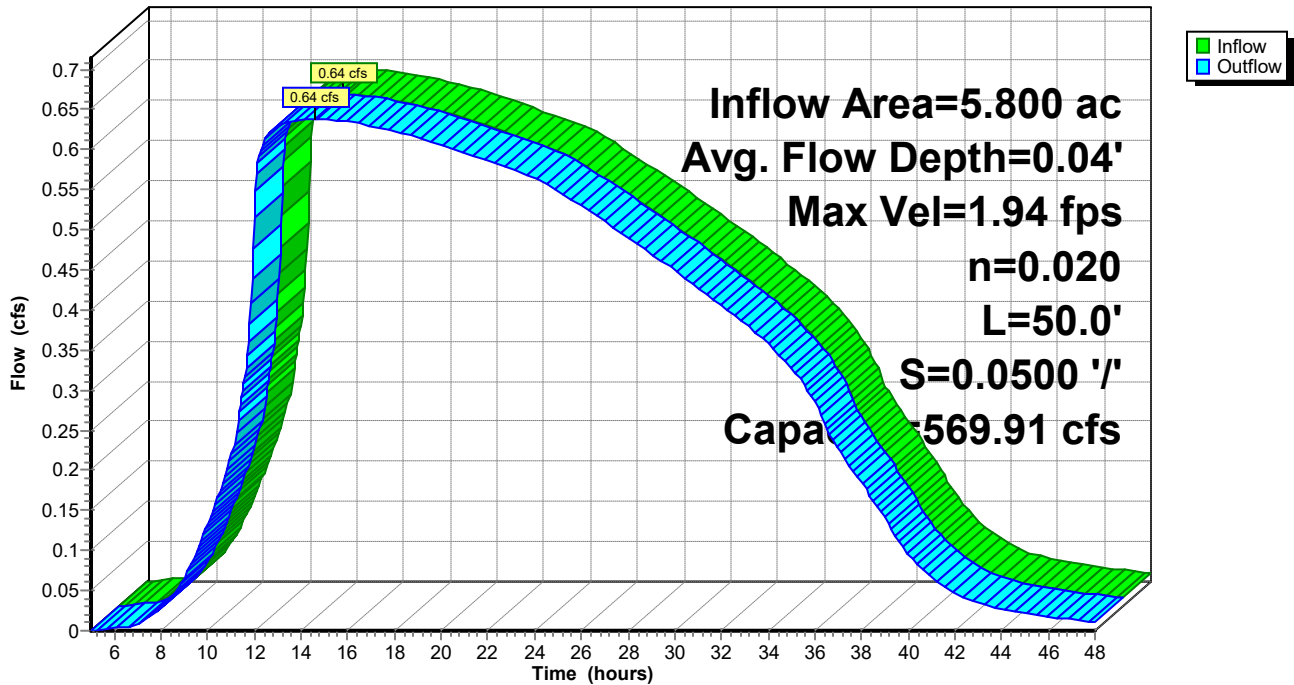
Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 1.94 fps, Min. Travel Time= 0.4 min
 Avg. Velocity = 1.56 fps, Avg. Travel Time= 0.5 min

Peak Storage= 16 cf @ 14.62 hrs
 Average Depth at Peak Storage= 0.04' , Surface Width= 8.24'
 Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 569.91 cfs

8.00' x 2.00' deep channel, n= 0.020 Corrugated PE, corrugated interior
 Side Slope Z-value= 3.0 '/' Top Width= 20.00'
 Length= 50.0' Slope= 0.0500 '/'
 Inlet Invert= 16.50', Outlet Invert= 14.00'



Reach 2R: Overflow
 Hydrograph



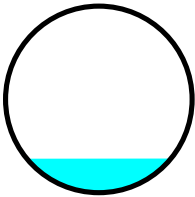
Summary for Reach 3R: Outlet Pipe

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 1.84" for 10-Year event
 Inflow = 5.17 cfs @ 17.95 hrs, Volume= 4.381 af
 Outflow = 5.17 cfs @ 17.95 hrs, Volume= 4.381 af, Atten= 0%, Lag= 0.4 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 4.73 fps, Min. Travel Time= 0.2 min
 Avg. Velocity = 2.76 fps, Avg. Travel Time= 0.4 min

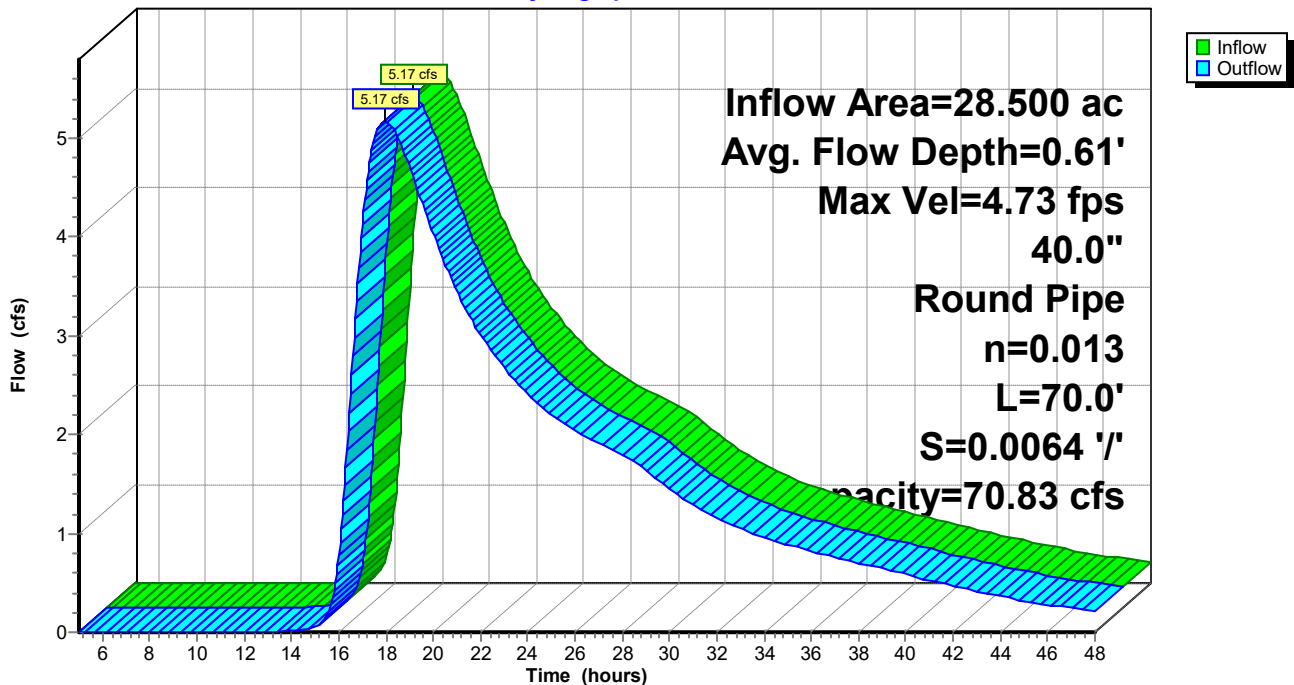
Peak Storage= 76 cf @ 17.95 hrs
 Average Depth at Peak Storage= 0.61' , Surface Width= 2.58'
 Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe
 n= 0.013 Corrugated PE, smooth interior
 Length= 70.0' Slope= 0.0064 '/'
 Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 3R: Outlet Pipe

Hydrograph



Summary for Reach 4R: Overflow

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 3.05" for 10-Year event
 Inflow = 4.69 cfs @ 11.98 hrs, Volume= 0.254 af
 Outflow = 4.56 cfs @ 12.00 hrs, Volume= 0.254 af, Atten= 3%, Lag= 0.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.73 fps, Min. Travel Time= 0.6 min
 Avg. Velocity = 0.70 fps, Avg. Travel Time= 2.4 min

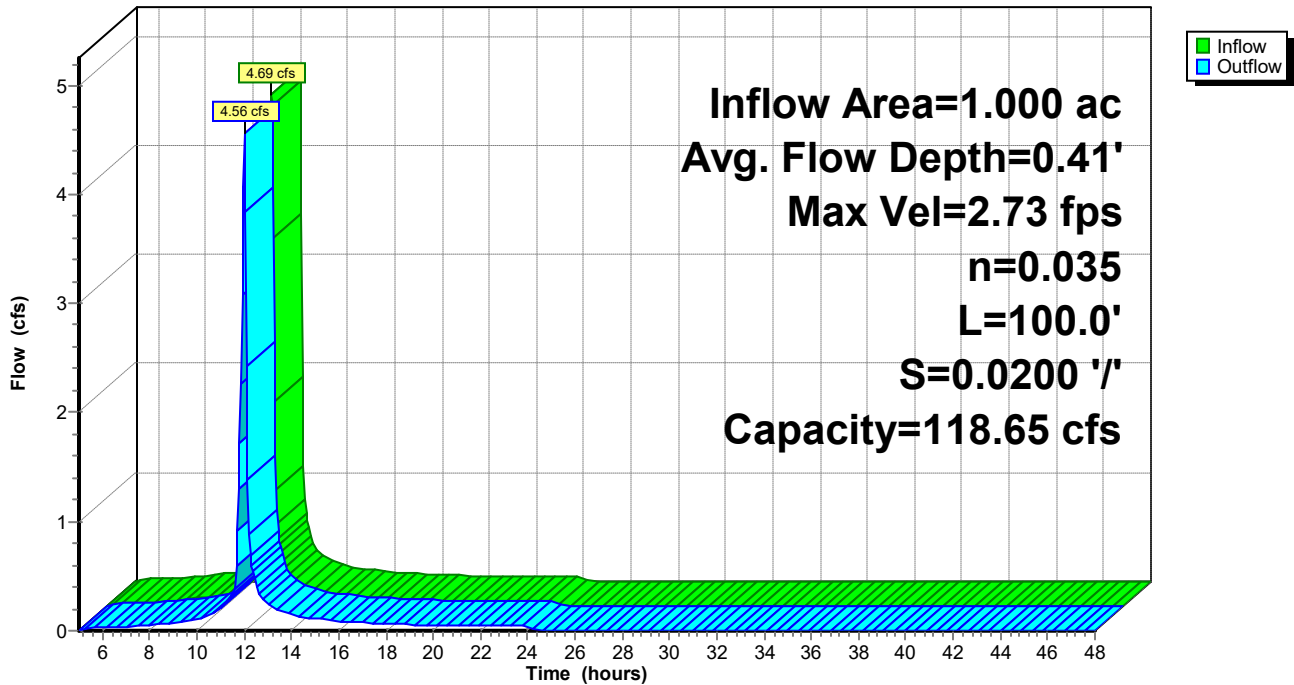
Peak Storage= 171 cf @ 11.99 hrs
 Average Depth at Peak Storage= 0.41' , Surface Width= 5.43'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 118.65 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'
 Length= 100.0' Slope= 0.0200 '/'
 Inlet Invert= 12.00', Outlet Invert= 10.00'



Reach 4R: Overflow

Hydrograph



Summary for Reach 5R: Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.00" for 10-Year event
 Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af
 Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min
 Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

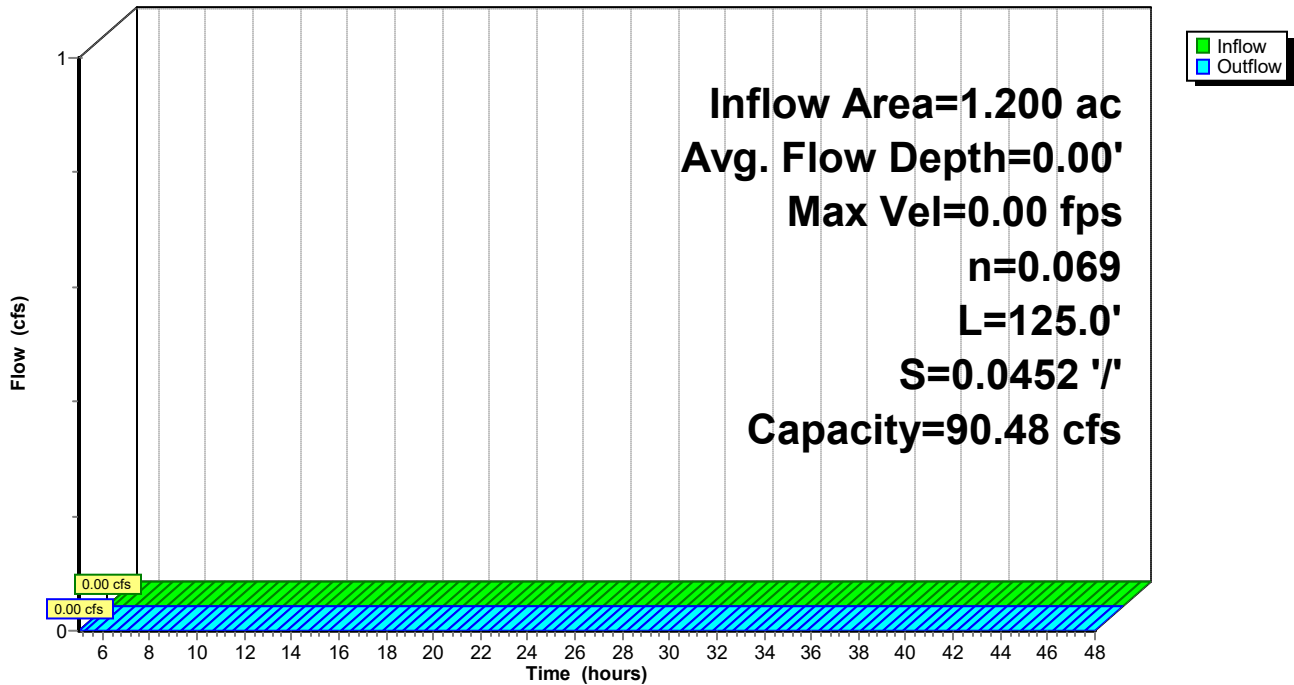
Peak Storage= 0 cf @ 5.00 hrs
 Average Depth at Peak Storage= 0.00'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 90.48 cfs

3.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'
 Length= 125.0' Slope= 0.0452 '/'
 Inlet Invert= 11.65', Outlet Invert= 6.00'



Reach 5R: Overflow

Hydrograph



Summary for Reach 6R: Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.00" for 10-Year event
 Inflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af
 Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min
 Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

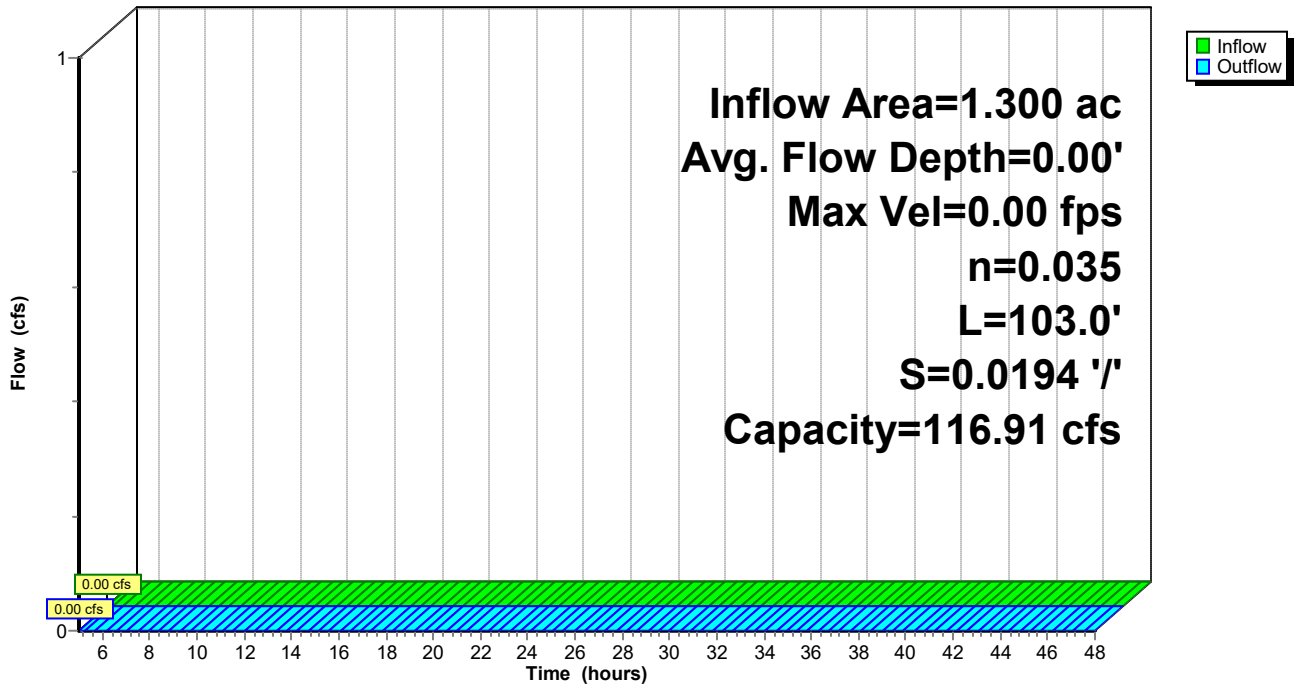
Peak Storage= 0 cf @ 5.00 hrs
 Average Depth at Peak Storage= 0.00'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 116.91 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'
 Length= 103.0' Slope= 0.0194 '/'
 Inlet Invert= 8.50', Outlet Invert= 6.50'



Reach 6R: Overflow

Hydrograph



Summary for Reach 7R: Overflow

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth > 2.70" for 10-Year event
 Inflow = 0.39 cfs @ 14.15 hrs, Volume= 0.652 af
 Outflow = 0.39 cfs @ 14.22 hrs, Volume= 0.652 af, Atten= 0%, Lag= 4.6 min

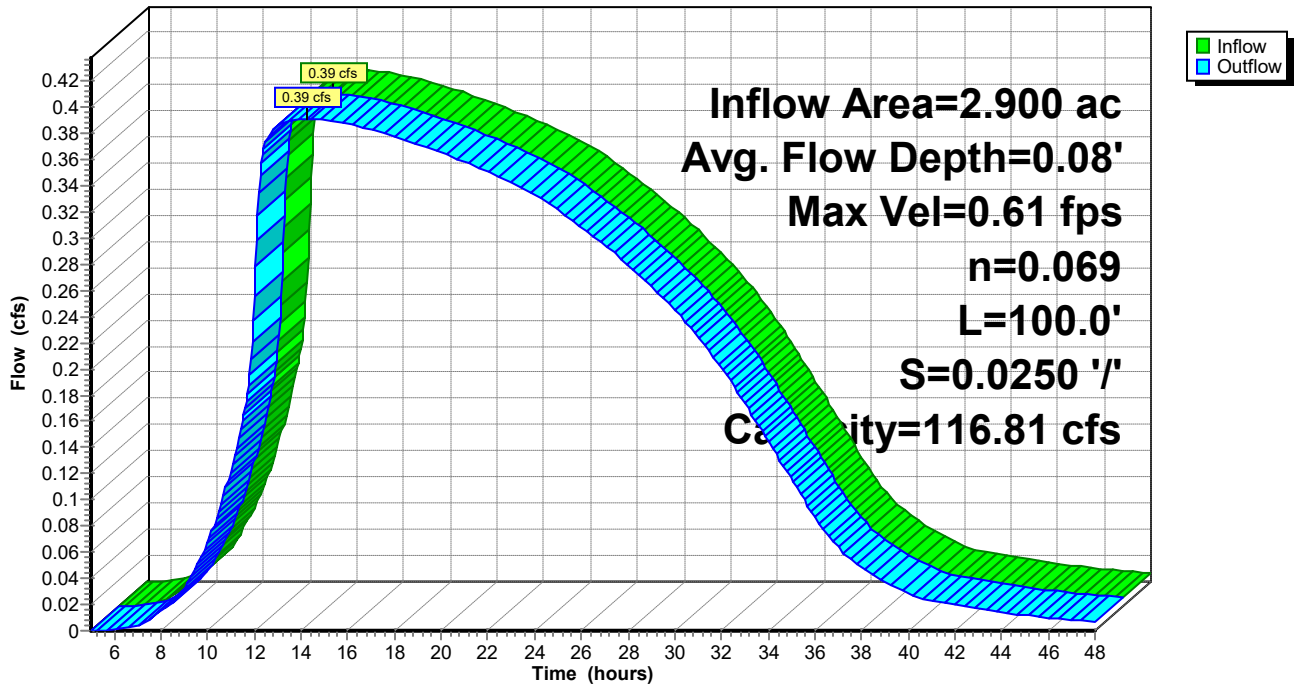
Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.61 fps, Min. Travel Time= 2.7 min
 Avg. Velocity = 0.43 fps, Avg. Travel Time= 3.9 min

Peak Storage= 64 cf @ 14.18 hrs
 Average Depth at Peak Storage= 0.08' , Surface Width= 8.47'
 Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 116.81 cfs

8.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 3.0 ' / ' Top Width= 20.00'
 Length= 100.0' Slope= 0.0250 ' / '
 Inlet Invert= 14.50', Outlet Invert= 12.00'



Reach 7R: Overflow
 Hydrograph



Summary for Reach 8R: Dry Swale #1

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 3.05" for 10-Year event
 Inflow = 4.79 cfs @ 11.96 hrs, Volume= 0.254 af
 Outflow = 4.69 cfs @ 11.98 hrs, Volume= 0.254 af, Atten= 2%, Lag= 1.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.92 fps, Min. Travel Time= 0.6 min
 Avg. Velocity = 0.77 fps, Avg. Travel Time= 2.3 min

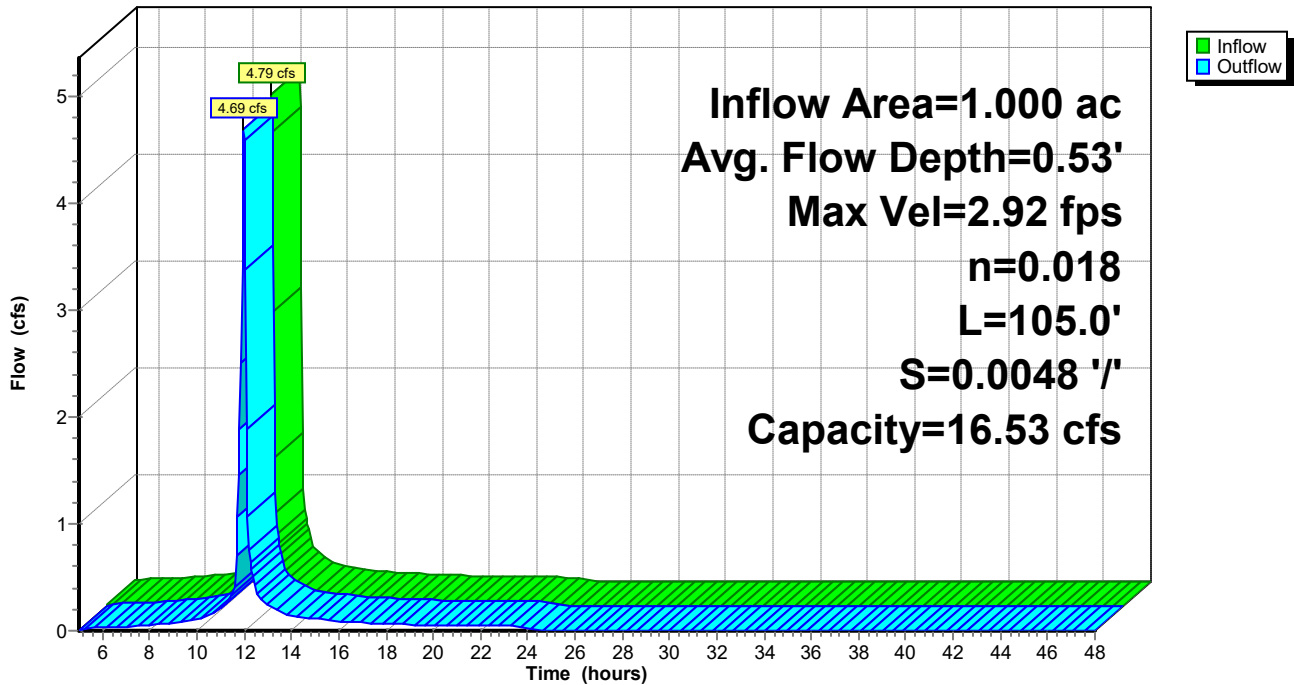
Peak Storage= 169 cf @ 11.97 hrs
 Average Depth at Peak Storage= 0.53' , Surface Width= 4.11'
 Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 16.53 cfs

2.00' x 1.00' deep channel, n= 0.018 Earth, clean & straight
 Side Slope Z-value= 2.0 ' / ' Top Width= 6.00'
 Length= 105.0' Slope= 0.0048 ' / '
 Inlet Invert= 10.00', Outlet Invert= 9.50'



Reach 8R: Dry Swale #1

Hydrograph



Summary for Reach 10R: Dry Swale #2

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 2.21" for 10-Year event
 Inflow = 2.69 cfs @ 12.01 hrs, Volume= 0.140 af
 Outflow = 2.62 cfs @ 12.02 hrs, Volume= 0.140 af, Atten= 3%, Lag= 0.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 4.08 fps, Min. Travel Time= 0.5 min
 Avg. Velocity = 1.13 fps, Avg. Travel Time= 1.7 min

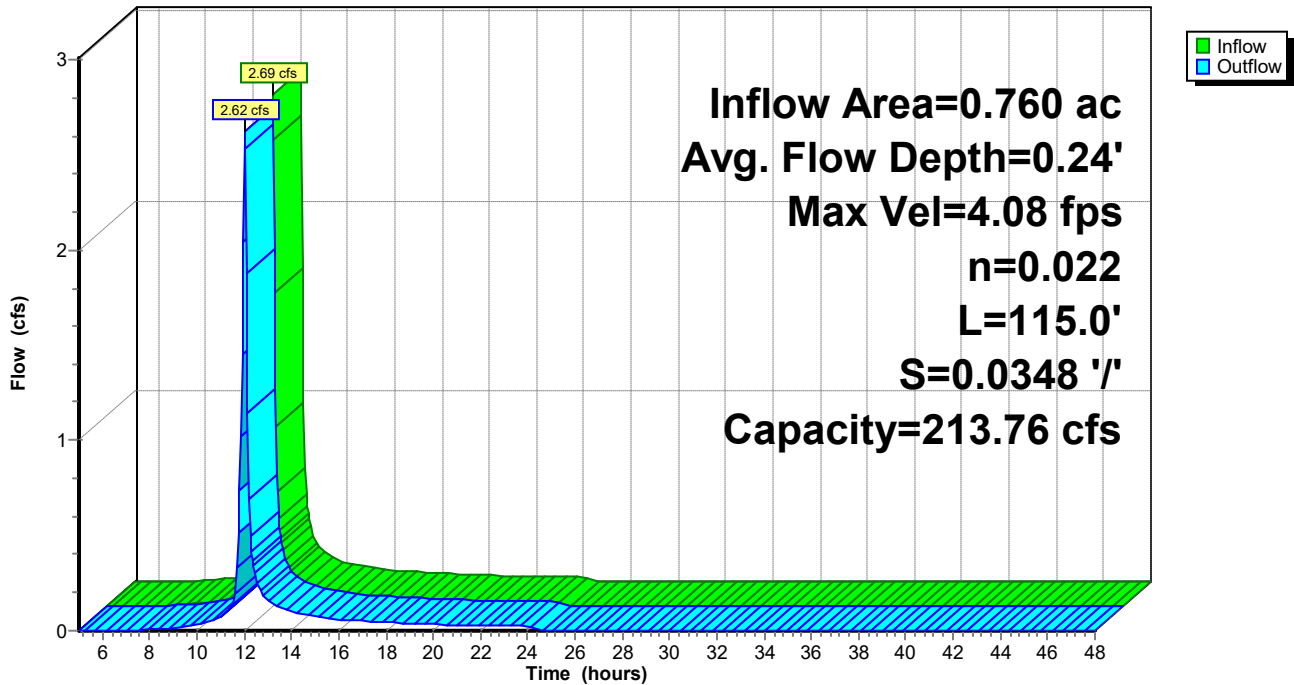
Peak Storage= 75 cf @ 12.01 hrs
 Average Depth at Peak Storage= 0.24' , Surface Width= 3.44'
 Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 213.76 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 14.00'
 Length= 115.0' Slope= 0.0348 ' / '
 Inlet Invert= 37.00', Outlet Invert= 33.00'



Reach 10R: Dry Swale #2

Hydrograph



Summary for Reach 12R: Sediment Basin Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.46" for 10-Year event
 Inflow = 0.26 cfs @ 12.31 hrs, Volume= 0.046 af
 Outflow = 0.26 cfs @ 12.32 hrs, Volume= 0.046 af, Atten= 1%, Lag= 0.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.42 fps, Min. Travel Time= 0.2 min
 Avg. Velocity = 0.19 fps, Avg. Travel Time= 0.5 min

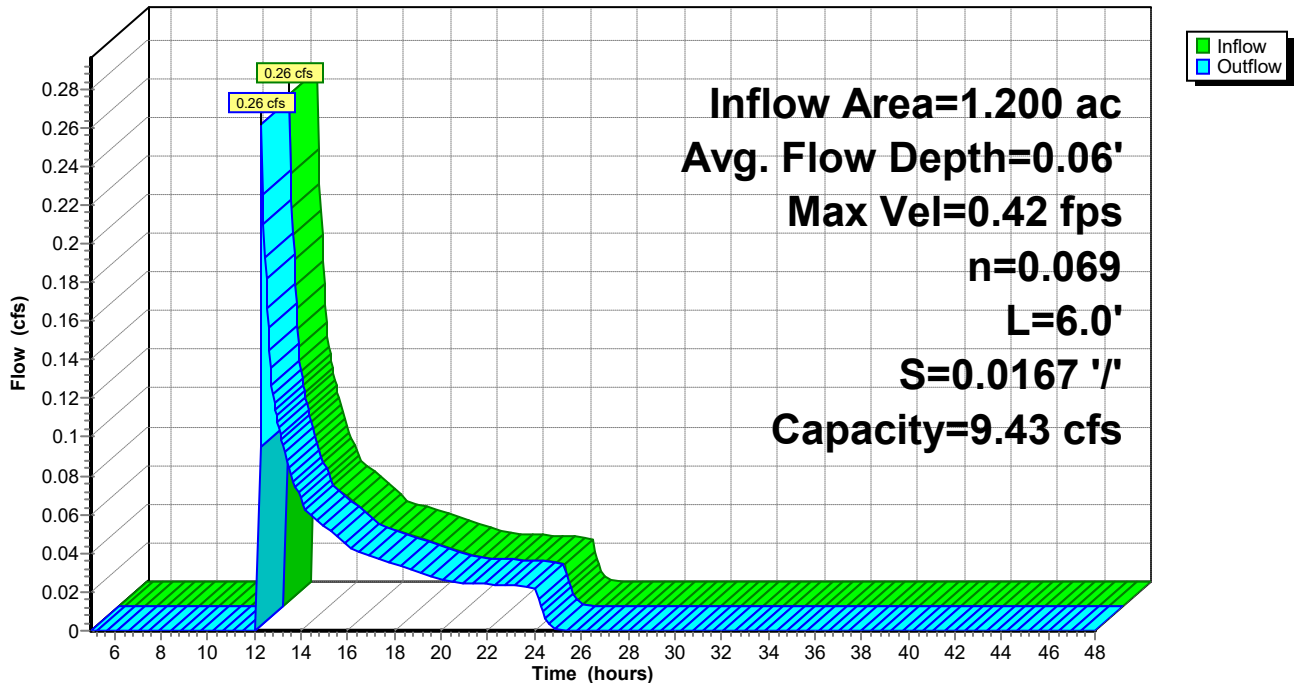
Peak Storage= 4 cf @ 12.32 hrs
 Average Depth at Peak Storage= 0.06' , Surface Width= 10.50'
 Bank-Full Depth= 0.50' Flow Area= 6.0 sf, Capacity= 9.43 cfs

10.00' x 0.50' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 4.0 ' / ' Top Width= 14.00'
 Length= 6.0' Slope= 0.0167 ' / '
 Inlet Invert= 12.00', Outlet Invert= 11.90'



Reach 12R: Sediment Basin Overflow

Hydrograph



Summary for Reach 13R: Roadside Swale

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.63" for 10-Year event
 Inflow = 1.16 cfs @ 11.99 hrs, Volume= 0.063 af
 Outflow = 1.03 cfs @ 12.06 hrs, Volume= 0.063 af, Atten= 11%, Lag= 3.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.18 fps, Min. Travel Time= 2.2 min
 Avg. Velocity = 0.77 fps, Avg. Travel Time= 6.3 min

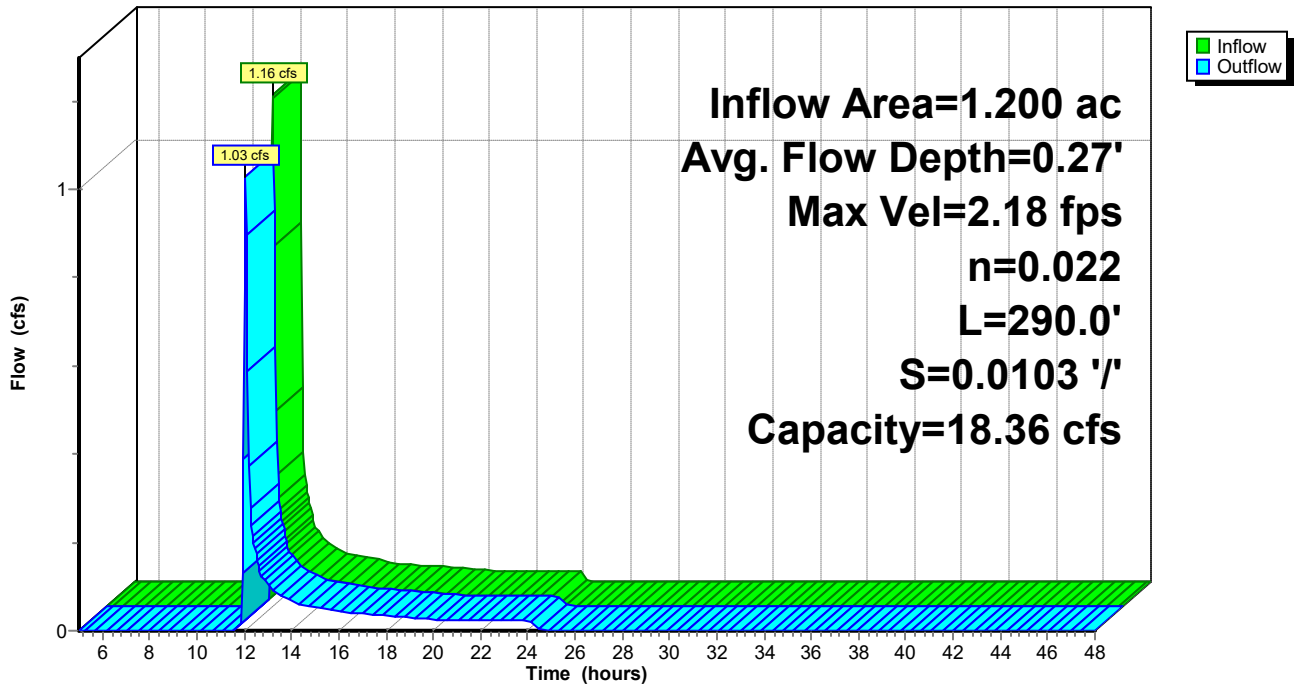
Peak Storage= 141 cf @ 12.02 hrs
 Average Depth at Peak Storage= 0.27' , Surface Width= 2.62'
 Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.36 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 7.00'
 Length= 290.0' Slope= 0.0103 ' / '
 Inlet Invert= 15.00', Outlet Invert= 12.00'



Reach 13R: Roadside Swale

Hydrograph



Summary for Reach 14R: Roadside Swale

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 2.21" for 10-Year event
 Inflow = 2.85 cfs @ 11.97 hrs, Volume= 0.140 af
 Outflow = 2.69 cfs @ 12.01 hrs, Volume= 0.140 af, Atten= 6%, Lag= 2.4 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 5.12 fps, Min. Travel Time= 1.5 min
 Avg. Velocity = 1.44 fps, Avg. Travel Time= 5.3 min

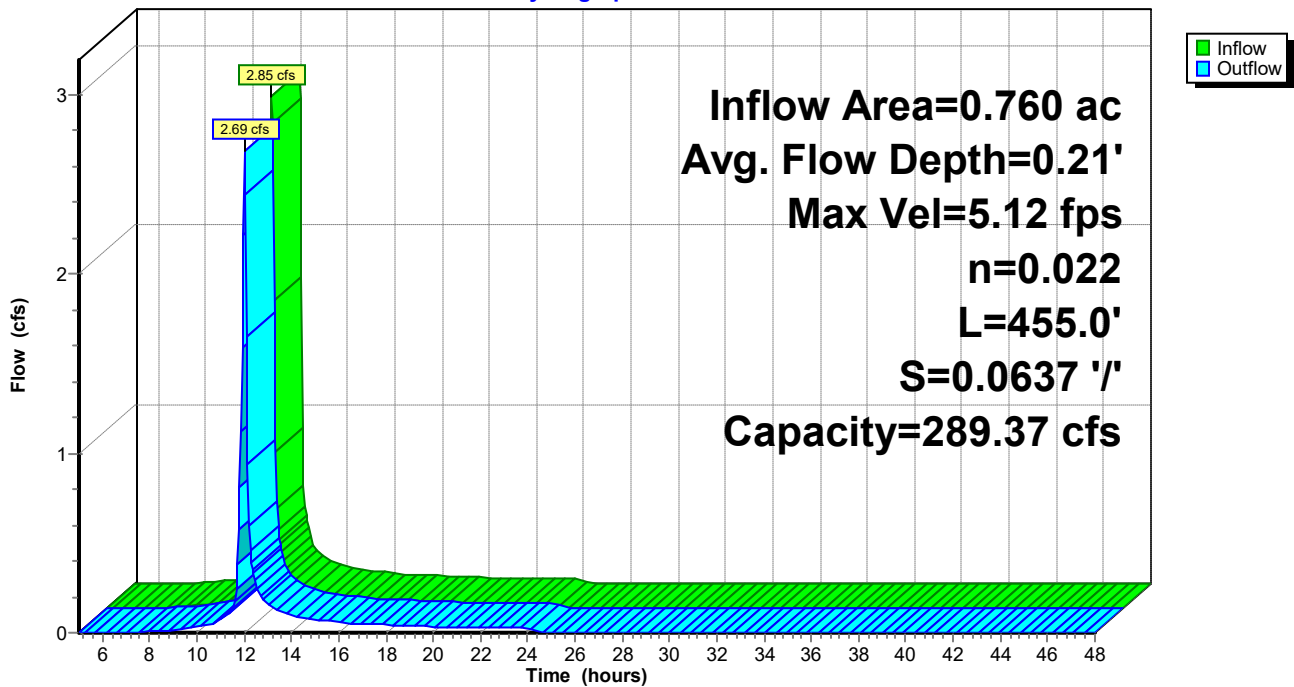
Peak Storage= 250 cf @ 11.99 hrs
 Average Depth at Peak Storage= 0.21' , Surface Width= 3.25'
 Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 289.37 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 14.00'
 Length= 455.0' Slope= 0.0637 ' / '
 Inlet Invert= 66.00', Outlet Invert= 37.00'



Reach 14R: Roadside Swale

Hydrograph



Summary for Reach 15R: Roadside Swale

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 1.27" for 10-Year event
 Inflow = 2.86 cfs @ 11.98 hrs, Volume= 0.137 af
 Outflow = 2.02 cfs @ 12.17 hrs, Volume= 0.137 af, Atten= 29%, Lag= 11.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.95 fps, Min. Travel Time= 7.5 min
 Avg. Velocity = 0.27 fps, Avg. Travel Time= 26.8 min

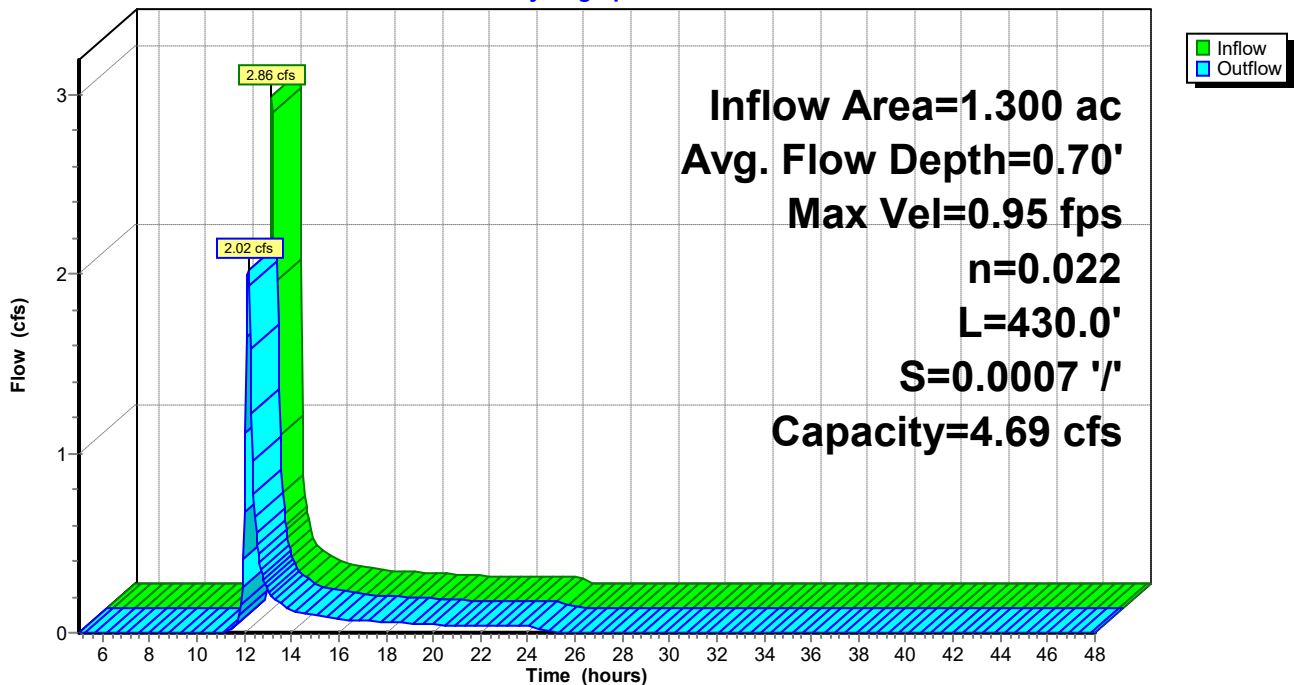
Peak Storage= 939 cf @ 12.04 hrs
 Average Depth at Peak Storage= 0.70' , Surface Width= 5.22'
 Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 4.69 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 7.00'
 Length= 430.0' Slope= 0.0007 ' / '
 Inlet Invert= 10.00', Outlet Invert= 9.71'



Reach 15R: Roadside Swale

Hydrograph



Summary for Reach 17R: Sediment Basin Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.91" for 10-Year event
 Inflow = 1.45 cfs @ 12.31 hrs, Volume= 0.098 af
 Outflow = 1.33 cfs @ 12.32 hrs, Volume= 0.098 af, Atten= 9%, Lag= 0.5 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.67 fps, Min. Travel Time= 0.1 min
 Avg. Velocity = 0.17 fps, Avg. Travel Time= 0.6 min

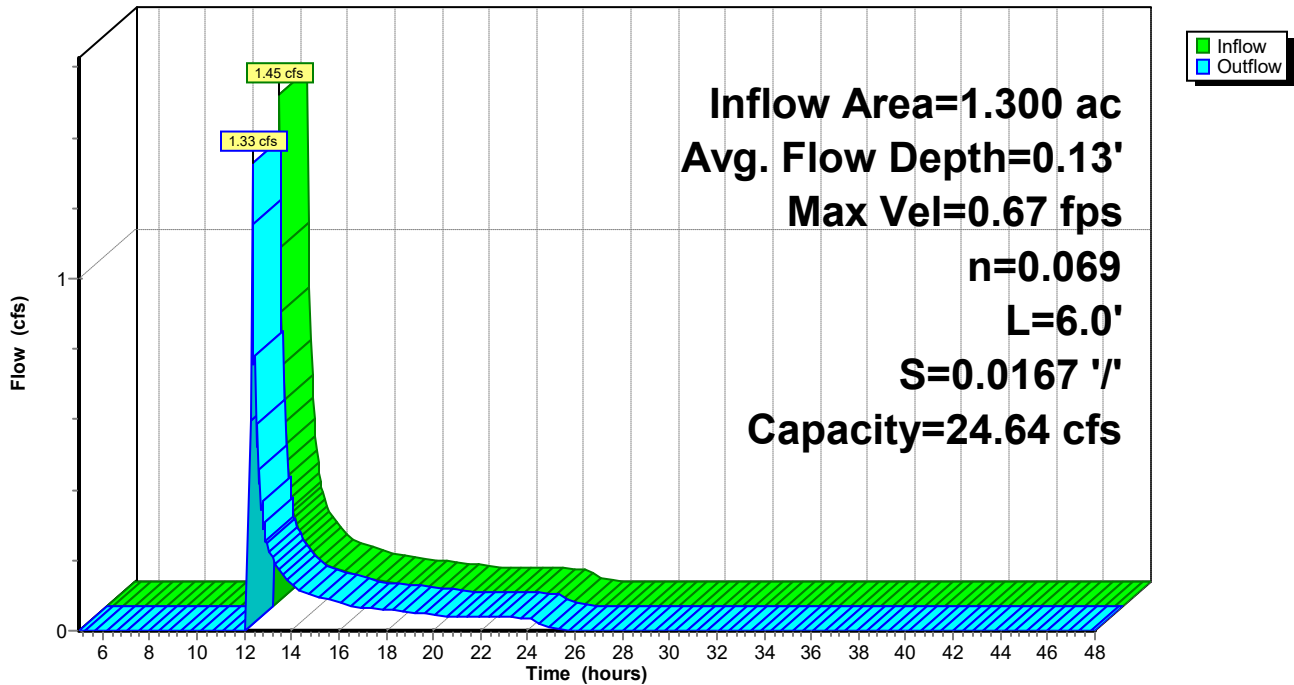
Peak Storage= 12 cf @ 12.32 hrs
 Average Depth at Peak Storage= 0.13' , Surface Width= 16.07'
 Bank-Full Depth= 0.70' Flow Area= 12.5 sf, Capacity= 24.64 cfs

15.00' x 0.70' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 4.0 '/' Top Width= 20.60'
 Length= 6.0' Slope= 0.0167 '/'
 Inlet Invert= 9.00', Outlet Invert= 8.90'



Reach 17R: Sediment Basin Overflow

Hydrograph



Summary for Pond 1P: WQv Pond #1

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth = 2.73" for 10-Year event
 Inflow = 8.78 cfs @ 12.07 hrs, Volume= 0.660 af
 Outflow = 0.39 cfs @ 14.15 hrs, Volume= 0.652 af, Atten= 96%, Lag= 125.0 min
 Primary = 0.39 cfs @ 14.15 hrs, Volume= 0.652 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Starting Elev= 14.00' Surf.Area= 9,229 sf Storage= 19,003 cf
 Peak Elev= 15.59' @ 14.15 hrs Surf.Area= 19,456 sf Storage= 36,781 cf (17,778 cf above start)

Plug-Flow detention time= 1,195.5 min calculated for 0.216 af (33% of inflow)
 Center-of-Mass det. time= 536.4 min (1,336.8 - 800.3)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,795 cf	Forebay (Prismatic) Listed below (Recalc)
#2	9.00'	57,882 cf	Permanent Pool (Prismatic) Listed below (Recalc)
		62,677 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	232	0	0
11.00	569	401	401
12.00	1,018	794	1,194
13.00	1,467	1,243	2,437
14.00	3,249	2,358	4,795

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
9.00	1,145	0	0
10.00	1,751	1,448	1,448
11.00	2,339	2,045	3,493
12.00	2,959	2,649	6,142
13.00	3,597	3,278	9,420
14.00	5,980	4,789	14,209
14.50	7,240	3,305	17,514
15.00	14,392	5,408	22,922
16.00	17,455	15,924	38,845
17.00	20,619	19,037	57,882

Device	Routing	Invert	Outlet Devices
#1	Primary	13.50'	12.0" Round Culvert L= 50.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 13.50' / 13.23' S= 0.0054 ' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	16.00'	24.0" x 24.0" Horiz. Outlet Structure Top Grate C= 0.600 in 24.0" x 24.0" Grate (100% open area) Limited to weir flow at low heads
#3	Device 1	14.00'	4.0" Round Reverse Slope Pipe L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 9.00' / 14.00' S= -0.1250 ' /' Cc= 0.900

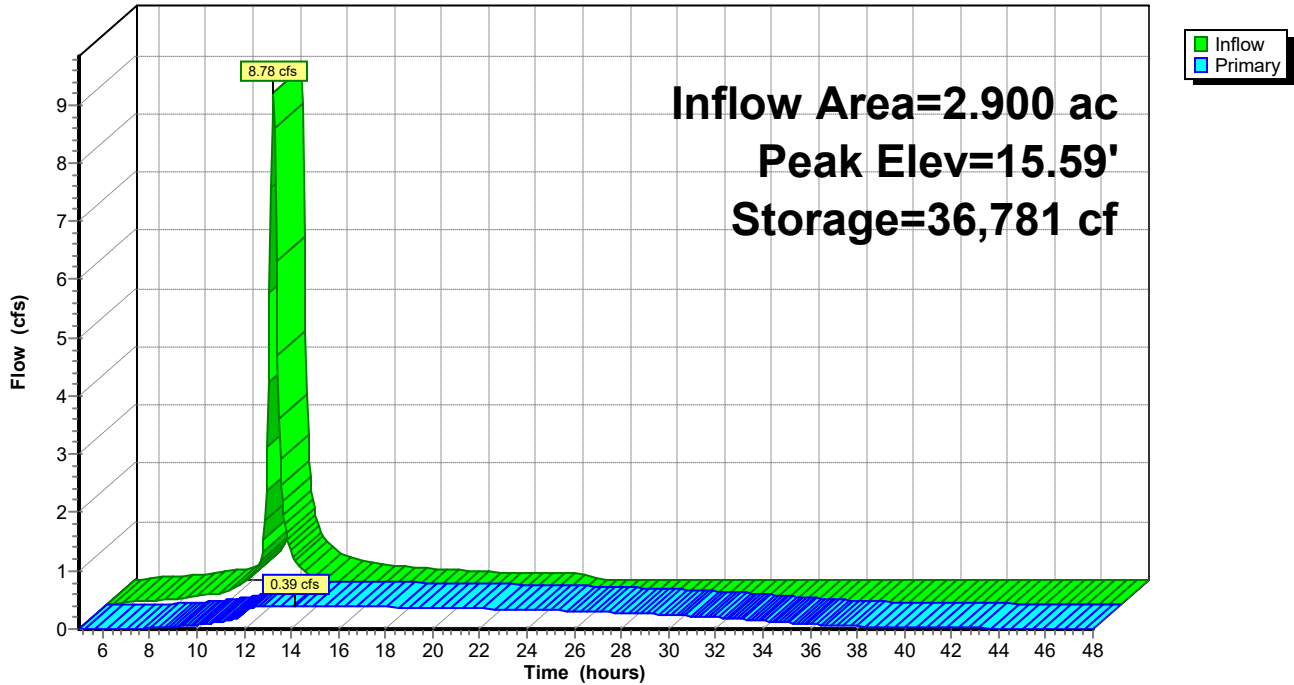
#4	Primary	16.25'	n= 0.010 PVC, smooth interior, Flow Area= 0.09 sf
			6.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Primary OutFlow Max=0.39 cfs @ 14.15 hrs HW=15.59' (Free Discharge)

- 1=Culvert (Passes 0.39 cfs of 4.20 cfs potential flow)
- 2=Outlet Structure Top Grate (Controls 0.00 cfs)
- 3=Reverse Slope Pipe (Outlet Controls 0.39 cfs @ 4.48 fps)
- 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: WQv Pond #1

Hydrograph



Summary for Pond 2P: WQv Pond #2

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 2.47" for 10-Year event
 Inflow = 21.14 cfs @ 11.97 hrs, Volume= 1.195 af
 Outflow = 0.64 cfs @ 14.62 hrs, Volume= 1.187 af, Atten= 97%, Lag= 158.7 min
 Primary = 0.64 cfs @ 14.62 hrs, Volume= 1.187 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Starting Elev= 14.00' Surf.Area= 5,917 sf Storage= 9,000 cf
 Peak Elev= 16.47' @ 14.62 hrs Surf.Area= 24,629 sf Storage= 41,496 cf (32,496 cf above start)

Plug-Flow detention time= 808.8 min calculated for 0.980 af (82% of inflow)
 Center-of-Mass det. time= 597.8 min (1,399.8 - 802.0)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,020 cf	Forebay #1 (Prismatic) Listed below (Recalc)
#2	10.00'	2,575 cf	Forebay #2 (Prismatic) Listed below (Recalc)
#3	10.00'	58,093 cf	Permanent Pool (Prismatic) Listed below (Recalc)
		64,688 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	141	0	0
11.00	330	236	236
12.00	562	446	682
13.00	866	714	1,396
14.00	2,023	1,445	2,840
14.50	2,696	1,180	4,020

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	82	0	0
11.00	202	142	142
12.00	351	277	419
13.00	535	443	862
14.00	1,323	929	1,791
14.50	1,815	785	2,575

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	375	0	0
11.00	653	514	514
12.00	957	805	1,319
13.00	1,286	1,122	2,441
14.00	2,571	1,929	4,369
14.50	3,307	1,470	5,839
15.00	13,814	4,280	10,119
16.00	17,852	15,833	25,952
17.00	22,659	20,256	46,207
17.50	24,884	11,886	58,093

18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 10-Year Rainfall=3.63"

Prepared by McFarland Johnson

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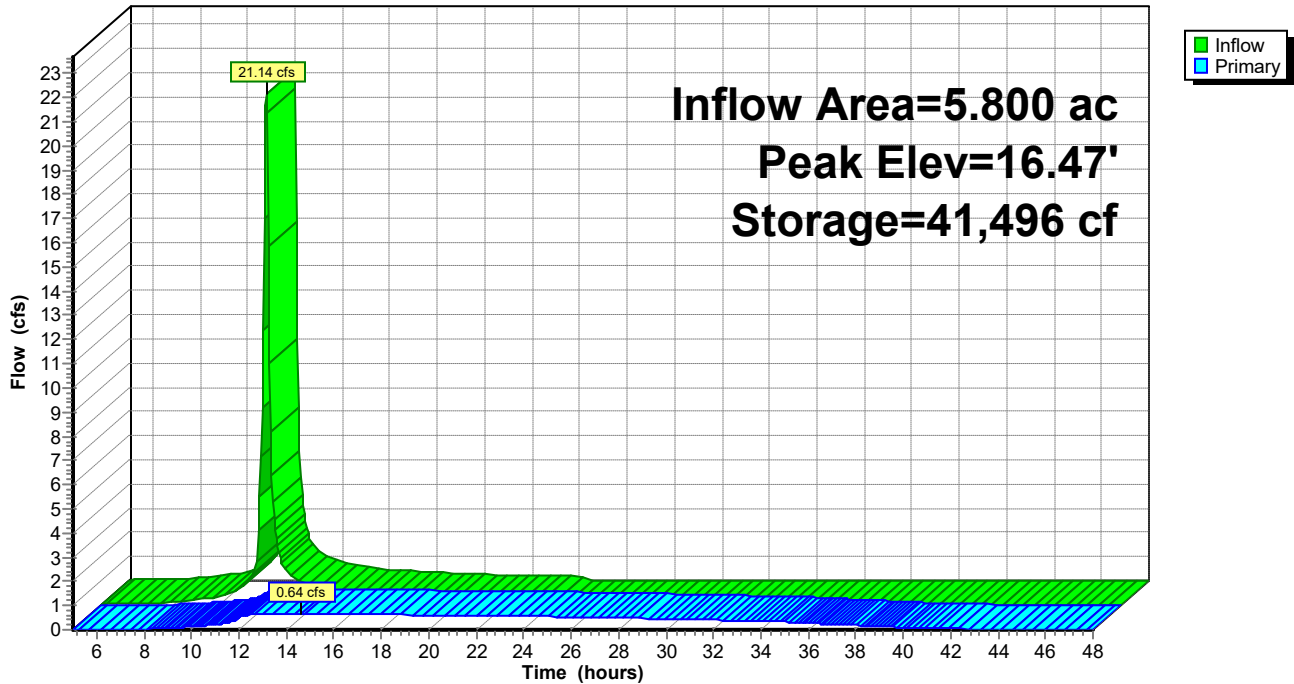
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Device	Routing	Invert	Outlet Devices
#1	Device 3	16.50'	24.0" x 24.0" Horiz. Orifice/Grate C= 0.600 in 24.0" x 24.0" Grate (100% open area) Limited to weir flow at low heads
#2	Device 3	14.00'	4.0" Vert. Reverse Slope Pipe C= 0.600 Limited to weir flow at low heads
#3	Primary	14.00'	12.0" Round Outlet Structure Discard Pipe L= 46.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 14.00' / 13.77' S= 0.0050 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#4	Primary	16.60'	10.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.64 cfs @ 14.62 hrs HW=16.47' (Free Discharge)
 3=Outlet Structure Discard Pipe (Passes 0.64 cfs of 4.79 cfs potential flow)
 1=Orifice/Grate (Controls 0.00 cfs)
 2=Reverse Slope Pipe (Orifice Controls 0.64 cfs @ 7.31 fps)
 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 2P: WQv Pond #2

Hydrograph



Summary for Pond 3P: Infiltration Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.46" for 10-Year event
 Inflow = 0.26 cfs @ 12.32 hrs, Volume= 0.046 af
 Outflow = 0.02 cfs @ 24.21 hrs, Volume= 0.034 af, Atten= 94%, Lag= 713.8 min
 Discarded = 0.02 cfs @ 24.21 hrs, Volume= 0.034 af
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 11.15' @ 24.21 hrs Surf.Area= 1,004 sf Storage= 1,468 cf

Plug-Flow detention time= 879.4 min calculated for 0.034 af (73% of inflow)
 Center-of-Mass det. time= 771.6 min (1,748.3 - 976.8)

Volume	Invert	Avail.Storage	Storage Description		
#1	8.10'	2,492 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
8.10	109	56.0	0	0	109
12.00	1,415	149.0	2,492	2,492	1,678

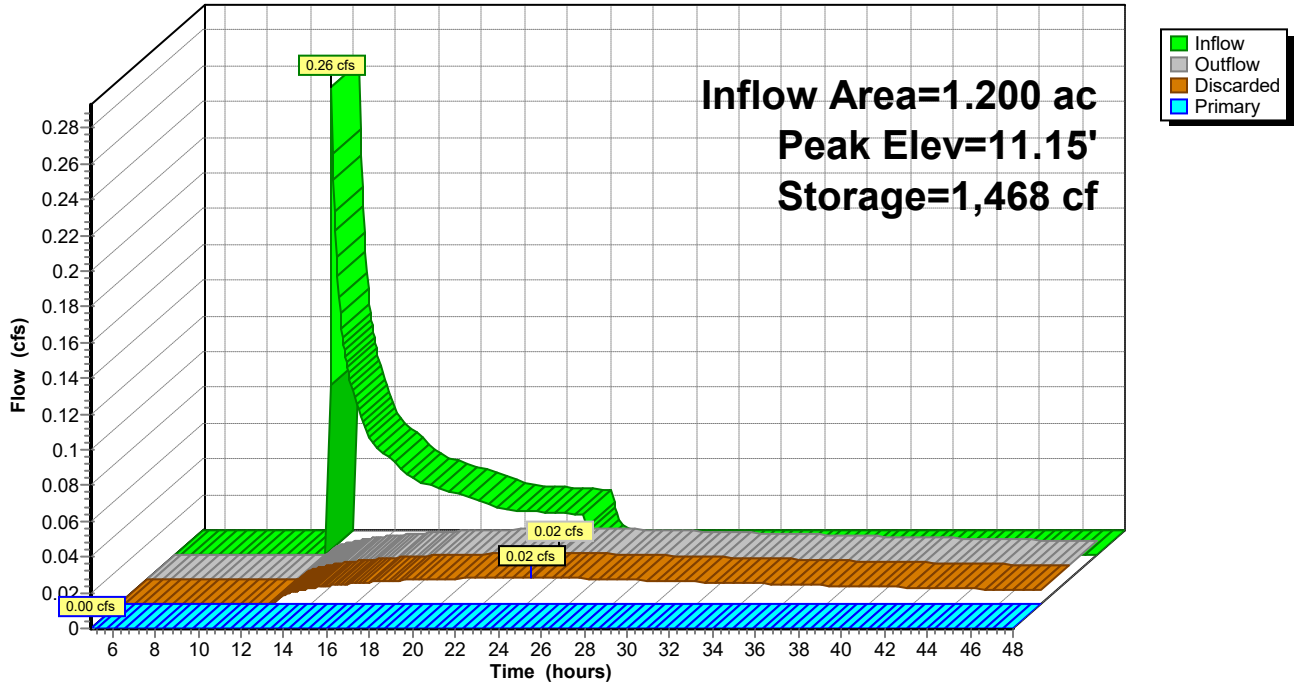
Device	Routing	Invert	Outlet Devices
#1	Primary	11.65'	Channel/Reach using Reach 5R: Overflow
#2	Discarded	8.10'	0.500 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 4.00'

Discarded OutFlow Max=0.02 cfs @ 24.21 hrs HW=11.15' (Free Discharge)
 ↑**2=Exfiltration** (Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=8.10' (Free Discharge)
 ↑**1=Channel/Reach** (Controls 0.00 cfs)

Pond 3P: Infiltration Basin #1

Hydrograph



Summary for Pond 4P: Infiltration Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 0.91" for 10-Year event
 Inflow = 1.33 cfs @ 12.32 hrs, Volume= 0.098 af
 Outflow = 0.26 cfs @ 12.92 hrs, Volume= 0.098 af, Atten= 80%, Lag= 35.5 min
 Discarded = 0.26 cfs @ 12.92 hrs, Volume= 0.098 af
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 8.10' @ 12.92 hrs Surf.Area= 701 sf Storage= 834 cf

Plug-Flow detention time= 35.0 min calculated for 0.098 af (100% of inflow)
 Center-of-Mass det. time= 35.0 min (973.5 - 938.5)

Volume	Invert	Avail.Storage	Storage Description			
#1	5.80'	2,495 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
5.80	110	56.0	0	0	110	
9.70	1,415	150.0	2,495	2,495	1,702	

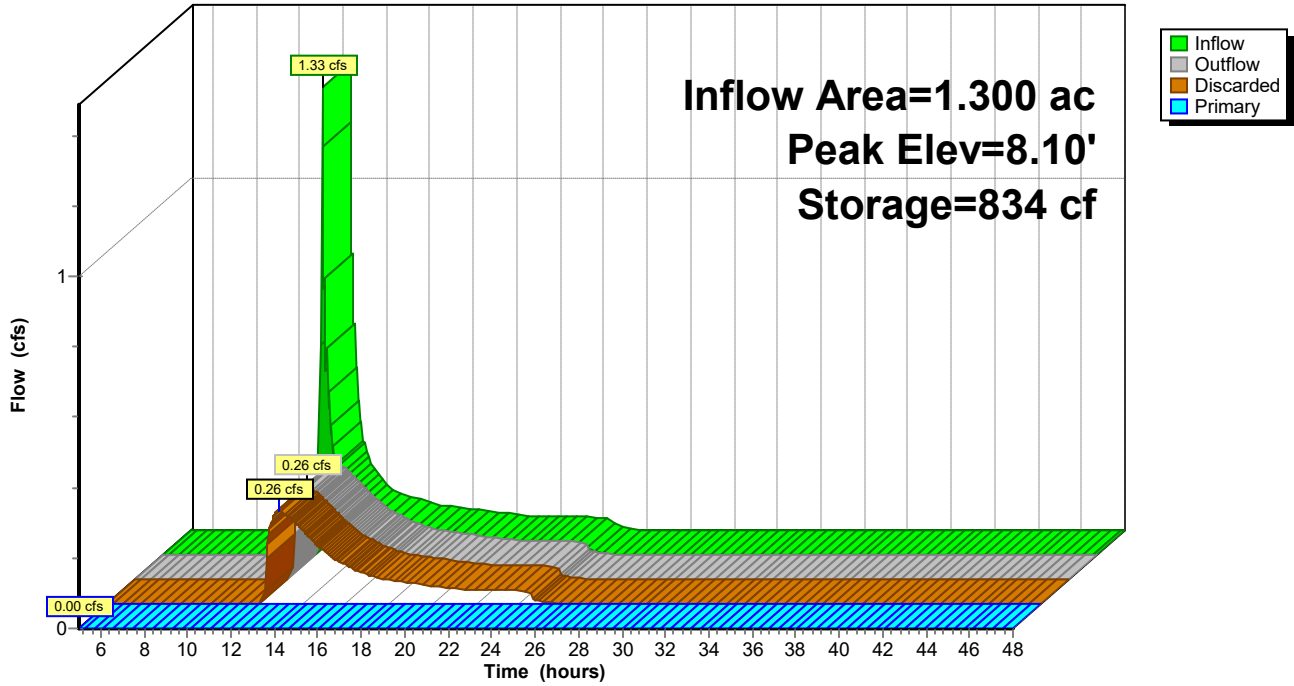
Device	Routing	Invert	Outlet Devices
#1	Primary	8.50'	Channel/Reach using Reach 6R: Overflow
#2	Discarded	5.80'	12.000 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 3.00'

Discarded OutFlow Max=0.26 cfs @ 12.92 hrs HW=8.10' (Free Discharge)
 ↑**2=Exfiltration** (Controls 0.26 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=5.80' (Free Discharge)
 ↑**1=Channel/Reach** (Controls 0.00 cfs)

Pond 4P: Infiltration Basin #2

Hydrograph



Summary for Pond 5P: Sedimentation Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 0.63" for 10-Year event
 Inflow = 1.03 cfs @ 12.06 hrs, Volume= 0.063 af
 Outflow = 0.26 cfs @ 12.31 hrs, Volume= 0.046 af, Atten= 74%, Lag= 15.4 min
 Primary = 0.26 cfs @ 12.31 hrs, Volume= 0.046 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 12.06' @ 12.32 hrs Surf.Area= 566 sf Storage= 783 cf

Plug-Flow detention time= 185.4 min calculated for 0.046 af (73% of inflow)
 Center-of-Mass det. time= 71.3 min (976.1 - 904.8)

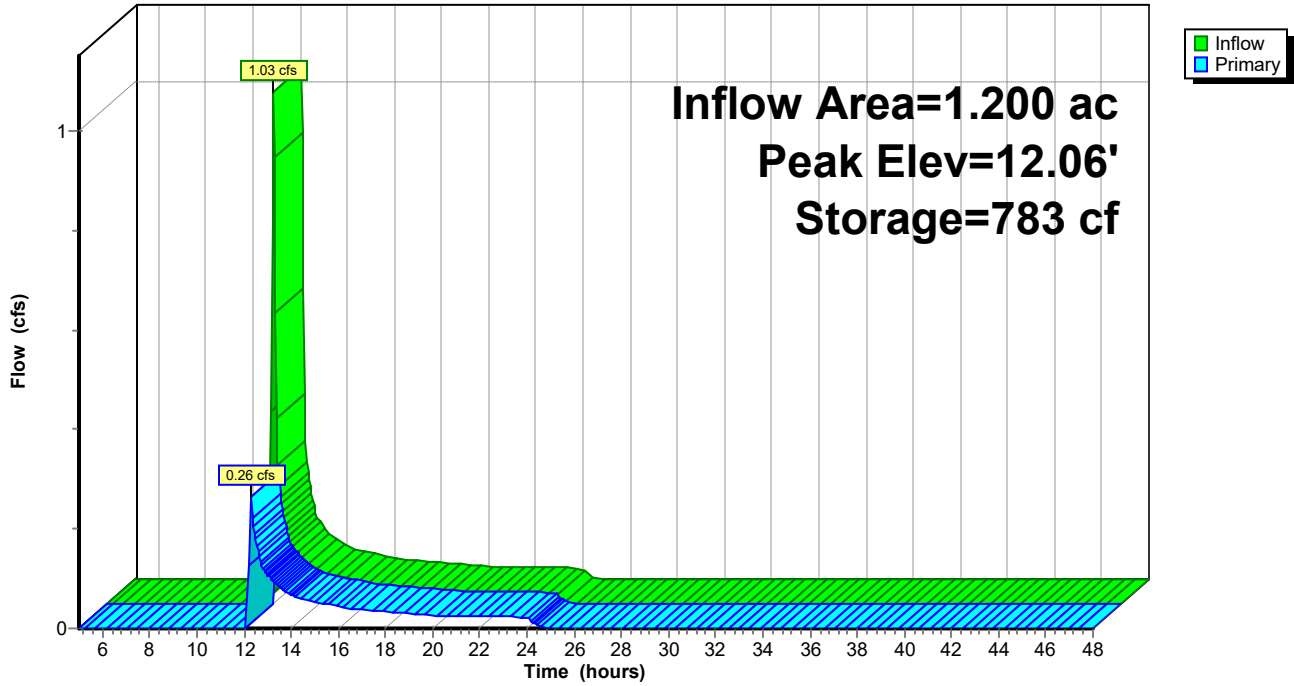
Volume	Invert	Avail.Storage	Storage Description		
#1	9.00'	1,058 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
9.00	41	25.8	0	0	41
10.00	150	46.7	90	90	167
11.00	320	66.6	230	320	355
12.00	550	86.4	430	749	608
12.50	687	96.2	309	1,058	758

Device	Routing	Invert	Outlet Devices
#1	Primary	12.00'	Channel/Reach using Reach 12R: Sediment Basin Overflow

Primary OutFlow Max=0.24 cfs @ 12.31 hrs HW=12.06' (Free Discharge)
 ↑1=Channel/Reach (Channel Controls 0.24 cfs @ 0.41 fps)

Pond 5P: Sedimentation Basin #1

Hydrograph



Summary for Pond 16P: Sedimentation Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 1.27" for 10-Year event
 Inflow = 2.02 cfs @ 12.17 hrs, Volume= 0.137 af
 Outflow = 1.45 cfs @ 12.31 hrs, Volume= 0.098 af, Atten= 28%, Lag= 8.9 min
 Primary = 1.45 cfs @ 12.31 hrs, Volume= 0.098 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 9.14' @ 12.32 hrs Surf.Area= 928 sf Storage= 1,826 cf

Plug-Flow detention time= 174.4 min calculated for 0.098 af (72% of inflow)
 Center-of-Mass det. time= 62.3 min (938.0 - 875.7)

Volume	Invert	Avail.Storage	Storage Description		
#1	5.80'	2,389 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
5.80	224	80.0	0	0	224
6.00	257	83.0	48	48	266
7.00	438	98.0	344	392	500
8.00	650	113.0	541	932	773
9.00	892	128.0	768	1,700	1,085
9.70	1,079	139.0	689	2,389	1,337

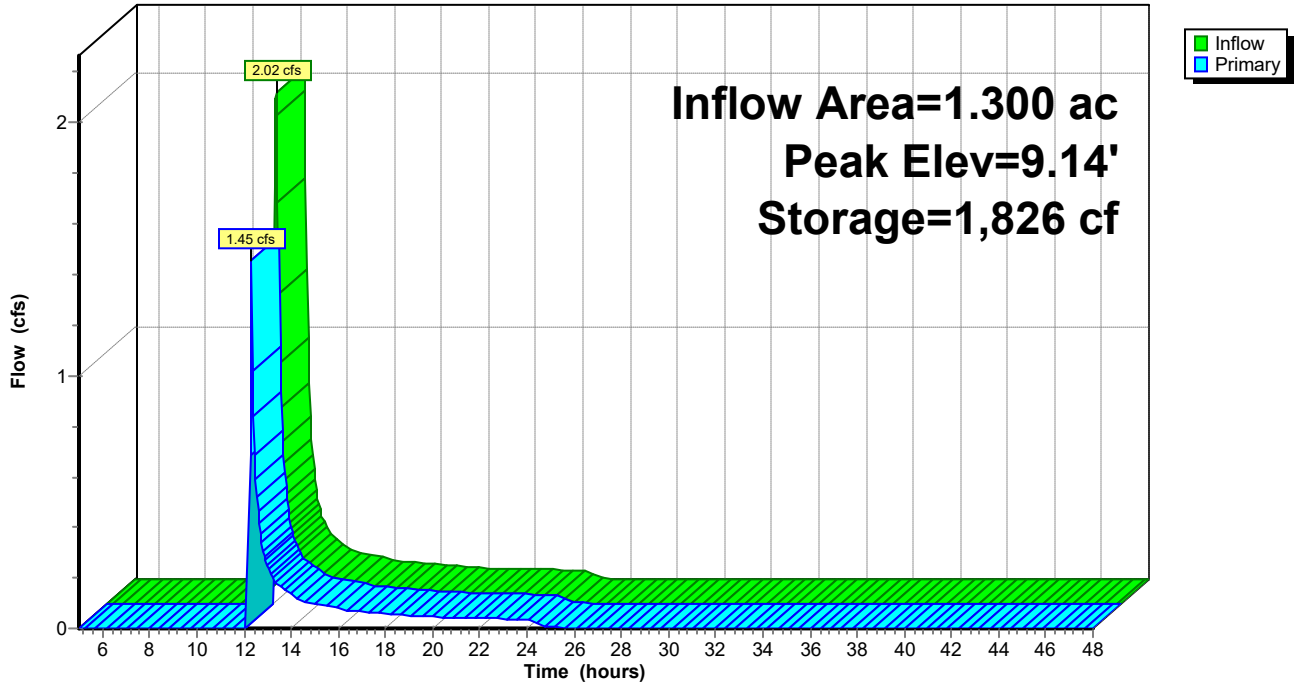
Device	Routing	Invert	Outlet Devices
#1	Primary	9.00'	Channel/Reach using Reach 17R: Sediment Basin Overflow

Primary OutFlow Max=1.25 cfs @ 12.31 hrs HW=9.12' (Free Discharge)

↑ **1=Channel/Reach** (Channel Controls 1.25 cfs @ 0.67 fps)

Pond 16P: Sedimentation Basin #2

Hydrograph



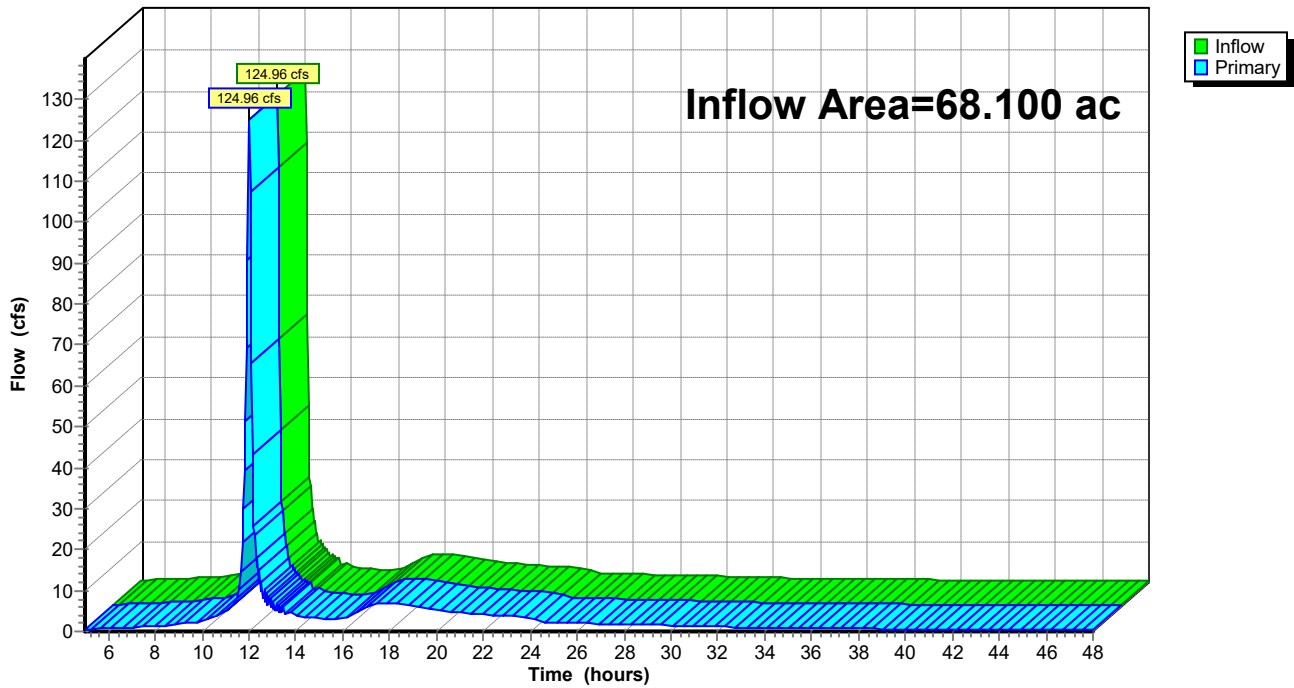
Summary for Pond AP-1: Analysis Point #1

Inflow Area = 68.100 ac, 20.36% Impervious, Inflow Depth > 1.94" for 10-Year event
Inflow = 124.96 cfs @ 12.01 hrs, Volume= 10.994 af
Primary = 124.96 cfs @ 12.01 hrs, Volume= 10.994 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1

Hydrograph



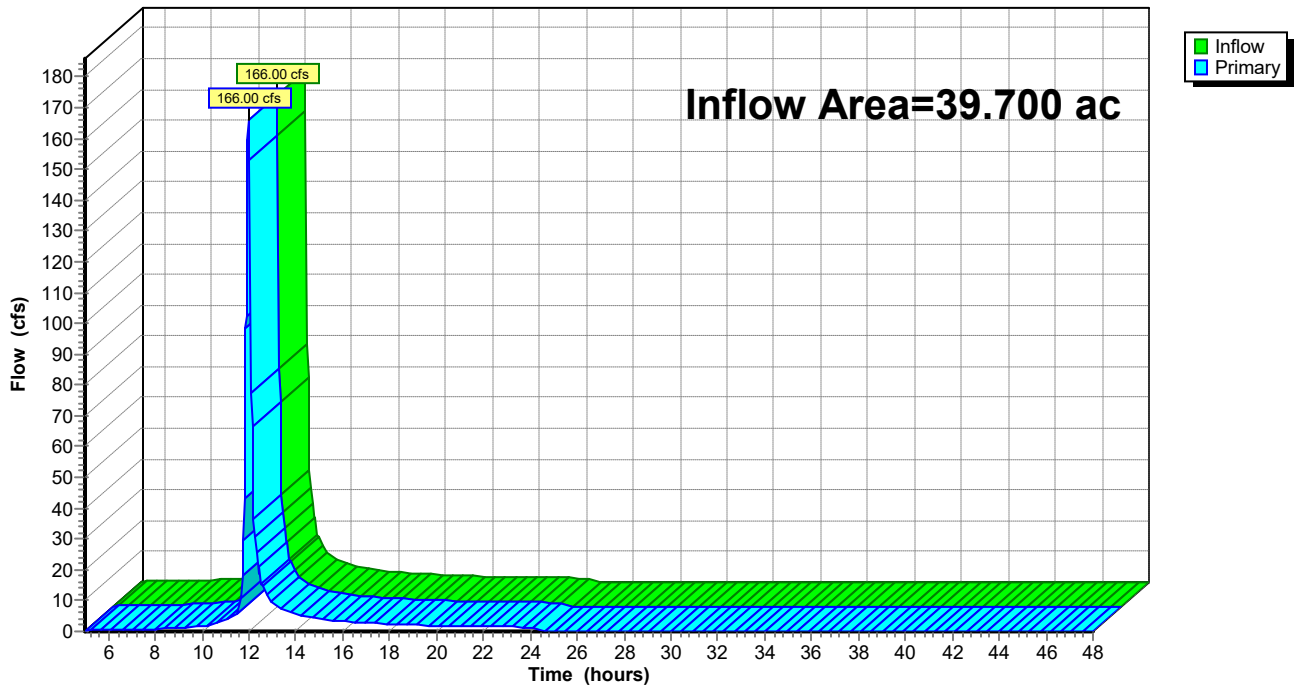
Summary for Pond AP-2: Analysis Point #2

Inflow Area = 39.700 ac, 23.10% Impervious, Inflow Depth > 2.53" for 10-Year event
Inflow = 166.00 cfs @ 11.97 hrs, Volume= 8.362 af
Primary = 166.00 cfs @ 11.97 hrs, Volume= 8.362 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2

Hydrograph



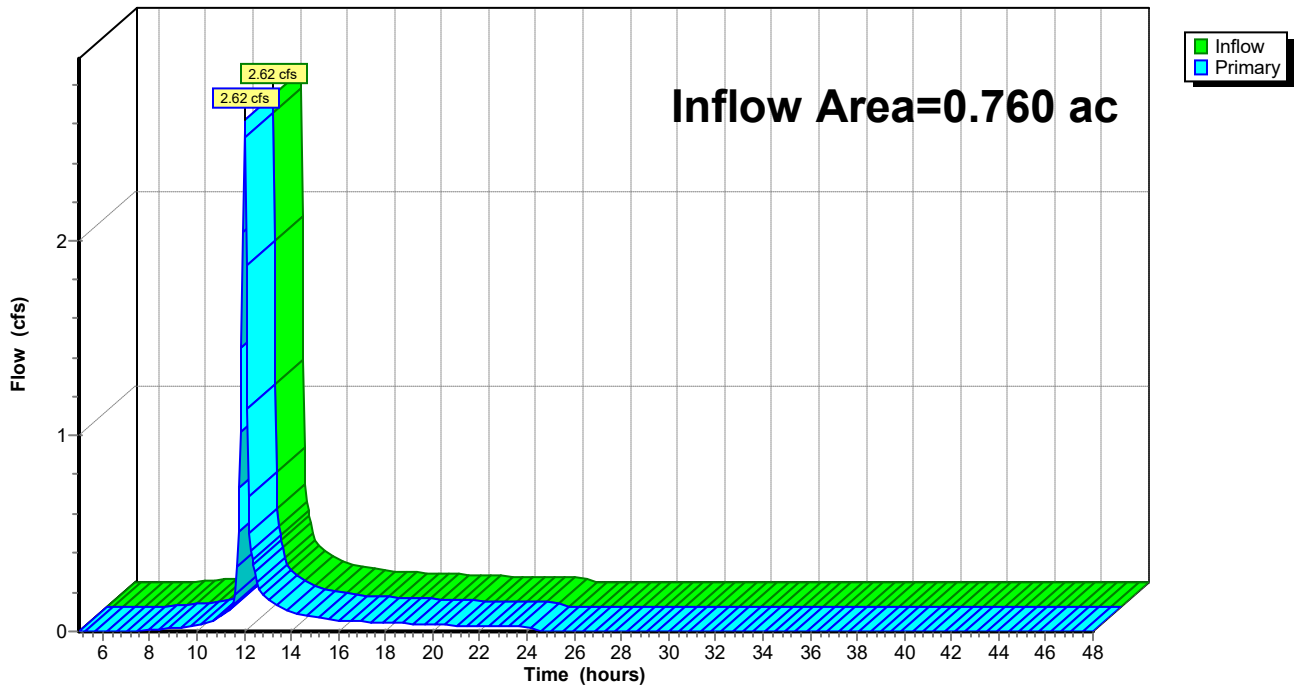
Summary for Pond AP-3: Analysis Point #3

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth = 2.21" for 10-Year event
Inflow = 2.62 cfs @ 12.02 hrs, Volume= 0.140 af
Primary = 2.62 cfs @ 12.02 hrs, Volume= 0.140 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3

Hydrograph



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Pond C-1: Chamber Series 1

Inflow Area = 10.300 ac, 66.70% Impervious, Inflow Depth > 3.23" for 10-Year event
 Inflow = 49.84 cfs @ 11.98 hrs, Volume= 2.772 af
 Outflow = 50.37 cfs @ 11.97 hrs, Volume= 2.412 af, Atten= 0%, Lag= 0.0 min
 Discarded = 0.13 cfs @ 11.97 hrs, Volume= 0.347 af
 Primary = 50.24 cfs @ 11.97 hrs, Volume= 2.065 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 13.64' @ 11.97 hrs Surf.Area= 12,440 sf Storage= 29,816 cf

Plug-Flow detention time= 222.6 min calculated for 2.411 af (87% of inflow)
 Center-of-Mass det. time= 160.8 min (929.8 - 769.0)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	11,722 cf	37.08'W x 227.97'L x 5.50'H Field B 46,496 cf Overall - 17,192 cf Embedded = 29,305 cf x 40.0% Voids
#2B	6.75'	17,192 cf	ADS_StormTech MC-3500 d +Cap x 155 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 155 Chambers in 5 Rows Cap Storage= +14.9 cf x 2 x 5 rows = 149.0 cf
#3	13.25'	6,100 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		35,013 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
13.25	600	0	0
13.75	4,900	1,375	1,375
14.00	8,200	1,638	3,013
14.25	16,500	3,088	6,100

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	10.00'	36.0" Round Culvert L= 55.9' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 10.00' / 7.59' S= 0.0431 ' / Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	14.24'	50.0' long x 0.7' breadth Concrete Curb Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 Coef. (English) 2.76 2.82 2.93 3.09 3.18 3.22 3.27 3.30 3.32 3.31 3.32

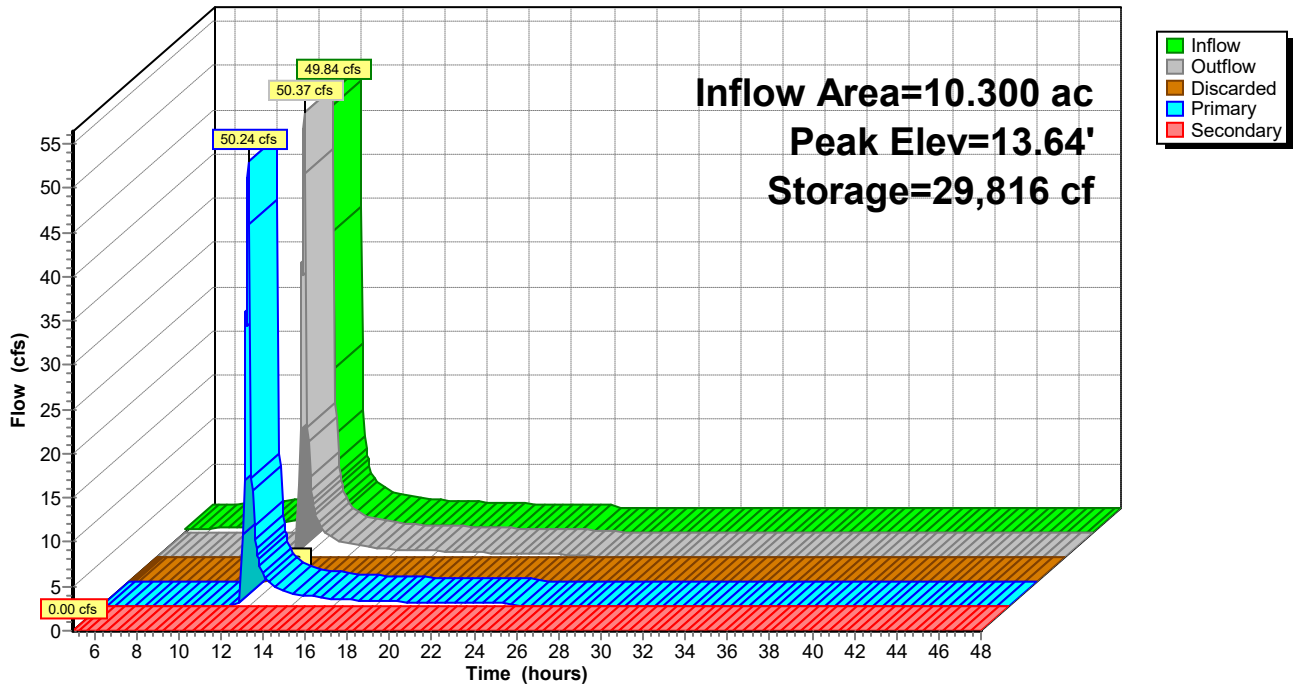
Discarded OutFlow Max=0.13 cfs @ 11.97 hrs HW=13.50' (Free Discharge)
 ↳1=Exfiltration (Exfiltration Controls 0.13 cfs)

Primary OutFlow Max=48.14 cfs @ 11.97 hrs HW=13.50' (Free Discharge)
 ↳2=Culvert (Inlet Controls 48.14 cfs @ 6.81 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.01' (Free Discharge)
 ↳3=Concrete Curb (Controls 0.00 cfs)

Pond C-1: Chamber Series 1

Hydrograph



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Pond C-4: Chamber Series 4

Inflow Area = 8.900 ac, 0.00% Impervious, Inflow Depth > 2.95" for 10-Year event
 Inflow = 39.82 cfs @ 11.99 hrs, Volume= 2.188 af
 Outflow = 44.40 cfs @ 11.96 hrs, Volume= 1.858 af, Atten= 0%, Lag= 0.0 min
 Discarded = 0.08 cfs @ 11.95 hrs, Volume= 0.261 af
 Primary = 44.32 cfs @ 11.96 hrs, Volume= 1.597 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 14.18' @ 11.96 hrs Surf.Area= 7,104 sf Storage= 21,828 cf

Plug-Flow detention time= 221.0 min calculated for 1.858 af (85% of inflow)
 Center-of-Mass det. time= 153.0 min (936.6 - 783.6)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	8,911 cf	29.92'W x 213.63'L x 5.50'H Field B 35,151 cf Overall - 12,874 cf Embedded = 22,277 cf x 40.0% Voids
#2B	6.75'	12,874 cf	ADS_StormTech MC-3500 d +Cap x 116 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 116 Chambers in 4 Rows Cap Storage= +14.9 cf x 2 x 4 rows = 119.2 cf
#3	14.10'	8,015 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		29,800 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
14.10	400	0	0
14.60	2,400	700	700
14.80	6,300	870	1,570
15.10	10,000	2,445	4,015
15.50	10,000	4,000	8,015

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	11.00'	36.0" Round Culvert L= 24.3' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 11.00' / 9.42' S= 0.0650 ' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

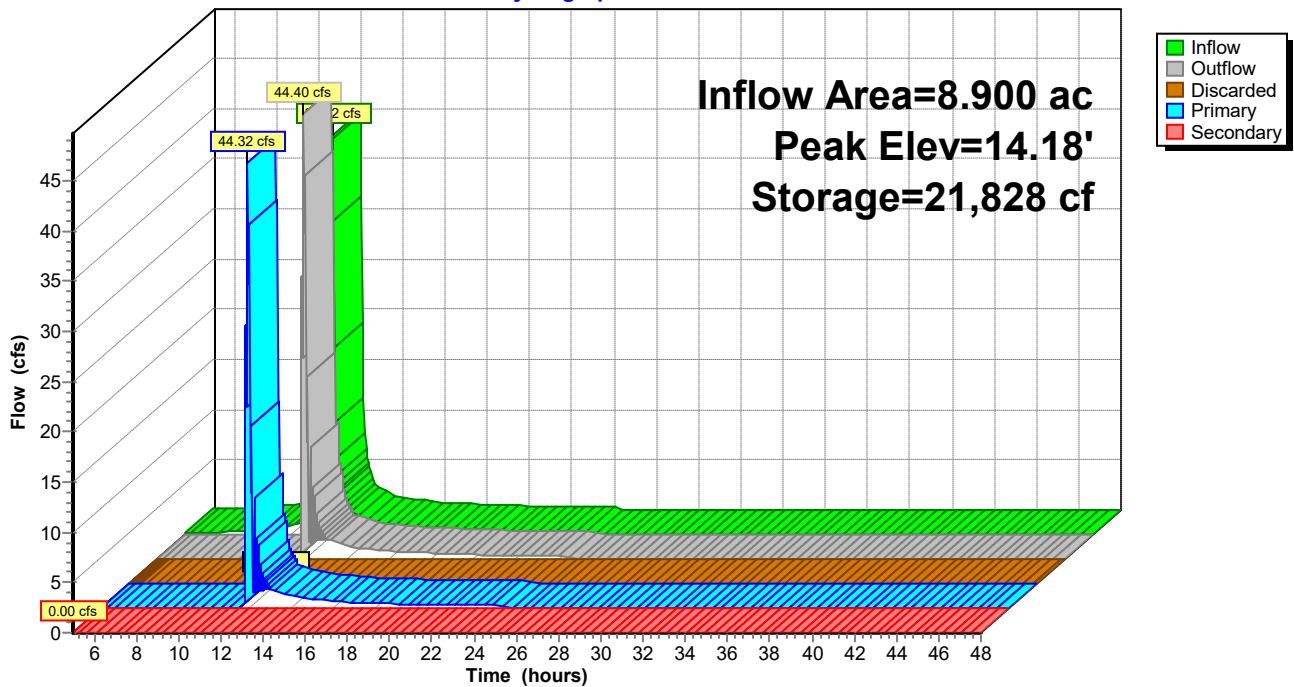
Discarded OutFlow Max=0.08 cfs @ 11.95 hrs HW=14.15' (Free Discharge)
 ↳1=Exfiltration (Exfiltration Controls 0.08 cfs)

Primary OutFlow Max=42.04 cfs @ 11.96 hrs HW=14.03' (Free Discharge)
 ↳2=Culvert (Inlet Controls 42.04 cfs @ 5.95 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge)
 ↳3=Wharf (Controls 0.00 cfs)

Pond C-4: Chamber Series 4

Hydrograph



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Pond C-5: Chamber Series 5

Inflow Area = 5.200 ac, 0.00% Impervious, Inflow Depth > 2.95" for 10-Year event
 Inflow = 23.53 cfs @ 11.98 hrs, Volume= 1.279 af
 Outflow = 24.69 cfs @ 12.02 hrs, Volume= 1.023 af, Atten= 0%, Lag= 2.2 min
 Discarded = 0.19 cfs @ 12.00 hrs, Volume= 0.391 af
 Primary = 24.51 cfs @ 12.02 hrs, Volume= 0.633 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 15.19' @ 12.02 hrs Surf.Area= 16,669 sf Storage= 24,121 cf

Plug-Flow detention time= 425.0 min calculated for 1.022 af (80% of inflow)
 Center-of-Mass det. time= 347.1 min (1,130.4 - 783.3)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	7,757 cf	28.50'W x 168.47'L x 6.75'H Field B 32,409 cf Overall - 13,016 cf Embedded = 19,393 cf x 40.0% Voids
#2B	6.75'	13,016 cf	ADS_StormTech MC-4500 b +Cap x 120 Inside #1 Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap 120 Chambers in 3 Rows Cap Storage= +39.5 cf x 2 x 3 rows = 237.0 cf
#3	14.60'	7,420 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		28,193 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
14.60	200	0	0
14.80	1,000	120	120
15.00	10,000	1,100	1,220
15.50	14,800	6,200	7,420

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	1.000 in/hr Exfiltration over Surface area
#2	Primary	12.60'	36.0" Round Culvert L= 62.8' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 12.60' / 12.29' S= 0.0049 ' / ' Cc= 0.900 n= 0.013 Cast iron, coated, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

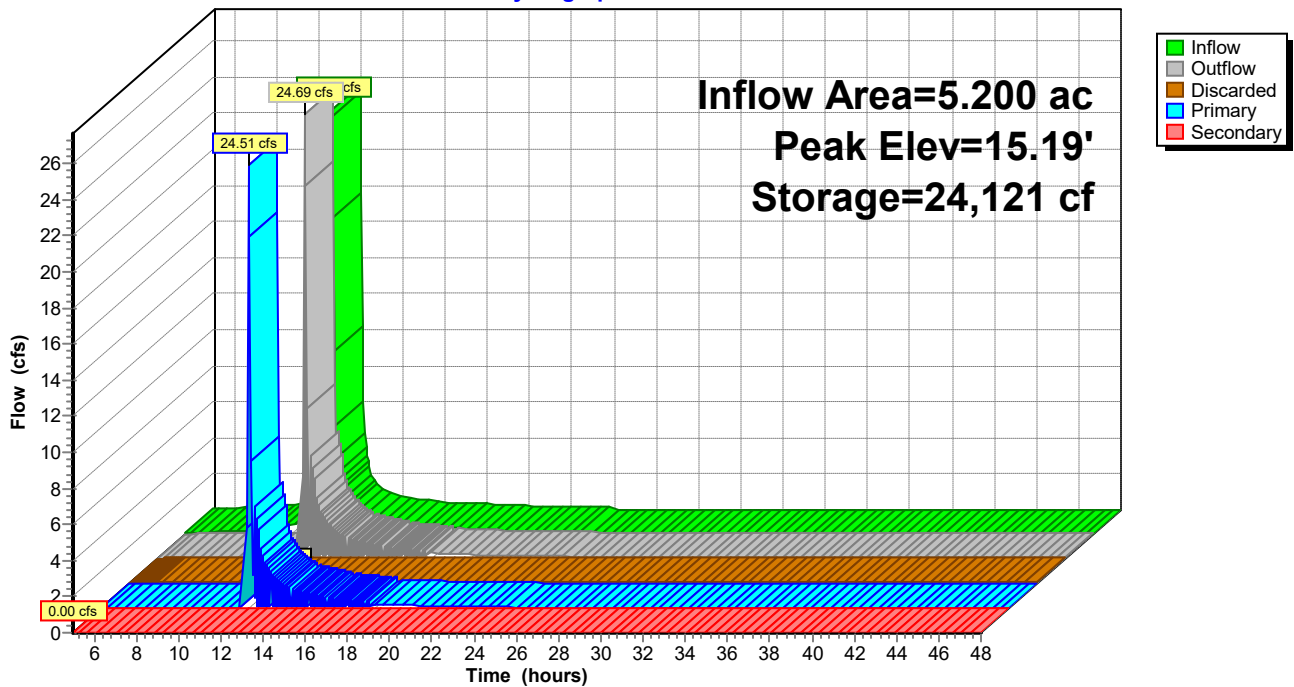
Discarded OutFlow Max=0.19 cfs @ 12.00 hrs HW=14.85' (Free Discharge)
↑1=Exfiltration (Exfiltration Controls 0.19 cfs)

Primary OutFlow Max=21.56 cfs @ 12.02 hrs HW=14.81' (Free Discharge)
↑2=Culvert (Barrel Controls 21.56 cfs @ 5.38 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.00' (Free Discharge)
↑3=Wharf (Controls 0.00 cfs)

Pond C-5: Chamber Series 5

Hydrograph



Summary for Subcatchment DR-1: Building A & Storage

Runoff = 84.97 cfs @ 11.98 hrs, Volume= 4.805 af, Depth> 5.60"

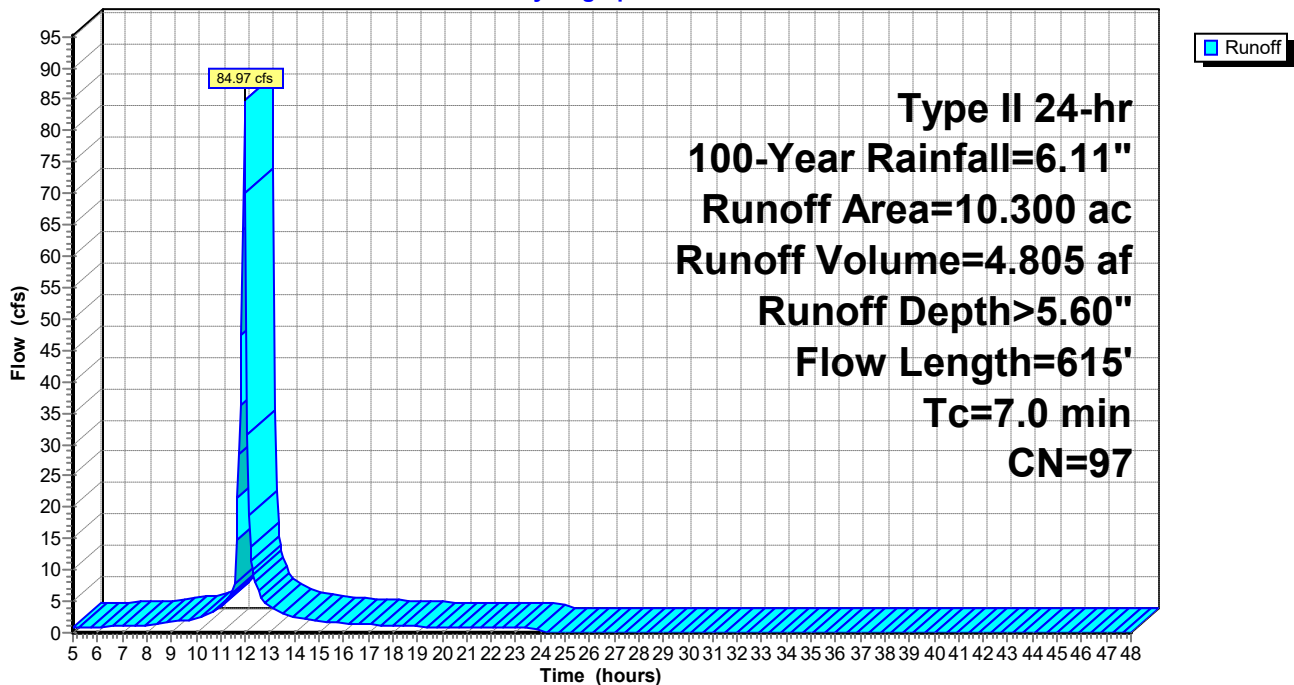
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 6.870	98	Building A
0.100	80	>75% Grass cover, Good, HSG D
* 3.330	95	Dense Graded Aggregate
10.300	97	Weighted Average
3.430		33.30% Pervious Area
6.870		66.70% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
3.1	300	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	215	0.0050	5.91	29.00	Pipe Channel, 30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63' n= 0.013
7.0	615	Total			

Subcatchment DR-1: Building A & Storage

Hydrograph



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 100-Year Rainfall=6.11"

Prepared by McFarland Johnson

Printed 6/8/2022

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Summary for Subcatchment DR-10: Undisturbed Area

Runoff = 26.67 cfs @ 13.16 hrs, Volume= 6.234 af, Depth= 3.78"

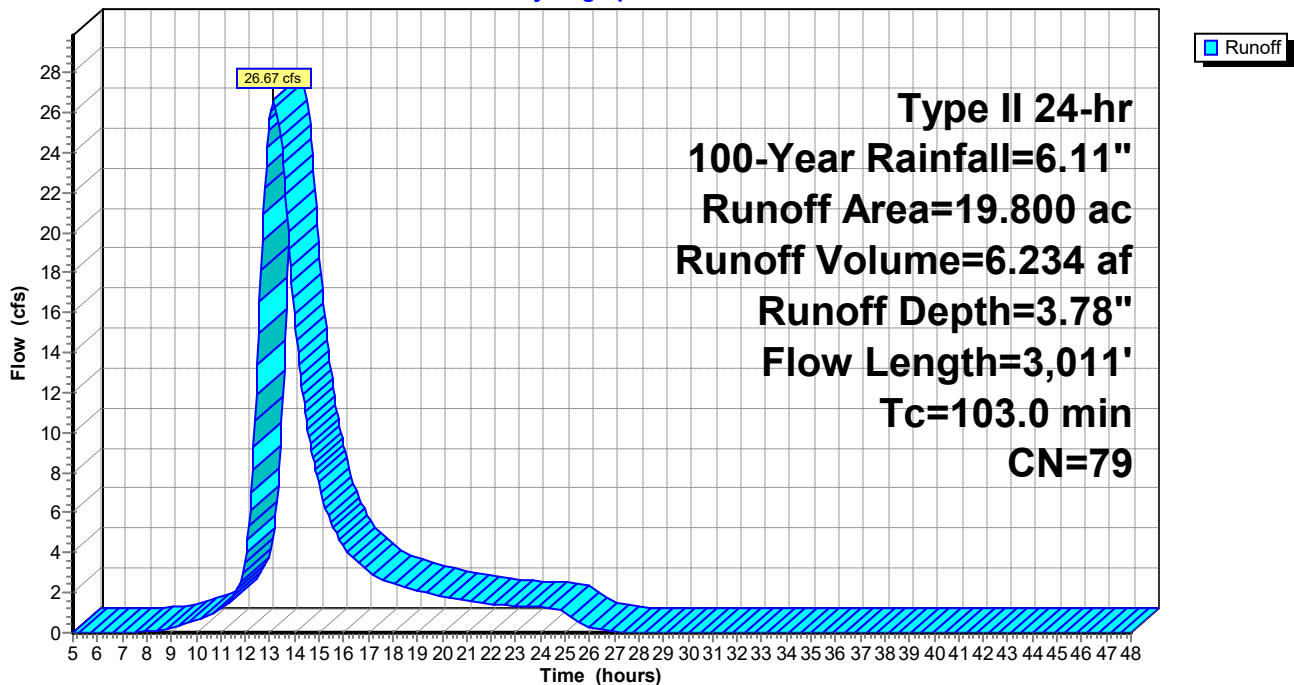
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
19.800	79	Woods, Fair, HSG D
19.800		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
19.7	150	0.0800	0.13		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"
3.0	200	0.0500	1.12		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
1.6	250	0.2600	2.55		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
78.7	2,361	0.0100	0.50		Shallow Concentrated Flow, Wetland Flow Woodland Kv= 5.0 fps
0.0	50	0.0500	22.86	161.57	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.012 Corrugated PP, smooth interior
103.0	3,011	Total			

Subcatchment DR-10: Undisturbed Area

Hydrograph



Summary for Subcatchment DR-11: Hudson River Bank

Runoff = 18.71 cfs @ 12.08 hrs, Volume= 1.259 af, Depth= 3.78"

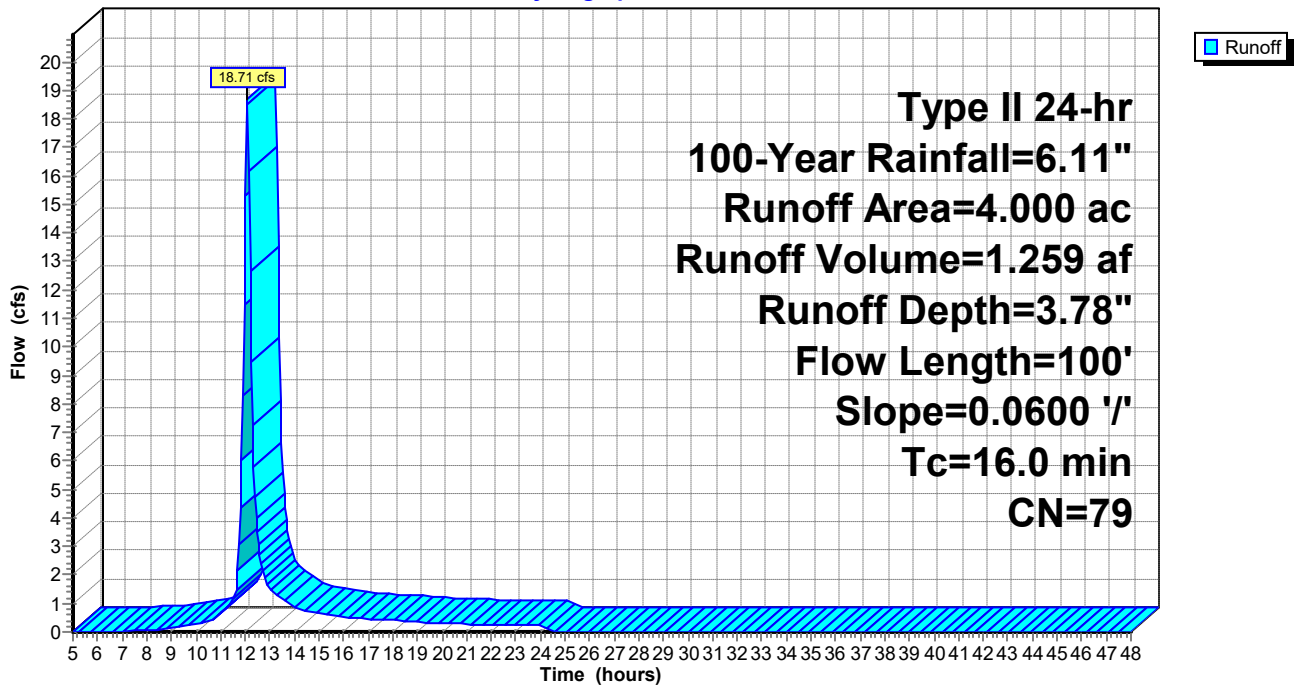
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
4.000	79	Woods, Fair, HSG D
4.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.0	100	0.0600	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-11: Hudson River Bank

Hydrograph



Summary for Subcatchment DR-12: Normans Kill Bank

Runoff = 11.17 cfs @ 11.96 hrs, Volume= 0.588 af, Depth> 5.04"

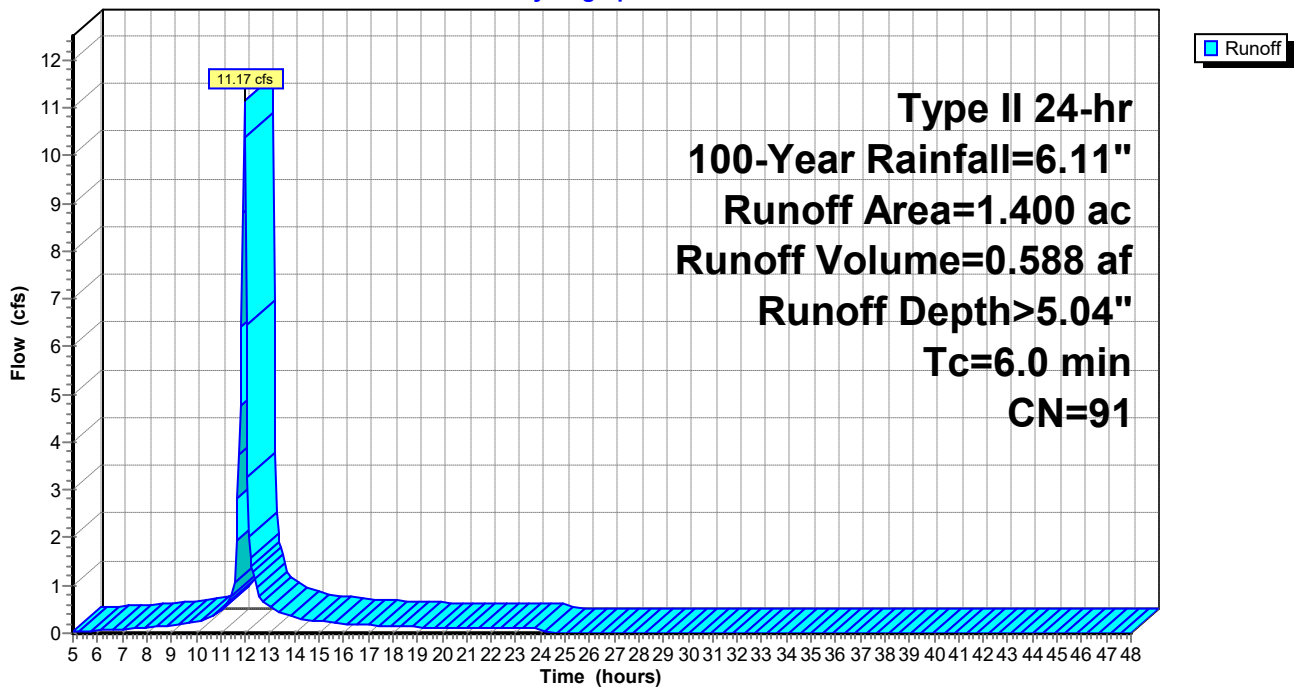
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
0.430	79	Woods, Fair, HSG D
0.970	96	Gravel surface, HSG D
1.400	91	Weighted Average
1.400		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-12: Normans Kill Bank

Hydrograph



Summary for Subcatchment DR-13: Roadway

Runoff = 4.32 cfs @ 11.98 hrs, Volume= 0.208 af, Depth= 2.08"

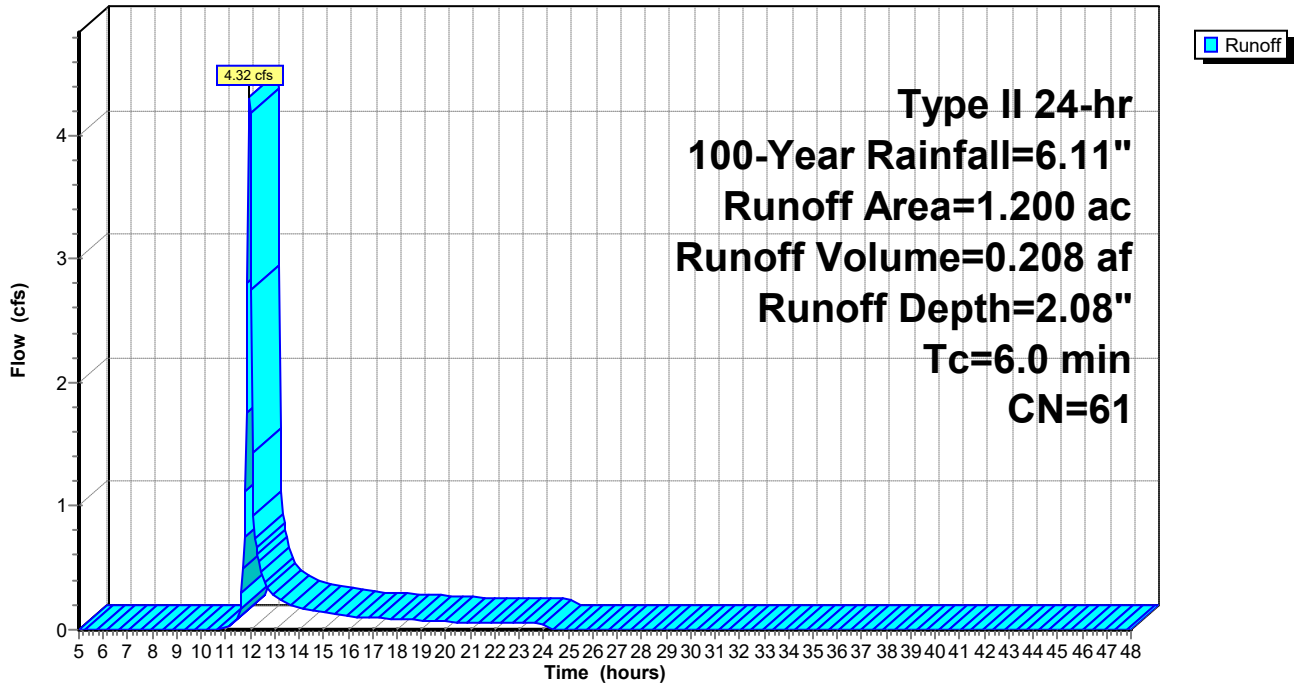
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 0.450	98	Pavement
0.750	39	>75% Grass cover, Good, HSG A
1.200	61	Weighted Average
0.750		62.50% Pervious Area
0.450		37.50% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-13: Roadway

Hydrograph



Summary for Subcatchment DR-14: Roadway

Runoff = 7.10 cfs @ 11.97 hrs, Volume= 0.345 af, Depth= 3.18"

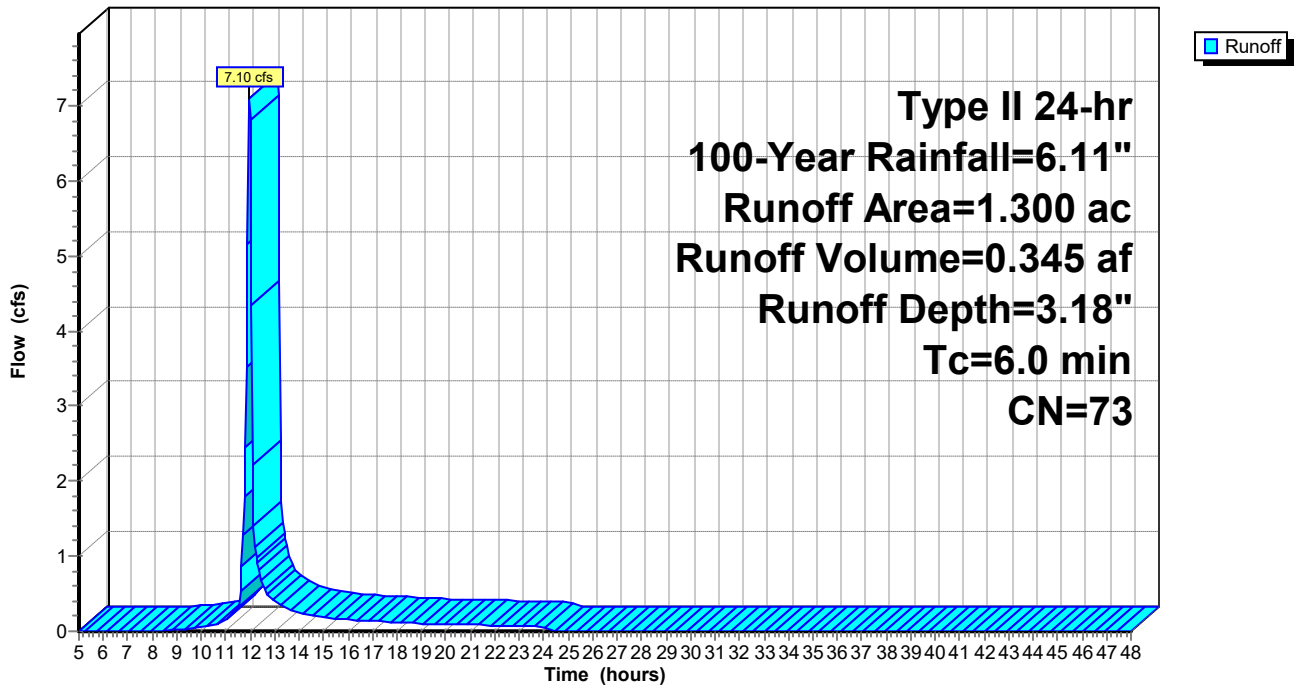
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 0.550	98	New Pavement
0.550	39	>75% Grass cover, Good, HSG A
* 0.200	98	Mill & Fill of Old Pavement
1.300	73	Weighted Average
0.550		42.31% Pervious Area
0.750		57.69% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-14: Roadway

Hydrograph



Summary for Subcatchment DR-15: Roadway

Runoff = 8.32 cfs @ 11.96 hrs, Volume= 0.453 af, Depth> 5.43"

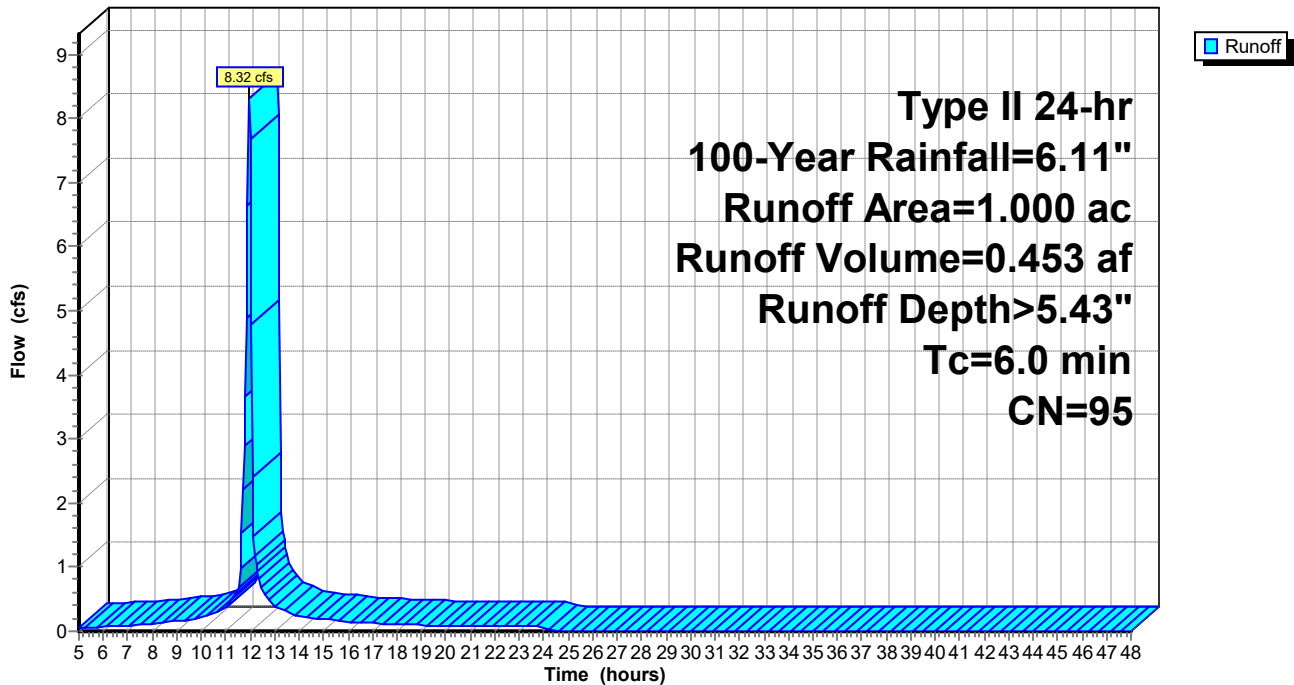
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 0.050	98	New Pavement
0.050	39	>75% Grass cover, Good, HSG A
* 0.900	98	Mill & Fill of Old Pavement
1.000	95	Weighted Average
0.050		5.00% Pervious Area
0.950		95.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min

Subcatchment DR-15: Roadway

Hydrograph



Summary for Subcatchment DR-16: Undisturbed Area

Runoff = 2.86 cfs @ 12.41 hrs, Volume= 0.537 af, Depth= 0.72"

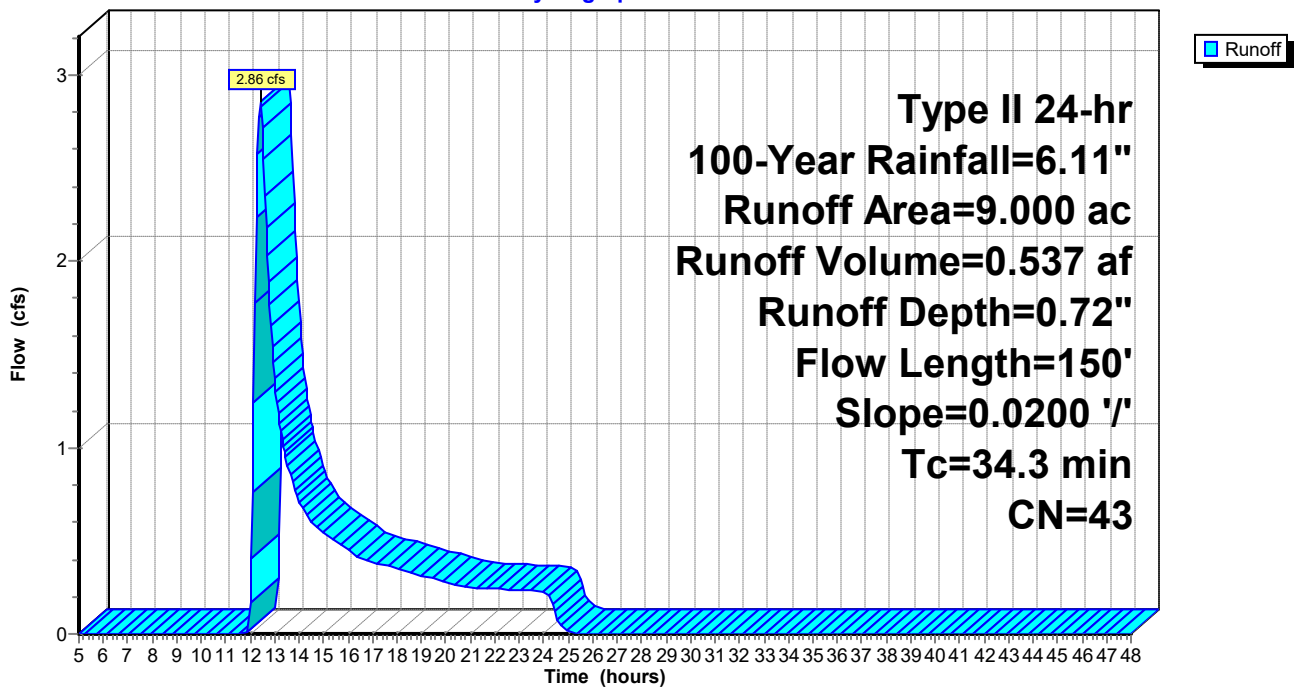
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
9.000	43	Woods/grass comb., Fair, HSG A
9.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
34.3	150	0.0200	0.07		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.40"

Subcatchment DR-16: Undisturbed Area

Hydrograph



Summary for Subcatchment DR-17: Roadway

Runoff = 5.62 cfs @ 11.97 hrs, Volume= 0.286 af, Depth> 4.51"

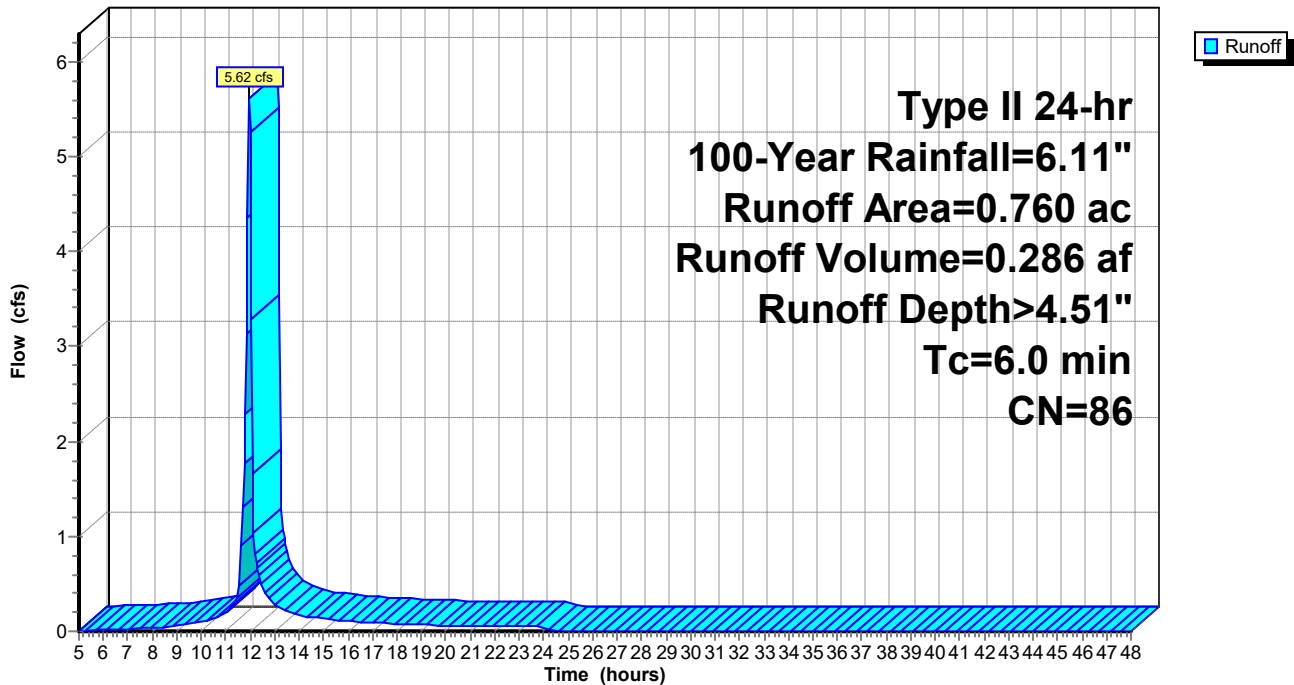
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 0.140	98	Road Widening
* 0.460	98	Roadway
0.160	39	>75% Grass cover, Good, HSG A
0.760	86	Weighted Average
0.160		21.05% Pervious Area
0.600		78.95% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-17: Roadway

Hydrograph



Summary for Subcatchment DR-2: Storage

Runoff = 42.20 cfs @ 12.00 hrs, Volume= 2.447 af, Depth> 5.34"

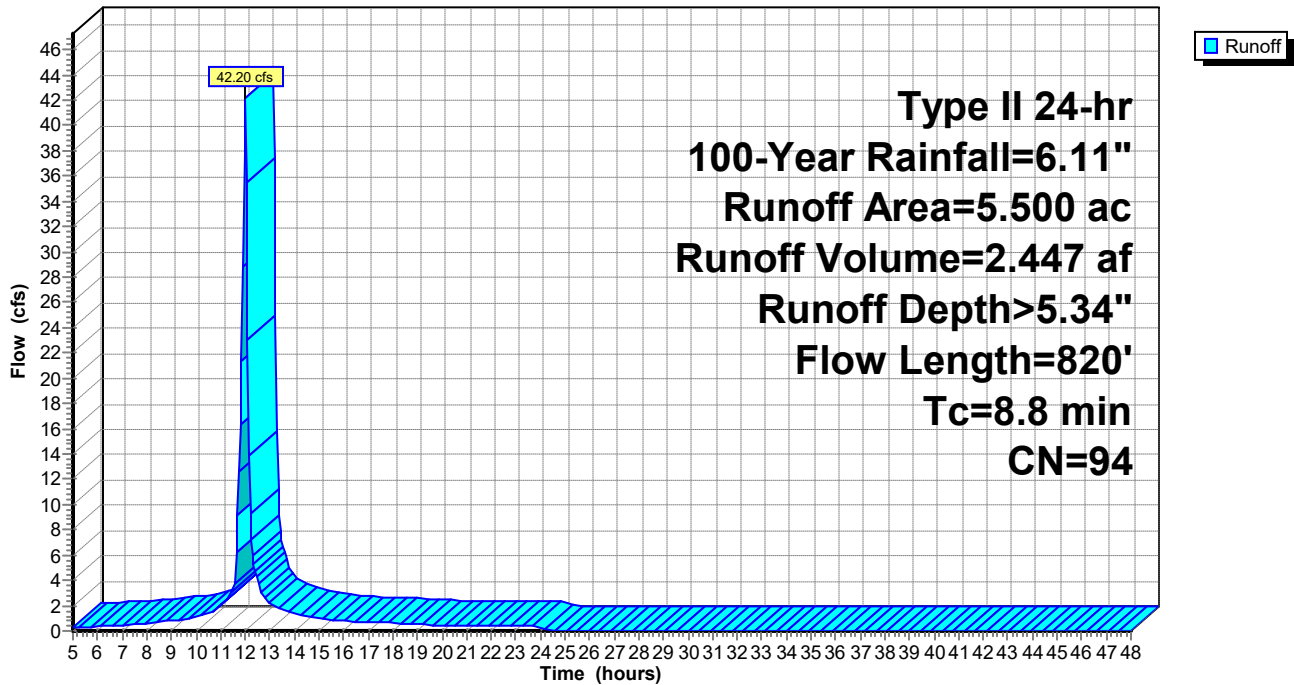
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 5.300	95	Dense Graded Aggregate
0.200	80	>75% Grass cover, Good, HSG D
5.500	94	Weighted Average
5.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
4.9	470	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	250	0.0050	6.67	47.16	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.013
8.8	820	Total			

Subcatchment DR-2: Storage

Hydrograph



Summary for Subcatchment DR-3: Rail & Storage

Runoff = 82.94 cfs @ 12.00 hrs, Volume= 4.980 af, Depth> 5.43"

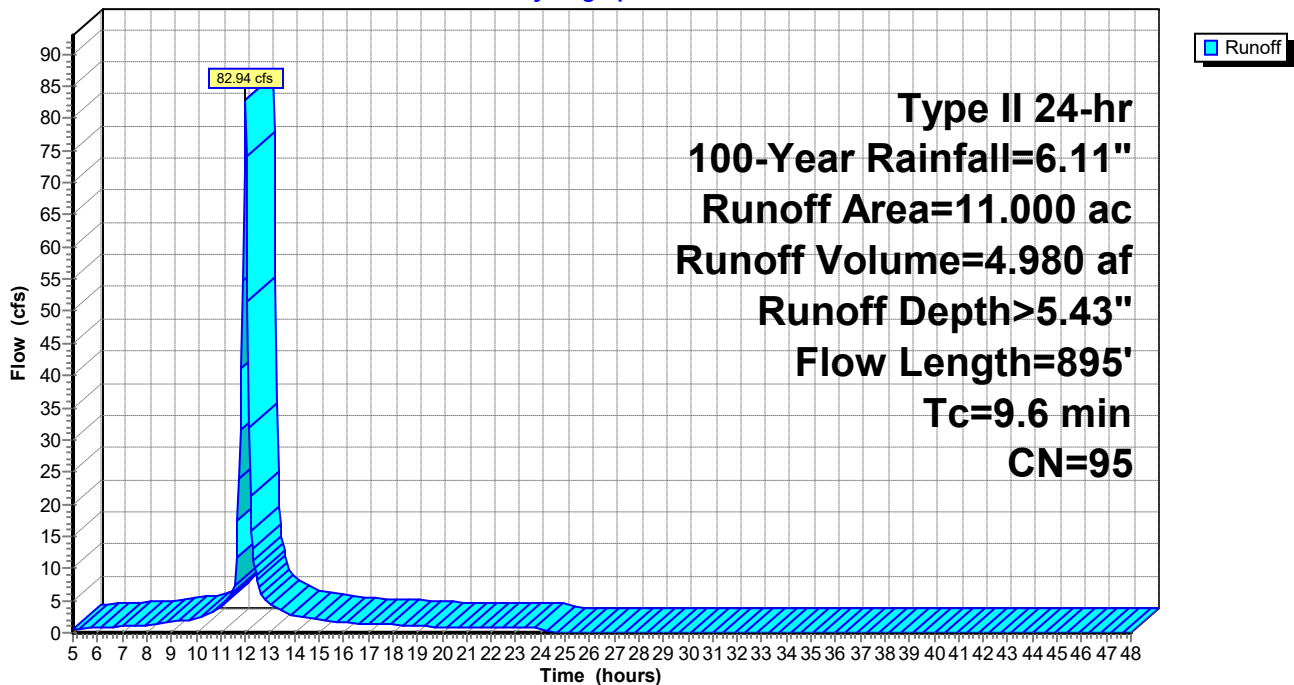
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 8.300	95	Compacted Gravel
0.400	80	>75% Grass cover, Good, HSG D
* 2.300	98	Rail
11.000	95	Weighted Average
8.700		79.09% Pervious Area
2.300		20.91% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
5.4	525	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.9	270	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
9.6	895	Total			

Subcatchment DR-3: Rail & Storage

Hydrograph



Summary for Subcatchment DR-4: Storage

Runoff = 69.96 cfs @ 11.99 hrs, Volume= 3.959 af, Depth> 5.34"

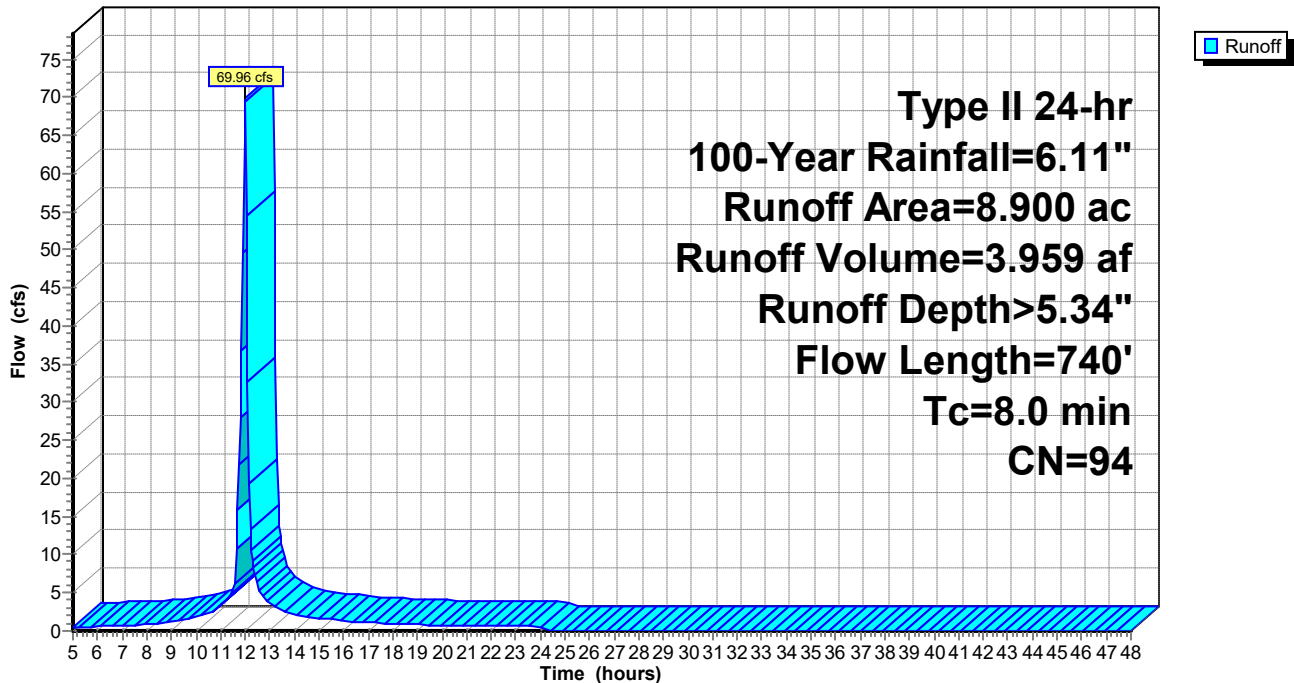
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 8.600	95	Compacted Gravel
0.300	80	>75% Grass cover, Good, HSG D
8.900	94	Weighted Average
8.900		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
4.1	400	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.6	240	0.0050	6.67	47.16	Pipe Channel, 36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75' n= 0.013 Corrugated PE, smooth interior
8.0	740	Total			

Subcatchment DR-4: Storage

Hydrograph



Summary for Subcatchment DR-5: Storage

Runoff = 41.34 cfs @ 11.98 hrs, Volume= 2.313 af, Depth> 5.34"

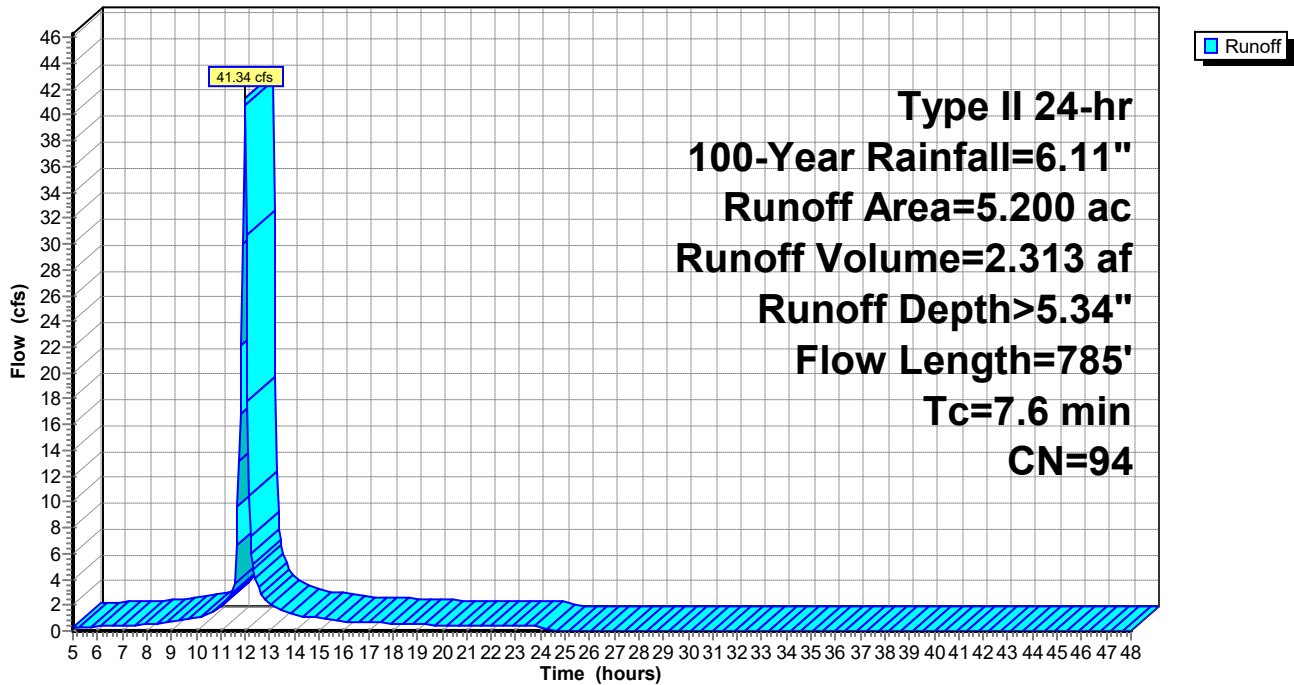
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 4.900	95	Dense Graded Aggregate
0.300	80	>75% Grass cover, Good, HSG D
5.200	94	Weighted Average
5.200		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
3.0	285	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.3	400	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
7.6	785	Total			

Subcatchment DR-5: Storage

Hydrograph



Summary for Subcatchment DR-6: Buldings B & D

Runoff = 92.04 cfs @ 11.99 hrs, Volume= 5.428 af, Depth> 5.52"

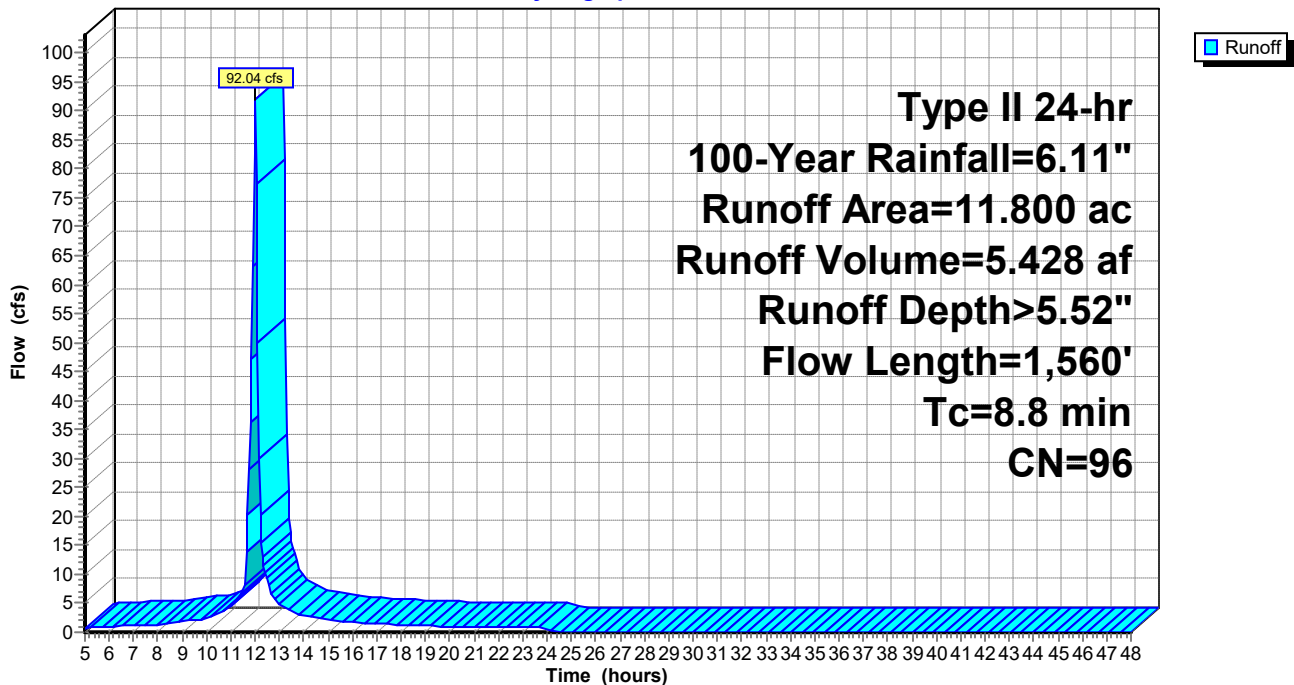
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 2.549	98	Building B
* 1.413	98	Building D
0.200	80	>75% Grass cover, Good, HSG D
* 7.638	95	Dense Graded Aggregate
11.800	96	Weighted Average
7.838		66.42% Pervious Area
3.962		33.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
1.0	100	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.5	1,360	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
8.8	1,560	Total			

Subcatchment DR-6: Buldings B & D

Hydrograph



Summary for Subcatchment DR-7: Building C & Rail

Runoff = 65.86 cfs @ 12.00 hrs, Volume= 4.003 af, Depth> 5.52"

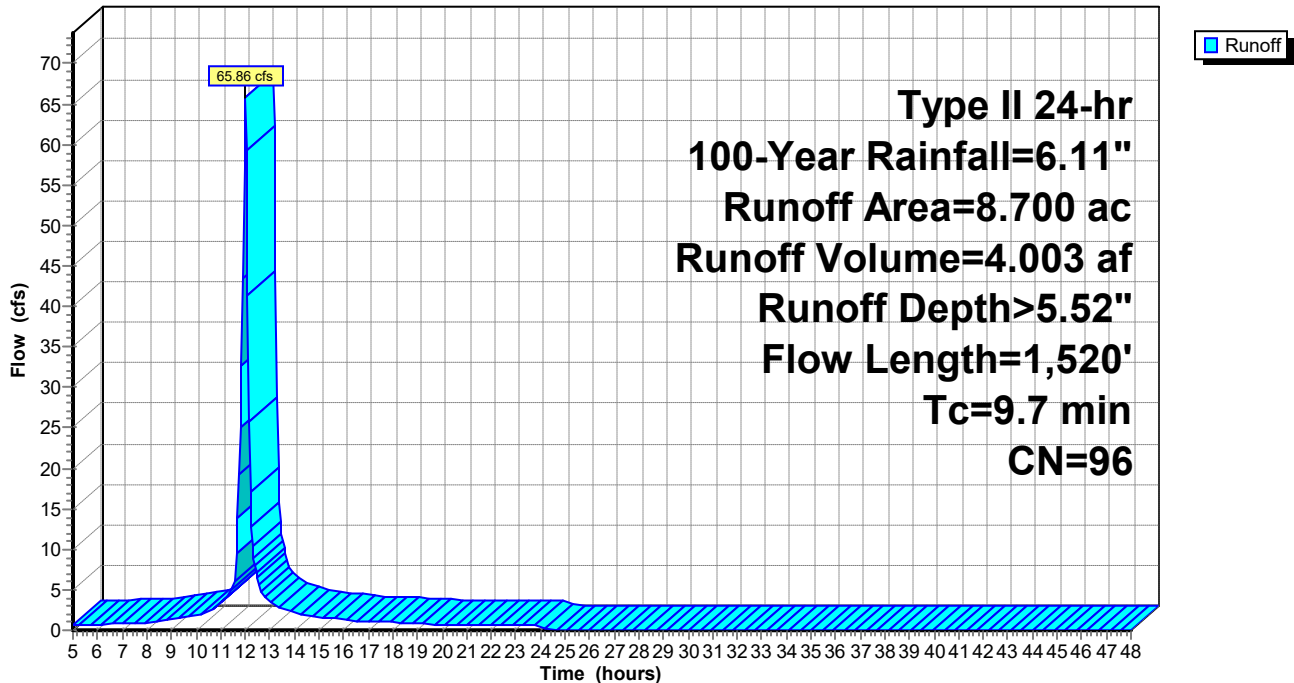
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 3.030	98	Building C
* 0.970	98	Rail
* 4.400	95	Dense Graded Aggregate
0.300	80	>75% Grass cover, Good, HSG D
8.700	96	Weighted Average
4.700		54.02% Pervious Area
4.000		45.98% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	100	0.0100	0.50		Sheet Flow, n= 0.023 P2= 2.40"
2.6	250	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
3.8	1,170	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
9.7	1,520	Total			

Subcatchment DR-7: Building C & Rail

Hydrograph



Summary for Subcatchment DR-8A: Parking

Runoff = 15.81 cfs @ 11.96 hrs, Volume= 0.860 af, Depth> 5.43"

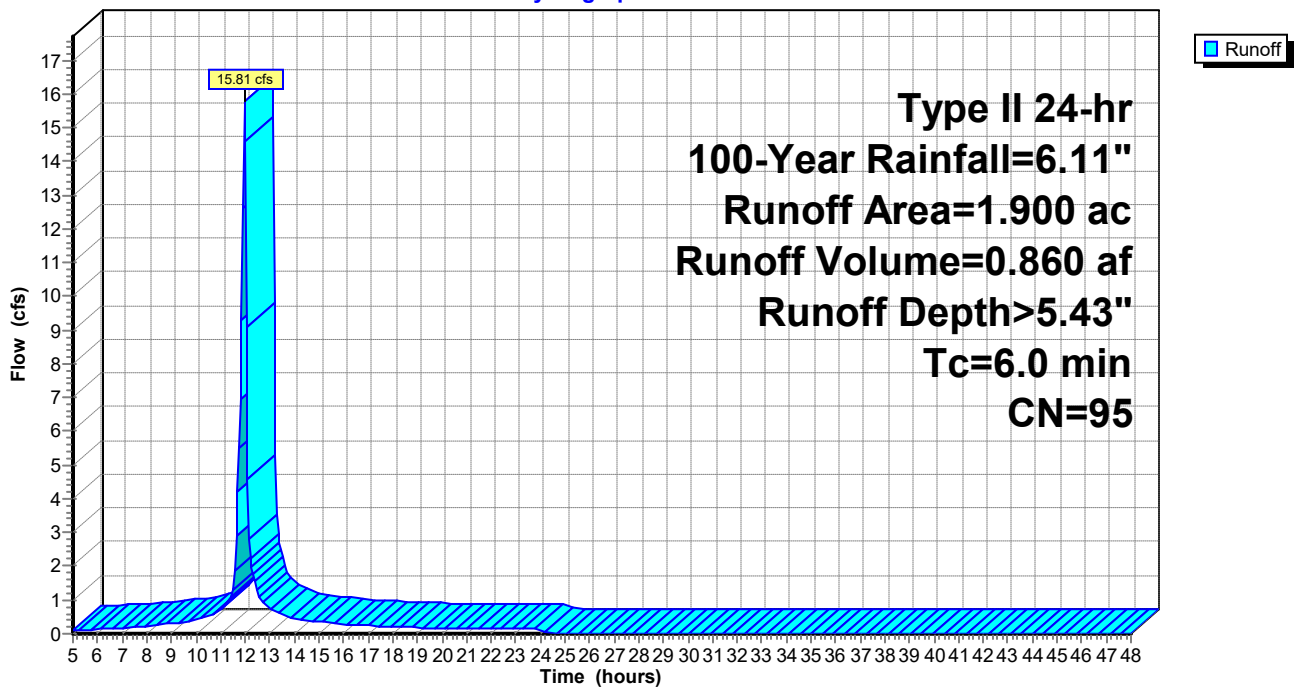
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 1.600	98	Parking
0.300	80	>75% Grass cover, Good, HSG D
1.900	95	Weighted Average
0.300		15.79% Pervious Area
1.600		84.21% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-8A: Parking

Hydrograph



Summary for Subcatchment DR-8B: Roadway & Pond

Runoff = 7.26 cfs @ 11.97 hrs, Volume= 0.367 af, Depth> 4.41"

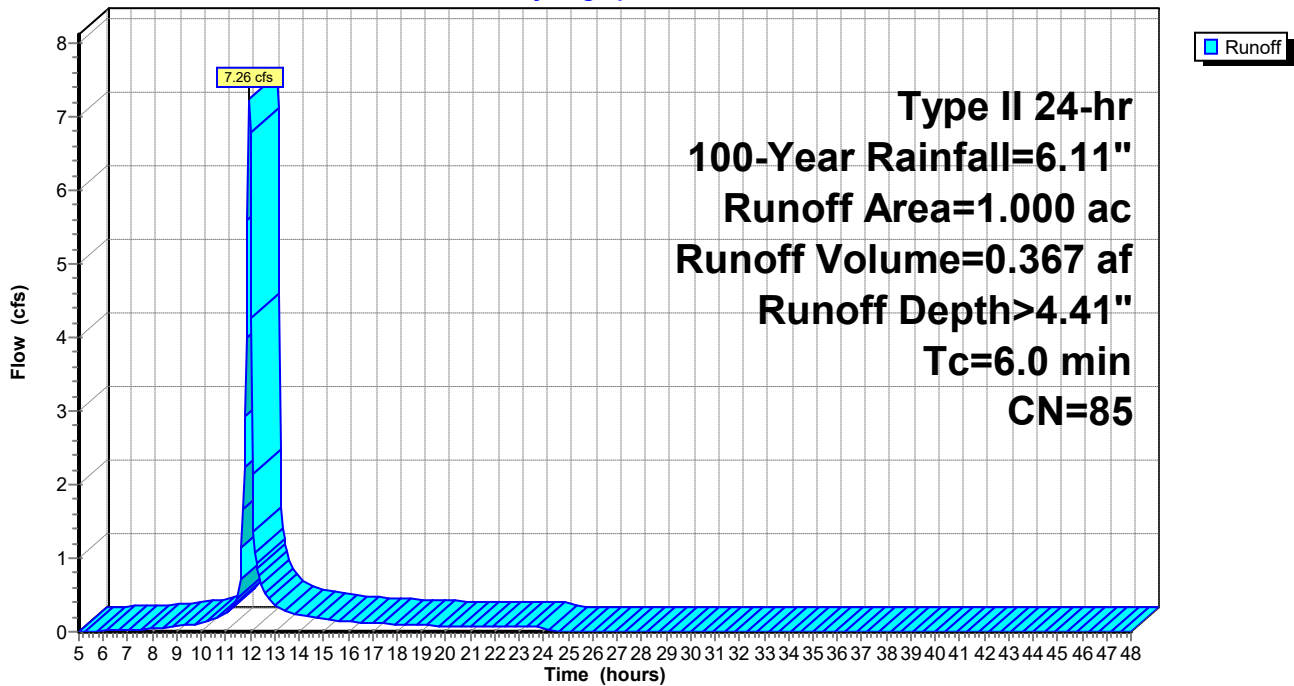
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 0.300	98	Roadway
0.700	80	>75% Grass cover, Good, HSG D
1.000	85	Weighted Average
0.700		70.00% Pervious Area
0.300		30.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Minimum

Subcatchment DR-8B: Roadway & Pond

Hydrograph



Summary for Subcatchment DR-9A: Parking & Substation

Runoff = 12.25 cfs @ 12.04 hrs, Volume= 0.815 af, Depth> 5.44"

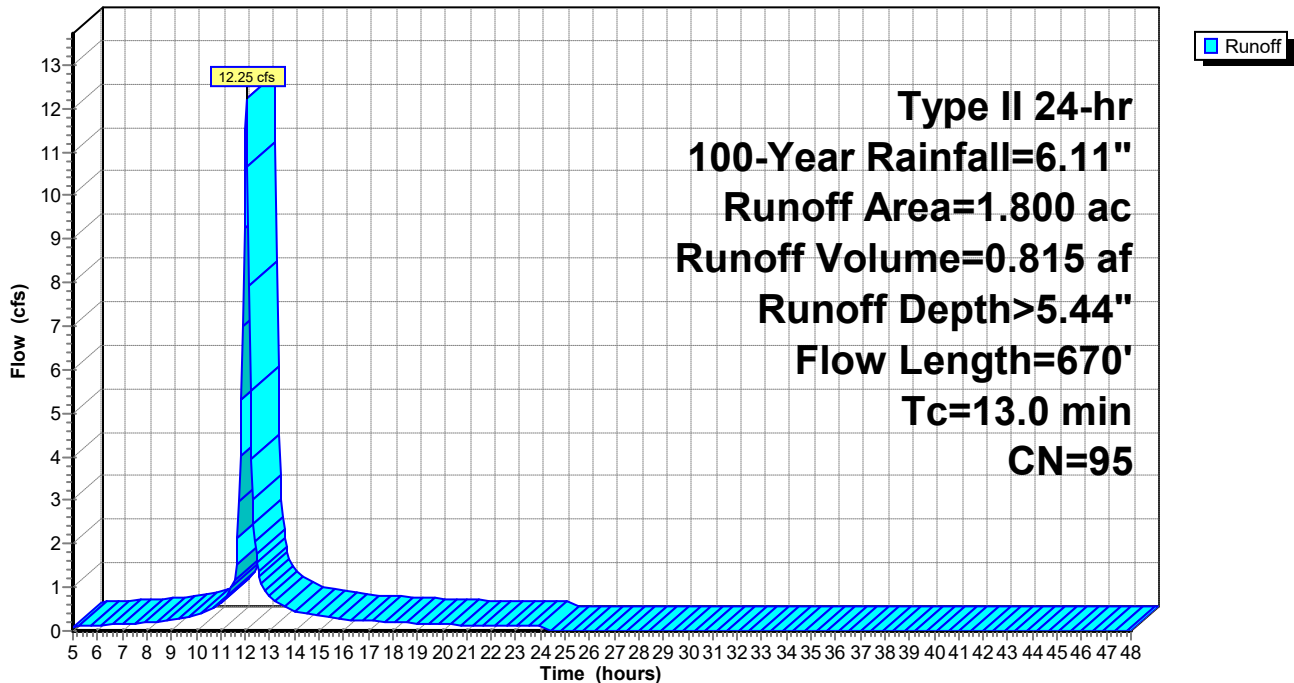
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
0.230	80	>75% Grass cover, Good, HSG D
* 0.200	92	Compacted Gravel
* 1.200	98	Parking and Road
* 0.170	98	Substation
1.800	95	Weighted Average
0.430		23.89% Pervious Area
1.370		76.11% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	100	0.0200	1.19		Sheet Flow, Parking Lot Runoff Smooth surfaces n= 0.011 P2= 2.40"
11.6	570	0.0030	0.82		Shallow Concentrated Flow, Grass Lined Ditch to Pond Grassed Waterway Kv= 15.0 fps
13.0	670	Total			

Subcatchment DR-9A: Parking & Substation

Hydrograph



Summary for Subcatchment DR-9B: Roadway

Runoff = 30.42 cfs @ 11.96 hrs, Volume= 1.504 af, Depth> 4.51"

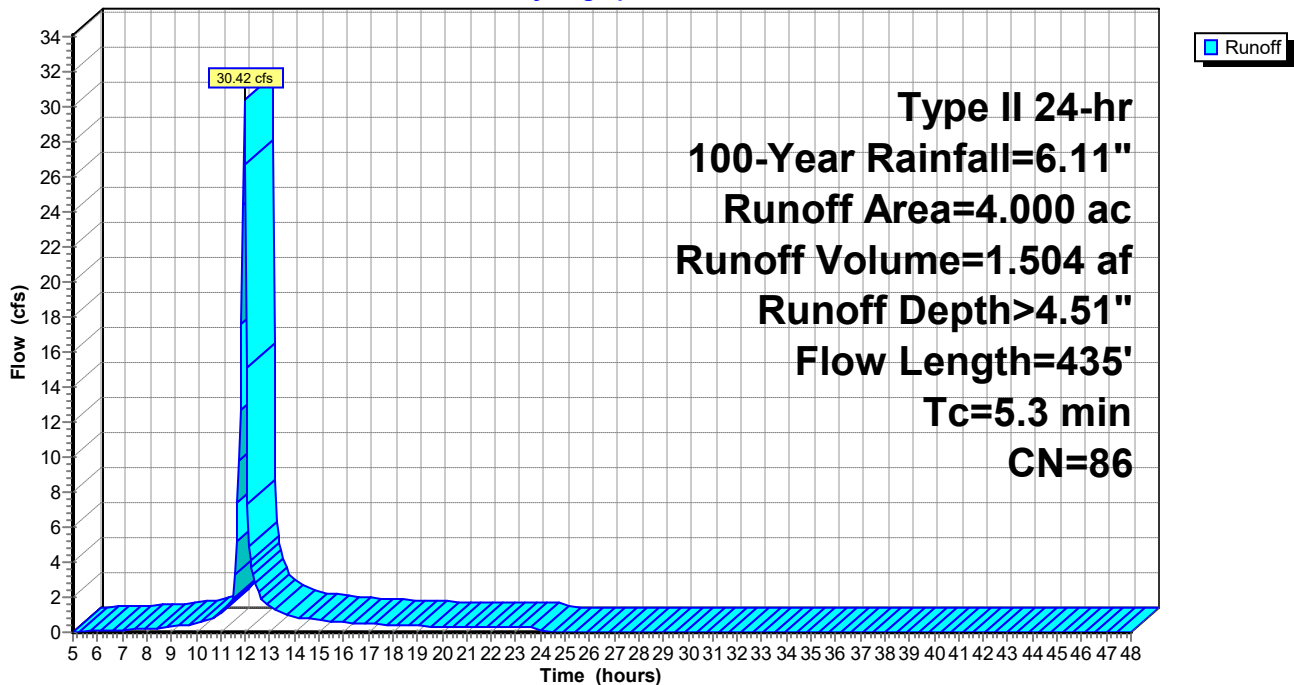
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Type II 24-hr 100-Year Rainfall=6.11"

Area (ac)	CN	Description
* 1.050	95	Dense Graded Aggregate
* 0.480	98	Roadway
2.470	80	>75% Grass cover, Good, HSG D
4.000	86	Weighted Average
3.520		88.00% Pervious Area
0.480		12.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.6	100	0.0250	0.46		Sheet Flow, Dense Graded Aggregate Yard n= 0.040 P2= 2.40"
1.3	230	0.0100	3.07	9.20	Channel Flow, Grass lined ditch Area= 3.0 sf Perim= 4.0' r= 0.75' n= 0.040 Earth, cobble bottom, clean sides
0.4	105	0.0050	4.20	7.43	Pipe Channel, driveway culvert 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013 Corrugated PE, smooth interior
5.3	435	Total			

Subcatchment DR-9B: Roadway

Hydrograph



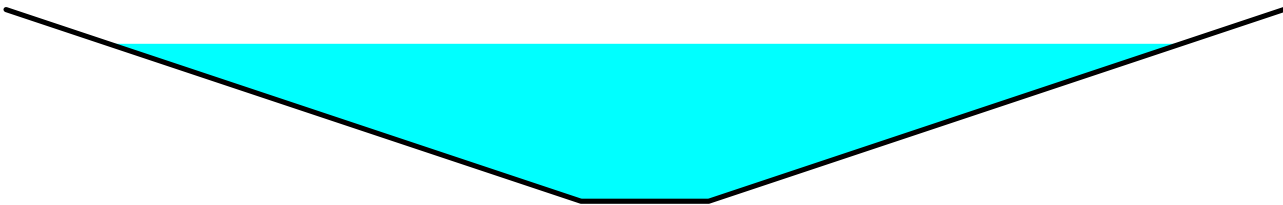
Summary for Reach 1R: Swale

Inflow Area = 1.900 ac, 84.21% Impervious, Inflow Depth > 5.43" for 100-Year event
 Inflow = 15.81 cfs @ 11.96 hrs, Volume= 0.860 af
 Outflow = 13.37 cfs @ 12.09 hrs, Volume= 0.860 af, Atten= 15%, Lag= 7.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.38 fps, Min. Travel Time= 4.8 min
 Avg. Velocity = 0.71 fps, Avg. Travel Time= 16.3 min

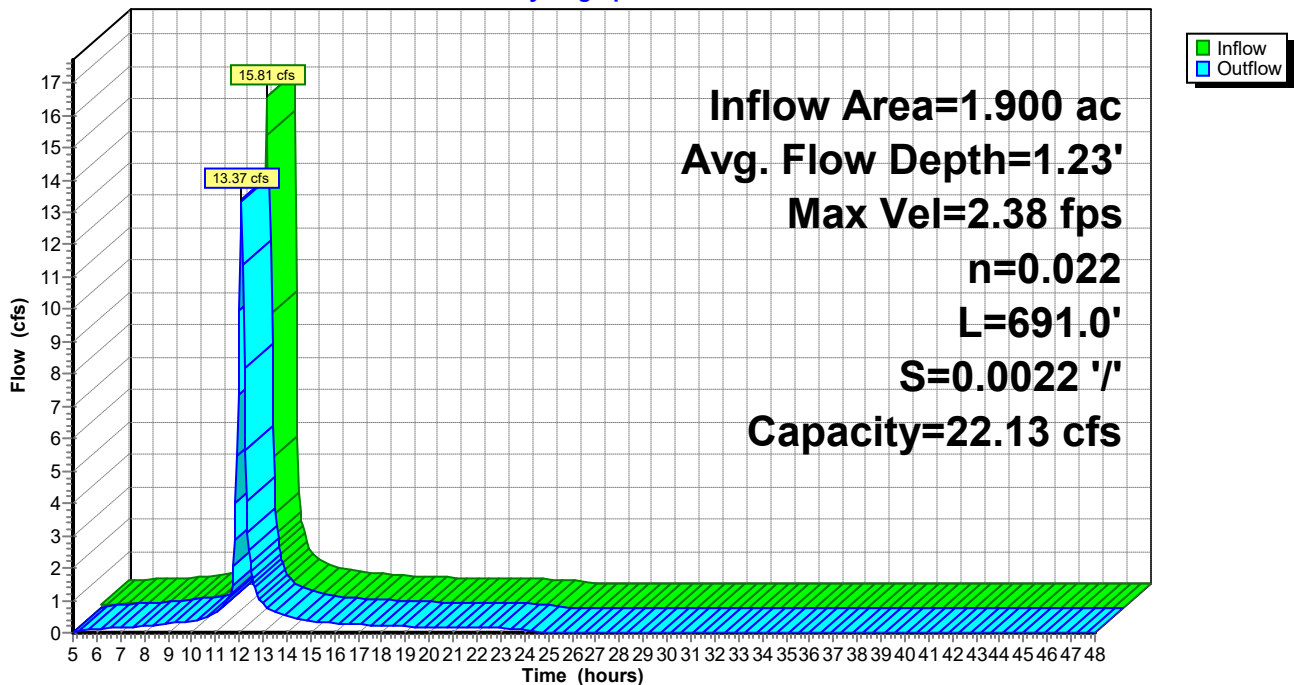
Peak Storage= 3,995 cf @ 12.01 hrs
 Average Depth at Peak Storage= 1.23' , Surface Width= 8.39'
 Bank-Full Depth= 1.50' Flow Area= 8.3 sf, Capacity= 22.13 cfs

1.00' x 1.50' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 10.00'
 Length= 691.0' Slope= 0.0022 ' / '
 Inlet Invert= 15.50', Outlet Invert= 14.00'



Reach 1R: Swale

Hydrograph



Summary for Reach 1W: Wetland #1 / Analysis Point 1A

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 4.11" for 100-Year event
 Inflow = 30.97 cfs @ 13.14 hrs, Volume= 9.753 af
 Outflow = 18.15 cfs @ 16.00 hrs, Volume= 9.491 af, Atten= 41%, Lag= 172.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 0.14 fps, Min. Travel Time= 118.8 min
 Avg. Velocity = 0.05 fps, Avg. Travel Time= 314.3 min

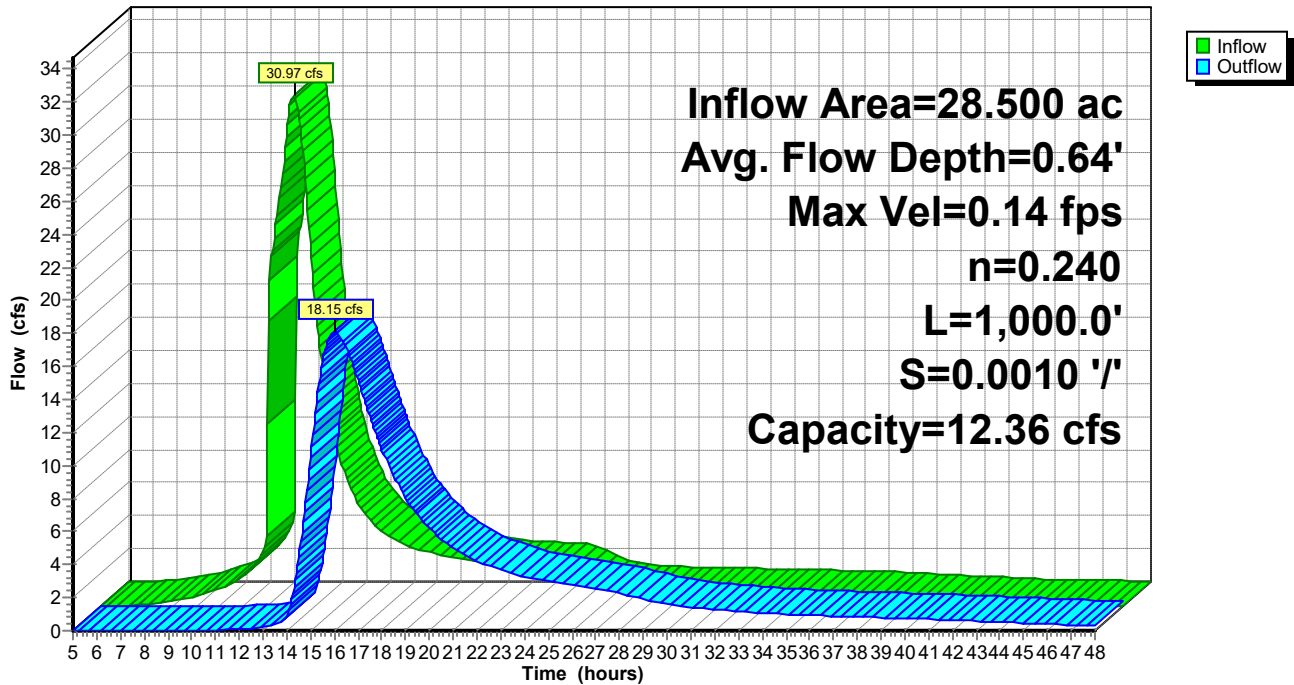
Peak Storage= 129,381 cf @ 14.02 hrs
 Average Depth at Peak Storage= 0.64' , Surface Width= 203.85'
 Bank-Full Depth= 0.50' Flow Area= 100.8 sf, Capacity= 12.36 cfs

200.00' x 0.50' deep channel, n= 0.240
 Side Slope Z-value= 3.0 '/' Top Width= 203.00'
 Length= 1,000.0' Slope= 0.0010 '/'
 Inlet Invert= 6.00', Outlet Invert= 5.00'



Reach 1W: Wetland #1 / Analysis Point 1A

Hydrograph



Summary for Reach 2R: Overflow

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 4.77" for 100-Year event
 Inflow = 15.27 cfs @ 12.13 hrs, Volume= 2.307 af
 Outflow = 15.48 cfs @ 12.14 hrs, Volume= 2.307 af, Atten= 0%, Lag= 0.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 6.51 fps, Min. Travel Time= 0.1 min
 Avg. Velocity = 1.77 fps, Avg. Travel Time= 0.5 min

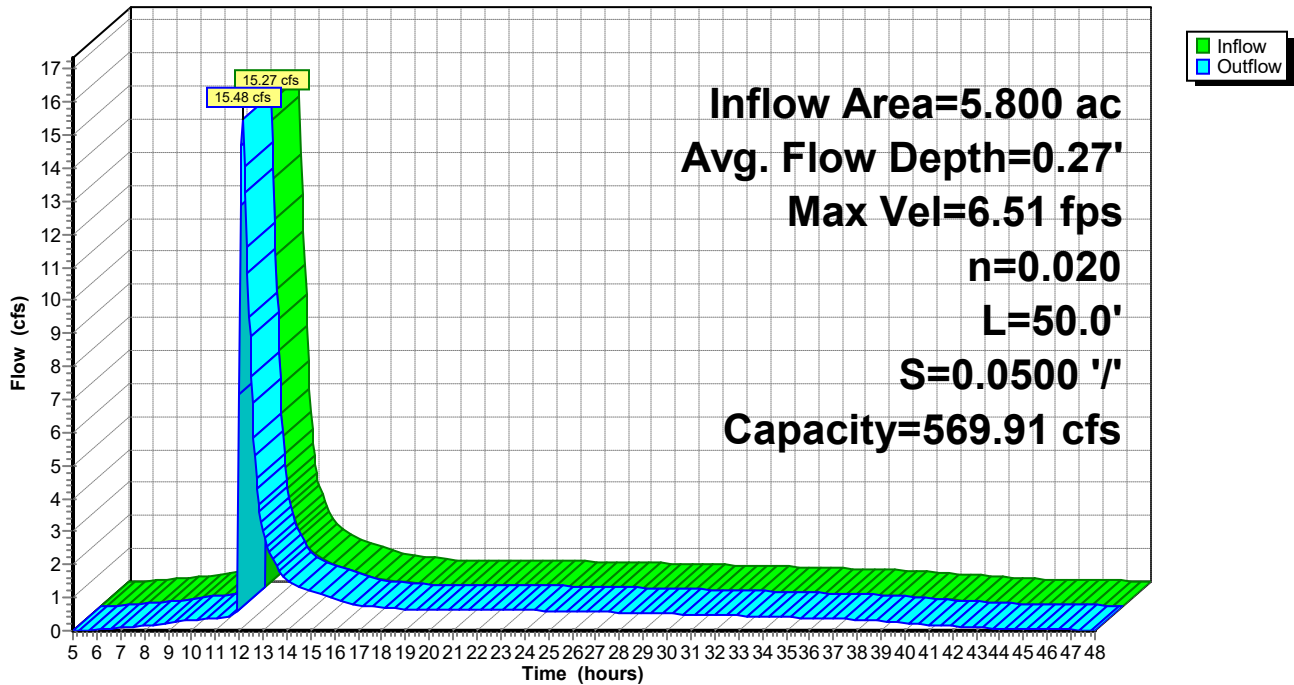
Peak Storage= 119 cf @ 12.14 hrs
 Average Depth at Peak Storage= 0.27' , Surface Width= 9.62'
 Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 569.91 cfs

8.00' x 2.00' deep channel, n= 0.020 Corrugated PE, corrugated interior
 Side Slope Z-value= 3.0 '/' Top Width= 20.00'
 Length= 50.0' Slope= 0.0500 '/'
 Inlet Invert= 16.50', Outlet Invert= 14.00'



Reach 2R: Overflow

Hydrograph



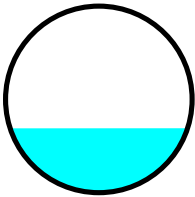
Summary for Reach 3R: Outlet Pipe

Inflow Area = 28.500 ac, 13.16% Impervious, Inflow Depth > 4.00" for 100-Year event
 Inflow = 18.15 cfs @ 16.00 hrs, Volume= 9.491 af
 Outflow = 18.15 cfs @ 16.01 hrs, Volume= 9.490 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 6.79 fps, Min. Travel Time= 0.2 min
 Avg. Velocity = 3.26 fps, Avg. Travel Time= 0.4 min

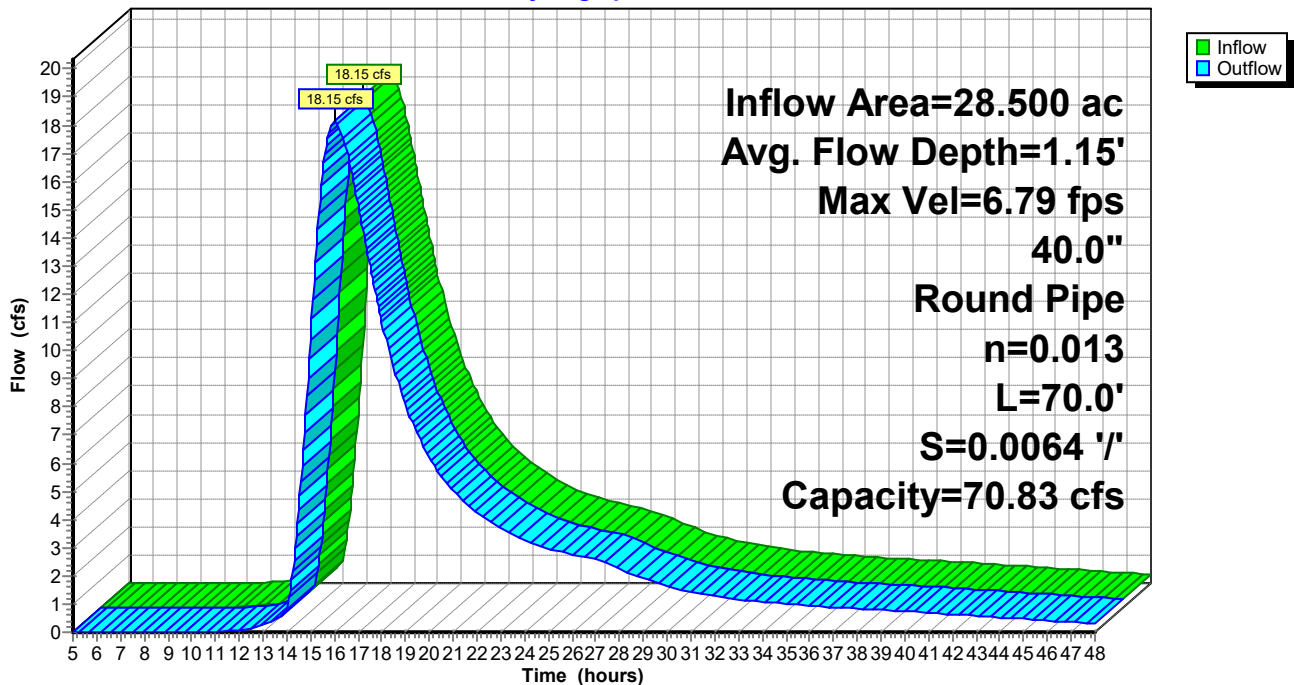
Peak Storage= 187 cf @ 16.00 hrs
 Average Depth at Peak Storage= 1.15' , Surface Width= 3.17'
 Bank-Full Depth= 3.33' Flow Area= 8.7 sf, Capacity= 70.83 cfs

40.0" Round Pipe
 n= 0.013 Corrugated PE, smooth interior
 Length= 70.0' Slope= 0.0064 '/'
 Inlet Invert= 4.25', Outlet Invert= 3.80'



Reach 3R: Outlet Pipe

Hydrograph



Summary for Reach 4R: Overflow

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 5.43" for 100-Year event
 Inflow = 8.17 cfs @ 11.98 hrs, Volume= 0.452 af
 Outflow = 8.00 cfs @ 11.99 hrs, Volume= 0.452 af, Atten= 2%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 3.21 fps, Min. Travel Time= 0.5 min
 Avg. Velocity = 0.87 fps, Avg. Travel Time= 1.9 min

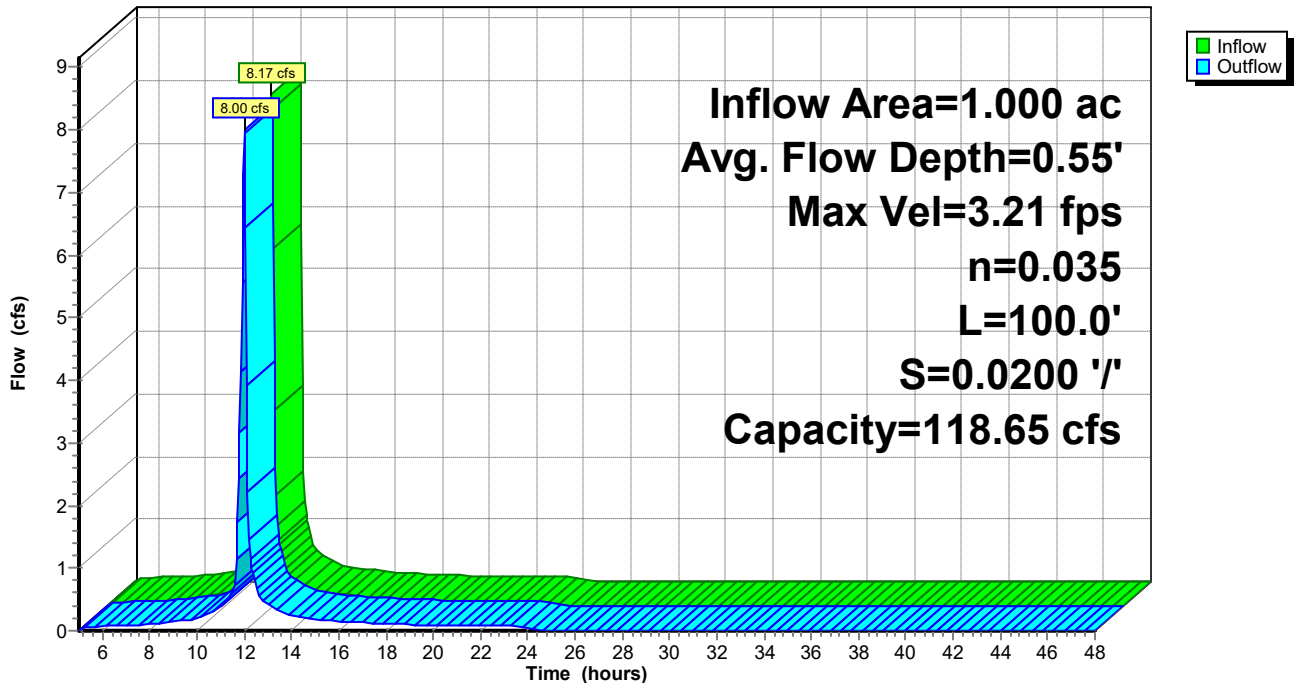
Peak Storage= 253 cf @ 11.98 hrs
 Average Depth at Peak Storage= 0.55' , Surface Width= 6.28'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 118.65 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'
 Length= 100.0' Slope= 0.0200 '/'
 Inlet Invert= 12.00', Outlet Invert= 10.00'



Reach 4R: Overflow

Hydrograph



Summary for Reach 5R: Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 1.24" for 100-Year event
 Inflow = 1.86 cfs @ 12.17 hrs, Volume= 0.124 af
 Outflow = 1.56 cfs @ 12.22 hrs, Volume= 0.124 af, Atten= 16%, Lag= 3.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 1.68 fps, Min. Travel Time= 1.2 min
 Avg. Velocity = 0.58 fps, Avg. Travel Time= 3.6 min

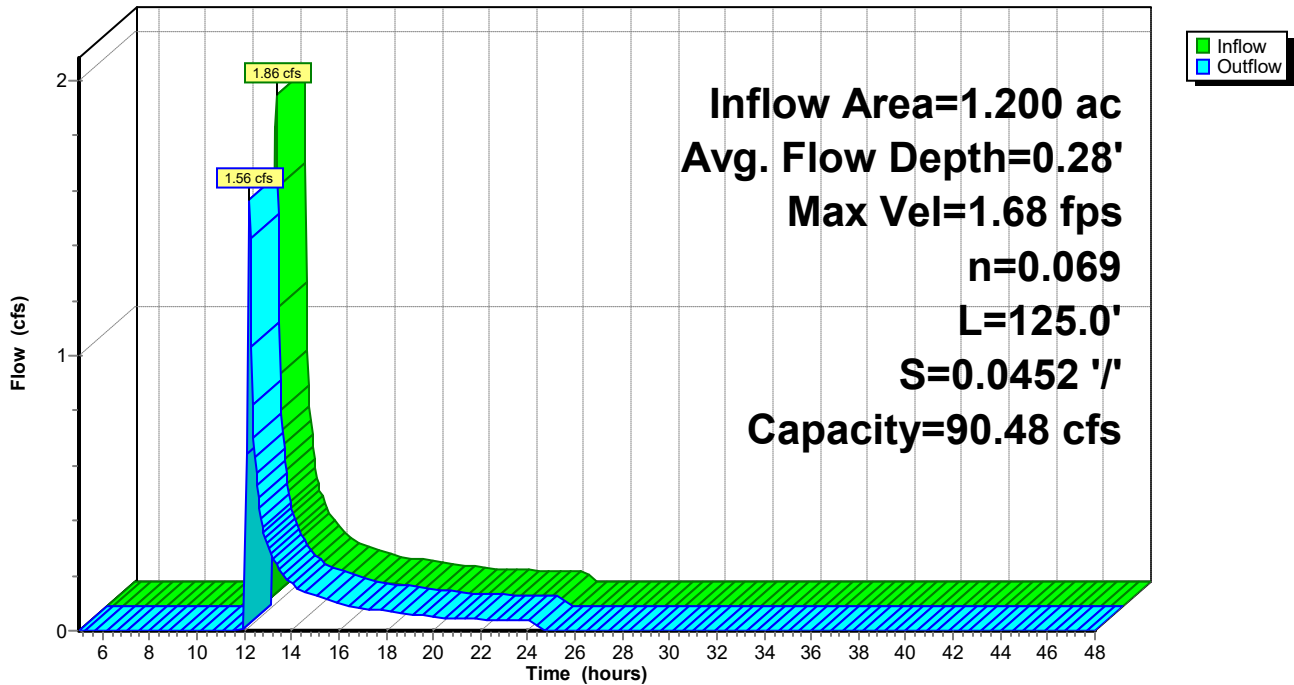
Peak Storage= 132 cf @ 12.20 hrs
 Average Depth at Peak Storage= 0.28' , Surface Width= 4.65'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 90.48 cfs

3.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'
 Length= 125.0' Slope= 0.0452 '/'
 Inlet Invert= 11.65', Outlet Invert= 6.00'



Reach 5R: Overflow

Hydrograph



Summary for Reach 6R: Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 1.08" for 100-Year event
 Inflow = 6.03 cfs @ 12.16 hrs, Volume= 0.117 af
 Outflow = 5.16 cfs @ 12.19 hrs, Volume= 0.117 af, Atten= 14%, Lag= 1.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.82 fps, Min. Travel Time= 0.6 min
 Avg. Velocity = 1.06 fps, Avg. Travel Time= 1.6 min

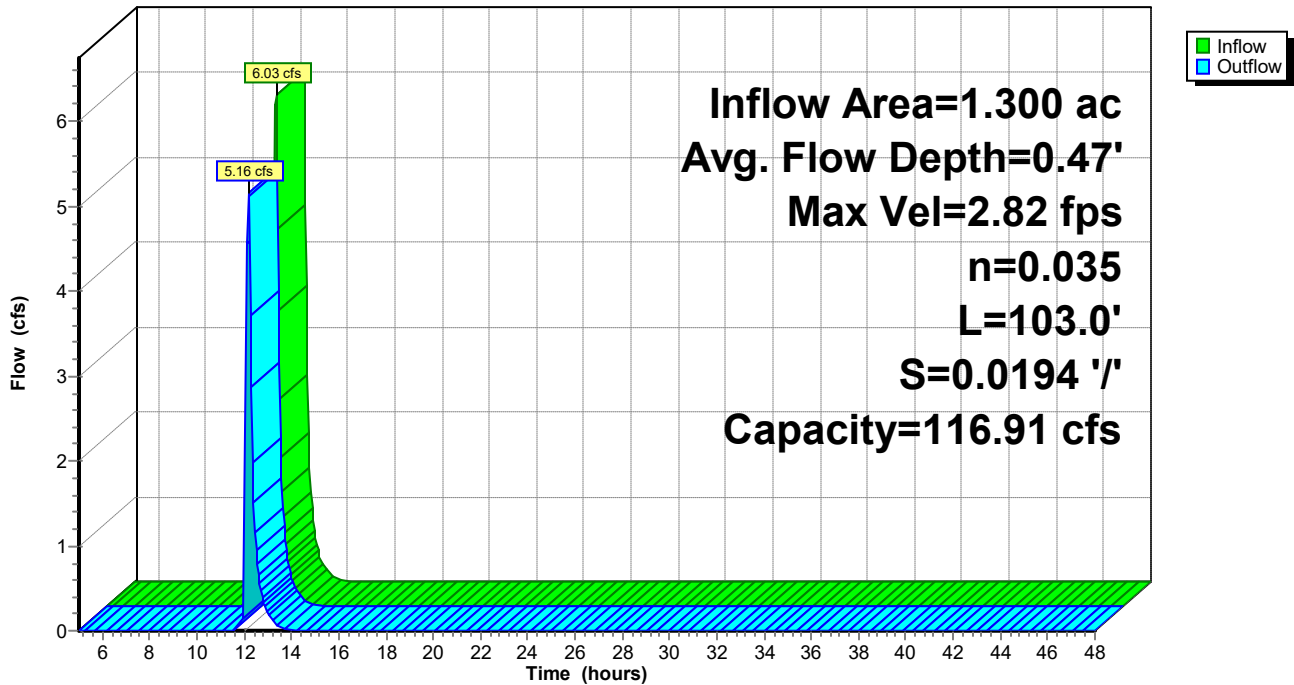
Peak Storage= 209 cf @ 12.17 hrs
 Average Depth at Peak Storage= 0.47' , Surface Width= 5.80'
 Bank-Full Depth= 2.00' Flow Area= 18.0 sf, Capacity= 116.91 cfs

3.00' x 2.00' deep channel, n= 0.035 Riprap, 6-inch
 Side Slope Z-value= 3.0 ' / ' Top Width= 15.00'
 Length= 103.0' Slope= 0.0194 ' / '
 Inlet Invert= 8.50', Outlet Invert= 6.50'



Reach 6R: Overflow

Hydrograph



Summary for Reach 7R: Overflow

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth > 5.02" for 100-Year event
 Inflow = 3.28 cfs @ 12.41 hrs, Volume= 1.212 af
 Outflow = 3.26 cfs @ 12.44 hrs, Volume= 1.212 af, Atten= 0%, Lag= 2.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 1.35 fps, Min. Travel Time= 1.2 min
 Avg. Velocity = 0.53 fps, Avg. Travel Time= 3.2 min

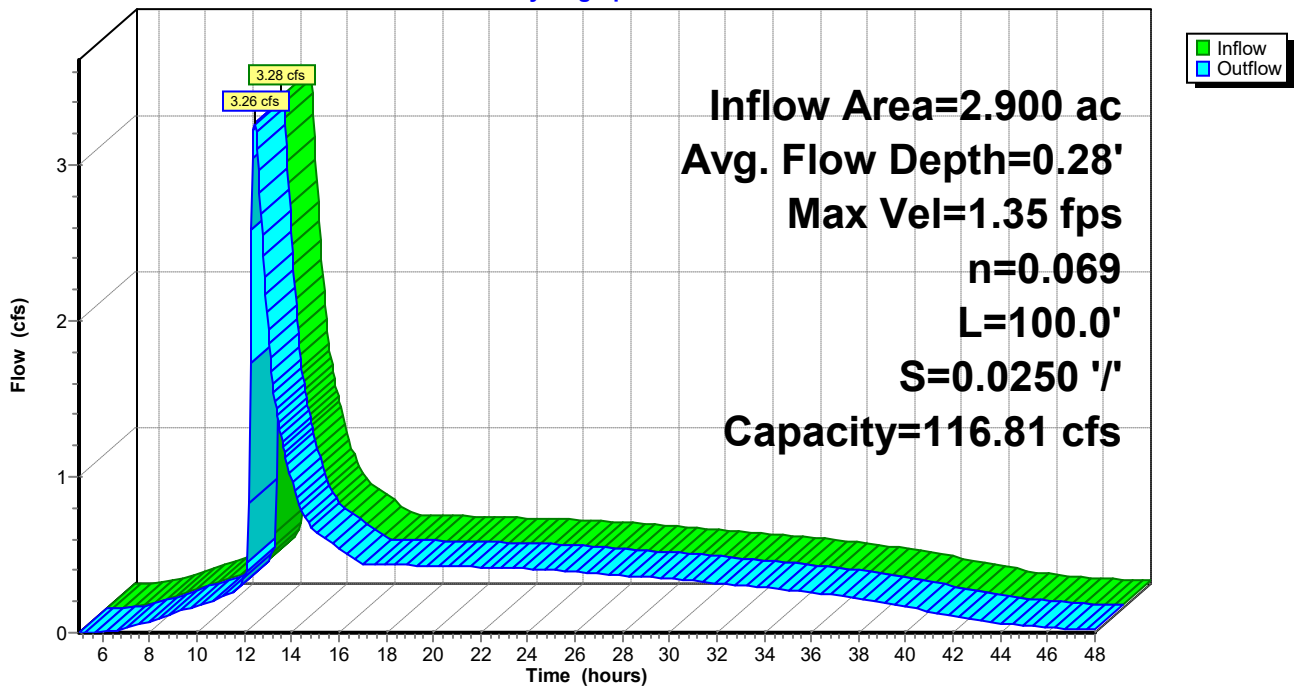
Peak Storage= 243 cf @ 12.42 hrs
 Average Depth at Peak Storage= 0.28' , Surface Width= 9.65'
 Bank-Full Depth= 2.00' Flow Area= 28.0 sf, Capacity= 116.81 cfs

8.00' x 2.00' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 3.0 '/' Top Width= 20.00'
 Length= 100.0' Slope= 0.0250 '/'
 Inlet Invert= 14.50', Outlet Invert= 12.00'



Reach 7R: Overflow

Hydrograph



Summary for Reach 8R: Dry Swale #1

Inflow Area = 1.000 ac, 95.00% Impervious, Inflow Depth > 5.43" for 100-Year event
Inflow = 8.32 cfs @ 11.96 hrs, Volume= 0.453 af
Outflow = 8.17 cfs @ 11.98 hrs, Volume= 0.452 af, Atten= 2%, Lag= 1.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
Max. Velocity= 3.41 fps, Min. Travel Time= 0.5 min
Avg. Velocity = 0.96 fps, Avg. Travel Time= 1.8 min

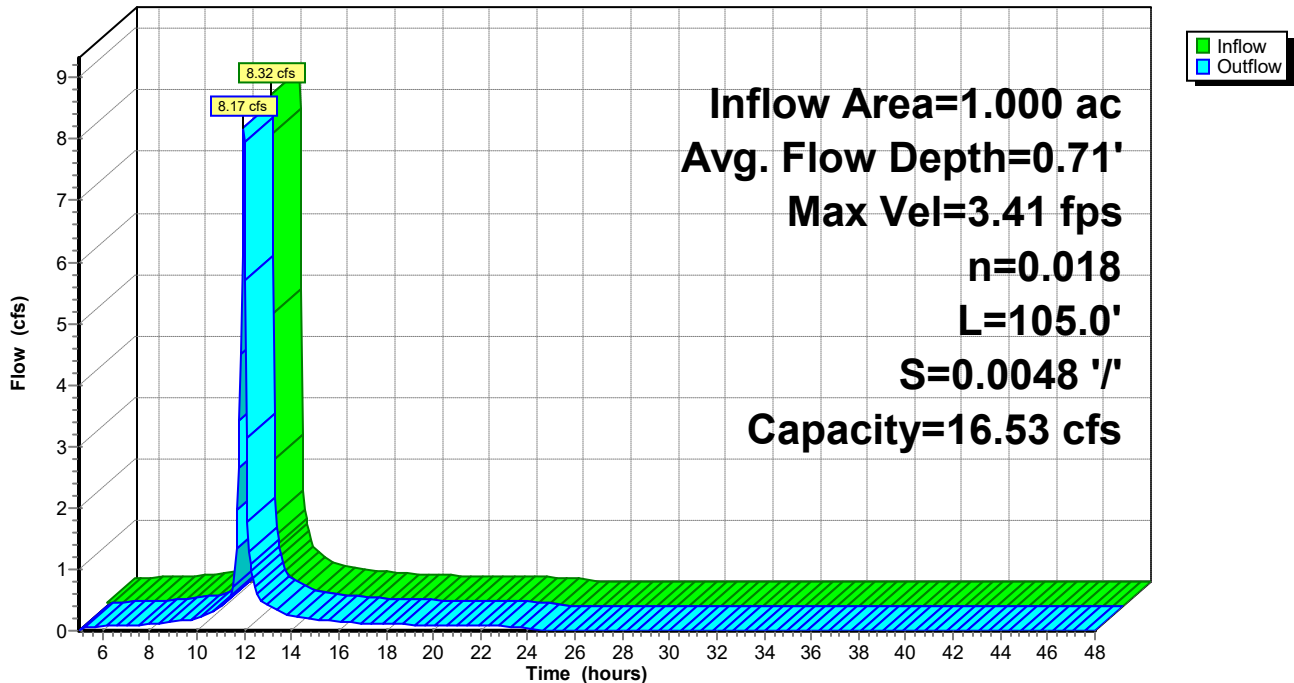
Peak Storage= 252 cf @ 11.97 hrs
Average Depth at Peak Storage= 0.71' , Surface Width= 4.82'
Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 16.53 cfs

2.00' x 1.00' deep channel, n= 0.018 Earth, clean & straight
Side Slope Z-value= 2.0 ' / ' Top Width= 6.00'
Length= 105.0' Slope= 0.0048 ' / '
Inlet Invert= 10.00', Outlet Invert= 9.50'



Reach 8R: Dry Swale #1

Hydrograph



Summary for Reach 10R: Dry Swale #2

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth > 4.51" for 100-Year event
 Inflow = 5.36 cfs @ 12.00 hrs, Volume= 0.286 af
 Outflow = 5.25 cfs @ 12.01 hrs, Volume= 0.286 af, Atten= 2%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 5.03 fps, Min. Travel Time= 0.4 min
 Avg. Velocity = 1.34 fps, Avg. Travel Time= 1.4 min

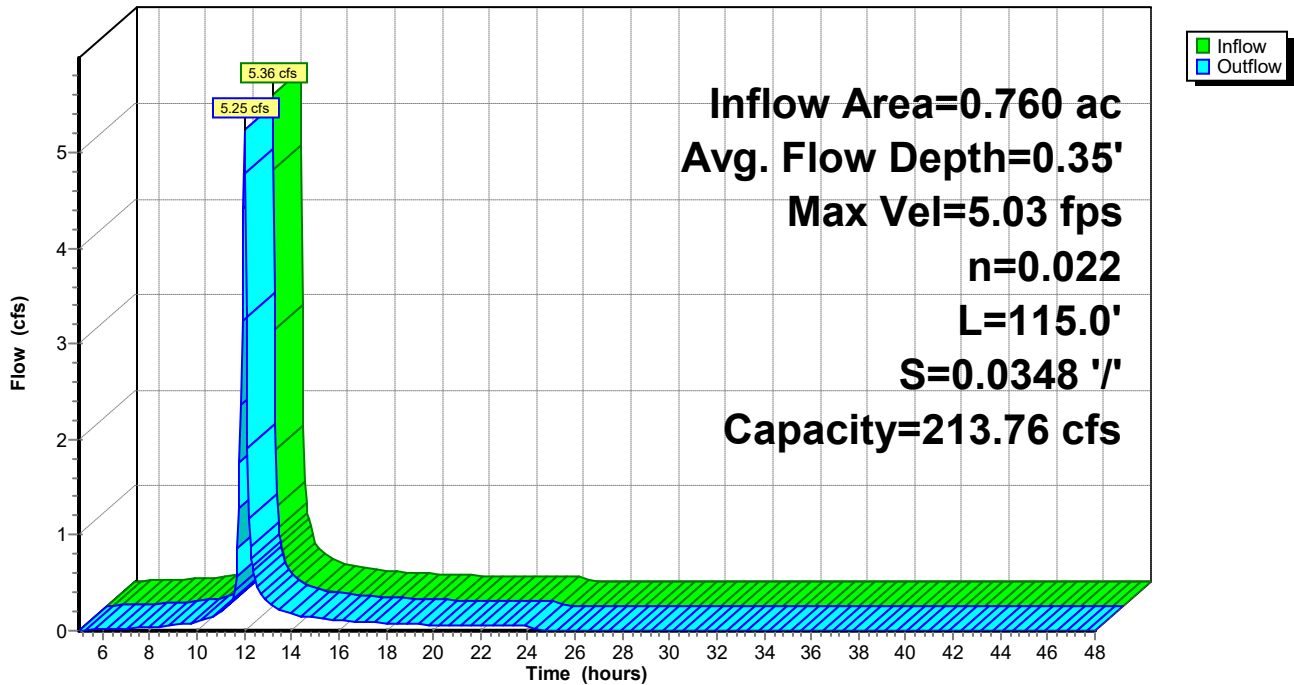
Peak Storage= 122 cf @ 12.00 hrs
 Average Depth at Peak Storage= 0.35' , Surface Width= 4.09'
 Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 213.76 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 '/' Top Width= 14.00'
 Length= 115.0' Slope= 0.0348 '/'
 Inlet Invert= 37.00', Outlet Invert= 33.00'



Reach 10R: Dry Swale #2

Hydrograph



Summary for Reach 12R: Sediment Basin Overflow

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 1.91" for 100-Year event
 Inflow = 4.02 cfs @ 12.04 hrs, Volume= 0.191 af
 Outflow = 3.89 cfs @ 12.04 hrs, Volume= 0.191 af, Atten= 3%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 1.16 fps, Min. Travel Time= 0.1 min
 Avg. Velocity = 0.28 fps, Avg. Travel Time= 0.4 min

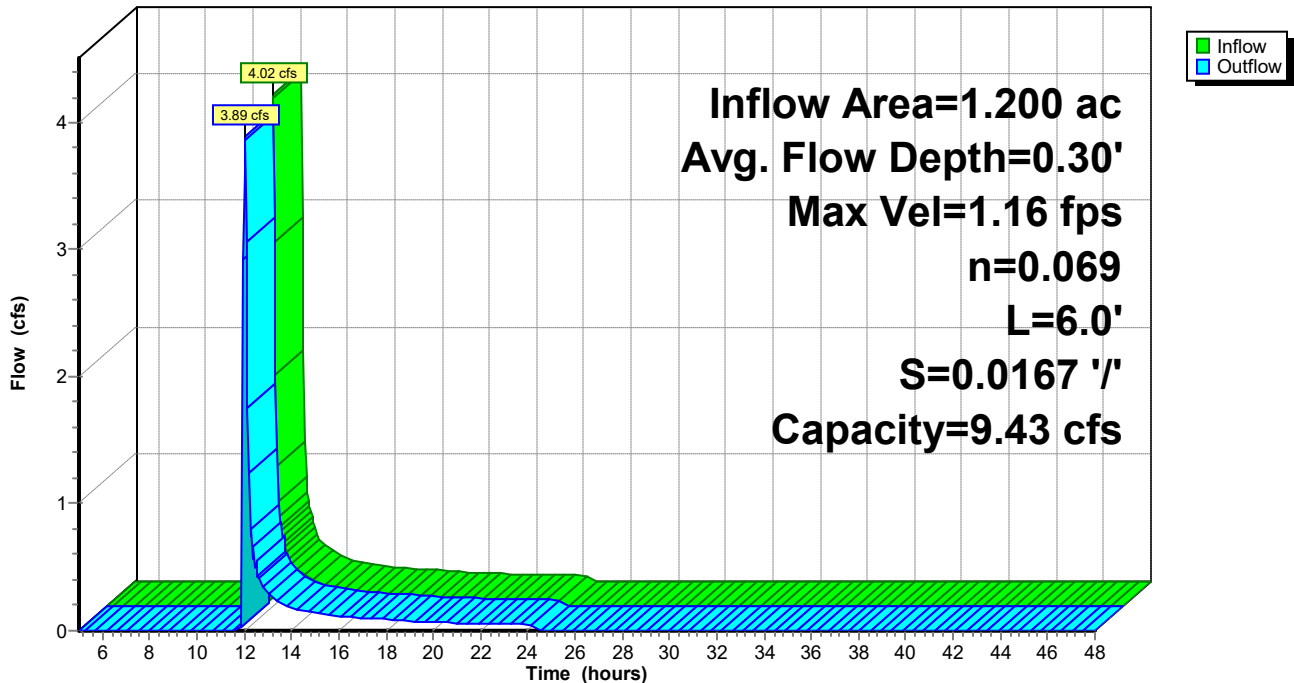
Peak Storage= 20 cf @ 12.04 hrs
 Average Depth at Peak Storage= 0.30', Surface Width= 12.40'
 Bank-Full Depth= 0.50' Flow Area= 6.0 sf, Capacity= 9.43 cfs

10.00' x 0.50' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 4.0 '/' Top Width= 14.00'
 Length= 6.0' Slope= 0.0167 '/'
 Inlet Invert= 12.00', Outlet Invert= 11.90'



Reach 12R: Sediment Basin Overflow

Hydrograph



Summary for Reach 13R: Roadside Swale

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 2.08" for 100-Year event
 Inflow = 4.32 cfs @ 11.98 hrs, Volume= 0.208 af
 Outflow = 3.95 cfs @ 12.02 hrs, Volume= 0.208 af, Atten= 9%, Lag= 2.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 3.15 fps, Min. Travel Time= 1.5 min
 Avg. Velocity = 1.04 fps, Avg. Travel Time= 4.6 min

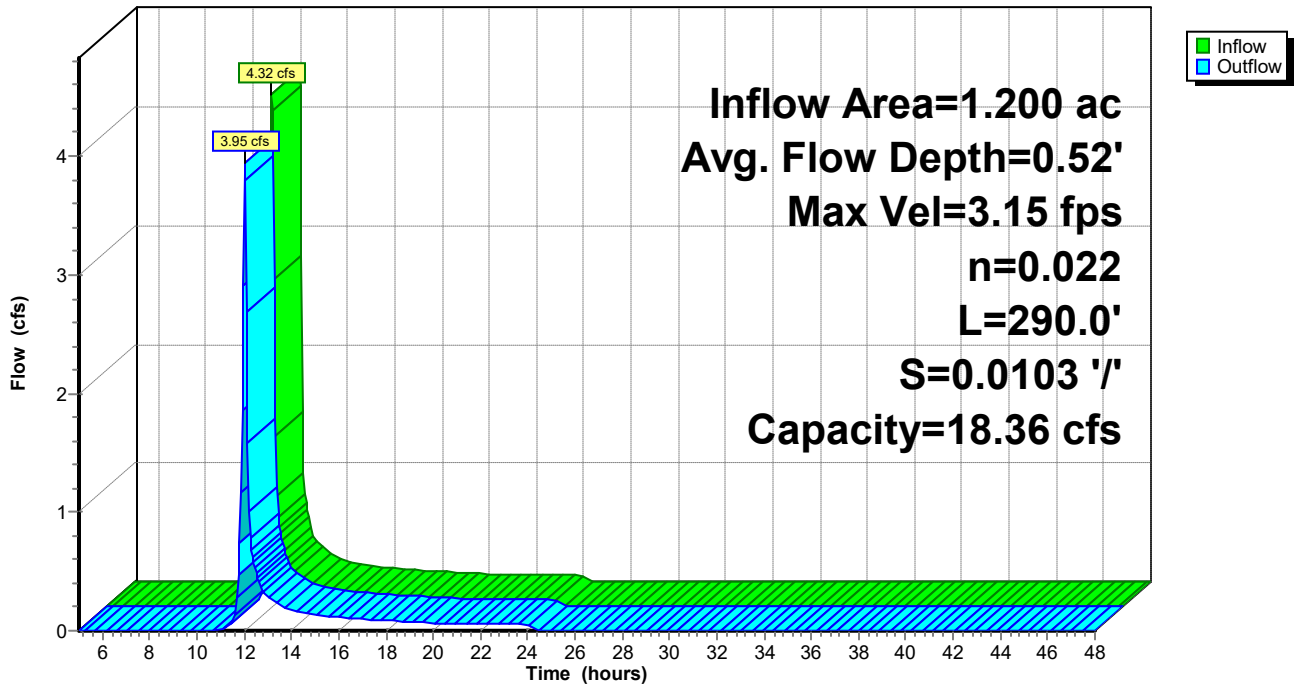
Peak Storage= 386 cf @ 12.00 hrs
 Average Depth at Peak Storage= 0.52' , Surface Width= 4.12'
 Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.36 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 7.00'
 Length= 290.0' Slope= 0.0103 ' / '
 Inlet Invert= 15.00', Outlet Invert= 12.00'



Reach 13R: Roadside Swale

Hydrograph



Summary for Reach 14R: Roadside Swale

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth > 4.51" for 100-Year event
 Inflow = 5.62 cfs @ 11.97 hrs, Volume= 0.286 af
 Outflow = 5.36 cfs @ 12.00 hrs, Volume= 0.286 af, Atten= 5%, Lag= 2.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 6.27 fps, Min. Travel Time= 1.2 min
 Avg. Velocity = 1.65 fps, Avg. Travel Time= 4.6 min

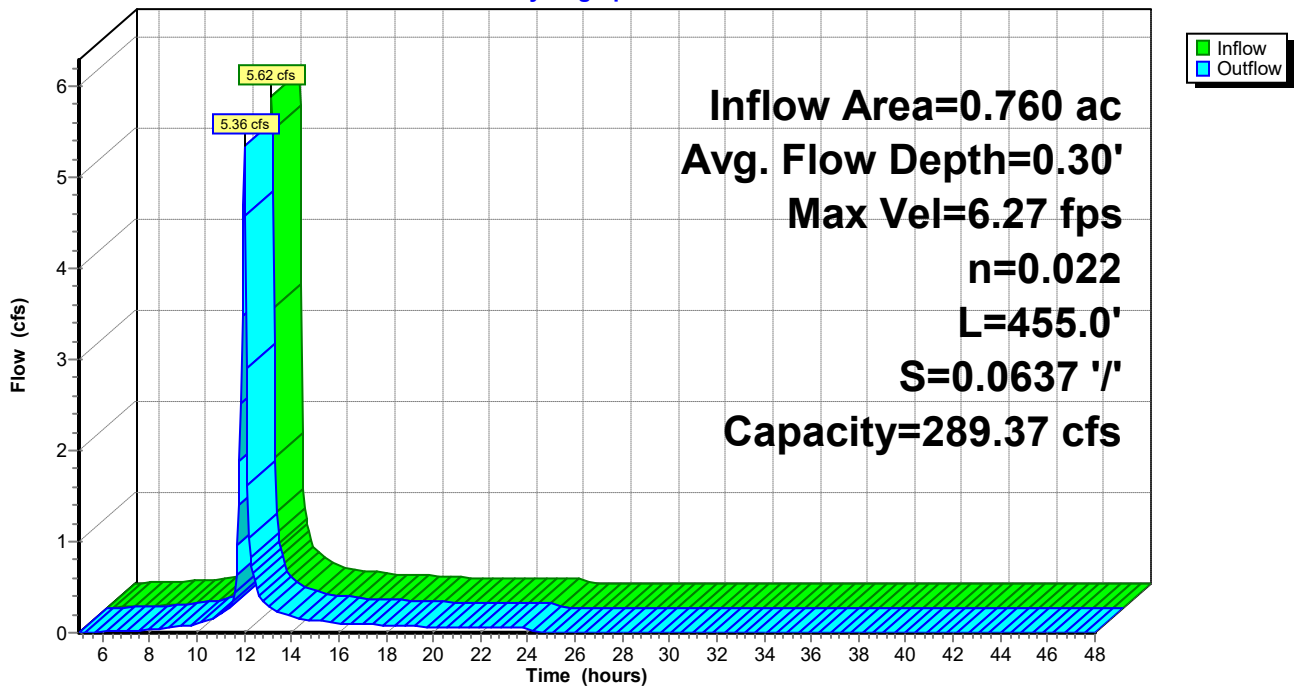
Peak Storage= 402 cf @ 11.98 hrs
 Average Depth at Peak Storage= 0.30' , Surface Width= 3.82'
 Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 289.37 cfs

2.00' x 2.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 '/' Top Width= 14.00'
 Length= 455.0' Slope= 0.0637 '/'
 Inlet Invert= 66.00', Outlet Invert= 37.00'



Reach 14R: Roadside Swale

Hydrograph



Summary for Reach 15R: Roadside Swale

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 3.18" for 100-Year event
 Inflow = 7.10 cfs @ 11.97 hrs, Volume= 0.345 af
 Outflow = 5.76 cfs @ 12.12 hrs, Volume= 0.345 af, Atten= 19%, Lag= 9.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 1.22 fps, Min. Travel Time= 5.9 min
 Avg. Velocity = 0.33 fps, Avg. Travel Time= 22.0 min

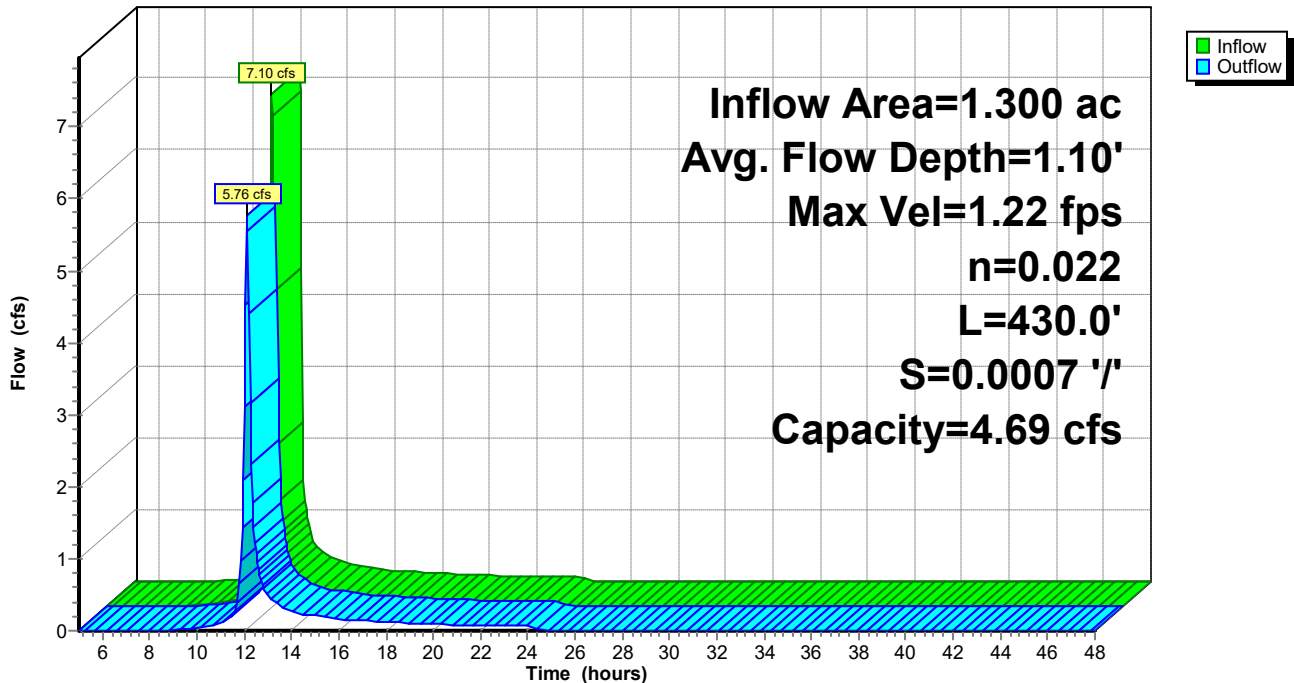
Peak Storage= 2,022 cf @ 12.02 hrs
 Average Depth at Peak Storage= 1.10' , Surface Width= 7.60'
 Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 4.69 cfs

1.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight
 Side Slope Z-value= 3.0 ' / ' Top Width= 7.00'
 Length= 430.0' Slope= 0.0007 ' / '
 Inlet Invert= 10.00', Outlet Invert= 9.71'



Reach 15R: Roadside Swale

Hydrograph



Summary for Reach 17R: Sediment Basin Overflow

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 2.82" for 100-Year event
 Inflow = 5.75 cfs @ 12.13 hrs, Volume= 0.305 af
 Outflow = 5.82 cfs @ 12.14 hrs, Volume= 0.305 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Max. Velocity= 1.19 fps, Min. Travel Time= 0.1 min
 Avg. Velocity = 0.23 fps, Avg. Travel Time= 0.4 min

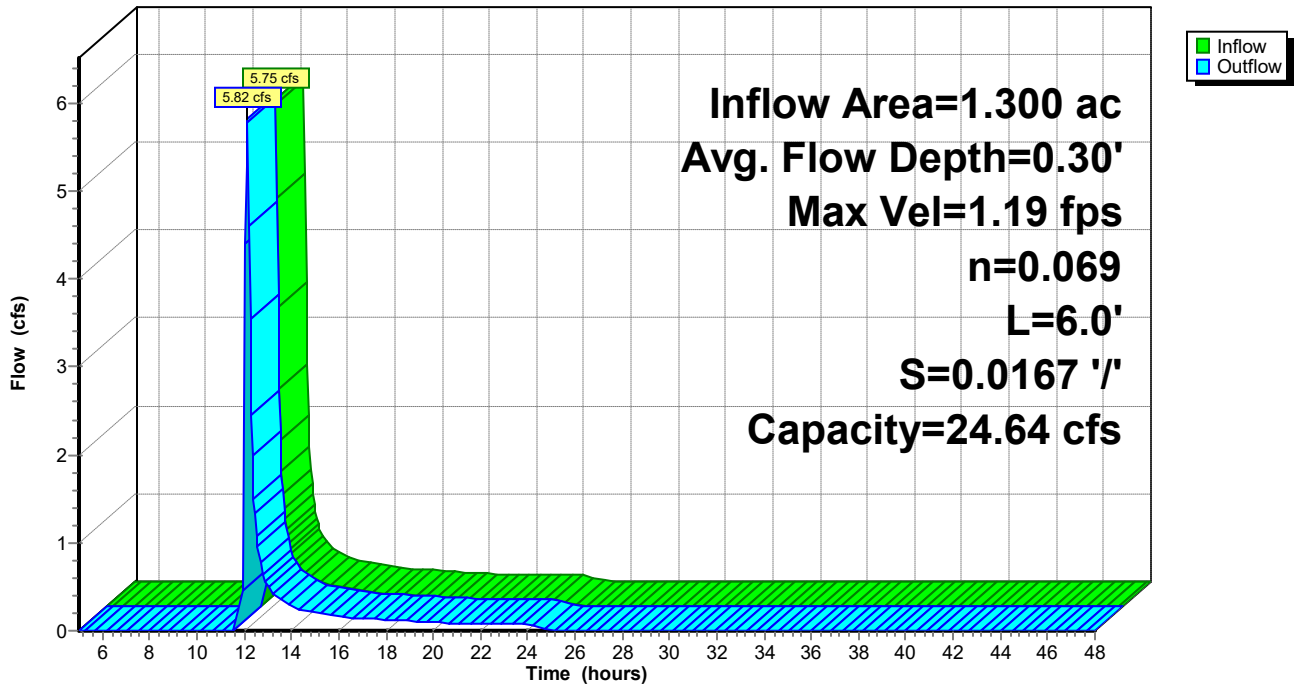
Peak Storage= 29 cf @ 12.14 hrs
 Average Depth at Peak Storage= 0.30' , Surface Width= 17.42'
 Bank-Full Depth= 0.70' Flow Area= 12.5 sf, Capacity= 24.64 cfs

15.00' x 0.70' deep channel, n= 0.069 Riprap, 6-inch
 Side Slope Z-value= 4.0 '/' Top Width= 20.60'
 Length= 6.0' Slope= 0.0167 '/'
 Inlet Invert= 9.00', Outlet Invert= 8.90'



Reach 17R: Sediment Basin Overflow

Hydrograph



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 100-Year Rainfall=6.11"

Prepared by McFarland Johnson

Printed 6/8/2022

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Summary for Pond 1P: WQv Pond #1

Inflow Area = 2.900 ac, 65.52% Impervious, Inflow Depth > 5.08" for 100-Year event
 Inflow = 16.96 cfs @ 12.03 hrs, Volume= 1.227 af
 Outflow = 3.28 cfs @ 12.41 hrs, Volume= 1.212 af, Atten= 81%, Lag= 22.8 min
 Primary = 3.28 cfs @ 12.41 hrs, Volume= 1.212 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Starting Elev= 14.00' Surf.Area= 9,229 sf Storage= 19,003 cf
 Peak Elev= 16.23' @ 12.41 hrs Surf.Area= 21,418 sf Storage= 47,659 cf (28,656 cf above start)

Plug-Flow detention time= 930.0 min calculated for 0.775 af (63% of inflow)
 Center-of-Mass det. time= 522.7 min (1,309.6 - 786.9)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,795 cf	Forebay (Prismatic) Listed below (Recalc)
#2	9.00'	57,882 cf	Permanent Pool (Prismatic) Listed below (Recalc)
		62,677 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	232	0	0
11.00	569	401	401
12.00	1,018	794	1,194
13.00	1,467	1,243	2,437
14.00	3,249	2,358	4,795

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
9.00	1,145	0	0
10.00	1,751	1,448	1,448
11.00	2,339	2,045	3,493
12.00	2,959	2,649	6,142
13.00	3,597	3,278	9,420
14.00	5,980	4,789	14,209
14.50	7,240	3,305	17,514
15.00	14,392	5,408	22,922
16.00	17,455	15,924	38,845
17.00	20,619	19,037	57,882

Device	Routing	Invert	Outlet Devices
#1	Primary	13.50'	12.0" Round Culvert L= 50.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 13.50' / 13.23' S= 0.0054 ' / Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	16.00'	24.0" x 24.0" Horiz. Outlet Structure Top Grate C= 0.600 in 24.0" x 24.0" Grate (100% open area) Limited to weir flow at low heads
#3	Device 1	14.00'	4.0" Round Reverse Slope Pipe L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 9.00' / 14.00' S= -0.1250 ' / Cc= 0.900

18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 100-Year Rainfall=6.11"

Prepared by McFarland Johnson

Printed 6/8/2022

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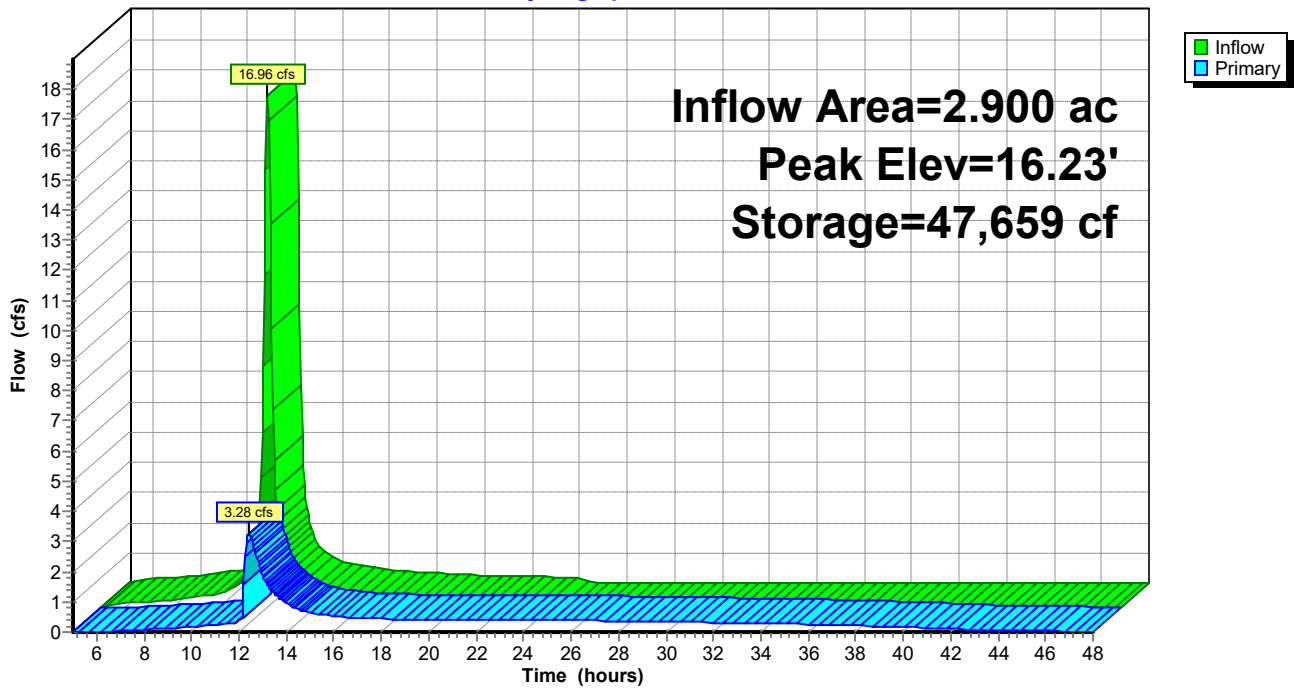
#4	Primary	16.25'	n= 0.010 PVC, smooth interior, Flow Area= 0.09 sf
			6.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Primary OutFlow Max=3.26 cfs @ 12.41 hrs HW=16.23' (Free Discharge)

- 1=Culvert (Passes 3.26 cfs of 5.08 cfs potential flow)
- 2=Outlet Structure Top Grate (Weir Controls 2.80 cfs @ 1.55 fps)
- 3=Reverse Slope Pipe (Outlet Controls 0.46 cfs @ 5.29 fps)
- 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: WQv Pond #1

Hydrograph



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 100-Year Rainfall=6.11"

Prepared by McFarland Johnson

Printed 6/8/2022

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Summary for Pond 2P: WQv Pond #2

Inflow Area = 5.800 ac, 31.90% Impervious, Inflow Depth > 4.80" for 100-Year event
 Inflow = 40.22 cfs @ 11.97 hrs, Volume= 2.320 af
 Outflow = 15.27 cfs @ 12.13 hrs, Volume= 2.307 af, Atten= 62%, Lag= 9.6 min
 Primary = 15.27 cfs @ 12.13 hrs, Volume= 2.307 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Starting Elev= 14.00' Surf.Area= 5,917 sf Storage= 9,000 cf
 Peak Elev= 17.07' @ 12.13 hrs Surf.Area= 27,493 sf Storage= 54,456 cf (45,456 cf above start)

Plug-Flow detention time= 493.6 min calculated for 2.098 af (90% of inflow)
 Center-of-Mass det. time= 393.8 min (1,180.5 - 786.7)

Volume	Invert	Avail.Storage	Storage Description
#1	10.00'	4,020 cf	Forebay #1 (Prismatic) Listed below (Recalc)
#2	10.00'	2,575 cf	Forebay #2 (Prismatic) Listed below (Recalc)
#3	10.00'	58,093 cf	Permanent Pool (Prismatic) Listed below (Recalc)
		64,688 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	141	0	0
11.00	330	236	236
12.00	562	446	682
13.00	866	714	1,396
14.00	2,023	1,445	2,840
14.50	2,696	1,180	4,020

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	82	0	0
11.00	202	142	142
12.00	351	277	419
13.00	535	443	862
14.00	1,323	929	1,791
14.50	1,815	785	2,575

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
10.00	375	0	0
11.00	653	514	514
12.00	957	805	1,319
13.00	1,286	1,122	2,441
14.00	2,571	1,929	4,369
14.50	3,307	1,470	5,839
15.00	13,814	4,280	10,119
16.00	17,852	15,833	25,952
17.00	22,659	20,256	46,207
17.50	24,884	11,886	58,093

18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 100-Year Rainfall=6.11"

Prepared by McFarland Johnson

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Device	Routing	Invert	Outlet Devices
#1	Device 3	16.50'	24.0" x 24.0" Horiz. Orifice/Grate C= 0.600 in 24.0" x 24.0" Grate (100% open area) Limited to weir flow at low heads
#2	Device 3	14.00'	4.0" Vert. Reverse Slope Pipe C= 0.600 Limited to weir flow at low heads
#3	Primary	14.00'	12.0" Round Outlet Structure Discard Pipe L= 46.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 14.00' / 13.77' S= 0.0050 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#4	Primary	16.60'	10.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=15.12 cfs @ 12.13 hrs HW=17.07' (Free Discharge)

3=Outlet Structure Discard Pipe (Barrel Controls 5.57 cfs @ 7.09 fps)

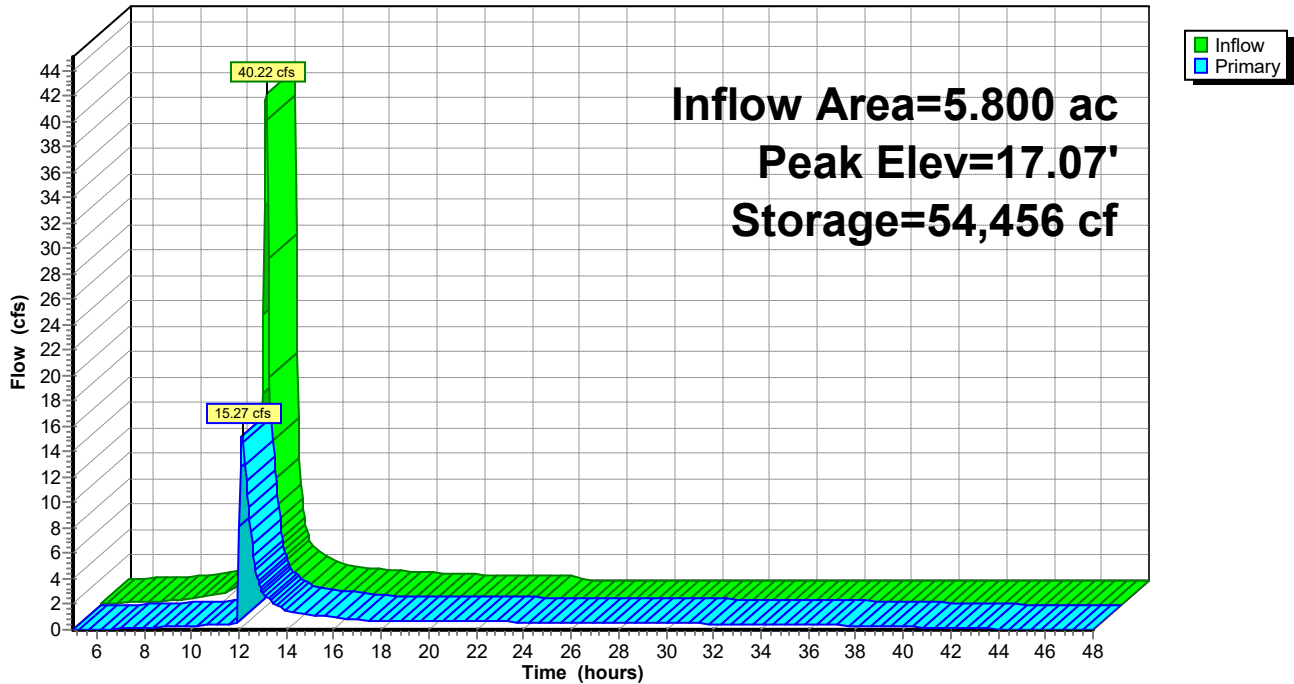
1=Orifice/Grate (Passes < 11.22 cfs potential flow)

2=Reverse Slope Pipe (Passes < 0.72 cfs potential flow)

4=Broad-Crested Rectangular Weir (Weir Controls 9.55 cfs @ 2.04 fps)

Pond 2P: WQv Pond #2

Hydrograph



Summary for Pond 3P: Infiltration Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 1.91" for 100-Year event
 Inflow = 3.89 cfs @ 12.04 hrs, Volume= 0.191 af
 Outflow = 1.88 cfs @ 12.17 hrs, Volume= 0.172 af, Atten= 52%, Lag= 7.9 min
 Discarded = 0.02 cfs @ 12.17 hrs, Volume= 0.048 af
 Primary = 1.86 cfs @ 12.17 hrs, Volume= 0.124 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 11.94' @ 12.17 hrs Surf.Area= 1,383 sf Storage= 2,406 cf

Plug-Flow detention time= 296.0 min calculated for 0.172 af (90% of inflow)
 Center-of-Mass det. time= 245.1 min (1,121.7 - 876.7)

Volume	Invert	Avail.Storage	Storage Description		
#1	8.10'	2,492 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
8.10	109	56.0	0	0	109
12.00	1,415	149.0	2,492	2,492	1,678

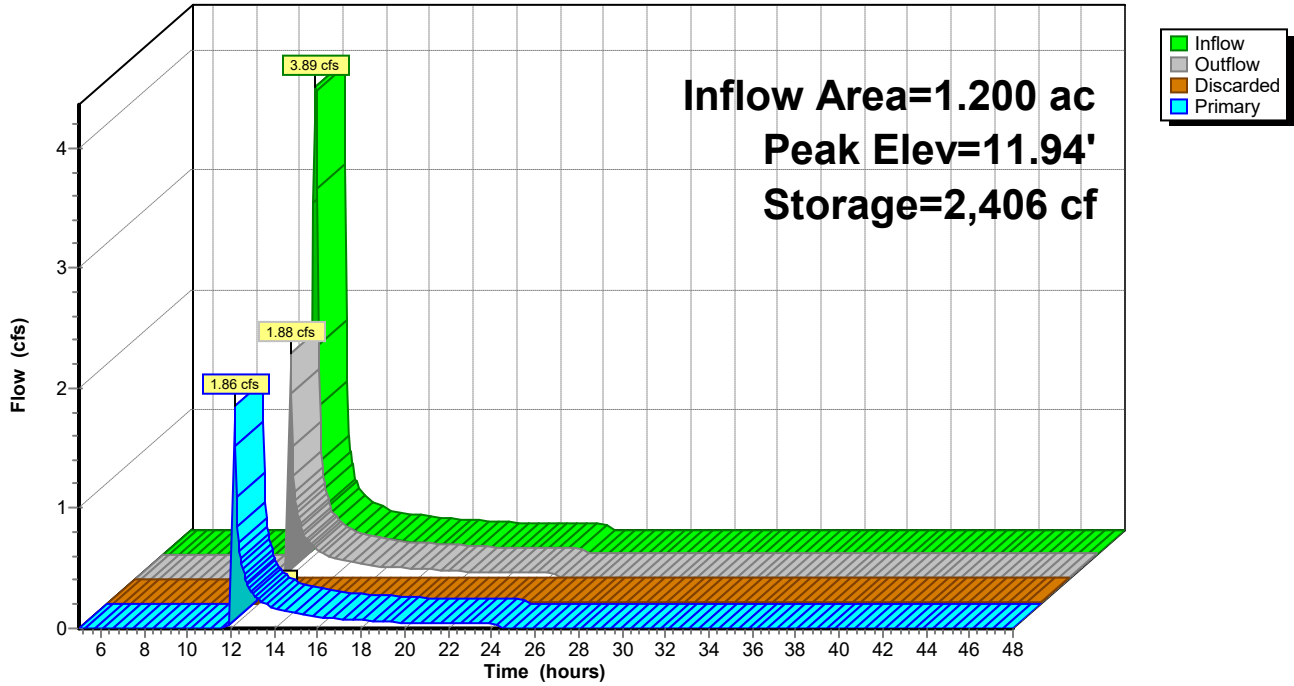
Device	Routing	Invert	Outlet Devices
#1	Primary	11.65'	Channel/Reach using Reach 5R: Overflow
#2	Discarded	8.10'	0.500 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 4.00'

Discarded OutFlow Max=0.02 cfs @ 12.17 hrs HW=11.91' (Free Discharge)
 ↑**2=Exfiltration** (Controls 0.02 cfs)

Primary OutFlow Max=1.65 cfs @ 12.17 hrs HW=11.91' (Free Discharge)
 ↑**1=Channel/Reach** (Channel Controls 1.65 cfs @ 1.64 fps)

Pond 3P: Infiltration Basin #1

Hydrograph



Summary for Pond 4P: Infiltration Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 2.82" for 100-Year event
 Inflow = 5.82 cfs @ 12.14 hrs, Volume= 0.305 af
 Outflow = 6.44 cfs @ 12.16 hrs, Volume= 0.305 af, Atten= 0%, Lag= 1.3 min
 Discarded = 0.42 cfs @ 12.16 hrs, Volume= 0.189 af
 Primary = 6.03 cfs @ 12.16 hrs, Volume= 0.117 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 8.97' @ 12.16 hrs Surf.Area= 1,059 sf Storage= 1,597 cf

Plug-Flow detention time= 29.1 min calculated for 0.305 af (100% of inflow)
 Center-of-Mass det. time= 29.1 min (895.2 - 866.1)

Volume	Invert	Avail.Storage	Storage Description		
#1	5.80'	2,495 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
5.80	110	56.0	0	0	110
9.70	1,415	150.0	2,495	2,495	1,702

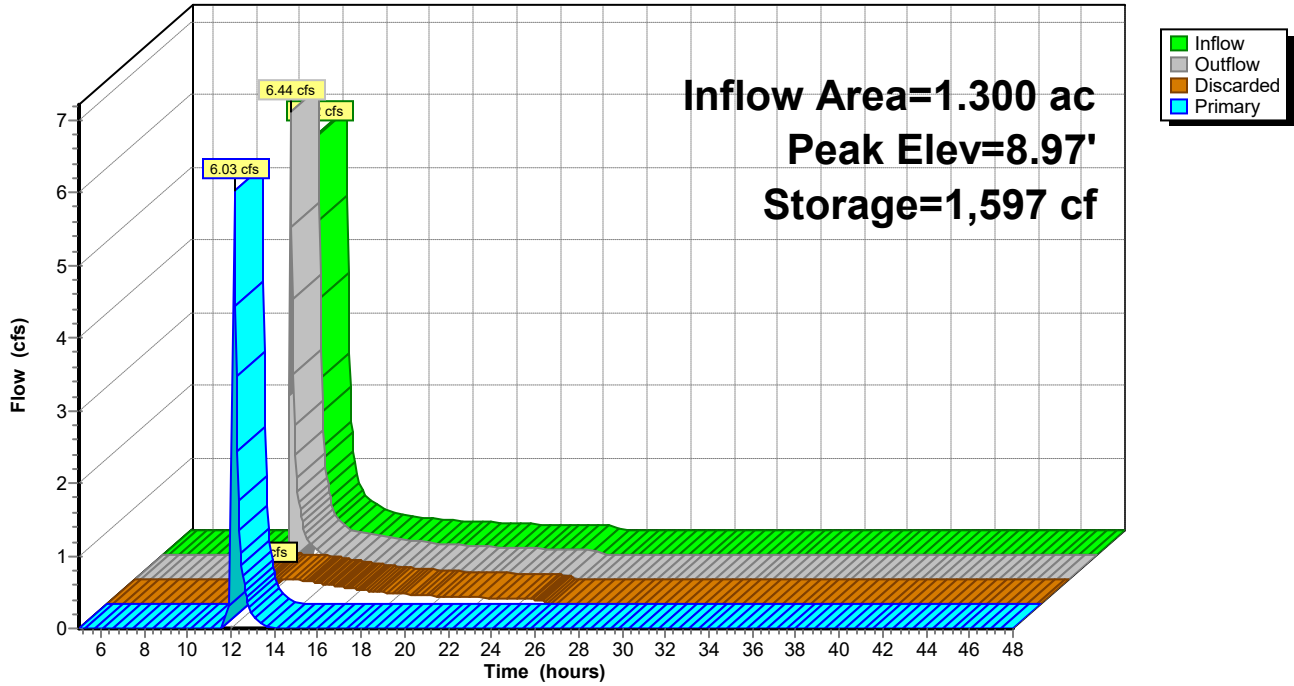
Device	Routing	Invert	Outlet Devices
#1	Primary	8.50'	Channel/Reach using Reach 6R: Overflow
#2	Discarded	5.80'	12.000 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 3.00'

Discarded OutFlow Max=0.41 cfs @ 12.16 hrs HW=8.95' (Free Discharge)
 ↑**2=Exfiltration** (Controls 0.41 cfs)

Primary OutFlow Max=5.55 cfs @ 12.16 hrs HW=8.95' (Free Discharge)
 ↑**1=Channel/Reach** (Channel Controls 5.55 cfs @ 2.85 fps)

Pond 4P: Infiltration Basin #2

Hydrograph



Summary for Pond 5P: Sedimentation Basin #1

Inflow Area = 1.200 ac, 37.50% Impervious, Inflow Depth = 2.08" for 100-Year event
 Inflow = 3.95 cfs @ 12.02 hrs, Volume= 0.208 af
 Outflow = 4.02 cfs @ 12.04 hrs, Volume= 0.191 af, Atten= 0%, Lag= 1.1 min
 Primary = 4.02 cfs @ 12.04 hrs, Volume= 0.191 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 12.31' @ 12.04 hrs Surf.Area= 632 sf Storage= 930 cf

Plug-Flow detention time= 59.3 min calculated for 0.191 af (92% of inflow)
 Center-of-Mass det. time= 15.9 min (876.3 - 860.4)

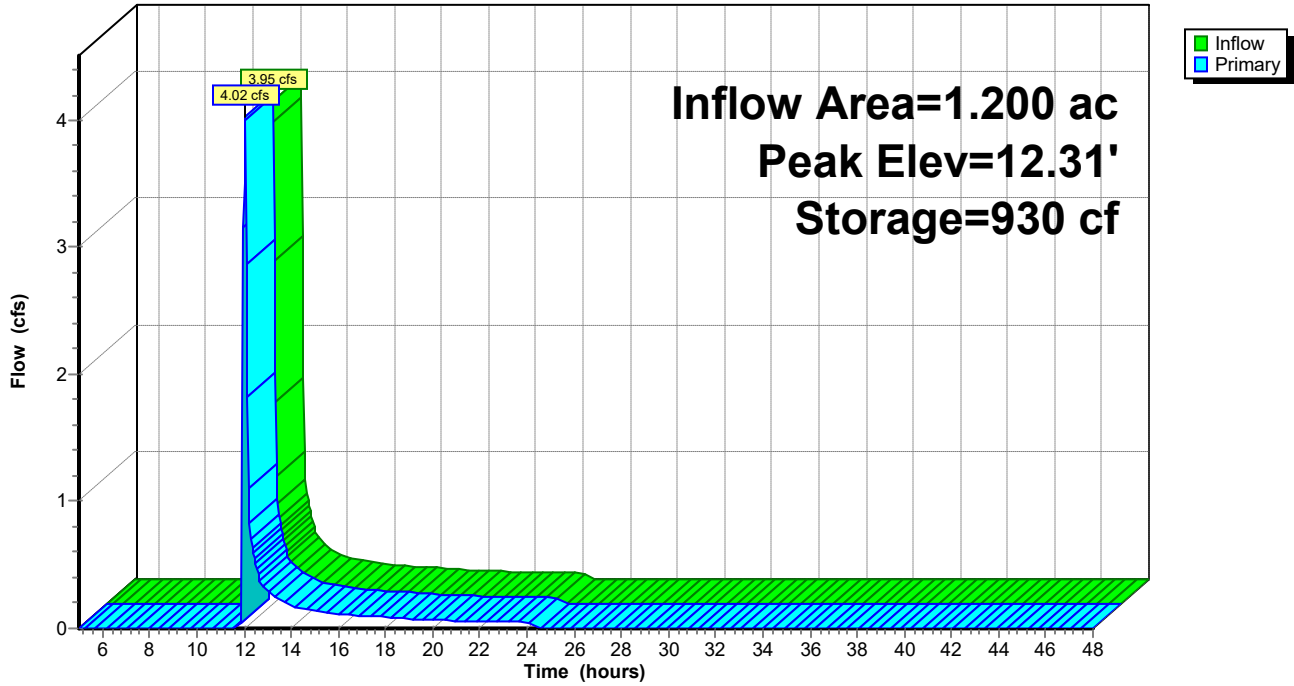
Volume	Invert	Avail.Storage	Storage Description		
#1	9.00'	1,058 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
9.00	41	25.8	0	0	41
10.00	150	46.7	90	90	167
11.00	320	66.6	230	320	355
12.00	550	86.4	430	749	608
12.50	687	96.2	309	1,058	758

Device	Routing	Invert	Outlet Devices
#1	Primary	12.00'	Channel/Reach using Reach 12R: Sediment Basin Overflow

Primary OutFlow Max=3.89 cfs @ 12.04 hrs HW=12.30' (Free Discharge)
 ↑1=Channel/Reach (Channel Controls 3.89 cfs @ 1.16 fps)

Pond 5P: Sedimentation Basin #1

Hydrograph



Summary for Pond 16P: Sedimentation Basin #2

Inflow Area = 1.300 ac, 57.69% Impervious, Inflow Depth = 3.18" for 100-Year event
 Inflow = 5.76 cfs @ 12.12 hrs, Volume= 0.345 af
 Outflow = 5.75 cfs @ 12.13 hrs, Volume= 0.305 af, Atten= 0%, Lag= 0.8 min
 Primary = 5.75 cfs @ 12.13 hrs, Volume= 0.305 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 9.30' @ 12.13 hrs Surf.Area= 970 sf Storage= 1,979 cf

Plug-Flow detention time= 79.9 min calculated for 0.305 af (89% of inflow)
 Center-of-Mass det. time= 21.8 min (865.8 - 843.9)

Volume	Invert	Avail.Storage	Storage Description		
#1	5.80'	2,389 cf	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
5.80	224	80.0	0	0	224
6.00	257	83.0	48	48	266
7.00	438	98.0	344	392	500
8.00	650	113.0	541	932	773
9.00	892	128.0	768	1,700	1,085
9.70	1,079	139.0	689	2,389	1,337

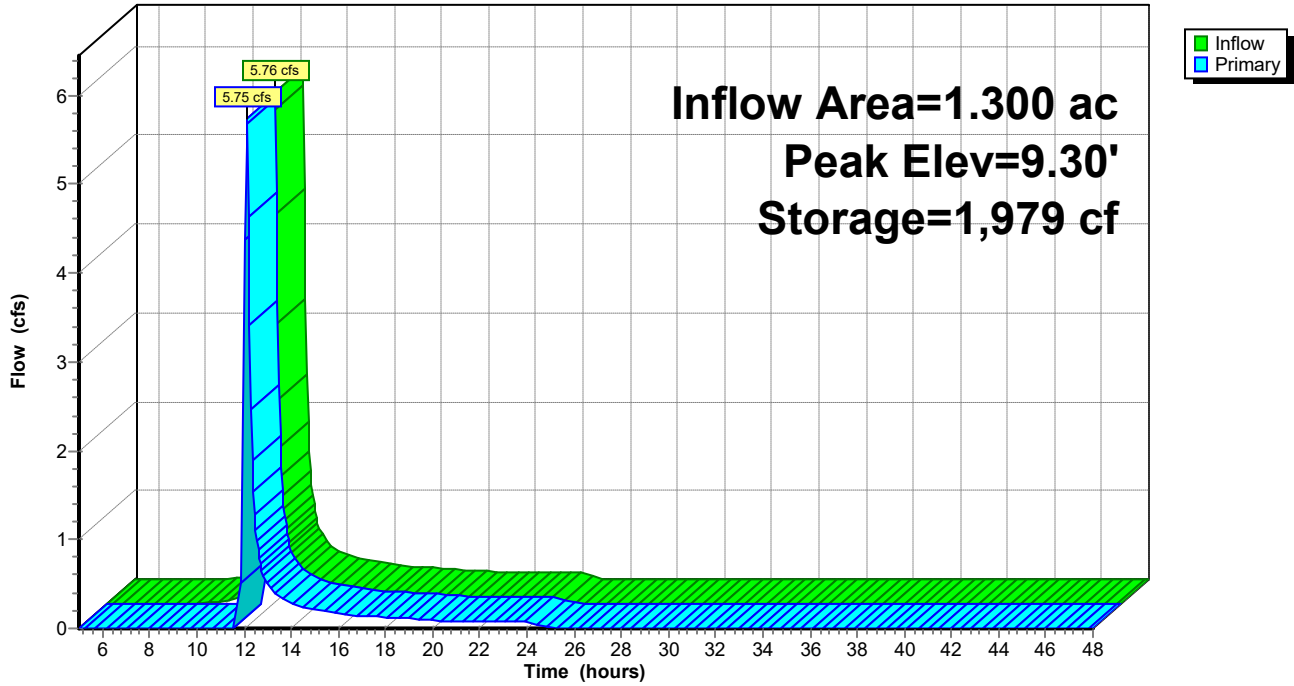
Device	Routing	Invert	Outlet Devices
#1	Primary	9.00'	Channel/Reach using Reach 17R: Sediment Basin Overflow

Primary OutFlow Max=5.60 cfs @ 12.13 hrs HW=9.30' (Free Discharge)

↑**1=Channel/Reach** (Channel Controls 5.60 cfs @ 1.17 fps)

Pond 16P: Sedimentation Basin #2

Hydrograph



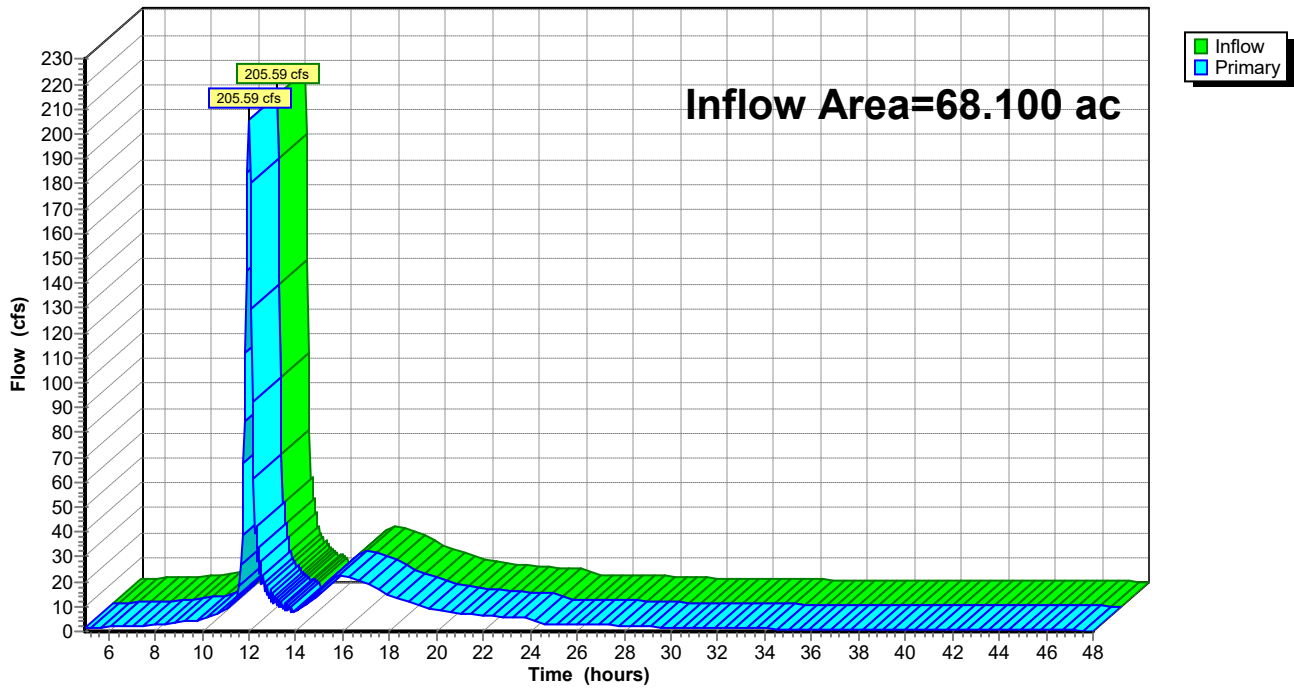
Summary for Pond AP-1: Analysis Point #1

Inflow Area = 68.100 ac, 20.36% Impervious, Inflow Depth > 3.95" for 100-Year event
Inflow = 205.59 cfs @ 12.00 hrs, Volume= 22.396 af
Primary = 205.59 cfs @ 12.00 hrs, Volume= 22.396 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-1: Analysis Point #1

Hydrograph



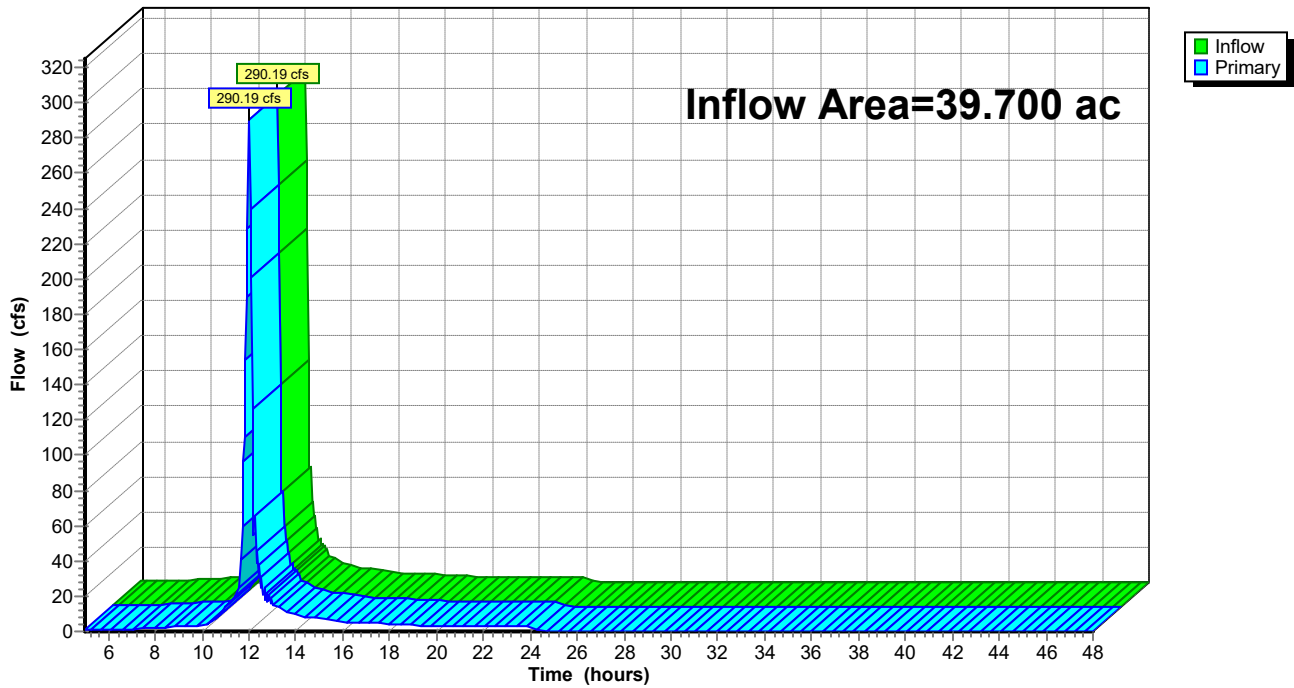
Summary for Pond AP-2: Analysis Point #2

Inflow Area = 39.700 ac, 23.10% Impervious, Inflow Depth > 4.88" for 100-Year event
Inflow = 290.19 cfs @ 12.00 hrs, Volume= 16.144 af
Primary = 290.19 cfs @ 12.00 hrs, Volume= 16.144 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-2: Analysis Point #2

Hydrograph



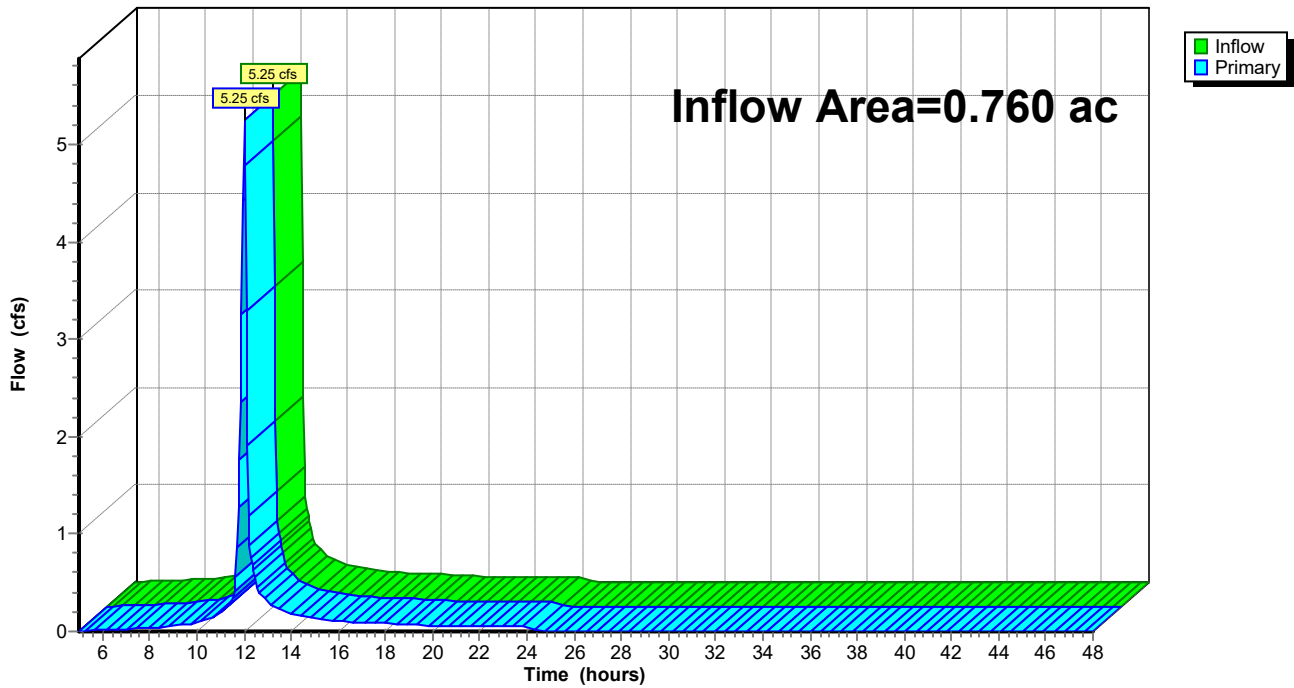
Summary for Pond AP-3: Analysis Point #3

Inflow Area = 0.760 ac, 78.95% Impervious, Inflow Depth > 4.51" for 100-Year event
Inflow = 5.25 cfs @ 12.01 hrs, Volume= 0.286 af
Primary = 5.25 cfs @ 12.01 hrs, Volume= 0.286 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs

Pond AP-3: Analysis Point #3

Hydrograph



18641.00-Proposed Condition_Chambers_CULVERTS Type II 24-hr 100-Year Rainfall=6.11"

Prepared by McFarland Johnson

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Summary for Pond C-1: Chamber Series 1

Inflow Area = 10.300 ac, 66.70% Impervious, Inflow Depth > 5.60" for 100-Year event
 Inflow = 84.97 cfs @ 11.98 hrs, Volume= 4.805 af
 Outflow = 95.05 cfs @ 12.00 hrs, Volume= 4.444 af, Atten= 0%, Lag= 1.4 min
 Discarded = 0.29 cfs @ 12.00 hrs, Volume= 0.351 af
 Primary = 60.22 cfs @ 12.00 hrs, Volume= 3.951 af
 Secondary = 34.55 cfs @ 12.00 hrs, Volume= 0.143 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 14.63' @ 12.00 hrs Surf.Area= 24,954 sf Storage= 35,013 cf

Plug-Flow detention time= 141.1 min calculated for 4.438 af (92% of inflow)
 Center-of-Mass det. time= 101.1 min (864.7 - 763.5)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	11,722 cf	37.08'W x 227.97'L x 5.50'H Field B 46,496 cf Overall - 17,192 cf Embedded = 29,305 cf x 40.0% Voids
#2B	6.75'	17,192 cf	ADS_StormTech MC-3500 d +Cap x 155 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 155 Chambers in 5 Rows Cap Storage= +14.9 cf x 2 x 5 rows = 149.0 cf
#3	13.25'	6,100 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		35,013 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
13.25	600	0	0
13.75	4,900	1,375	1,375
14.00	8,200	1,638	3,013
14.25	16,500	3,088	6,100

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	10.00'	36.0" Round Culvert L= 55.9' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 10.00' / 7.59' S= 0.0431 ' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	14.24'	50.0' long x 0.7' breadth Concrete Curb Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 Coef. (English) 2.76 2.82 2.93 3.09 3.18 3.22 3.27 3.30 3.32 3.31 3.32

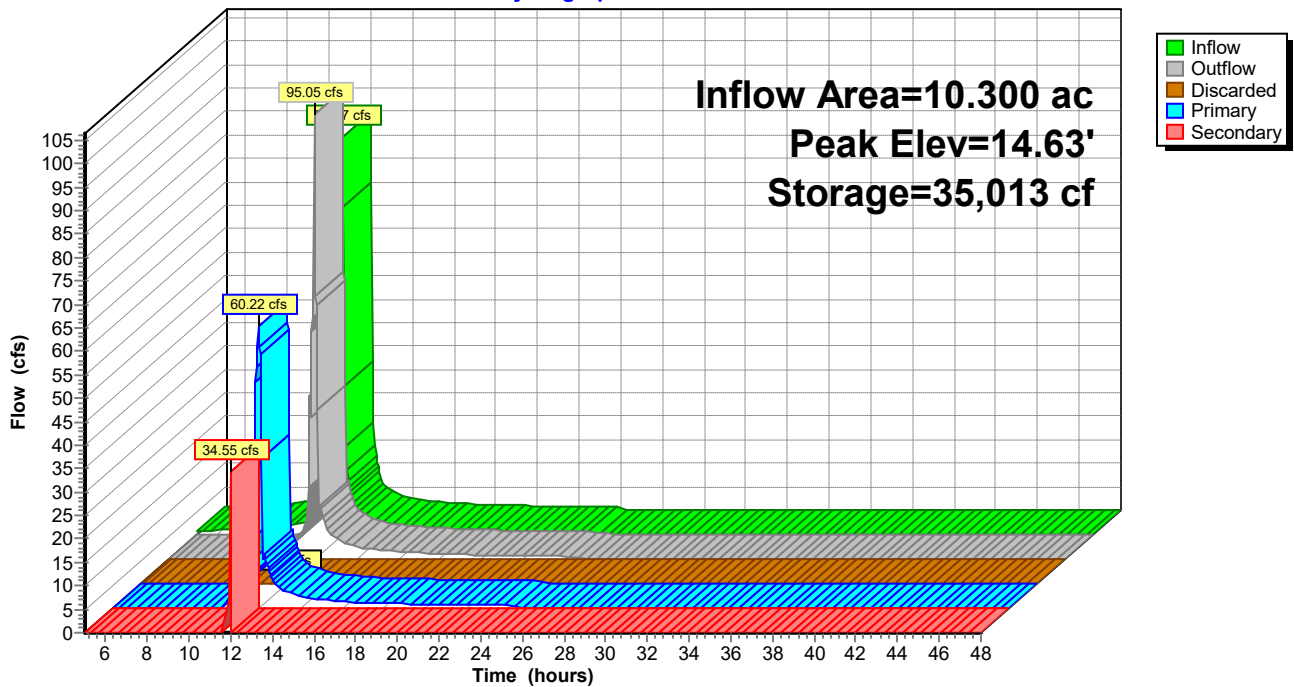
Discarded OutFlow Max=0.29 cfs @ 12.00 hrs HW=14.61' (Free Discharge)
 ↳1=Exfiltration (Exfiltration Controls 0.29 cfs)

Primary OutFlow Max=60.19 cfs @ 12.00 hrs HW=14.63' (Free Discharge)
 ↳2=Culvert (Inlet Controls 60.19 cfs @ 8.52 fps)

Secondary OutFlow Max=34.34 cfs @ 12.00 hrs HW=14.63' (Free Discharge)
 ↳3=Concrete Curb (Weir Controls 34.34 cfs @ 1.76 fps)

Pond C-1: Chamber Series 1

Hydrograph



Summary for Pond C-4: Chamber Series 4

Inflow Area = 8.900 ac, 0.00% Impervious, Inflow Depth > 5.34" for 100-Year event
 Inflow = 69.96 cfs @ 11.99 hrs, Volume= 3.959 af
 Outflow = 56.32 cfs @ 12.04 hrs, Volume= 3.628 af, Atten= 20%, Lag= 3.3 min
 Discarded = 0.19 cfs @ 12.03 hrs, Volume= 0.264 af
 Primary = 56.13 cfs @ 12.04 hrs, Volume= 3.364 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 15.22' @ 12.04 hrs Surf.Area= 16,391 sf Storage= 26,993 cf

Plug-Flow detention time= 137.4 min calculated for 3.627 af (92% of inflow)
 Center-of-Mass det. time= 92.3 min (865.1 - 772.9)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	8,911 cf	29.92'W x 213.63'L x 5.50'H Field B 35,151 cf Overall - 12,874 cf Embedded = 22,277 cf x 40.0% Voids
#2B	6.75'	12,874 cf	ADS_StormTech MC-3500 d +Cap x 116 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 116 Chambers in 4 Rows Cap Storage= +14.9 cf x 2 x 4 rows = 119.2 cf
#3	14.10'	8,015 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		29,800 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
14.10	400	0	0
14.60	2,400	700	700
14.80	6,300	870	1,570
15.10	10,000	2,445	4,015
15.50	10,000	4,000	8,015

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	0.500 in/hr Exfiltration over Surface area
#2	Primary	11.00'	36.0" Round Culvert L= 24.3' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 11.00' / 9.42' S= 0.0650 ' / ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

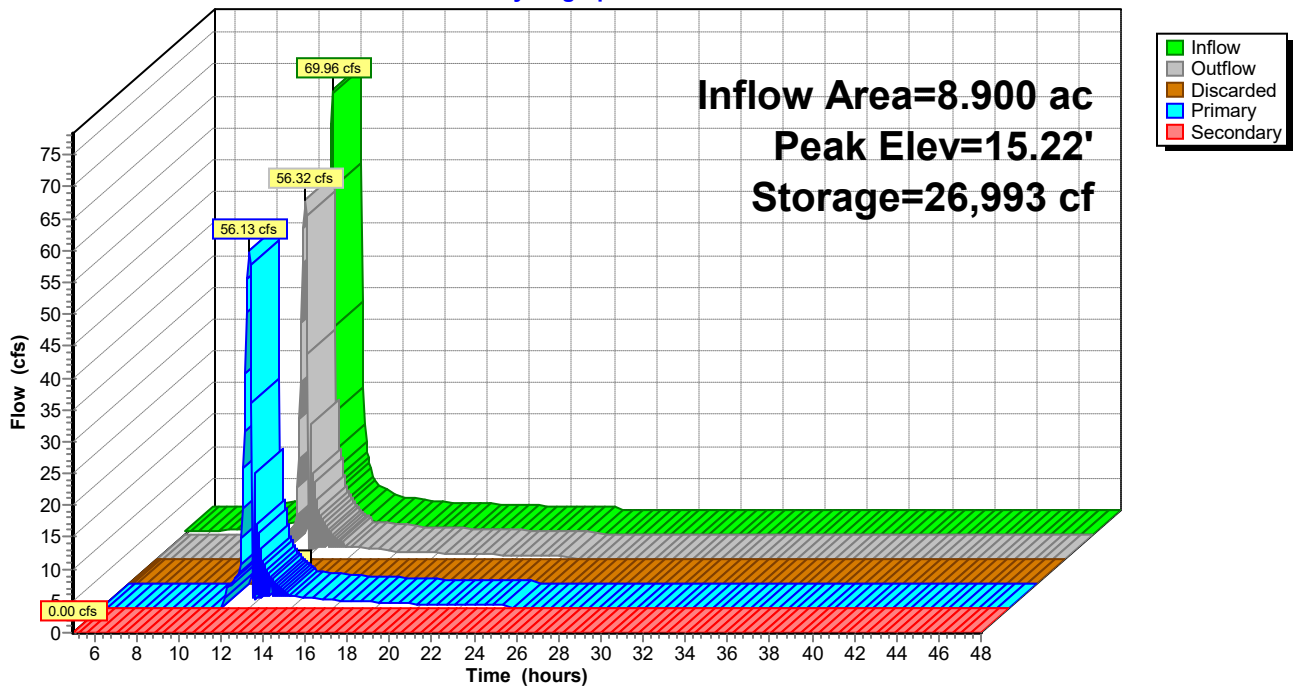
Discarded OutFlow Max=0.19 cfs @ 12.03 hrs HW=15.16' (Free Discharge)
↑1=Exfiltration (Exfiltration Controls 0.19 cfs)

Primary OutFlow Max=55.90 cfs @ 12.04 hrs HW=15.20' (Free Discharge)
↑2=Culvert (Inlet Controls 55.90 cfs @ 7.91 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.01' (Free Discharge)
↑3=Wharf (Controls 0.00 cfs)

Pond C-4: Chamber Series 4

Hydrograph



Summary for Pond C-5: Chamber Series 5

Inflow Area = 5.200 ac, 0.00% Impervious, Inflow Depth > 5.34" for 100-Year event
 Inflow = 41.34 cfs @ 11.98 hrs, Volume= 2.313 af
 Outflow = 30.89 cfs @ 12.05 hrs, Volume= 2.057 af, Atten= 25%, Lag= 3.9 min
 Discarded = 0.42 cfs @ 12.05 hrs, Volume= 0.401 af
 Primary = 30.47 cfs @ 12.05 hrs, Volume= 1.656 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-48.00 hrs, dt= 0.05 hrs
 Peak Elev= 15.35' @ 12.05 hrs Surf.Area= 18,202 sf Storage= 26,138 cf

Plug-Flow detention time= 242.1 min calculated for 2.054 af (89% of inflow)
 Center-of-Mass det. time= 188.6 min (961.1 - 772.5)

Volume	Invert	Avail.Storage	Storage Description
#1B	6.00'	7,757 cf	28.50'W x 168.47'L x 6.75'H Field B 32,409 cf Overall - 13,016 cf Embedded = 19,393 cf x 40.0% Voids
#2B	6.75'	13,016 cf	ADS_StormTech MC-4500 b +Cap x 120 Inside #1 Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap 120 Chambers in 3 Rows Cap Storage= +39.5 cf x 2 x 3 rows = 237.0 cf
#3	14.60'	7,420 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		28,193 cf	Total Available Storage

Storage Group B created with Chamber Wizard

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
14.60	200	0	0
14.80	1,000	120	120
15.00	10,000	1,100	1,220
15.50	14,800	6,200	7,420

Device	Routing	Invert	Outlet Devices
#1	Discarded	6.00'	1.000 in/hr Exfiltration over Surface area
#2	Primary	12.60'	36.0" Round Culvert L= 62.8' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 12.60' / 12.29' S= 0.0049 ' / Cc= 0.900 n= 0.013 Cast iron, coated, Flow Area= 7.07 sf
#3	Secondary	15.50'	100.0' long x 0.5' breadth Wharf Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

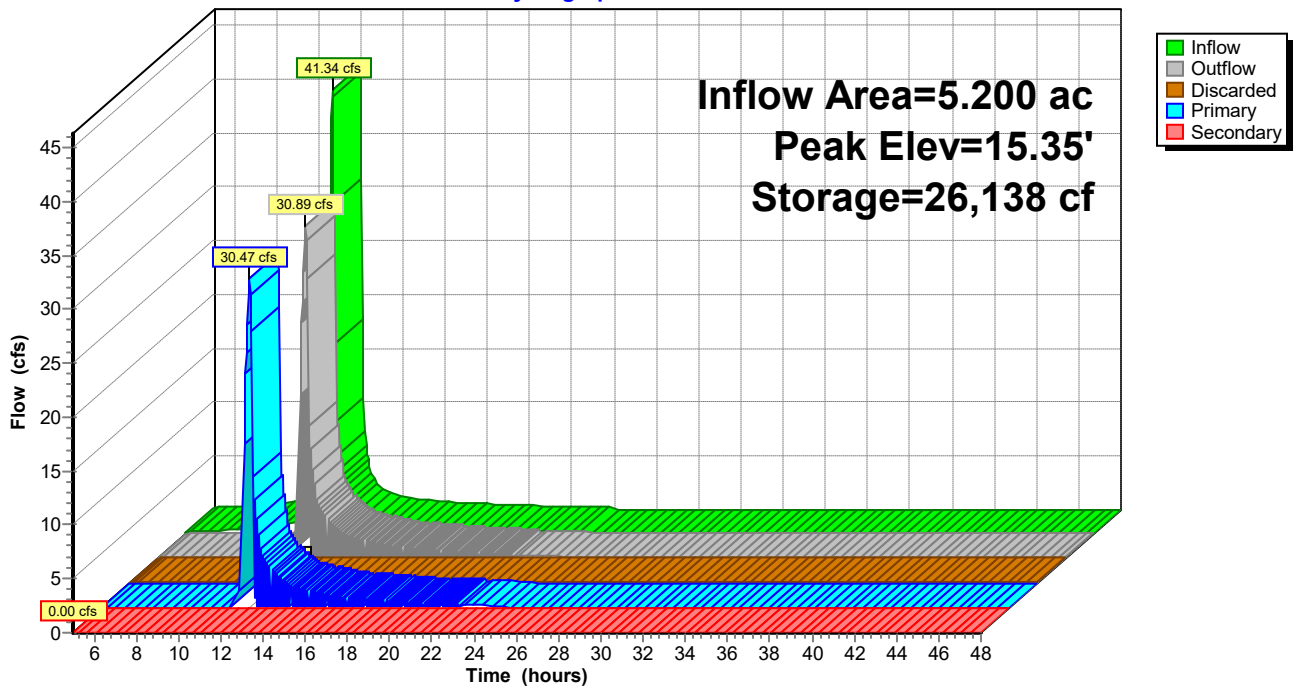
Discarded OutFlow Max=0.42 cfs @ 12.05 hrs HW=15.35' (Free Discharge)
 ↳1=Exfiltration (Exfiltration Controls 0.42 cfs)

Primary OutFlow Max=30.43 cfs @ 12.05 hrs HW=15.35' (Free Discharge)
 ↳2=Culvert (Barrel Controls 30.43 cfs @ 5.87 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=6.01' (Free Discharge)
 ↳3=Wharf (Controls 0.00 cfs)

Pond C-5: Chamber Series 5

Hydrograph



Appendix C

Water Quality and Runoff Reduction Volume Calculations

Is this project subject to Chapter 10 of the NYS Design Manual (i.e. WQv is equal to post-development 1 year runoff volume)?..... No

Design Point: _____
 P= 1.20 inch *Manually enter P, Total Area and Impervious Cover.*

Breakdown of Subcatchments						
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Description
1	10.30	10.20	99%	0.94	42,055	
2	5.50	5.30	96%	0.92	21,884	
3	11.00	10.60	96%	0.92	43,769	
4	8.90	8.60	97%	0.92	35,505	
5	5.20	4.90	94%	0.90	20,258	
6	11.80	11.60	98%	0.93	47,846	
7	8.70	8.40	97%	0.92	34,681	
8	2.90	2.00	69%	0.67	8,437	
9	5.80	3.10	53%	0.53	13,361	
10	0.00	0.00				
Subtotal (1-30)	76.70	65.89	86%	0.82	273,874	Subtotal 1
Total	76.70	65.89	86%	0.82	273,874	Initial WQv

Identify Runoff Reduction Techniques By Area			
Technique	Total Contributing Area	Contributing Impervious Area	Notes
	(Acre)	(Acre)	
Conservation of Natural Areas	4.00	0.00	<i>minimum 10,000 sf</i>
Riparian Buffers	0.00	0.00	<i>maximum contributing length 75 feet to 150 feet</i>
Filter Strips	0.00	0.00	
Tree Planting	0.00	0.00	<i>Up to 100 sf directly connected impervious area may be subtracted per tree</i>
Total	4.00	0.00	

Recalculate WQv after application of Area Reduction Techniques					
	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Runoff Coefficient Rv	WQv (ft ³)
"<<Initial WQv"	76.70	65.89	86%	0.82	273,874
Subtract Area	-4.00	0.00			
WQv adjusted after Area Reductions	72.70	65.89	91%	0.87	273,007
Disconnection of Rooftops		0.00			
Adjusted WQv after Area Reduction and Rooftop Disconnect	72.70	65.89	91%	0.87	273,007
WQv reduced by Area Reduction techniques					868

Total Water Quality Volume Calculation

$$WQv(\text{acre-feet}) = [(P)(Rv)(A)] / 12$$

Additional Subcatchments						
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Description
11	4.00	0.00	0%	0.05	868	Conservation of Natural Areas
12	0.00	0.00				
13	1.10	0.45	41%	0.42	1,995	Infiltration Basin
14	1.10	0.55	50%	0.50	2,386	Infiltration Basin
15	0.10	0.05	50%	0.50	217	Dry Swale
16	0.00	0.00				
17	0.30	0.14	47%	0.47	612	Dry Swale
18						
19						
20						
21						
22						
23						
24						
25						
26						
27						
28						
29						
30						
Subtotal	6.60	1.19	18%	0.21	6,077	Subtotal

Total Water Quality Volume Calculation

$$WQv(\text{acre-feet}) = [(P)(Rv)(A)] / 12$$

All Subcatchments						
Catchment	Total Area (Acres)	Impervious Cover (Acres)	Percent Impervious %	Runoff Coefficient Rv	WQv (ft ³)	Description
1	10.30	10.20	0.99	0.94	42055.46	
2	5.50	5.30	0.96	0.92	21,884	
3	11.00	10.60	0.96	0.92	43768.91	
4	8.90	8.60	0.97	0.92	35505.30	
5	5.20	4.90	0.94	0.90	20257.76	
6	11.80	11.60	0.98	0.93	47846.49	
7	8.70	8.40	0.97	0.92	34681.11	
8	2.90	2.00	0.69	0.67	8437.12	
9	5.80	3.10	0.53	0.53	13360.58	
10	0.00	0.00				
11	4.00	0.00	0.00	0.05	867.57	Conservation of Natural Areas
12	0.00	0.00				
13	1.10	0.45	0.41	0.42	1995.41	Infiltration Basin
14	1.10	0.55	0.50	0.50	2385.82	Infiltration Basin
15	0.10	0.05	0.50	0.50	216.89	Dry Swale
16	0.00	0.00				
17	0.30	0.14	0.47	0.47	611.64	Dry Swale
18						
19						
20						
21						
22						
23						
24						
25						
26						
27						
28						
29						
30						

Runoff Reduction Volume and Treated volumes							
	Runoff Reduction Techniques/Standard SMPs		Total Contributing Area	Total Contributing Impervious Area	WQv Reduced (RRv)	WQv Treated	
			(acres)	(acres)	cf	cf	
Area/Volume Reduction	Conservation of Natural Areas	RR-1	4.00	0.00			
	Sheetflow to Riparian Buffers/Filter Strips	RR-2	0.00	0.00			
	Tree Planting/Tree Pit	RR-3	0.00	0.00			
	Disconnection of Rooftop Runoff	RR-4		0.00			
	Vegetated Swale	RR-5	0.00	0.00	0		
	Rain Garden	RR-6	0.00	0.00	0		
	Stormwater Planter	RR-7	0.00	0.00	0		
	Rain Barrel/Cistern	RR-8	0.00	0.00	0		
	Porous Pavement	RR-9	0.00	0.00	0		
	Green Roof (Intensive & Extensive)	RR-10	0.00	0.00	0		
Standard SMPs w/RRv Capacity	Infiltration Trench	I-1	0.00	0.00	0	0	
	Infiltration Basin	I-2	26.60	24.70	62378	7042	
	Dry Well	I-3	0.00	0.00	0	0	
	Underground Infiltration System	I-4					
	Bioretention & Infiltration Bioretention	F-5	0.00	0.00	0	0	
	Dry swale	O-1	0.40	0.19	87	766	
Standard SMPs	Micropool Extended Detention (P-1)	P-1				21798.000	
	Wet Pond (P-2)	P-2					
	Wet Extended Detention (P-3)	P-3					
	Multiple Pond system (P-4)	P-4					
	Pocket Pond (p-5)	P-5					
	Surface Sand filter (F-1)	F-1					
	Underground Sand filter (F-2)	F-2					
	Perimeter Sand Filter (F-3)	F-3					
	Organic Filter (F-4)	F-4					181790.000
	Shallow Wetland (W-1)	W-1					
	Extended Detention Wetland (W-2)	W-2					
	Pond/Wetland System (W-3)	W-3					
	Pocket Wetland (W-4)	W-4					
	Wet Swale (O-2)	O-2					
Totals by Area Reduction →			4.00	0.00	868		
Totals by Volume Reduction →			0.00	0.00	0		
Totals by Standard SMP w/RRV →			27.00	24.89	62466	7808	
Totals by Standard SMP →			0.00	0.00		203588	
Totals (Area + Volume + all SMPs) →			31.00	24.89	63,333	211,396	
Impervious Cover v		error					

Minimum RRv

Enter the Soils Data for the site

Soil Group	Acres	S
A	2.30	55%
B		40%
C		30%
D	70.40	20%
Total Area	72.7	

Calculate the Minimum RRv

S =	0.21	
Impervious =	65.89	<i>acre</i>
Precipitation	1.195	<i>in</i>
Rv	0.95	
Minimum RRv	57,313	<i>ft3</i>
	1.32	<i>af</i>

Planning

Practice	Description	Application
Preservation of Undisturbed Areas	Delineate and place into permanent conservation undisturbed forests, native vegetated areas, riparian corridors, wetlands, and natural terrain.	Considered & Applied
Preservation of Buffers	Define, delineate and preserve naturally vegetated buffers along perennial streams, rivers, shorelines and wetlands.	Considered & Not Applied
Reduction of Clearing and Grading	Limit clearing and grading to the minimum amount needed for roads, driveways, foundations, utilities and stormwater management facilities.	Considered & Applied
Locating Development in Less Sensitive Areas	Avoid sensitive resource areas such as floodplains, steep slopes, erodible soils, wetlands, mature forests and critical habitats by locating development to fit the terrain in areas that will create the least impact.	Considered & Applied
Open Space Design	Use clustering, conservation design or open space design to reduce impervious cover, preserve more open space and protect water resources.	N/A
Soil Restoration	Restore the original properties and porosity of the soil by deep till and amendment with compost to reduce the generation of runoff and enhance the runoff reduction performance of post construction practices.	N/A
Roadway Reduction	Minimize roadway widths and lengths to reduce site impervious area	Considered & Applied
Sidewalk Reduction	Minimize sidewalk lengths and widths to reduce site impervious area	Considered & Applied
Driveway Reduction	Minimize driveway lengths and widths to reduce site impervious area	N/A
Cul-de-sac Reduction	Minimize the number of cul-de-sacs and incorporate landscaped areas to reduce their impervious cover.	N/A
Building Footprint Reduction	Reduce the impervious footprint of residences and commercial buildings by using alternate or taller buildings while maintaining the same floor to area ratio.	Considered & Applied
Parking Reduction	Reduce imperviousness on parking lots by eliminating unneeded spaces, providing compact car spaces and efficient parking lanes, minimizing stall dimensions, using porous pavement surfaces in overflow parking areas, and using multi-storied parking decks where appropriate.	Considered & Applied

NOI QUESTIONS

#	NOI Question	Reported Value	
		cf	af
28	Total Water Quality Volume (WQv) Required	273874	6.287
30	Total RRV Provided	63333	1.454
31	Is RRV Provided \geq WQv Required?	No	
32	Minimum RRV	57313	1.316
32a	Is RRV Provided \geq Minimum RRV Required?	Yes	
33a	Total WQv Treated	211396	4.853
34	Sum of Volume Reduced & Treated	274729	6.307
34	Sum of Volume Reduced and Treated	274729	6.307
35	Is Sum RRV Provided and WQv Provided \geq WQv Required?	Yes	

Apply Peak Flow Attenuation			
36	Channel Protection	<i>Cpv</i>	
37	Overbank	<i>Qp</i>	
37	Extreme Flood Control	<i>Qf</i>	
	Are Quantity Control requirements met?	Yes	Plan Completed

Infiltration Basin Worksheet

Design Point:							
Enter Site Data For Drainage Area to be Treated by Practice							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
1	10.30	10.20	0.99	0.94	42055.46	1.20	
Enter Impervious Area Reduced by Disconnection of Practice		0.00	99%	0.94	42,055	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.					0	ft ³	
Pretreatment Techniques to Prevent Clogging							
Infiltration Rate			1.50	in/hour	Okay		
Pretreatment Sizing			25	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour		
Pretreatment Required Volume			10,514	ft ³			
Pretreatment Provided			11,000	ft ³			
Pretreatment Techniques utilized			<i>Other</i>				
Size An Infiltration Basin							
Design Volume	42,055	ft ³	WQv				
Basal Area Required	42,055	ft ²	<i>Infiltration practices shall be designed to exfiltrate the entire WQv through the floor of each practice.</i>				
Basal Area Provided	23,609	ft ²					
Design Depth	1.00	ft					
Volume Provided	23,609	ft ³	<i>Storage Volume provided in infiltration basin area (not including pretreatment.</i>				
Determine Runoff Reduction							
RRv	21,248	ft³	90% of the storage provided in the basin or WQv whichever is smaller				
Volume Treated	20,807	ft ³	<i>This is the portion of the WQv that is not reduced/infiltrated</i>				
Sizing v			<i>The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.</i>				

Infiltration Basin Worksheet

Design Point:							
Enter Site Data For Drainage Area to be Treated by Practice							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
4	8.90	8.60	0.97	0.92	35505.30	1.20	
Enter Impervious Area Reduced by Disconnection of Paved Areas		0.00	97%	0.92	35,505	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.					0	ft ³	
Pretreatment Techniques to Prevent Clogging							
Infiltration Rate			0.80	in/hour	Okay		
Pretreatment Sizing			25	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour		
Pretreatment Required Volume			8,876	ft ³			
Pretreatment Provided			10,000	ft ³			
Pretreatment Techniques utilized			Other				
Size An Infiltration Basin							
Design Volume	35,505	ft ³	WQv				
Basal Area Required	35,505	ft ²	Infiltration practices shall be designed to exfiltrate the entire WQv through the floor of each practice.				
Basal Area Provided	20,516	ft ²					
Design Depth	1.00	ft					
Volume Provided	20,516	ft ³	Storage Volume provided in infiltration basin area (not including pretreatment).				
Determine Runoff Reduction							
RRv	18,464	ft³	90% of the storage provided in the basin or WQv whichever is smaller				
Volume Treated	17,041	ft ³	This is the portion of the WQv that is not reduced/infiltrated				
Sizing v			The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.				

Infiltration Basin Worksheet

Design Point:							
Enter Site Data For Drainage Area to be Treated by Practice							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
5	5.20	4.90	0.94	0.90	20257.76	1.20	
Enter Impervious Area Reduced by Disconnection of Paved Areas			94%	0.90	20,258	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.						ft ³	
Pretreatment Techniques to Prevent Clogging							
Infiltration Rate			0.50	in/hour	Okay		
Pretreatment Sizing			25	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour		
Pretreatment Required Volume			5,064	ft ³			
Pretreatment Provided			5,100	ft ³			
Pretreatment Techniques utilized			Other				
Size An Infiltration Basin							
Design Volume	20,258	ft ³	WQv				
Basal Area Required	20,258	ft ²	<i>Infiltration practices shall be designed to exfiltrate the entire WQv through the floor of each practice.</i>				
Basal Area Provided	20,473	ft ²					
Design Depth	1.00	ft					
Volume Provided	20,473	ft ³	<i>Storage Volume provided in infiltration basin area (not including pretreatment.</i>				
Determine Runoff Reduction							
RRv	18,426	ft³	90% of the storage provided in the basin or WQv whichever is smaller				
Volume Treated	1,832	ft ³	<i>This is the portion of the WQv that is not reduced/infiltrated</i>				
Sizing v	OK		<i>The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.</i>				

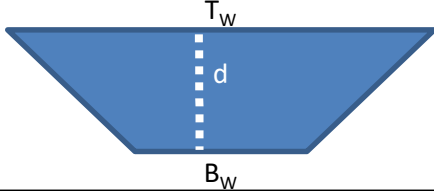
Infiltration Basin Worksheet

Design Point:							
Enter Site Data For Drainage Area to be Treated by Practice							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
13	1.10	0.45	0.41	0.42	1995.41	1.20	Infiltration Basin
Enter Impervious Area Reduced by Disconnection of Paved Areas			41%	0.42	1,995	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.						ft ³	
Pretreatment Techniques to Prevent Clogging							
Infiltration Rate			4.50	in/hour	Okay		
Pretreatment Sizing			50	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour		
Pretreatment Required Volume			998	ft ³			
Pretreatment Provided			1,058	ft ³			
Pretreatment Techniques utilized			Sedimentation Basin				
Size An Infiltration Basin							
Design Volume	1,995	ft ³	WQv				
Basal Area Required	512	ft ²	<i>Infiltration practices shall be designed to exfiltrate the entire WQv through the floor of each practice.</i>				
Basal Area Provided	639	ft ²					
Design Depth	3.90	ft					
Volume Provided	2,492	ft ³	<i>Storage Volume provided in infiltration basin area (not including pretreatment.</i>				
Determine Runoff Reduction							
RRv	1,995	ft³	90% of the storage provided in the basin or WQv whichever is smaller				
Volume Treated	0	ft ³	<i>This is the portion of the WQv that is not reduced/infiltrated</i>				
Sizing v	OK		<i>The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.</i>				

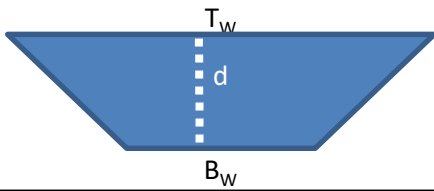
Infiltration Basin Worksheet

Design Point:							
Enter Site Data For Drainage Area to be Treated by Practice							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
14	1.10	0.55	0.50	0.50	2385.82	1.20	Infiltration Basin
Enter Impervious Area Reduced by Disconnection of Practice		0.00	50%	0.50	2,386	<<WQv after adjusting for Disconnected Rooftops	
Enter the portion of the WQv that is not reduced for all practices routed to this practice.					0	ft ³	
Pretreatment Techniques to Prevent Clogging							
Infiltration Rate			12.00	in/hour	Okay		
Pretreatment Sizing			100	% WQv	25% minimum; 50% if >2 in/hr 100% if >5in/hour		
Pretreatment Required Volume			2,386	ft ³			
Pretreatment Provided			2,389	ft ³			
Pretreatment Techniques utilized			Sedimentation Basin				
Size An Infiltration Basin							
Design Volume	2,386	ft ³	WQv				
Basal Area Required	612	ft ²	Infiltration practices shall be designed to exfiltrate the entire WQv through the floor of each practice.				
Basal Area Provided	640	ft ²					
Design Depth	3.90	ft					
Volume Provided	2,494	ft ³	Storage Volume provided in infiltration basin area (not including pretreatment).				
Determine Runoff Reduction							
RRv	2,245	ft³	90% of the storage provided in the basin or WQv whichever is smaller				
Volume Treated	141	ft ³	This is the portion of the WQv that is not reduced/infiltrated				
Sizing v	OK		The infiltration basin must provide storage equal to or greater than the WQv of the contributing area.				

Dry Swale Worksheet

Design Point:							
Enter Site Data For Drainage Area to be Treated by Practice							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
15	0.10	0.05	0.50	0.50	216.89	1.20	Dry Swale
Enter Impervious Area Reduced by Disconnection of Rooftops		0.00	50%	0.50	217	<<WQv after adjusting for Disconnected Rooftops	
Pretreatment Provided				Pretreatment Technique			
Pretreatment (10% of WQv)			22	ft ³			
Calculate Available Storage Capacity							
Bottom Width	1	ft	Design with a bottom width no greater than eight feet to avoid potential gullyng and channel braiding, but no less than two feet				
Side Slope (X:1)	2	Okay	Channels shall be designed with moderate side slopes (flatter than 3:1) for most conditions. 2:1 is the absolute maximum side slope				
Longitudinal Slope	0%	Okay	Maximum longitudinal slope shall be 4%				
Flow Depth	0.75	ft	Maximum ponding depth of one foot at the mid-point of the channel, and a maximum depth of 18" at the end point of the channel (for storage of the WQv)				
Top Width	4	ft					
Area	1.88	sf					
Minimum Length	104	ft					
Actual Length	105	ft					
End Point Depth check	1.00	Okay	A maximum depth of 18" at the end point of the channel (for storage of the WQv)				
Storage Capacity	219	ft ³					
Soil Group (HSG)			A				
Runoff Reduction							
Is the Dry Swale contributing flow to another practice?			No	Select Practice			
RRv	87	ft ³	Runoff Reduction equals 40% in HSG A and B and 20% in HSG C and D up to the WQv				
Volume Treated	129	ft ³	This is the difference between the WQv calculated and the runoff reduction achieved in the swale				
Volume Directed	0	ft ³	This volume is directed another practice				
Volume V	Okay		Check to be sure that channel is long enough to store WQv				

Dry Swale Worksheet

Design Point:							
Enter Site Data For Drainage Area to be Treated by Practice							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
17	0.30	0.14	0.47	0.47	611.64	1.20	Dry Swale
Enter Impervious Area Reduced by Disconnection of Rooftops		0.00	47%	0.47	612	<<WQv after adjusting for Disconnected Rooftops	
Pretreatment Provided				Pretreatment Technique			
Pretreatment (10% of WQv)			61	ft ³			
Calculate Available Storage Capacity							
Bottom Width	2	ft	Design with a bottom width no greater than eight feet to avoid potential gullyng and channel braiding, but no less than two feet				
Side Slope (X:1)	3	Okay	Channels shall be designed with moderate side slopes (flatter than 3:1) for most conditions. 2:1 is the absolute maximum side slope				
Longitudinal Slope	3%	Okay	Maximum longitudinal slope shall be 4%				
Flow Depth	1	ft	Maximum ponding depth of one foot at the mid-point of the channel, and a maximum depth of 18" at the end point of the channel (for storage of the WQv)				
Top Width	8	ft					
Area	5.00	sf					
Minimum Length	110	ft					
Actual Length	115	ft					
End Point Depth check	1.50	Okay	A maximum depth of 18" at the end point of the channel (for storage of the WQv)				
Storage Capacity	636	ft ³					
Soil Group (HSG)			D				
Runoff Reduction							
Is the Dry Swale contributing flow to another practice?			No	Select Practice			
RRv	127	ft ³	Runoff Reduction equals 40% in HSG A and B and 20% in HSG C and D up to the WQv				
Volume Treated	484	ft ³	This is the difference between the WQv calculated and the runoff reduction achieved in the swale				
Volume Directed	0	ft ³	This volume is directed another practice				
Volume V	Okay		Check to be sure that channel is long enough to store WQv				

Conservation of Natural Areas

Design Point:							
Enter Site Data For Drainage Area to be Treated by Practice							
Catchment Number	Total Area (Acres)	Impervious Area (Acres)	Percent Impervious %	Rv	WQv (ft ³)	Precipitation (in)	Description
11	4.00	0.00	0.00	0.05	867.57	1.20	Conservation of Natural Areas
Design Elements							
Is Contiguous Area ≥ 10,000 ft ² ?						Yes	
Will limits of disturbance be clearly shown on all construction drawings and marked in field/project development site with structural barriers?						Yes	
Is the Conservation area located in an acceptable conservation easement instrument that ensures perpetual protection of proposed area?						Yes	
Does the easement specify how the natural area vegetation will be managed and boundaries will be marked?						Yes	
Does the conservation area receive runoff from other contributing areas?						No	
Does Conservation Area drain to a Design Point?						Yes	
Is Sheet Flow to Riparian Buffer or another area based practice already being Used for this area?						No	
Are All Criteria in Section 5.3.1 Met?				Yes			
Area Reduction Adjustments							
<i>Subtract</i>	<i>4.00</i>	<i>Acres from Total Area</i>					
<i>Subtract</i>	<i>0.00</i>	<i>Acres from Total Impervious Area</i>					

Date: 1/18/2022
Project: Port of Albany
Location: Albany, NY
Prepared For: Natalie Olivieri

Purpose: To calculate the water quality flow rate (Qwq) over a given site area. In this situation the WQv to be analyzed is the runoff produced by the first 1.2 inch(es) of rainfall, per Fig 4.1 of the New York State Stormwater Management Design Manual

Reference: United States Department of Agriculture Natural Resources Conservation Service TR-55 Manual, New York State Stormwater Management Design Manual - 2015

Formulas:
$$WQv = \frac{(P)(R_v)(A)}{12}$$

$$R_v = (0.05+0.009(I))$$

$$CN = 1000/[10+5P+10Qa-10(Qa^2+1.25QaP)^{1/2}]$$

$$Qwq = (q_u)*(A)*(Qa)$$

Structure:	WQU 1	Structure:	WQU 2	Structure:	WQU 3
P	1.20 in.	P	1.20 in.	P	1.20 in.
A	10.300 ac	A	5.500 ac	A	11.000 ac
I	99.03 %	I	96.36 %	I	96.36 %
t _c	10.0 min.	t _c	10.0 min.	t _c	10.4 min.
t _c	0.167 hr.	t _c	0.167 hr.	t _c	0.173 hr.
R _v	0.941	R _v	0.917	R _v	0.917
43% WQv	0.413 ac-ft	90% WQv	0.504 ac-ft	90% WQv	1.009 ac-ft
43% WQv	18003.65 ft ³	90% WQv	21971.66 ft ³	90% WQv	43938.97 ft ³
Qa	1.129 in.	Qa	1.101 in.	Qa	1.100 in.
CN	97.00	CN	94.00	CN	95.00
I _a	0.062	I _a	0.128	I _a	0.105
I _a /P	0.052	I _a /P	0.107	I _a /P	0.088
q _u	1000 (csm/in)	q _u	1000 (csm/in)	q _u	1000 (csm/in)
A	0.01609 miles ²	A	0.00859 miles ²	A	0.01719 miles ²
Qwq	7.81 cfs	Qwq	9.46 cfs	Qwq	18.91 cfs

Date: 1/18/2022
Project: Port of Albany
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Purpose: To calculate the water quality flow rate (Qwq) over a given site area. In this situation the WQv to be analyzed is the runoff produced by the first 1.2 inch(es) of rainfall, per Fig 4.1 of the New York State Stormwater Management Design Manual

Reference: United States Department of Agriculture Natural Resources Conservation Service TR-55 Manual, New York State Stormwater Management Design Manual - 2015

Formulas:
$$WQv = \frac{(P)(R_v)(A)}{12}$$

$$R_v = (0.05+0.009(I))$$

$$CN = 1000/[10+5P+10Qa-10(Qa^2+1.25QaP)^{1/2}]$$

$$Qwq = (q_u)*(A)*(Qa)$$

Structure: WQU 4

P	1.20	in.
A	8.900	ac
I	96.63	%
t _c	10.0	min.
t _c	0.167	hr.
R _v	0.92	
42% WQv	0.342	ac-ft
42% WQv	14912.10	ft ³
Qa	1.104	in.
CN	94.00	
I _a	0.128	
I _a /P	0.107	
q _u	1000	(csm/in)
A	0.01391	miles ²
Qwq	6.44	cfs

Structure: WQU 6

P	1.20	in.
A	11.800	ac
I	98.31	%
t _c	10.0	min.
t _c	0.167	hr.
R _v	0.935	
90% WQv	1.103	ac-ft
90% WQv	48059.75	ft ³
Qa	1.122	in.
CN	96.00	
I _a	0.083	
I _a /P	0.069	
q _u	1000	(csm/in)
A	0.01844	miles ²
Qwq	20.69	cfs

Date: 1/18/2022
Project: Port of Albany
Location: Albany, NY
Prepared For: Natalie Olivieri

Purpose: To calculate the water quality flow rate (Qwq) over a given site area. In this situation the WQv to be analyzed is the runoff produced by the first 1.2 inch(es) of rainfall, per Fig 4.1 of the New York State Stormwater Management Design Manual

Reference: United States Department of Agriculture Natural Resources Conservation Service TR-55 Manual, New York State Stormwater Management Design Manual - 2015

Formulas:
$$WQv = \frac{(P)(R_v)(A)}{12}$$

$$R_v = (0.05+0.009(I))$$

$$CN = 1000/[10+5P+10Qa-10(Qa^2+1.25QaP)^{1/2}]$$

$$Qwq = (q_u)*(A)*(Qa)$$

Structure: WQU 7

P	1.20	in.
A	8.700	ac
I	96.55	%
t _c	10.5	min.
t _c	0.175	hr.
R _v	0.919	
90% WQv	0.800	ac-ft
90% WQv	34826.22	ft ³
Qa	1.103	in.
CN	96.00	
I _a	0.083	
I _a /P	0.069	
q _u	1000	(csm/in)
A	0.01359	miles ²
Qwq	14.99	cfs

Analyze Gravity Network - Drainage Area 1

Analysis Result AEP: 1/2 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP1	3.00'	26.218 cubic	14.802 ft/s	3.50%	Flooded	DV-1
2	JP-1A	3.00'	26.250 cubic	7.277 ft/s	0.50%	Flooded	J-1
3	DP1-1	3.00'	22.911 cubic	7.031 ft/s	0.50%	Flooded	DS1-1
4	DP1-2	3.00'	23.222 cubic	7.056 ft/s	0.50%	Surcharge	DS1-2
5	DP1-3	3.00'	23.805 cubic	7.101 ft/s	0.50%	Surcharge	DS1-3
6	DP1-4	3.00'	23.946 cubic	7.118 ft/s	0.50%	Surcharge	DS1-4
7	DP1-5	3.00'	23.913 cubic	7.109 ft/s	0.50%	Surcharge	DS1-5
8	DP1-6	3.00'	21.904 cubic	6.950 ft/s	0.50%	Surcharge	DS1-6
9	DP1-7	2.50'	19.124 cubic	6.713 ft/s	0.50%	Surcharge	DS1-7
10	DP1-8	2.50'	16.379 cubic	6.468 ft/s	0.50%	Surcharge	DS1-8
11	DP1-9	2.50'	14.354 cubic	6.256 ft/s	0.50%	Surcharge	DS1-9
12	DP1-10	2.50'	14.063 cubic	6.224 ft/s	0.50%	Surcharge	DS1-10
13	DP1-11	2.50'	12.360 cubic	6.018 ft/s	0.50%	Surcharge	DS1-11
14	DP1-12	2.00'	8.023 cubic f	5.410 ft/s	0.50%	Surcharge	DS1-12
15	DP1-13	1.50'	4.009 cubic f	4.549 ft/s	0.50%	Surcharge	DS1-13
16	DP1-14	1.50'	3.460 cubic f	4.382 ft/s	0.50%	Normal	DS1-14

DP1

HGL Up	10.90'
HGL Down	8.94'
EGL Up	14.30'
EGL Down	12.35'
Invert Up	10.00'
Invert Down	8.04'

DV-1

Structure Type	Manhole
Rim Elevation	13.96'
HGL	14.30' ✘
EGL	14.30' ✘

Apply Cancel Help

Analyze Gravity Network - Drainage Area 1

Analysis Result AEP: 1/10 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP1	3.00'	41.089 cubic	16.777 ft/s	3.50%	Flooded	DV-1
2	JP-1A	3.00'	41.175 cubic	8.041 ft/s	0.50%	Flooded	J-1
3	DP1-1	3.00'	36.190 cubic	7.840 ft/s	0.50%	Flooded	DS1-1
4	DP1-2	3.00'	36.636 cubic	7.860 ft/s	0.50%	Flooded	DS1-2
5	DP1-3	3.00'	37.438 cubic	7.896 ft/s	0.50%	Surcharge	DS1-3
6	DP1-4	3.00'	37.539 cubic	7.908 ft/s	0.50%	Surcharge	DS1-4
7	DP1-5	3.00'	37.435 cubic	7.895 ft/s	0.50%	Surcharge	DS1-5
8	DP1-6	3.00'	34.180 cubic	7.744 ft/s	0.50%	Surcharge	DS1-6
9	DP1-7	2.50'	29.766 cubic	7.282 ft/s	0.50%	Surcharge	DS1-7
10	DP1-8	2.50'	25.419 cubic	7.126 ft/s	0.50%	Flooded	DS1-8
11	DP1-9	2.50'	22.253 cubic	6.943 ft/s	0.50%	Flooded	DS1-9
12	DP1-10	2.50'	21.767 cubic	6.910 ft/s	0.50%	Flooded	DS1-10
13	DP1-11	2.50'	19.095 cubic	6.710 ft/s	0.50%	Flooded	DS1-11
14	DP1-12	2.00'	12.356 cubic	5.992 ft/s	0.50%	Flooded	DS1-12
15	DP1-13	1.50'	6.157 cubic f	5.017 ft/s	0.50%	Flooded	DS1-13
16	DP1-14	1.50'	5.305 cubic f	4.863 ft/s	0.50%	Flooded	DS1-14

DP1

HGL Up	11.13'
HGL Down	9.18'
EGL Up	15.51'
EGL Down	13.55'
Invert Up	10.00'
Invert Down	8.04'

DV-1

Structure Type	Manhole
Rim Elevation	13.96'
HGL	15.51' ✘
EGL	15.51' ✘

Apply Cancel Help

Analyze Gravity Network - Drainage Area 2

Analysis Result AEP: 1/2 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DS2	2.50'	17.264 cubic	6.504 ft/s	0.49%	Normal	J-2
2	JP-2	2.50'	17.294 cubic	7.321 ft/s	0.67%	Normal	DS2
3	DP2-3	2.00'	6.111 cubic f	5.038 ft/s	0.50%	Surcharge	DS2-3
4	DP2-4	1.50'	1.972 cubic f	3.764 ft/s	0.50%	Surcharge	DS2-4
5	DP2-1	2.00'	8.461 cubic f	5.483 ft/s	0.50%	Surcharge	DS2-1
6	DP2-2	1.50'	4.832 cubic f	4.760 ft/s	0.50%	Surcharge	DS2-2

DS2

HGL Up	9.26'
HGL Down	9.11'
EGL Up	9.92'
EGL Down	9.77'
Invert Up	7.93'
Invert Down	7.78'

J-2

Structure Type	<none>
Rim Elevation	15.00'
HGL	10.07'
EGL	10.07'

Apply Cancel Help

Analysis Result

AEP: 1/10

Profile

Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DS2	2.50'	26.656 cubic	7.124 ft/s	0.49%	Normal	J-2
2	JP-2	2.50'	26.697 cubic	8.102 ft/s	0.67%	Normal	DS2
3	DP2-3	2.00'	9.412 cubic f	5.630 ft/s	0.50%	Surcharge	DS2-3
4	DP2-4	1.50'	3.025 cubic f	4.230 ft/s	0.50%	Surcharge	DS2-4
5	DP2-1	2.00'	13.018 cubic	6.056 ft/s	0.50%	Surcharge	DS2-1
6	DP2-2	1.50'	7.411 cubic f	5.167 ft/s	0.50%	Surcharge	DS2-2

DS2	
HGL Up	9.71'
HGL Down	9.56'
EGL Up	10.50'
EGL Down	10.35'
Invert Up	7.93'
Invert Down	7.78'
J-2	
Structure Type	<none>
Rim Elevation	15.00'
HGL	10.80'
EGL	10.80'

Start Over

Apply

Cancel

Help

Analysis Result

AEP: 1/2

Profile

Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP3	3.00'	30.945 cubic	7.572 ft/s	0.50%	Normal	JM-3B
2	JP-3E	3.00'	30.986 cubic	7.574 ft/s	0.50%	Normal	DS3
3	DP3-15	2.00'	9.982 cubic f	5.696 ft/s	0.50%	Surcharge	DS3-15
4	DP3-16	2.00'	6.872 cubic f	5.197 ft/s	0.50%	Surcharge	DS3-16
5	DP3-17	1.50'	3.591 cubic f	6.326 ft/s	1.33%	Surcharge	DS3-17
6	DP3-18	1.50'	2.869 cubic f	4.171 ft/s	0.50%	Normal	DS3-18
7	DP3-19	1.50'	4.895 cubic f	4.784 ft/s	0.50%	Surcharge	DS3-19
8	DP3-20	1.50'	3.479 cubic f	4.388 ft/s	0.50%	Surcharge	DS3-20
9	DP3-1	2.50'	16.137 cubic	7.337 ft/s	0.71%	Surcharge	DS3-1
10	DP3-2	2.00'	13.260 cubic	7.955 ft/s	1.00%	Surcharge	DS3-2
11	DP3-3	2.00'	11.621 cubic	7.698 ft/s	1.00%	Surcharge	DS3-3
12	DP3-13	1.50'	1.907 cubic f	3.729 ft/s	0.50%	Normal	DS3-13
13	DP3-14	1.00'	1.181 cubic f	3.350 ft/s	0.50%	Normal	DS3-14
14	DP3-4	2.00'	9.494 cubic f	5.642 ft/s	0.50%	Normal	DS3-4
15	DP3-5	2.00'	7.871 cubic f	5.384 ft/s	0.50%	Normal	DS3-5
16	DP3-6	2.00'	6.221 cubic f	5.062 ft/s	0.50%	Normal	DS3-6
17	DP3-7	1.50'	4.448 cubic f	4.667 ft/s	0.50%	Normal	DS3-7
18	DP3-8	1.50'	3.351 cubic f	4.345 ft/s	0.50%	Normal	DS3-8
19	DP3-9	1.50'	2.488 cubic f	4.013 ft/s	0.50%	Normal	DS3-9
20	DP3-10	1.50'	1.807 cubic f	3.673 ft/s	0.50%	Normal	DS3-10
21	DP3-12	1.00'	0.411 cubic f	2.503 ft/s	0.50%	Normal	DS3-12
22	DP3-11	1.00'	0.946 cubic f	3.159 ft/s	0.50%	Normal	DS3-11

DP3	
HGL Up	10.48'
HGL Down	10.36'
EGL Up	11.38'
EGL Down	11.25'
Invert Up	8.80'
Invert Down	8.67'
JM-3B	
Structure Type	Manhole
Rim Elevation	15.40'
HGL	11.61'
EGL	11.61'

Start Over

Apply

Cancel

Help

Analysis Result

AEP: 1/10

Profile

Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP3	3.00'	48.079 cubic	8.219 ft/s	0.50%	Normal	JM-3B
2	JP-3E	3.00'	48.136 cubic	8.220 ft/s	0.50%	Normal	DS3
3	DP3-15	2.00'	15.473 cubic	6.218 ft/s	0.50%	Surcharge	DS3-15
4	DP3-16	2.00'	10.617 cubic	5.794 ft/s	0.50%	Flooded	DS3-16
5	DP3-17	1.50'	5.530 cubic f	7.104 ft/s	1.33%	Flooded	DS3-17
6	DP3-18	1.50'	4.400 cubic f	4.655 ft/s	0.50%	Surcharge	DS3-18
7	DP3-19	1.50'	7.530 cubic f	5.187 ft/s	0.50%	Flooded	DS3-19
8	DP3-20	1.50'	5.336 cubic f	4.869 ft/s	0.50%	Flooded	DS3-20
9	DP3-1	2.50'	25.295 cubic	8.181 ft/s	0.71%	Surcharge	DS3-1
10	DP3-2	2.00'	20.712 cubic	8.749 ft/s	1.00%	Surcharge	DS3-2
11	DP3-3	2.00'	18.115 cubic	8.536 ft/s	1.00%	Surcharge	DS3-3
12	DP3-13	1.50'	2.940 cubic f	4.198 ft/s	0.50%	Surcharge	DS3-13
13	DP3-14	1.00'	1.812 cubic f	3.717 ft/s	0.50%	Surcharge	DS3-14
14	DP3-4	2.00'	14.773 cubic	6.195 ft/s	0.50%	Surcharge	DS3-4
15	DP3-5	2.00'	12.222 cubic	5.978 ft/s	0.50%	Surcharge	DS3-5
16	DP3-6	2.00'	9.638 cubic f	5.663 ft/s	0.50%	Surcharge	DS3-6
17	DP3-7	1.50'	6.885 cubic f	5.116 ft/s	0.50%	Surcharge	DS3-7
18	DP3-8	1.50'	5.181 cubic f	4.837 ft/s	0.50%	Surcharge	DS3-8
19	DP3-9	1.50'	3.841 cubic f	4.501 ft/s	0.50%	Surcharge	DS3-9
20	DP3-10	1.50'	2.788 cubic f	4.139 ft/s	0.50%	Surcharge	DS3-10
21	DP3-12	1.00'	0.631 cubic f	2.826 ft/s	0.50%	Surcharge	DS3-12
22	DP3-11	1.00'	1.451 cubic f	3.528 ft/s	0.50%	Surcharge	DS3-11

DP3	
HGL Up	11.11'
HGL Down	10.99'
EGL Up	12.16'
EGL Down	12.04'
Invert Up	8.80'
Invert Down	8.67'
JM-3B	
Structure Type	Manhole
Rim Elevation	15.40'
HGL	12.59'
EGL	12.59'

Start Over

Apply

Cancel

Help

Analysis Result AEP: 1/2 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP4	3.00'	25.477 cubic	14.682 ft/s	3.50%	✓ Normal	DV-4
2	JP-4D	3.00'	25.512 cubic	12.012 ft/s	2.00%	✗ Flooded	J-5
3	JP-4E	3.00'	25.604 cubic	7.232 ft/s	0.50%	✗ Flooded	DS4
4	DP4-3	2.00'	10.117 cubic	5.729 ft/s	0.50%	✗ Flooded	DS4-3
5	DP4-4	2.00'	5.708 cubic f	4.802 ft/s	0.46%	✗ Flooded	DS4-4
6	DP4-5	1.50'	4.288 cubic f	4.611 ft/s	0.50%	✗ Flooded	DS4-5
7	DP4-6	1.50'	3.154 cubic f	5.435 ft/s	0.96%	⚠ Surcharge	DS4-6
9	DP4-7	2.00'	11.141 cubic	5.858 ft/s	0.50%	✗ Flooded	DS4-7
10	DP4-8	2.00'	7.176 cubic f	5.256 ft/s	0.50%	✗ Flooded	DS4-8
11	DP4-1	1.50'	4.603 cubic f	4.957 ft/s	0.57%	✗ Flooded	DS4-1
12	DP4-2	1.00'	2.034 cubic f	4.914 ft/s	0.97%	⚠ Surcharge	DS4-2

DP4

HGL Up	11.88'
HGL Down	11.03'
EGL Up	15.23'
EGL Down	14.38'
Invert Up	11.00'
Invert Down	10.15'

DV-4

Structure Type	Manhole
Rim Elevation	15.37'
HGL	15.23'
EGL	15.23'

Start Over Apply Cancel Help

Analysis Result AEP: 1/10 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP4	3.00'	39.442 cubic	16.590 ft/s	3.50%	✗ Flooded	DV-4
2	JP-4D	3.00'	39.489 cubic	13.528 ft/s	2.00%	✗ Flooded	J-5
3	JP-4E	3.00'	39.616 cubic	7.984 ft/s	0.50%	✗ Flooded	DS4
4	DP4-3	2.00'	15.613 cubic	6.243 ft/s	0.50%	✗ Flooded	DS4-3
5	DP4-4	2.00'	8.782 cubic f	5.369 ft/s	0.46%	✗ Flooded	DS4-4
6	DP4-5	1.50'	6.577 cubic f	5.060 ft/s	0.50%	✗ Flooded	DS4-5
7	DP4-6	1.50'	4.836 cubic f	6.094 ft/s	0.96%	✗ Flooded	DS4-6
9	DP4-7	2.00'	17.128 cubic	6.288 ft/s	0.50%	✗ Flooded	DS4-7
10	DP4-8	2.00'	11.006 cubic	5.842 ft/s	0.50%	✗ Flooded	DS4-8
11	DP4-1	1.50'	7.059 cubic f	5.440 ft/s	0.57%	✗ Flooded	DS4-1
12	DP4-2	1.00'	3.119 cubic f	5.392 ft/s	0.97%	✗ Flooded	DS4-2

DP4

HGL Up	12.11'
HGL Down	11.26'
EGL Up	16.39'
EGL Down	15.54'
Invert Up	11.00'
Invert Down	10.15'

DV-4

Structure Type	Manhole	
Rim Elevation	15.37'	
HGL	16.39'	✗
EGL	16.39'	✗

Start Over Apply Cancel Help

Analysis Result AEP: 1/2 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP5	3.00'	14.640 cubic	6.239 ft/s	0.50%	✓ Normal	DV-5
2	DP5-4	1.50'	3.963 cubic f	8.186 ft/s	2.51%	⚠ Surcharge	DSS-4
3	DP5-5	1.50'	3.561 cubic f	4.414 ft/s	0.50%	⚠ Surcharge	DSS-5
4	DP5-6	1.50'	2.984 cubic f	4.215 ft/s	0.50%	⚠ Surcharge	DSS-6
5	DP5-7	1.00'	1.762 cubic f	3.694 ft/s	0.50%	⚠ Surcharge	DSS-7
6	IS 5-2	2.00'	10.652 cubic	5.798 ft/s	0.50%	⚠ Surcharge	DSS
7	DP5-1	2.00'	11.072 cubic	5.850 ft/s	0.50%	⚠ Surcharge	DSS-1
8	DP5-2	2.00'	10.862 cubic	5.824 ft/s	0.50%	✗ Flooded	DSS-2
9	DP5-3	2.00'	8.456 cubic f	5.477 ft/s	0.50%	✗ Flooded	DSS-3

DP5

HGL Up	13.70'
HGL Down	13.39'
EGL Up	14.30'
EGL Down	13.99'
Invert Up	12.60'
Invert Down	12.29'

DV-5

Structure Type	Grate inlet
Rim Elevation	17.62'
HGL	14.30'
EGL	14.30'

Start Over Apply Cancel Help

Analysis Result AEP: 1/10 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP5	3.00'	22.607 cubic	7.007 ft/s	0.50%	✓ Normal	DV-5
2	DP5-4	1.50'	6.153 cubic f	9.242 ft/s	2.51%	⚠ Surcharge	DS5-4
3	DP5-5	1.50'	5.499 cubic f	4.901 ft/s	0.50%	⚠ Surcharge	DS5-5
4	DP5-6	1.50'	4.588 cubic f	4.702 ft/s	0.50%	⚠ Surcharge	DS5-6
5	DP5-7	1.00'	2.703 cubic f	3.962 ft/s	0.50%	⚠ Surcharge	DS5-7
6	IS 5-2	2.00'	16.445 cubic	6.277 ft/s	0.50%	⚠ Surcharge	DSS
7	DP5-1	2.00'	17.044 cubic	6.288 ft/s	0.50%	✖ Flooded	DSS-1
8	DP5-2	2.00'	16.702 cubic	6.283 ft/s	0.50%	✖ Flooded	DSS-2
9	DP5-3	2.00'	12.968 cubic	6.044 ft/s	0.50%	✖ Flooded	DSS-3

DP5

HGL Up	14.00'
HGL Down	13.68'
EGL Up	14.76'
EGL Down	14.45'
Invert Up	12.60'
Invert Down	12.29'

DV-5

Structure Type	Grate inlet
Rim Elevation	17.62'
HGL	14.97'
EGL	14.97'

Start Over Apply Cancel Help

Analysis Result AEP: 1/2 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP6	3.00'	31.765 cubic	7.618 ft/s	0.50%	✓ Normal	JM-6A
2	JP-6E	3.00'	31.820 cubic	7.621 ft/s	0.50%	✓ Normal	DS6
3	DP6-1	3.00'	30.573 cubic	7.550 ft/s	0.50%	✓ Normal	DS6-1
4	DP6-2	3.00'	28.195 cubic	7.406 ft/s	0.50%	✓ Normal	DS6-2
5	DP6-3	3.00'	26.141 cubic	7.270 ft/s	0.50%	✓ Normal	DS6-3
6	DP6-4	3.00'	26.008 cubic	7.261 ft/s	0.50%	✓ Normal	DS6-4
7	DP6-13	1.50'	2.396 cubic f	8.464 ft/s	4.14%	⚠ Surcharge	DS6-13
8	DP6-5	3.00'	23.739 cubic	7.096 ft/s	0.50%	✓ Normal	DS6-5
9	DP6-6	3.00'	20.873 cubic	6.863 ft/s	0.50%	✓ Normal	DS6-6
10	DP6-7	2.50'	17.671 cubic	6.588 ft/s	0.50%	✓ Normal	DS6-7
11	DP6-8	2.50'	14.393 cubic	6.261 ft/s	0.50%	✓ Normal	DS6-8
12	DP6-9	2.50'	13.518 cubic	6.160 ft/s	0.50%	✓ Normal	DS6-9
13	DP6-10	2.50'	12.286 cubic	6.008 ft/s	0.50%	✓ Normal	DS6-10
14	DP6-11	2.00'	10.578 cubic	5.789 ft/s	0.50%	✓ Normal	DS6-11
15	DP6-12	1.50'	5.114 cubic f	5.014 ft/s	0.55%	⚠ Surcharge	DS6-12
16	DP6-14	1.50'	1.715 cubic f	8.104 ft/s	4.84%	⚠ Surcharge	DS6-14

DP6

HGL Up	9.50'
HGL Down	9.29'
EGL Up	10.40'
EGL Down	10.19'
Invert Up	7.79'
Invert Down	7.57'

JM-6A

Structure Type	<none>
Rim Elevation	17.98'
HGL	10.74'
EGL	10.74'

Start Over Apply Cancel Help

Analysis Result AEP: 1/10 Profile Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP6	3.00'	49.209 cubic	8.233 ft/s	0.50%	✓ Normal	JM-6A
2	JP-6E	3.00'	49.287 cubic	8.234 ft/s	0.50%	✓ Normal	DS6
3	DP6-1	3.00'	47.358 cubic	8.208 ft/s	0.50%	⚠ Surcharge	DS6-1
4	DP6-2	3.00'	43.904 cubic	8.127 ft/s	0.50%	⚠ Surcharge	DS6-2
5	DP6-3	3.00'	40.609 cubic	8.021 ft/s	0.50%	⚠ Surcharge	DS6-3
6	DP6-4	3.00'	40.336 cubic	8.011 ft/s	0.50%	⚠ Surcharge	DS6-4
7	DP6-13	1.50'	3.675 cubic f	9.579 ft/s	4.14%	⚠ Surcharge	DS6-13
8	DP6-5	3.00'	36.644 cubic	7.861 ft/s	0.50%	⚠ Surcharge	DS6-5
9	DP6-6	3.00'	32.096 cubic	7.636 ft/s	0.50%	⚠ Surcharge	DS6-6
10	DP6-7	2.50'	27.101 cubic	7.201 ft/s	0.50%	⚠ Surcharge	DS6-7
11	DP6-8	2.50'	22.273 cubic	6.944 ft/s	0.50%	⚠ Surcharge	DS6-8
12	DP6-9	2.50'	20.868 cubic	6.847 ft/s	0.50%	⚠ Surcharge	DS6-9
13	DP6-10	2.50'	18.899 cubic	6.694 ft/s	0.50%	⚠ Surcharge	DS6-10
14	DP6-11	2.00'	16.246 cubic	6.270 ft/s	0.50%	✖ Flooded	DS6-11
15	DP6-12	1.50'	7.842 cubic f	5.438 ft/s	0.55%	✖ Flooded	DS6-12
16	DP6-14	1.50'	2.630 cubic f	9.188 ft/s	4.84%	⚠ Surcharge	DS6-14

DP6

HGL Up	10.15'
HGL Down	9.94'
EGL Up	11.21'
EGL Down	10.99'
Invert Up	7.79'
Invert Down	7.57'

JM-6A

Structure Type	<none>
Rim Elevation	17.98'
HGL	11.79'
EGL	11.79'

Start Over Apply Cancel Help

Analysis Result

AEP: 1/2

Profile

Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP7	3.00'	23.333 cubic	7.064 ft/s	0.50%	✓ Normal	JM-7A
2	JP-7E	3.00'	23.428 cubic	7.072 ft/s	0.50%	✓ Normal	DS7
3	DP7-1	2.00'	9.069 cubic f	5.579 ft/s	0.50%	⚠ Surcharge	DS7-1
4	DP7-2	2.00'	9.243 cubic f	5.605 ft/s	0.50%	✓ Normal	DS7-2
5	DP7-3	2.00'	8.515 cubic f	5.492 ft/s	0.50%	✓ Normal	DS7-3
6	DP7-4	2.00'	7.954 cubic f	5.398 ft/s	0.50%	✓ Normal	DS7-4
7	DP7-5	2.00'	6.997 cubic f	5.222 ft/s	0.50%	✓ Normal	DS7-5
8	DP7-6	2.00'	6.803 cubic f	5.183 ft/s	0.50%	✓ Normal	DS7-6
9	DP7-7	2.00'	6.353 cubic f	5.090 ft/s	0.50%	✓ Normal	DS7-7
10	DP7-8	1.00'	0.725 cubic f	2.938 ft/s	0.50%	✓ Normal	DS7-8
11	DP7-9	1.50'	4.632 cubic f	4.713 ft/s	0.50%	✓ Normal	DS7-9
12	DP7-10	1.50'	2.031 cubic f	3.795 ft/s	0.50%	✓ Normal	DS7-10
13	DP7-11	2.50'	14.891 cubic	6.315 ft/s	0.50%	⚠ Surcharge	DS7-11
14	DP7-12	2.50'	14.289 cubic	6.249 ft/s	0.50%	✓ Normal	DS7-12
15	DP7-13	2.50'	13.324 cubic	6.137 ft/s	0.50%	✓ Normal	DS7-13
16	DP7-14	2.50'	11.724 cubic	5.940 ft/s	0.50%	✓ Normal	DS7-14
17	DP7-15	2.00'	10.385 cubic	5.764 ft/s	0.50%	✓ Normal	DS7-15
18	DP7-16	2.00'	9.391 cubic f	5.628 ft/s	0.50%	✓ Normal	DS7-16
19	DP7-17	2.00'	7.082 cubic f	5.240 ft/s	0.50%	✓ Normal	DS7-17
20	DP7-18	1.50'	4.704 cubic f	4.727 ft/s	0.50%	✓ Normal	DS7-18
21	DP7-19	1.50'	2.494 cubic f	4.022 ft/s	0.50%	✓ Normal	DS7-19
22	DP7-20	1.50'	1.843 cubic f	3.694 ft/s	0.50%	✓ Normal	DS7-20

DP7	
HGL Up	12.21'
HGL Down	12.04'
EGL Up	12.99'
EGL Down	12.82'
Invert Up	10.79'
Invert Down	10.62'

JM-7A	
Structure Type	<none>
Rim Elevation	19.21'
HGL	13.22'
EGL	13.22'

Start Over

Apply

Cancel

Help

Analysis Result

AEP: 1/10

Profile

Report

Line	Pipe	Pipe Diameter	Pipe Flow	Velocity	Pipe Slope	Performance	Structure
1	DP7	3.00'	36.341 cubic	7.847 ft/s	0.50%	✓ Normal	JM-7A
2	JP-7E	3.00'	36.473 cubic	7.853 ft/s	0.50%	✓ Normal	DS7
3	DP7-1	2.00'	14.091 cubic	6.146 ft/s	0.50%	⚠ Surcharge	DS7-1
4	DP7-2	2.00'	14.333 cubic	6.164 ft/s	0.50%	⚠ Surcharge	DS7-2
5	DP7-3	2.00'	13.152 cubic	6.068 ft/s	0.50%	⚠ Surcharge	DS7-3
6	DP7-4	2.00'	12.242 cubic	5.980 ft/s	0.50%	⚠ Surcharge	DS7-4
7	DP7-5	2.00'	10.731 cubic	5.808 ft/s	0.50%	⚠ Surcharge	DS7-5
8	DP7-6	2.00'	10.525 cubic	5.782 ft/s	0.50%	⚠ Surcharge	DS7-6
9	DP7-7	2.00'	9.798 cubic f	5.685 ft/s	0.50%	⚠ Surcharge	DS7-7
10	DP7-8	1.00'	1.112 cubic f	3.297 ft/s	0.50%	⚠ Surcharge	DS7-8
11	DP7-9	1.50'	7.115 cubic f	5.141 ft/s	0.50%	⚠ Surcharge	DS7-9
12	DP7-10	1.50'	3.115 cubic f	4.263 ft/s	0.50%	⚠ Surcharge	DS7-10
13	DP7-11	2.50'	23.425 cubic	7.016 ft/s	0.50%	⚠ Surcharge	DS7-11
14	DP7-12	2.50'	22.427 cubic	6.954 ft/s	0.50%	⚠ Surcharge	DS7-12
15	DP7-13	2.50'	20.839 cubic	6.845 ft/s	0.50%	⚠ Surcharge	DS7-13
16	DP7-14	2.50'	18.260 cubic	6.646 ft/s	0.50%	⚠ Surcharge	DS7-14
17	DP7-15	2.00'	16.160 cubic	6.267 ft/s	0.50%	⚠ Surcharge	DS7-15
18	DP7-16	2.00'	14.574 cubic	6.182 ft/s	0.50%	⚠ Surcharge	DS7-16
19	DP7-17	2.00'	10.964 cubic	5.839 ft/s	0.50%	⚠ Surcharge	DS7-17
20	DP7-18	1.50'	7.266 cubic f	5.152 ft/s	0.50%	⚠ Surcharge	DS7-18
21	DP7-19	1.50'	3.840 cubic f	4.507 ft/s	0.50%	⚠ Surcharge	DS7-19
22	DP7-20	1.50'	2.826 cubic f	4.154 ft/s	0.50%	⚠ Surcharge	DS7-20

DP7	
HGL Up	12.66'
HGL Down	12.49'
EGL Up	13.62'
EGL Down	13.45'
Invert Up	10.79'
Invert Down	10.62'

JM-7A	
Structure Type	<none>
Rim Elevation	19.21'
HGL	14.20'
EGL	14.20'

Start Over

Apply

Cancel

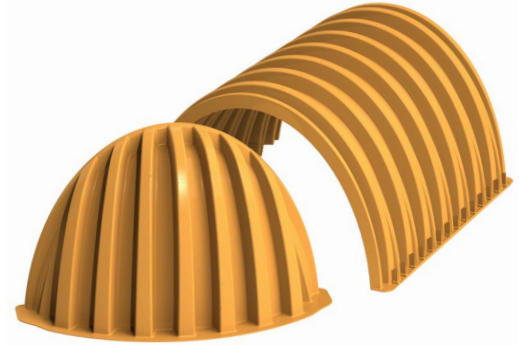
Help

Appendix D

Stormwater Practice Specifications

StormTech[®] MC-3500 Chamber

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots, thus maximizing land usage for private (commercial) and public applications. StormTech chambers can also be used in conjunction with Green Infrastructure, thus enhancing the performance and extending the service life of these practices.



Nominal Chamber Specifications (not to scale)

Size (L x W x H)
90" x 77" x 45"
2286 mm x 1956 mm x 1143 mm

Chamber Storage
109.9 ft³ (3.11 m³)

Min. Installed Storage*
175.0 ft³ (4.96 m³)

Weight
134 lbs (60.8 kg)

Shipping
15 chambers/pallet
7 end caps/pallet
7 pallets/truck

*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below chambers, 6" (150 mm) of stone between chambers/ end caps and 40% stone porosity.

Nominal End Cap Specifications (not to scale)

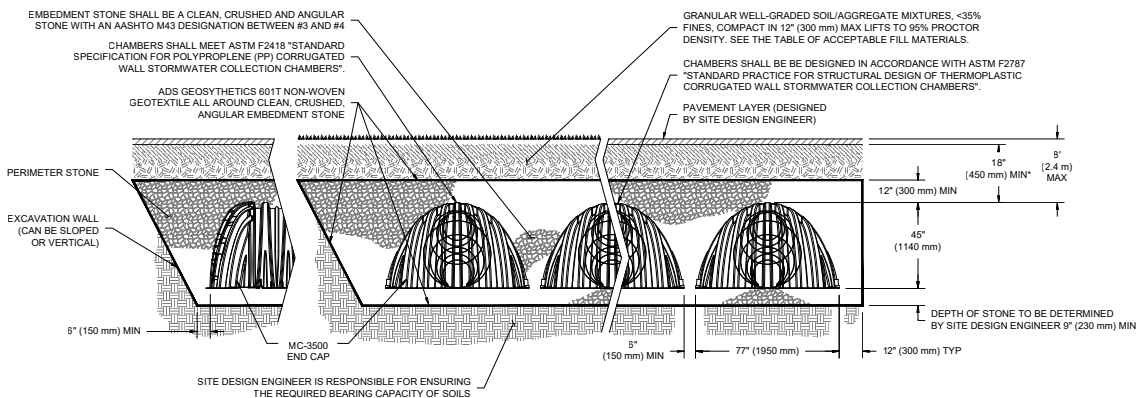
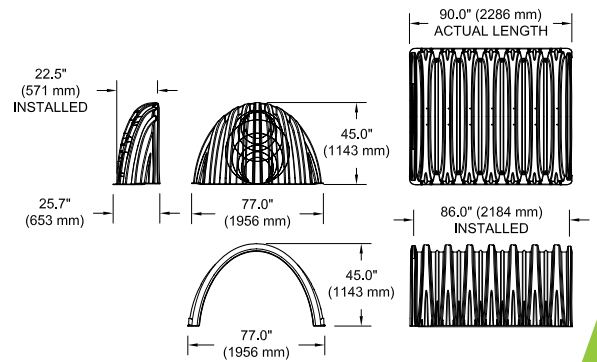
Size (L x W x H)
26.5" x 71" x 45.1"
673 mm x 1803 mm x 1145 mm

End Cap Storage
14.9 ft³ (0.42 m³)

Min. Installed Storage*
45.1 ft³ (1.28 m³)

Weight
49 lbs (22.2 kg)

*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below, 6" (150 mm) of stone perimeter, 6" (150 mm) of stone between chambers/ end caps and 40% stone porosity.



*MINIMUM COVER TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY OCCUR, INCREASE COVER TO 24" (600 mm).

StormTech MC-3500 Specifications

Storage Volume Per Chamber

	Bare Chamber Storage ft ³ (m ³)	Chamber and Stone Foundation Depth in. (mm)			
		9 in (230 mm)	12 in (300 mm)	15 in (375 mm)	18 in (450 mm)
Chamber	109.9 (3.11)	175.0 (4.96)	179.9 (5.09)	184.9 (5.24)	189.9 (5.38)
End Cap	14.9 (0.42)	45.1 (1.28)	46.6 (1.32)	48.3 (1.37)	49.9 (1.41)

Note: Assumes 6" (150 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume.

Amount of Stone Per Chamber

English Tons (yds ³)	Stone Foundation Depth			
	9 in	12 in	15 in	18 in
Chamber	8.5 (6.0)	9.1 (6.5)	9.7 (6.9)	10.4 (7.4)
End Cap	3.9 (2.8)	4.1 (2.9)	4.3 (3.1)	4.5 (3.2)
Metric Kilograms (m ³)	230 mm	300 mm	375 mm	450 mm
Chamber	7711 (4.6)	8255 (5.0)	8800 (5.3)	9435 (5.7)
End Cap	3538 (2.1)	3719 (2.2)	3901 (2.4)	4082 (2.5)

Note: Assumes 12" (300 mm) of stone above and 6" (150 mm) row spacing and 6" (150 mm) of perimeter stone in front of end caps.

Volume Excavation Per Chamber yd³ (m³)

	Stone Foundation Depth			
	9 in (230 mm)	12 in (300 mm)	15 in (375mm)	18 in (450 mm)
Chamber	11.9 (9.1)	12.4 (9.5)	12.8 (9.8)	13.3 (10.2)
End Cap	4.0 (3.1)	4.1 (3.3)	4.3 (3.3)	4.4 (3.4)

Note: Assumes 6" (150 mm) of separation between chamber rows and 24" (600 mm) of cover. The volume of excavation will vary as depth of cover increases.

Working on a project?

Visit us at www.stormtech.com and utilize the Design Tool

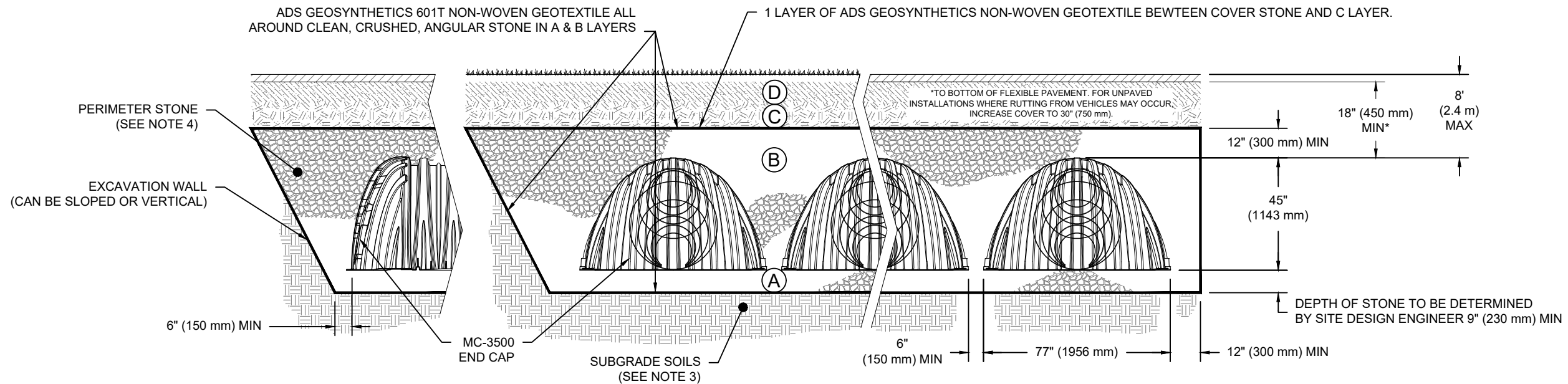


ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

MATERIAL LOCATION		DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
C	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 24" (600 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 12" (300 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.
B	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 ¹ 3, 4	NO COMPACTION REQUIRED.
A	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 ¹ 3, 4	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. ^{2,3}

PLEASE NOTE:

- THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
- STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
- WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.
- ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.



*FOR COVER DEPTHS GREATER THAN 8.0' (2.4 m) PLEASE CONTACT STORMTECH

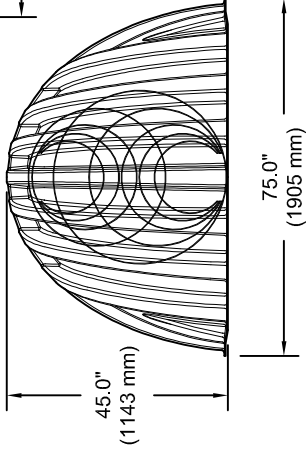
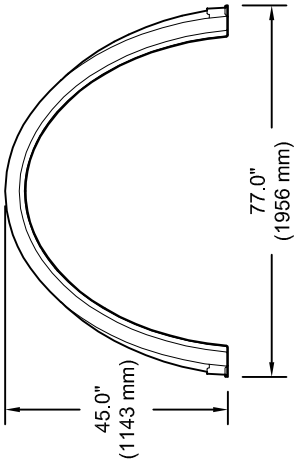
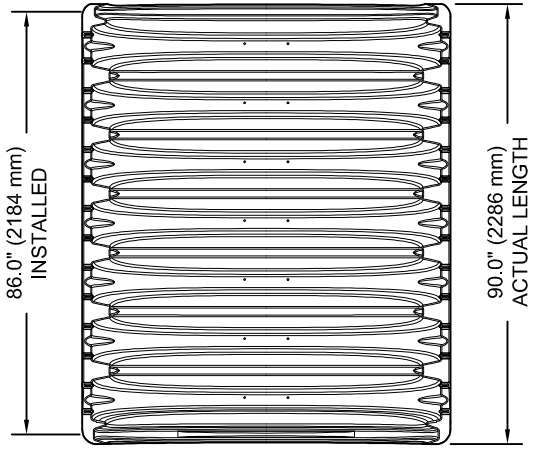
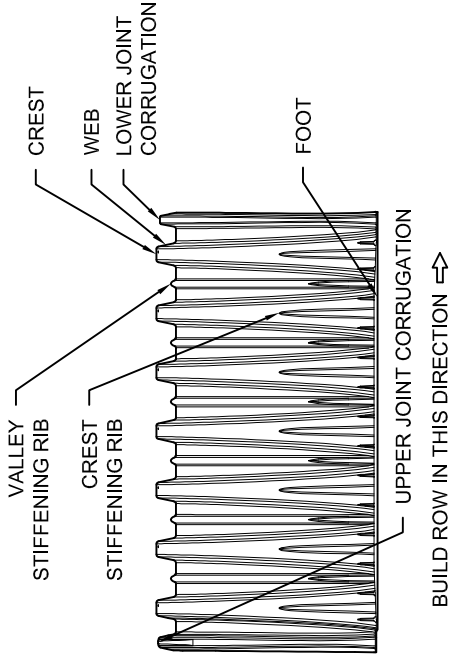
NOTES:

- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418-16a, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 45x76 DESIGNATION SS.
- MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 500 LBS/IN/IN. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

MC-3500	STANDARD CROSS SECTION	DATE: 05-10-19	DRAWN: KR	CHECKED: KR
DESCRIPTION		DATE	DRWN	CHKD
THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.				
		70 INWOOD ROAD, SUITE 3 ROCKY HILL CT 06867 860-525-8188 888-892-2694 WWW.STORMTECH.COM		
		4640 TRUEMAN BLVD HILLIARD, OH 43026 ADVANCED DRAINAGE SYSTEMS, INC.		
1		SHEET		1
1		OF		1

MC-3500 TECHNICAL SPECIFICATION

NTS



NOMINAL CHAMBER SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH)
 CHAMBER STORAGE
 MINIMUM INSTALLED STORAGE*
 WEIGHT

77.0" X 45.0" X 86.0"
 109.9 CUBIC FEET
 175.0 CUBIC FEET
 134 lbs.

(1956 mm X 1143 mm X 2184 mm)
 (3.11 m³)
 (4.96 m³)
 (60.8 kg)

NOMINAL END CAP SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH)
 END CAP STORAGE
 MINIMUM INSTALLED STORAGE*
 WEIGHT

75.0" X 45.0" X 22.2"
 14.9 CUBIC FEET
 45.1 CUBIC FEET
 49 lbs.

(1905 mm X 1143 mm X 564 mm)
 (0.42 m³)
 (1.28 m³)
 (22.2 kg)

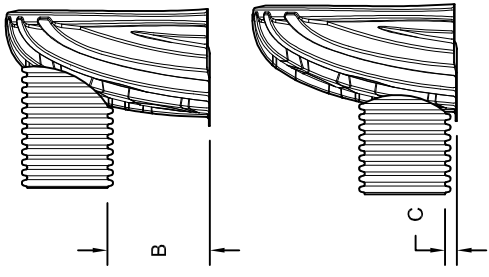
*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION, 6" (152 mm) OF STONE BETWEEN CHAMBERS, 6" (152 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY

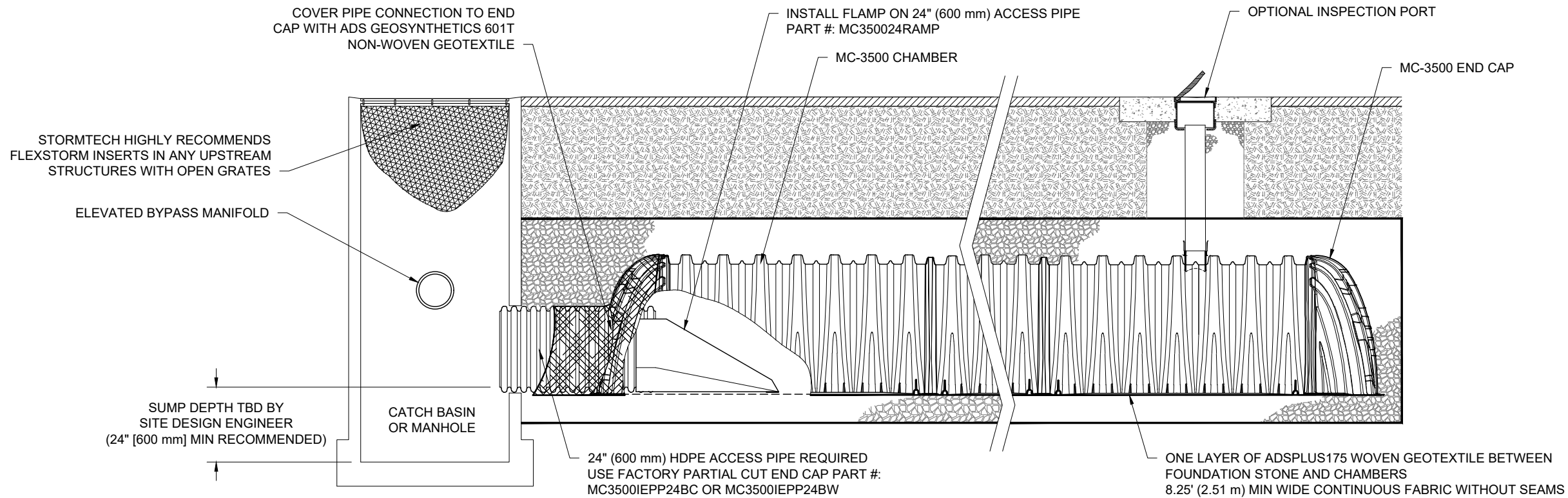
STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B"
 STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T"
 END CAPS WITH A WELDED CROWN PLATE END WITH "C"
 END CAPS WITH A PREFABRICATED WELDED STUB END WITH "W"

PART #	STUB	B	C
MC3500IEPP06T	6" (150 mm)	33.21" (844 mm)	---
MC3500IEPP06B	6" (150 mm)	---	0.66" (17 mm)
MC3500IEPP08T	8" (200 mm)	31.16" (791 mm)	---
MC3500IEPP08B	8" (200 mm)	---	0.81" (21 mm)
MC3500IEPP10T	10" (250 mm)	29.04" (738 mm)	---
MC3500IEPP10B	10" (250 mm)	---	0.93" (24 mm)
MC3500IEPP12T	12" (300 mm)	26.36" (670 mm)	---
MC3500IEPP12B	12" (300 mm)	---	1.35" (34 mm)
MC3500IEPP15T	15" (375 mm)	23.39" (594 mm)	---
MC3500IEPP15B	15" (375 mm)	---	1.50" (38 mm)
MC3500IEPP18TC	18" (450 mm)	20.03" (509 mm)	---
MC3500IEPP18TW	18" (450 mm)	---	---
MC3500IEPP18BC	18" (450 mm)	---	1.77" (45 mm)
MC3500IEPP18BW	18" (450 mm)	---	---
MC3500IEPP24TC	24" (600 mm)	14.48" (368 mm)	---
MC3500IEPP24TW	24" (600 mm)	---	---
MC3500IEPP24BC	24" (600 mm)	---	2.06" (52 mm)
MC3500IEPP24BW	24" (600 mm)	---	---
MC3500IEPP30BC	30" (750 mm)	---	2.75" (70 mm)

NOTE: ALL DIMENSIONS ARE NOMINAL

CUSTOM PRECURED INVERTS ARE AVAILABLE UPON REQUEST.
 INVENTORIED MANIFOLDS INCLUDE 12-24" (300-600 mm) SIZE ON SIZE AND 15-48" (375-1200 mm) ECCENTRIC MANIFOLDS. CUSTOM INVERT LOCATIONS ON THE MC-3500 END CAP CUT IN THE FIELD ARE NOT RECOMMENDED FOR PIPE SIZES GREATER THAN 10" (250 mm). THE INVERT LOCATION IN COLUMN 'B' ARE THE HIGHEST POSSIBLE FOR THE PIPE SIZE.





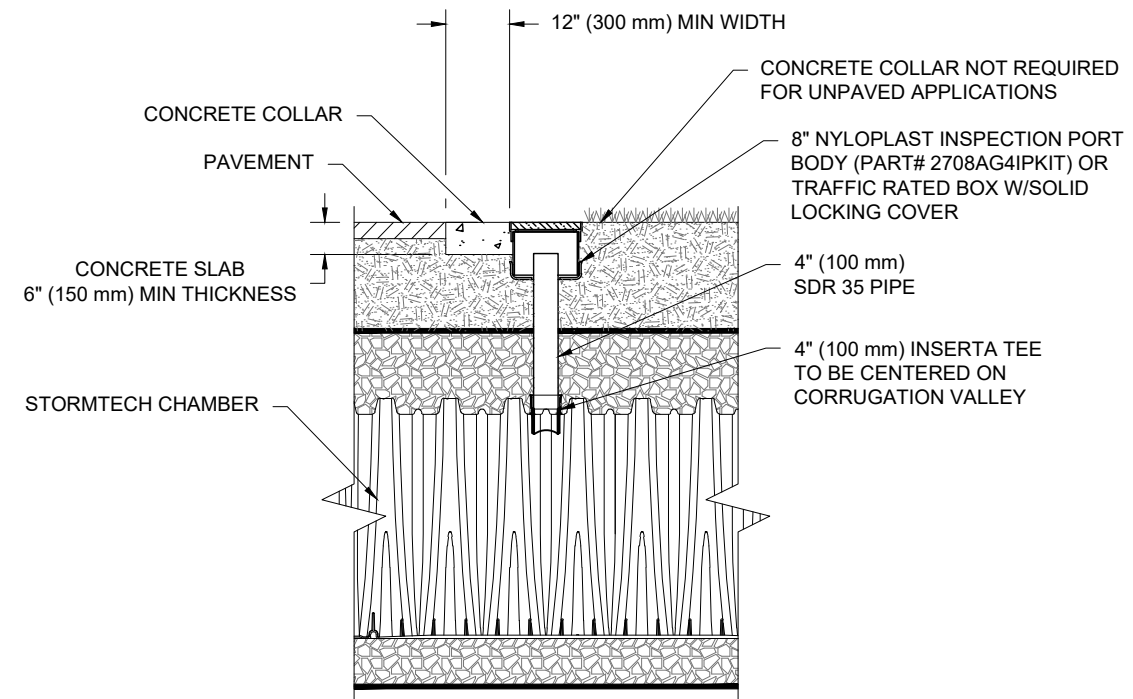
MC-3500 ISOLATOR ROW PLUS DETAIL
NTS

INSPECTION & MAINTENANCE

- STEP 1) INSPECT ISOLATOR ROW PLUS FOR SEDIMENT
- A. INSPECTION PORTS (IF PRESENT)
 - A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
 - A.2. REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
 - A.3. USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG
 - A.4. LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
 - A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
 - B. ALL ISOLATOR PLUS ROWS
 - B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
 - B.2. USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
 - B.3. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- STEP 2) CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
- A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - B. APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



NOTE:
INSPECTION PORTS MAY BE CONNECTED THROUGH ANY CHAMBER CORRUGATION VALLEY.

4" PVC INSPECTION PORT DETAIL
(MC SERIES CHAMBER)
NTS

MC-3500	
ISOLATOR ROW PLUS DETAILS	
DATE: 08/26/20	DRAWN: ALI
PROJECT #: ----	CHECKED: ALI
	DESCRIPTION
	DATE
	DRWN
	CHKD

StormTech
Advanced Drainage Systems, Inc.

520 CROMWELL AVENUE | ROCKY HILL, CT | 06067
860-528-8188 | 888-892-2694 | WWW.STORMTECH.COM

4640 TRUEMAN BLVD
HILLIARD, OH 43026

ADS
ADVANCED DRAINAGE SYSTEMS, INC.

THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.

MC-4500 CHAMBER

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots, thus maximizing land usage for private (commercial) and public applications. StormTech chambers can also be used in conjunction with Green Infrastructure, thus enhancing the performance and extending the service life of these practices.

STORMTECH MC-4500 CHAMBER (not to scale)

Nominal Chamber Specifications

Size (L x W x H)
52" x 100" x 60"
1321 mm x 2540 mm x 1524 mm

Chamber Storage
106.5 ft³ (3.01 m³)

Min. Installed Storage*
162.6 ft³ (4.60 m³)

Weight
Nominal 125 lbs (56.7 kg)

Shipping
7 chambers/pallet
5 end caps/pallet
11 pallets/truck

*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below chambers, 9" (230 mm) of stone between chambers/end caps and 40% stone porosity.

STORMTECH MC-4500 END CAP (not to scale)

Nominal End Cap Specifications

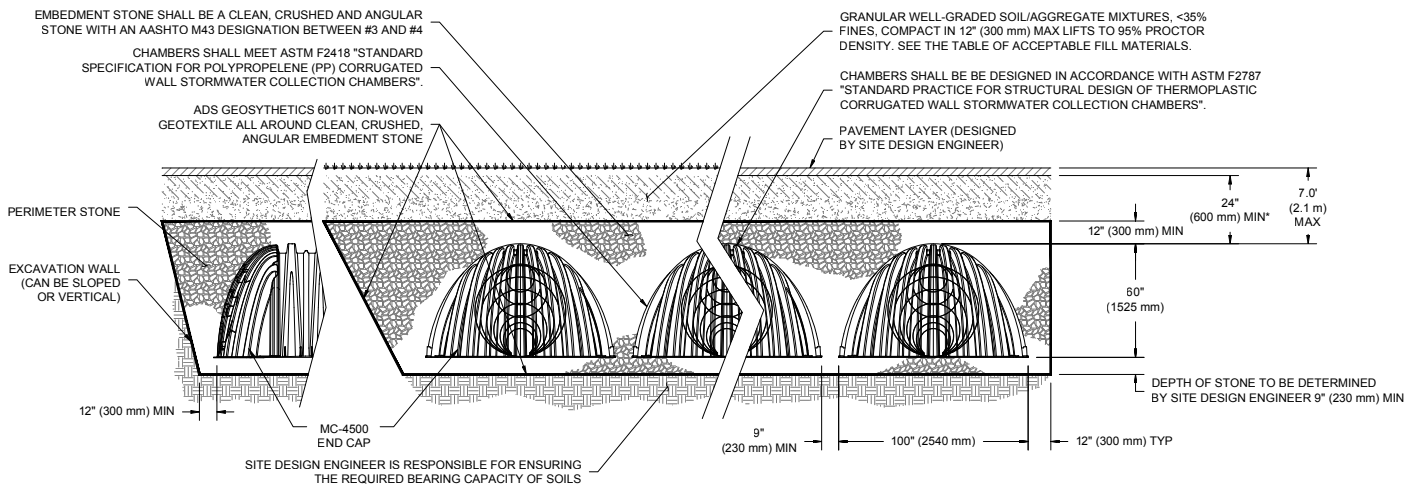
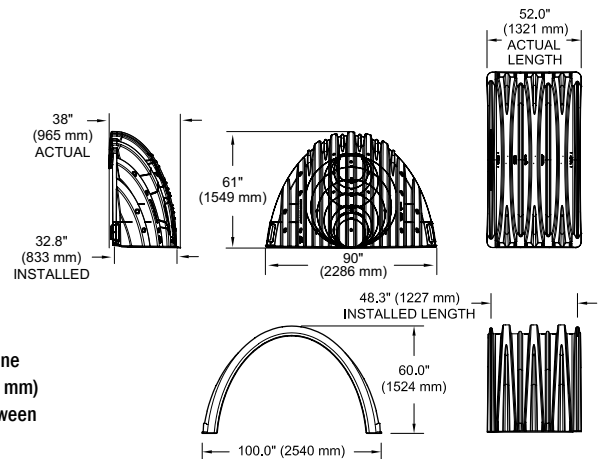
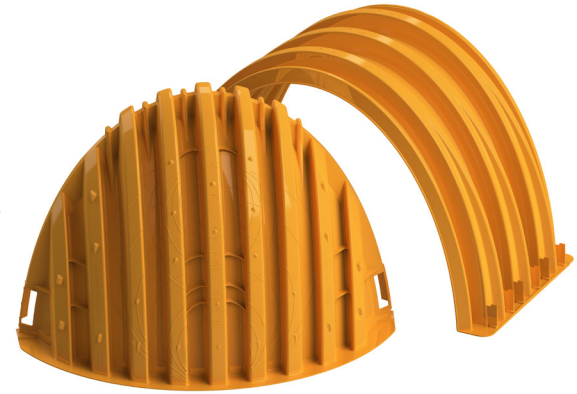
Size (L x W x H)
38" x 90" x 61"
965 mm x 2286 mm x 1549 mm

End Cap Storage
39.5 ft³ (1.12 m³)

Min. Installed Storage*
115.3 ft³ (3.26 m³)

Weight
Nominal 90.0 lbs (40.8 kg)

*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below, 12" (300 mm) of stone perimeter, 9" (230 mm) of stone between chambers/end caps and 40% stone porosity.



*MINIMUM COVER TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY OCCUR, INCREASE COVER TO 30" (750 mm).

MC-4500 CHAMBER SPECIFICATIONS

STORAGE VOLUME PER CHAMBER FT³ (M³)

	Bare Chamber Storage ft ³ (m ³)	Chamber and Stone Foundation Depth in. (mm)			
		9" (230 mm)	12" (300 mm)	15" (375 mm)	18" (450 mm)
MC-4500 Chamber	106.5 (3.01)	162.6 (4.60)	166.3 (4.71)	169.9 (4.81)	173.6 (4.91)
MC-4500 End Cap	39.5 (1.12)	115.3 (3.26)	118.6 (3.36)	121.9 (3.45)	125.2 (3.54)

Note: Assumes 9" (230 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume. End cap volume assumes 12" (300 mm) stone perimeter in front of end cap.

AMOUNT OF STONE PER CHAMBER

ENGLISH TONS (yds ³)	Stone Foundation Depth			
	9"	12"	15"	18"
MC-4500 Chamber	7.4 (5.2)	7.8 (5.5)	8.3 (5.9)	8.8 (6.2)
MC-4500 End Cap	9.8 (7.0)	10.2 (7.3)	10.6 (7.6)	11.1 (7.9)
METRIC KILOGRAMS (m ³)	230 mm	300 mm	375 mm	450 mm
MC-4500 Chamber	6713 (4.0)	7076 (4.2)	7529 (4.5)	7983 (4.7)
MC-4500 End Cap	8890 (5.3)	9253 (5.5)	9616 (5.8)	10069 (6.0)

Note: Assumes 12" (300 mm) of stone above and 9" (230 mm) row spacing and 12" (300 mm) of perimeter stone in front of end caps.

VOLUME EXCAVATION PER CHAMBER YD³ (M³)

	Stone Foundation Depth			
	9" (230 mm)	12" (300 mm)	15" (375mm)	18" (450 mm)
MC-4500 Chamber	10.5 (8.0)	10.8 (8.3)	11.2 (8.5)	11.5 (8.8)
MC-4500 End Cap	9.7 (7.4)	10.0 (7.6)	10.3 (7.9)	10.6 (8.1)

Note: Assumes 9" (230 mm) of separation between chamber rows, 12" (300 mm) of perimeter in front of the end caps, and 24" (600 mm) of cover. The volume of excavation will vary as depth of cover increases.



Working on a project?
 Visit us at www.stormtech.com
 and utilize the StormTech Design Tool

For more information on the StormTech MC-4500 Chamber and other ADS products, please contact our Customer Service Representatives at 1-800-821-6710

THE MOST **ADVANCED** NAME IN WATER MANAGEMENT SOLUTIONS™

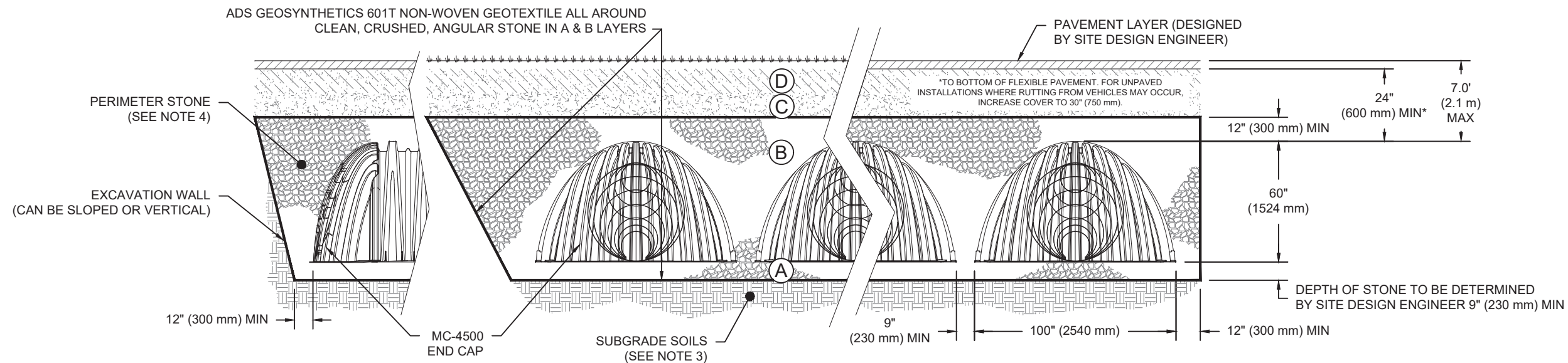
Advanced Drainage Systems, Inc.
 4640 Trueman Blvd., Hilliard, OH 43026
 1-800-821-6710 www.ads-pipe.com

ACCEPTABLE FILL MATERIALS: STORMTECH MC-4500 CHAMBER SYSTEMS

MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
C	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	AASHTO M145' A-1, A-2-4, A-3 OR AASHTO M43' 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 24" (600 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 12" (300 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.
B	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	AASHTO M43' 3, 4	NO COMPACTION REQUIRED.
A	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	AASHTO M43' 3, 4	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. ^{2,3}

PLEASE NOTE:

1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.
4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.



*FOR COVER DEPTHS GREATER THAN 7.0' (2.1 m) PLEASE CONTACT STORMTECH

NOTES:

1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418-16a, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 60x101
2. MC-4500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 500 LBS/IN/IN. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

MC-4500

STANDARD CROSS SECTION

DATE: 05-10-19

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PROJECT #:

CHECKED: KR

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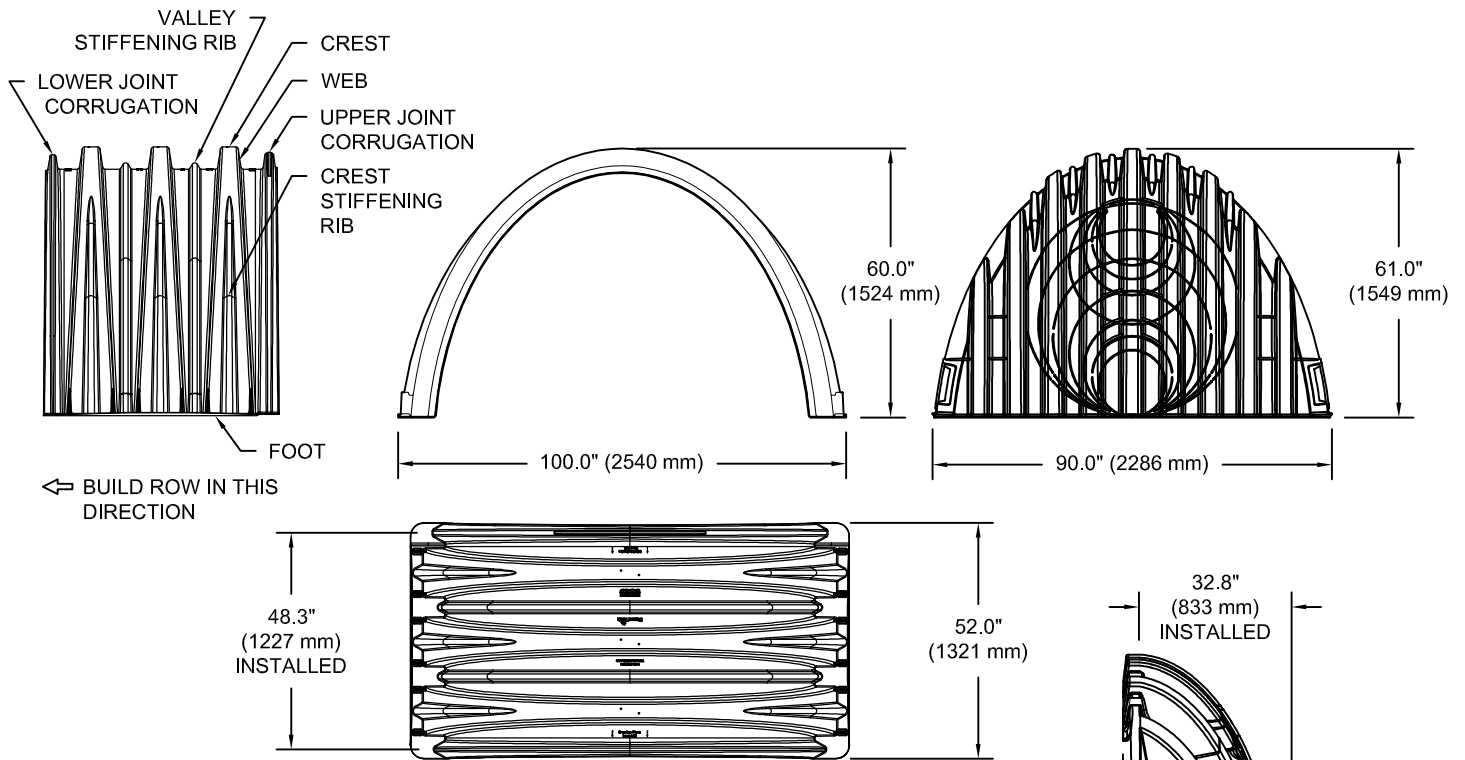
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MC-4500 TECHNICAL SPECIFICATION

NTS



NOMINAL CHAMBER SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH)	100.0" X 60.0" X 48.3"	(2540 mm X 1524 mm X 1227 mm)
CHAMBER STORAGE	106.5 CUBIC FEET	(3.01 m ³)
MINIMUM INSTALLED STORAGE*	162.6 CUBIC FEET	(4.60 m ³)
WEIGHT (NOMINAL)	125.0 lbs.	(56.7 kg)

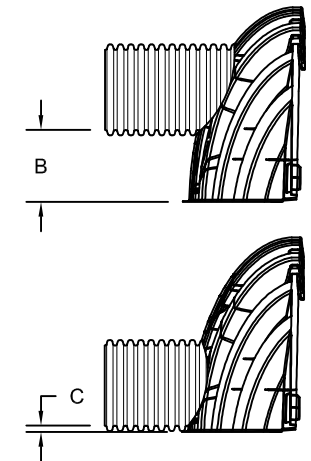
NOMINAL END CAP SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH)	90.0" X 61.0" X 32.8"	(2286 mm X 1549 mm X 833 mm)
END CAP STORAGE	39.5 CUBIC FEET	(1.12 m ³)
MINIMUM INSTALLED STORAGE*	115.3 CUBIC FEET	(3.26 m ³)
WEIGHT (NOMINAL)	90 lbs.	(40.8 kg)

*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION AND BETWEEN CHAMBERS, 12" (305 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY.

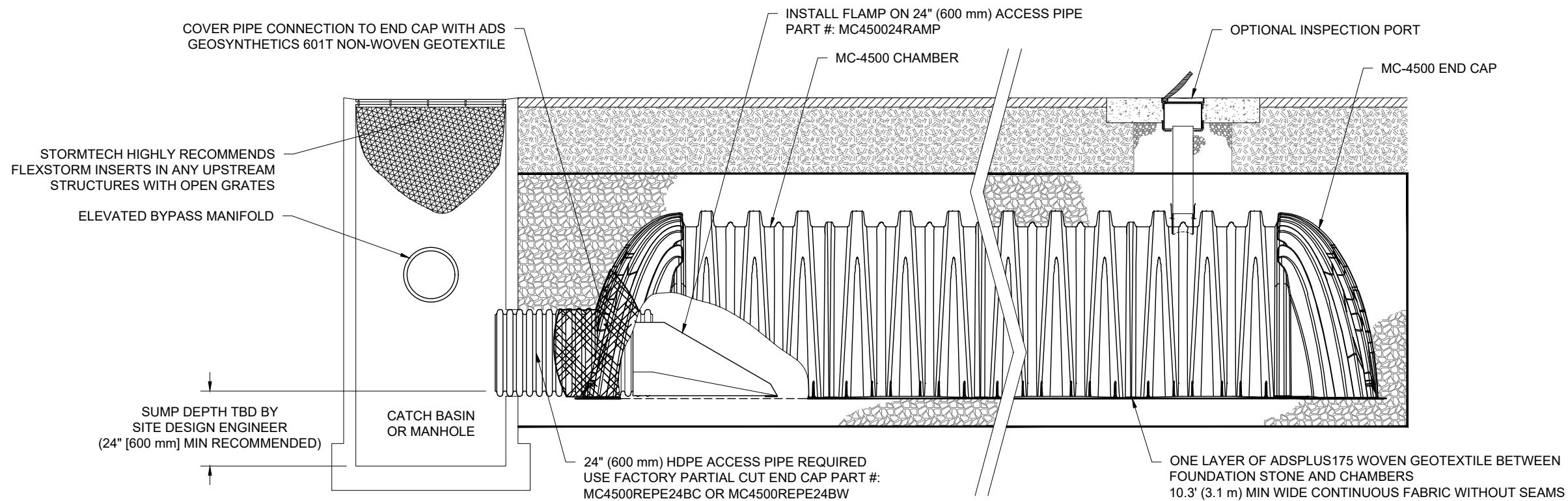
PARTIAL CUT HOLES AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B"
 PARTIAL CUT HOLES AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T"
 END CAPS WITH A PREFABRICATED WELDED STUB END WITH "W"

PART #	STUB	B	C
MC4500IEPP06T	6" (150 mm)	42.54" (1081 mm)	---
MC4500IEPP06B		---	0.86" (22 mm)
MC4500IEPP08T	8" (200 mm)	40.50" (1029 mm)	---
MC4500IEPP08B		---	1.01" (26 mm)
MC4500IEPP10T	10" (250 mm)	38.37" (975 mm)	---
MC4500IEPP10B		---	1.33" (34 mm)
MC4500IEPP12T	12" (300 mm)	35.69" (907 mm)	---
MC4500IEPP12B		---	1.55" (39 mm)
MC4500IEPP15T	15" (375 mm)	32.72" (831 mm)	---
MC4500IEPP15B		---	1.70" (43 mm)
MC4500IEPP18T	18" (450 mm)	29.36" (746 mm)	---
MC4500IEPP18TW		---	---
MC4500IEPP18B		---	1.97" (50 mm)
MC4500IEPP18BW	24" (600 mm)	---	---
MC4500IEPP24T		23.05" (585 mm)	---
MC4500IEPP24TW		---	---
MC4500IEPP24B		---	2.26" (57 mm)
MC4500IEPP24BW	30" (750 mm)	---	2.95" (75 mm)
MC4500IEPP30BW		---	2.95" (75 mm)
MC4500IEPP36BW	36" (900 mm)	---	3.25" (83 mm)
MC4500IEPP42BW	42" (1050 mm)	---	3.55" (90 mm)



CUSTOM PRECORED INVERTS ARE AVAILABLE UPON REQUEST. INVENTORIED MANIFOLDS INCLUDE 12-24" (300-600 mm) SIZE ON SIZE AND 15-48" (375-1200 mm) ECCENTRIC MANIFOLDS. CUSTOM INVERT LOCATIONS ON THE MC-4500 END CAP CUT IN THE FIELD ARE NOT RECOMMENDED FOR PIPE SIZES GREATER THAN 10" (250 mm). THE INVERT LOCATION IN COLUMN 'B' ARE THE HIGHEST POSSIBLE FOR THE PIPE SIZE.

NOTE: ALL DIMENSIONS ARE NOMINAL



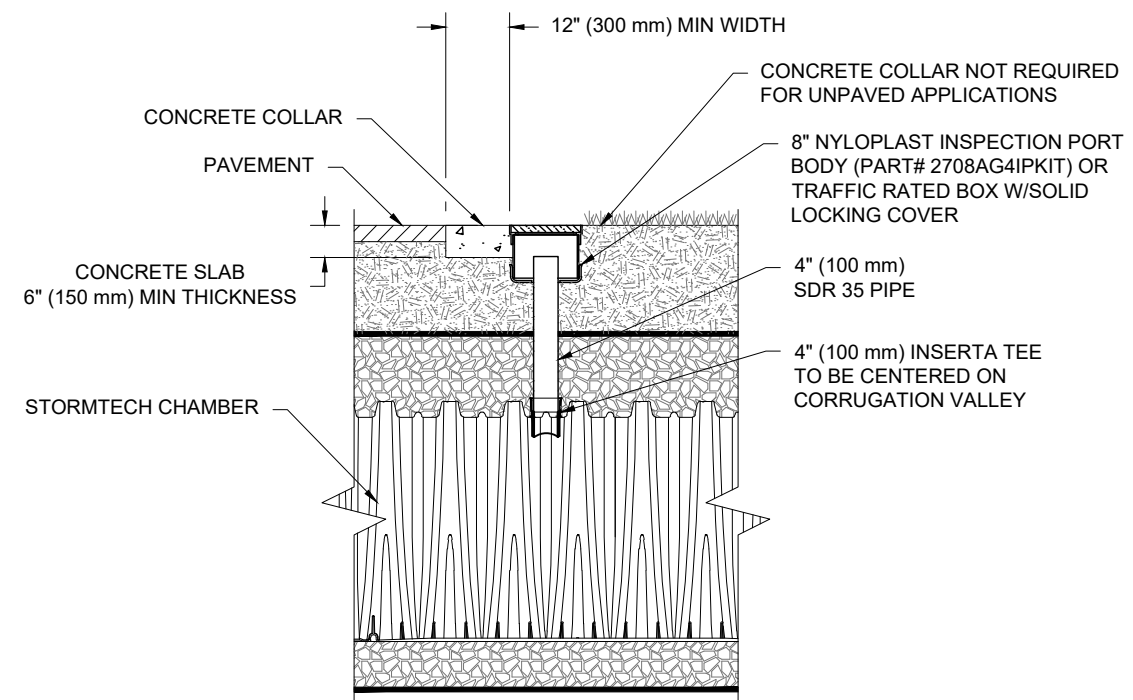
MC-4500 ISOLATOR ROW PLUS DETAIL
NTS

INSPECTION & MAINTENANCE

- STEP 1) INSPECT ISOLATOR ROW PLUS FOR SEDIMENT
- A. INSPECTION PORTS (IF PRESENT)
 - A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
 - A.2. REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
 - A.3. USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG
 - A.4. LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
 - A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
 - B. ALL ISOLATOR PLUS ROWS
 - B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
 - B.2. USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
 - B.3. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- STEP 2) CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
- A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - B. APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



NOTE:
INSPECTION PORTS MAY BE CONNECTED THROUGH ANY CHAMBER CORRUGATION VALLEY.

4" PVC INSPECTION PORT DETAIL
(MC SERIES CHAMBER)
NTS

MC-4500	ISOLATOR ROW PLUS DETAILS	DATE: 08/26/20	DRAWN: ALI	CHECKED: ALI	
		PROJECT #: ----			
DATE	DRWN	CHKD	DESCRIPTION		
		520 CROMWELL AVENUE ROCKY HILL, CT 06067 860-528-8188 888-892-2694 WWW.STORMTECH.COM			
		4640 TRUEMAN BLVD HILLIARD, OH 43026 ADVANCED DRAINAGE SYSTEMS, INC.			
THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.					
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Jellyfish[®] Filter

Stormwater Treatment



The experts you need to solve your stormwater challenges



Contech is the leader in stormwater solutions, helping engineers, contractors and owners with infrastructure and land development projects throughout North America.

With our responsive team of stormwater experts, local regulatory expertise and flexible solutions, Contech is the trusted partner you can count on for stormwater management solutions.

Your Contech Team



STORMWATER CONSULTANT

It's my job to recommend the best solution to meet permitting requirements.



STORMWATER DESIGN ENGINEER

I work with consultants to design the best approved solution to meet your project's needs.



REGULATORY MANAGER

I understand the local stormwater regulations and what solutions will be approved.



SALES ENGINEER

I make sure our solutions meet the needs of the contractor during construction.

Contech is your partner in stormwater management solutions



Setting new standards in Stormwater Treatment – Jellyfish® Filter

The Jellyfish Filter has been tested in the field and laboratory, and has received approval from numerous stormwater regulatory agencies.

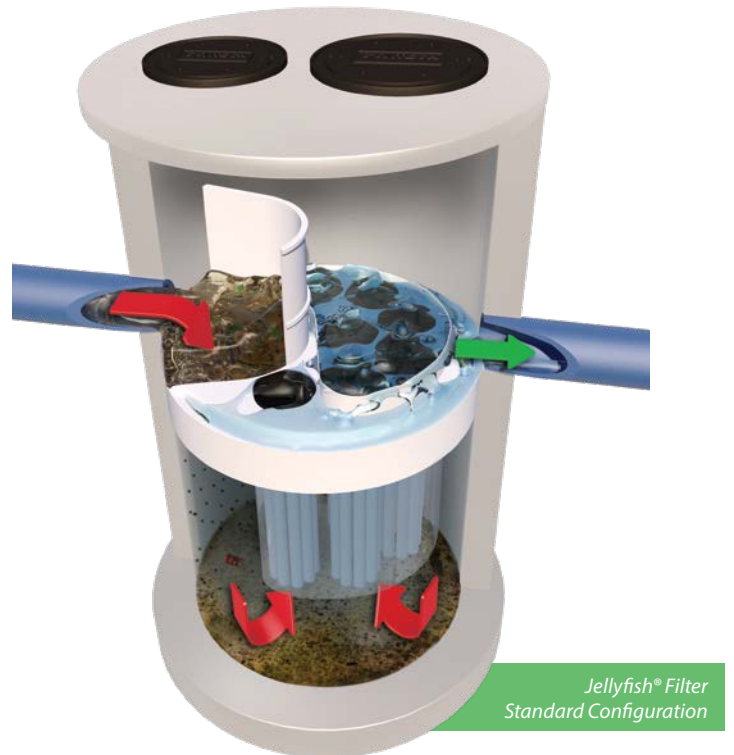
The Jellyfish Filter is a stormwater quality treatment technology featuring high flow pretreatment and membrane filtration in a compact stand-alone system. Jellyfish removes floatables, trash, oil, debris, TSS, fine silt-sized particles, and a high percentage of particulate-bound pollutants; including phosphorus, nitrogen, metals and hydrocarbons. The high surface area membrane cartridges, combined with up-flow hydraulics, frequent, passive backwashing, and rinseable/reusable cartridges ensure long-lasting performance.

Jellyfish® Filter

How the Jellyfish® Filter Treats Stormwater

Tested in the field and laboratory ...

- Stormwater enters the Jellyfish through the inlet pipe and traps floating pollutants behind the maintenance access wall and below the cartridge deck.
- Water is conveyed below the cartridge deck where a separation skirt around the cartridges isolates oil, trash and debris outside the filtration zone.
- Water is directed to the filtration zone and up through the top of the cartridge where it exits via the outlet pipe.
- The membrane filters provide a very large surface area to effectively remove fine sand and silt-sized particles, and a high percentage of particulate-bound pollutants such as nitrogen, phosphorus, metals, and hydrocarbons while ensuring long-lasting treatment.
- As influent flow subsides, the water in the backwash pool flows back into the lower chamber. This passive backwash extends cartridge life.
- The draindown cartridge(s) located outside the backwash pool enables water levels to balance.

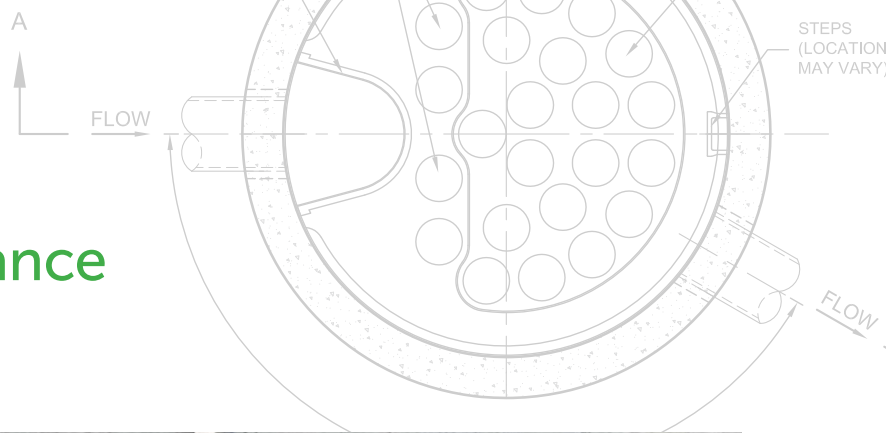


Learn More:
www.ContechES.com/jellyfish



Pretreat bioretention or infiltration with Jellyfish to extend service life.

Jellyfish® Filter Performance Testing Results



APPLICATION TIPS

- The Peak Diversion Jellyfish provides treatment and high-flow bypass in one structure, eliminating the need for a separate bypass structure.
- LID and GI are complemented by filtration solutions, as they help keep sites free from fine sediments that can impede performance, remove unsightly trash, and provide a single point of maintenance.
- Selecting a filter with a long maintenance cycle and low maintenance cost will result in healthy waterways and happy property owners.



The pleated tentacles of the Jellyfish® Filter provide a large surface area for pollutant removal.

POLLUTANT OF CONCERN	% REMOVAL
Total Trash	99%
Total Suspended Solids (TSS)	89%
Total Phosphorus (TP)	59%
Total Nitrogen (TN)	51%
Total Copper (TCu)	> 50%
Total Zinc (TZn)	> 50%



Sources:
 TARP II Field Study – 2012 JF 4-2-1 Configuration
 MRDC Floatables Testing – 2008 JF6-6-1 Configuration

Jellyfish[®] Filter Features and Benefits

FEATURE	BENEFITS
High surface area membrane filtration	Low flux rate promotes cake filtration and slows membrane occlusion
High design treatment flow rate per cartridge (up to 80 gpm (5 L/s))	Compact system with a small footprint, lower construction cost
Low driving head (typically 18 inches or less (457 mm))	Design flexibility, lower construction cost
Lightweight cartridges with passive backwash	Easy maintenance and low life-cycle cost

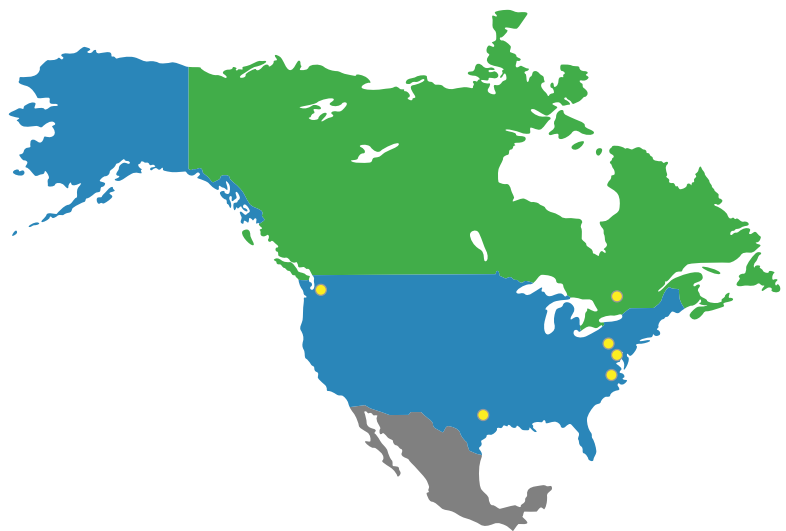


The Jellyfish Filter can be configured in a manhole, catch basin, or vault.

Select Jellyfish[®] Filter Certifications and Verifications

The Jellyfish Filter has been reviewed by numerous state and federal programs, including:

- Washington State Department of Ecology (TAPE) GULD – BASIC, Phosphorus
- Virginia Department of Environmental Quality (VA DEQ)
- Texas Commission of Environmental Quality (TCEQ)
- Canada ISO 14034 Environmental Management – Environmental Technology Verification (ETV)
- Philadelphia Water District (PWD)
- Maryland Department of the Environment (MD DOE)

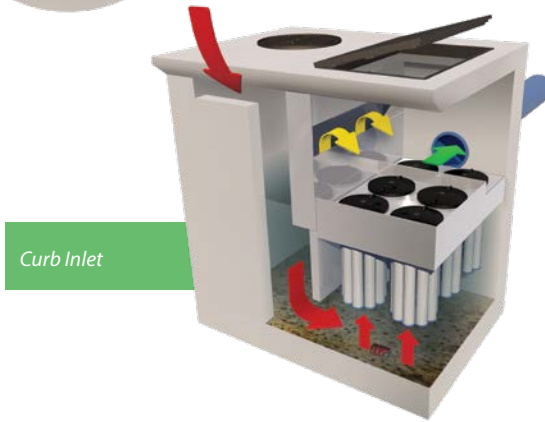
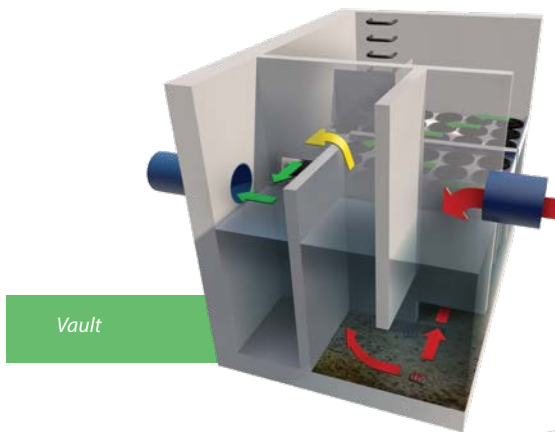
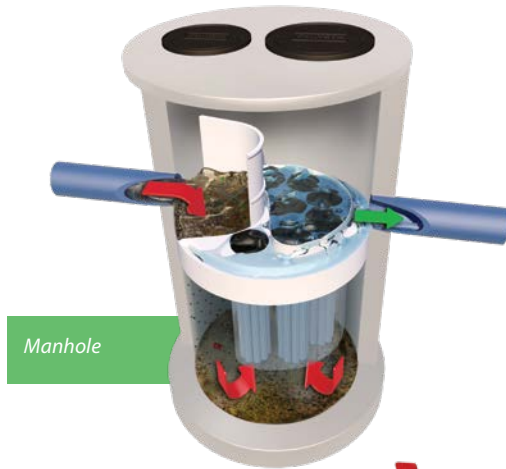
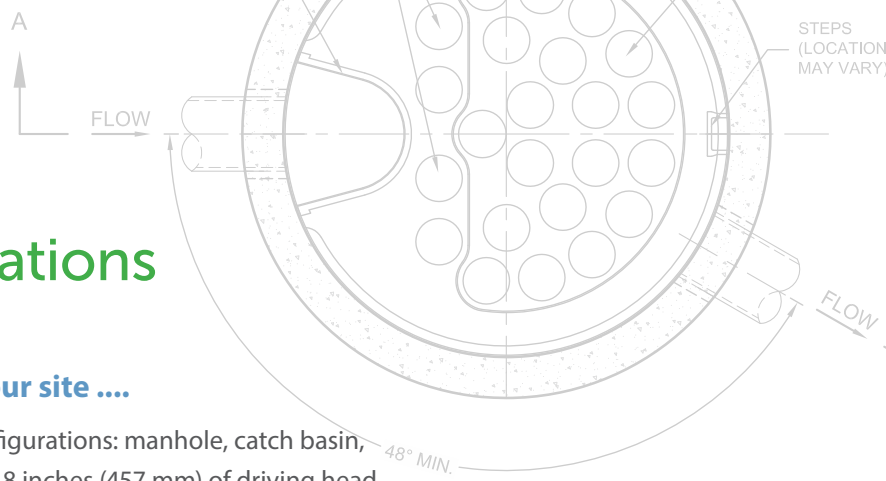


Field tested and performance verified

Jellyfish[®] Filter Configurations

Multiple system configurations to optimize your site

The Jellyfish Filter can be manufactured in a variety of configurations: manhole, catch basin, vault, fiberglass tank, or custom configurations. Typically, 18 inches (457 mm) of driving head is designed into the system. For low drop sites, the designed driving head can be less.



Jellyfish[®] Filter Maintenance

- Jellyfish Filter cartridges are light weight and reusable
- Maintenance of the filter cartridges is performed by removing, rinsing and reusing the cartridge tentacles.
- Vacuum extraction of captured pollutants in the sump is recommended at the same time.
- Full cartridge replacement intervals differ by site due to varying pollutant loading and type, and maintenance frequency. Replacement is anticipated every 2-5 years.
- Contech[®] has created a network of Certified Maintenance Providers to provide maintenance on stormwater BMP's.



The Jellyfish[®] Filter tentacle is light and easy to clean.

A partner you can rely on



STORMWATER
SOLUTIONS



PIPE
SOLUTIONS



STRUCTURES
SOLUTIONS

Few companies offer the wide range of high-quality stormwater resources you can find with us — state-of-the-art products, decades of expertise, and all the maintenance support you need to operate your system cost-effectively.

THE CONTECH WAY

Contech® Engineered Solutions provides innovative, cost-effective site solutions to engineers, contractors, and developers on projects across North America. Our portfolio includes bridges, drainage, erosion control, retaining wall, sanitary sewer and stormwater management products.

TAKE THE NEXT STEP

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Appendix E

NRCS Soils Report



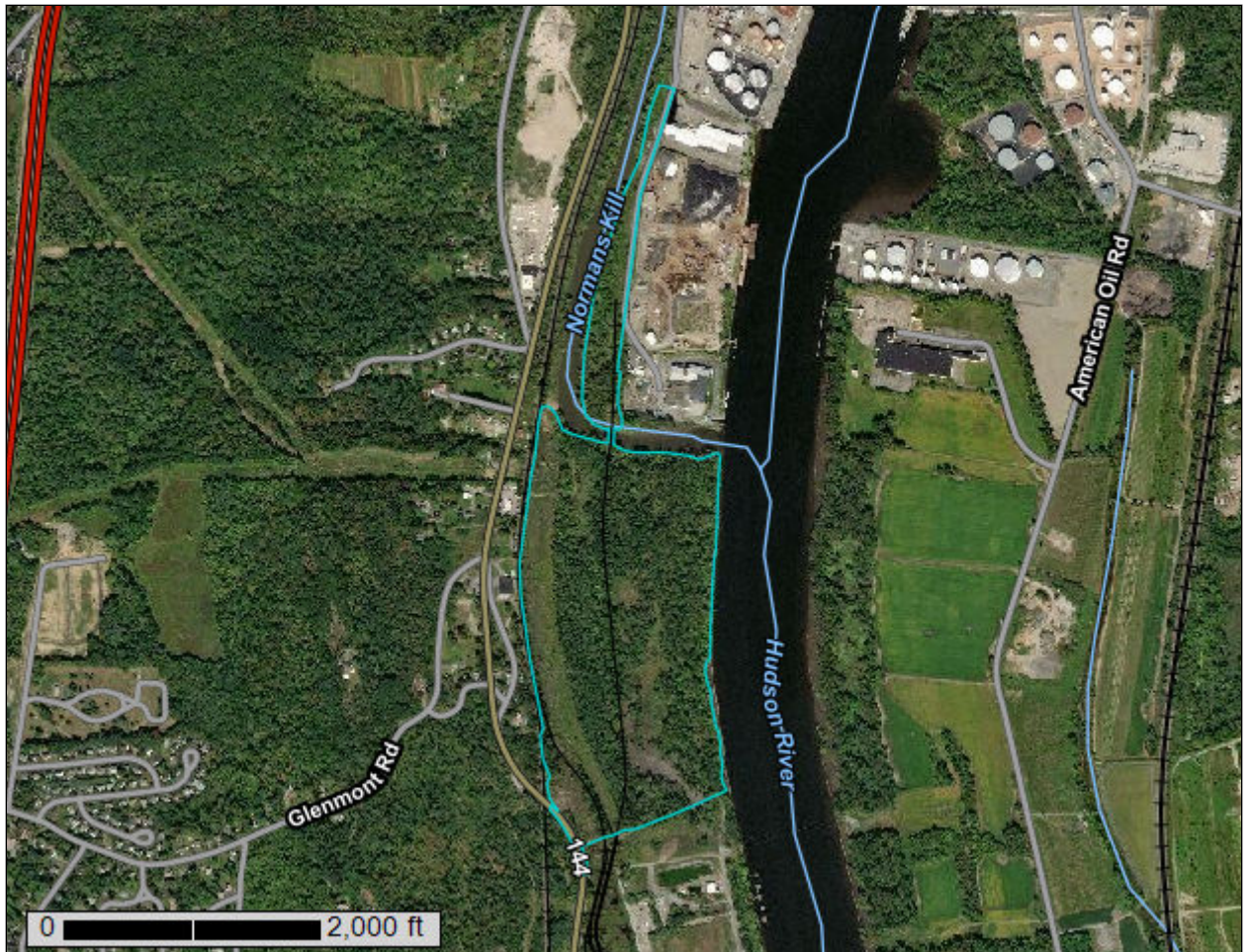
United States
Department of
Agriculture

NRCS

Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for **Albany County, New York**



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

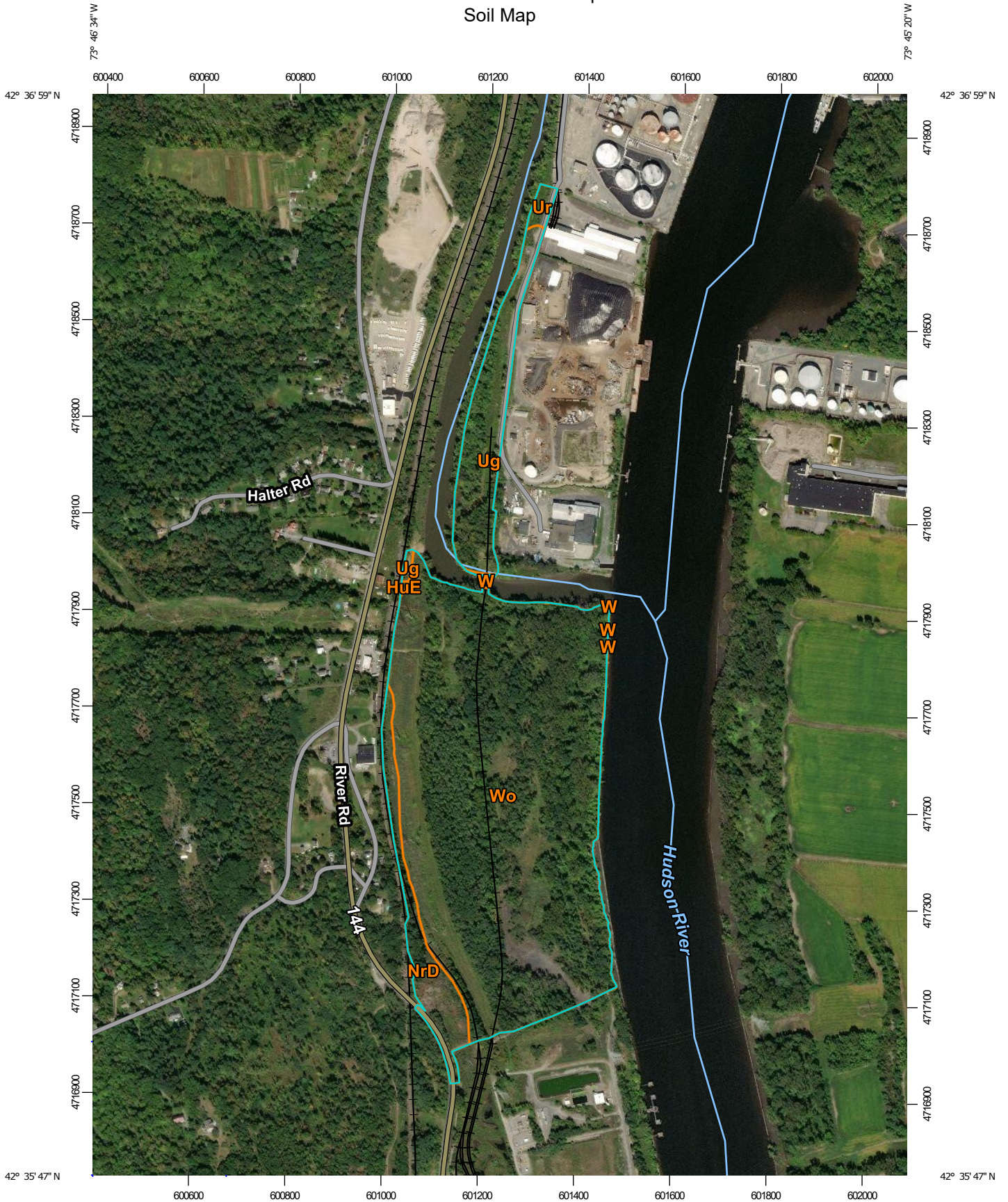
Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

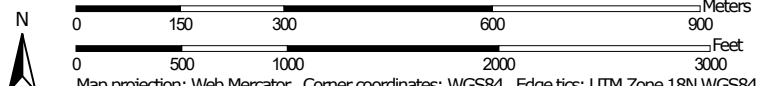
Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report Soil Map




Map Scale: 1:10,900 if printed on A portrait (8.5" x 11") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines


 Soil Map Unit Points

Special Point Features






-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features


Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Albany County, New York
 Survey Area Data: Version 19, Aug 29, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 1, 2014—Sep 22, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
HuE	Hudson silt loam, 25 to 45 percent slopes	0.1	0.1%
NrD	Nassau very channery silt loam, hilly, very rocky	7.2	6.7%
Ug	Udorthents, loamy	11.6	10.7%
Ur	Urban land	0.8	0.8%
W	Water	0.1	0.1%
Wo	Wayland soils complex, non-calcareous substratum, 0 to 3 percent slopes, frequently flooded	88.7	81.7%
Totals for Area of Interest		108.6	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

Custom Soil Resource Report

was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Albany County, New York

HuE—Hudson silt loam, 25 to 45 percent slopes

Map Unit Setting

National map unit symbol: 9pg8
Elevation: 300 to 1,800 feet
Mean annual precipitation: 36 to 41 inches
Mean annual air temperature: 45 to 48 degrees F
Frost-free period: 100 to 170 days
Farmland classification: Not prime farmland

Map Unit Composition

Hudson and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hudson

Setting

Landform: Lake plains
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Riser
Down-slope shape: Concave
Across-slope shape: Convex
Parent material: Clayey and silty glaciolacustrine deposits

Typical profile

H1 - 0 to 11 inches: silt loam
H2 - 11 to 16 inches: silty clay loam
H3 - 16 to 31 inches: silty clay
H4 - 31 to 60 inches: clay

Properties and qualities

Slope: 25 to 45 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 18 to 24 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Available water supply, 0 to 60 inches: High (about 9.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7e
Hydrologic Soil Group: C/D
Ecological site: F144AY018NY - Moist Lake Plain
Hydric soil rating: No

Minor Components

Unnamed soils

Percent of map unit: 5 percent

Unadilla

Percent of map unit: 5 percent
Hydric soil rating: No

Colonie

Percent of map unit: 3 percent
Hydric soil rating: No

Udifluvents

Percent of map unit: 1 percent
Hydric soil rating: No

Fluvaquents

Percent of map unit: 1 percent
Landform: Flood plains
Hydric soil rating: Yes

NrD—Nassau very channery silt loam, hilly, very rocky

Map Unit Setting

National map unit symbol: 9ph1
Elevation: 600 to 1,800 feet
Mean annual precipitation: 36 to 41 inches
Mean annual air temperature: 45 to 48 degrees F
Frost-free period: 100 to 170 days
Farmland classification: Not prime farmland

Map Unit Composition

Nassau, hilly, and similar soils: 70 percent
Minor components: 30 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Nassau, Hilly

Setting

Landform: Benches, ridges, till plains
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Channery loamy till derived mainly from local slate or shale

Typical profile

H1 - 0 to 8 inches: very channery silt loam
H2 - 8 to 16 inches: very channery silt loam
H3 - 16 to 20 inches: unweathered bedrock

Properties and qualities

Slope: 15 to 25 percent
Depth to restrictive feature: 10 to 20 inches to lithic bedrock
Drainage class: Somewhat excessively drained

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Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

Minor Components

Rock outcrop

Percent of map unit: 9 percent

Hydric soil rating: Unranked

Manlius

Percent of map unit: 8 percent

Hydric soil rating: No

Unnamed soils

Percent of map unit: 8 percent

Lordstown

Percent of map unit: 5 percent

Hydric soil rating: No

Ug—Udorthents, loamy

Map Unit Setting

National map unit symbol: 9pj1

Elevation: 0 to 1,640 feet

Mean annual precipitation: 36 to 41 inches

Mean annual air temperature: 45 to 48 degrees F

Frost-free period: 100 to 170 days

Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, loamy, and similar soils: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Loamy

Typical profile

H1 - 0 to 4 inches: loam

H2 - 4 to 70 inches: channery loam

Properties and qualities

Slope: 0 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high
(0.06 to 5.95 in/hr)
Depth to water table: About 36 to 72 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Available water supply, 0 to 60 inches: Low (about 5.5 inches)

Minor Components

Unnamed soils

Percent of map unit: 10 percent

Ur—Urban land

Map Unit Setting

National map unit symbol: 9pj8
Mean annual precipitation: 36 to 41 inches
Mean annual air temperature: 45 to 48 degrees F
Frost-free period: 100 to 170 days
Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Typical profile

H1 - 0 to 6 inches: variable

Minor Components

Unnamed soils

Percent of map unit: 10 percent

Udorthents

Percent of map unit: 5 percent
Hydric soil rating: No

W—Water

Map Unit Composition

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Wo—Wayland soils complex, non-calcareous substratum, 0 to 3 percent slopes, frequently flooded

Map Unit Setting

National map unit symbol: 2srgt

Elevation: 160 to 1,970 feet

Mean annual precipitation: 31 to 70 inches

Mean annual air temperature: 43 to 52 degrees F

Frost-free period: 105 to 180 days

Farmland classification: Not prime farmland

Map Unit Composition

Wayland and similar soils: 60 percent

Wayland, very poorly drained, and similar soils: 30 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wayland

Setting

Landform: Flood plains

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Silty and clayey alluvium derived from interbedded sedimentary rock

Typical profile

Ap - 0 to 9 inches: silt loam

Bg - 9 to 21 inches: silt loam

Cg1 - 21 to 28 inches: silt loam

Cg2 - 28 to 47 inches: silt loam

Cg3 - 47 to 54 inches: silt loam

Cg4 - 54 to 60 inches: silt loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Custom Soil Resource Report

Frequency of flooding: FrequentNone
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Very high (about 13.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 5w
Hydrologic Soil Group: B/D
Hydric soil rating: Yes

Description of Wayland, Very Poorly Drained

Setting

Landform: Flood plains
Landform position (three-dimensional): Tread
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Silty and clayey alluvium derived from interbedded sedimentary rock

Typical profile

A - 0 to 9 inches: mucky silt loam
Bg - 9 to 21 inches: silt loam
Cg1 - 21 to 28 inches: silt loam
Cg2 - 28 to 47 inches: silt loam
Cg3 - 47 to 54 inches: silt loam
Cg4 - 54 to 60 inches: silt loam

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: NoneFrequent
Frequency of ponding: Frequent
Calcium carbonate, maximum content: 5 percent
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Very high (about 13.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 5w
Hydrologic Soil Group: B/D
Hydric soil rating: Yes

Minor Components

Holderton

Percent of map unit: 10 percent
Landform: Flood plains
Landform position (three-dimensional): Tread
Down-slope shape: Linear
Across-slope shape: Linear

Custom Soil Resource Report

Hydric soil rating: No

Soil Information for All Uses

Soil Properties and Qualities

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

Hydrologic Soil Group

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

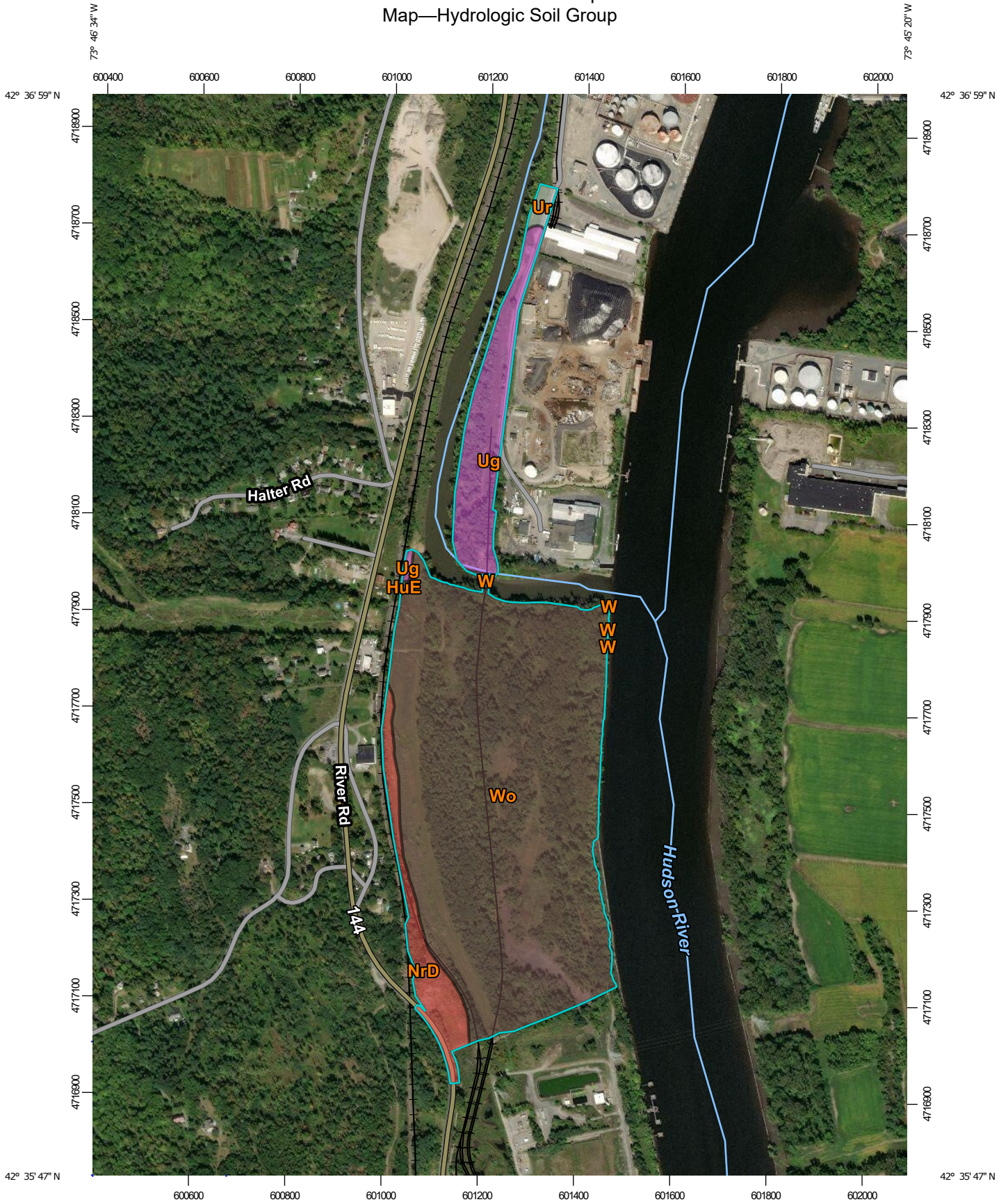
Custom Soil Resource Report

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

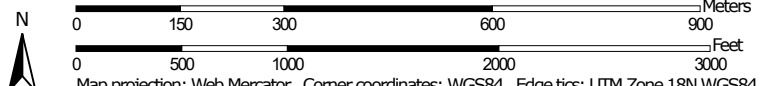
Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Custom Soil Resource Report Map—Hydrologic Soil Group




Map Scale: 1:10,900 if printed on A portrait (8.5" x 11") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84

MAP LEGEND

Area of Interest (AOI)









 Area of Interest (AOI)

Soils

Soil Rating Polygons





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Lines


-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

Soil Rating Points






-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Albany County, New York
 Survey Area Data: Version 19, Aug 29, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 1, 2014—Sep 22, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
HuE	Hudson silt loam, 25 to 45 percent slopes	C/D	0.1	0.1%
NrD	Nassau very channery silt loam, hilly, very rocky	D	7.2	6.7%
Ug	Udorthents, loamy	A	11.6	10.7%
Ur	Urban land		0.8	0.8%
W	Water		0.1	0.1%
Wo	Wayland soils complex, non-calcareous substratum, 0 to 3 percent slopes, frequently flooded	B/D	88.7	81.7%
Totals for Area of Interest			108.6	100.0%

Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

References

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- United States Department of Agriculture, Natural Resources Conservation Service. National range and pasture handbook. <http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/landuse/rangepasture/?cid=stelprdb1043084>

Custom Soil Resource Report

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/scientists/?cid=nrcs142p2_054242

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United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210. http://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/nrcs142p2_052290.pdf

Appendix F

Infiltration Test Results



June 7, 2022

McFarland-Johnson, Inc.
66 Railroad Place – Suite 402
Saratoga Springs, NY 12866

Attn: Mr. Steven Boisvert, P.E.
p: (518) 580-9380
e: sboisvert@mjinc.com

Re: Infiltration Testing
Proposed Marmen Manufacturing Facility
Port of Albany, NY
Terracon Project No. JB215020

Dear Mr. Boisvert:

This report presents the results of the supplemental subsurface investigation and infiltration testing program completed by Terracon at the referenced site.

A total of 21 test borings (IT-1 thru IT-15, along with IT-1A, IT-7A, IT-8A, IT-10A, IT-10B and IT-12A) were completed as part of the investigation, with their locations and depths specified by McFarland-Johnson. Individual subsurface logs for each borehole are attached herewith, along with a subsurface investigation plan(s) indicating their locations.

Infiltration tests were performed adjacent to each of these test borings and were numbered correspondingly. The tests were conducted using 4-inch diameter PVC pipe in general accord with the guidelines in Appendix D of the NYS Stormwater Management Design Manual. Results of this testing are presented for your use on the attached infiltration test data sheets, along with a tabular summary.

We appreciate the opportunity to be of service on this project. Please contact us at your convenience if you have any questions or if anything further is needed.

Respectfully,
Terracon Consultants – NY, Inc.

John S. Hutchison, P.E.
Senior Geotechnical Engineer

Joseph Robichaud, Jr., P.E.
Principal / Office Manager

- Attachments:
- Subsurface investigation plan(s)
 - Test boring logs
 - Infiltration test results summary table
 - Infiltration test data sheets

Terracon Consultants – NY, Inc. 30 Corporate Circle, Suite 201 Albany, NY 12203
p (518) 266-0310 f (518) 266-9238 terracon.com



McFarland Johnson
 60 RAILROAD PLACE
 SUITE 402
 SARATOGA SPRINGS, NEW YORK 12866
 P: 518-580-9380 F: 518-580-9383
 SaratogaROM@mjinc.com

PROJECT MILESTONE
FINAL DESIGN PLANS

NO.	DATE	DESCRIPTION

CLIENT:
ALBANY PORT DISTRICT COMMISSION
 ALBANY, NEW YORK

PROJECT:
PORT OF ALBANY EXPANSION SITE

DRAWN	JES
DESIGNED	NSO
CHECKED	AJF
SCALE	AS SHOWN
DATE	04/19/2022
PROJECT	18641.00

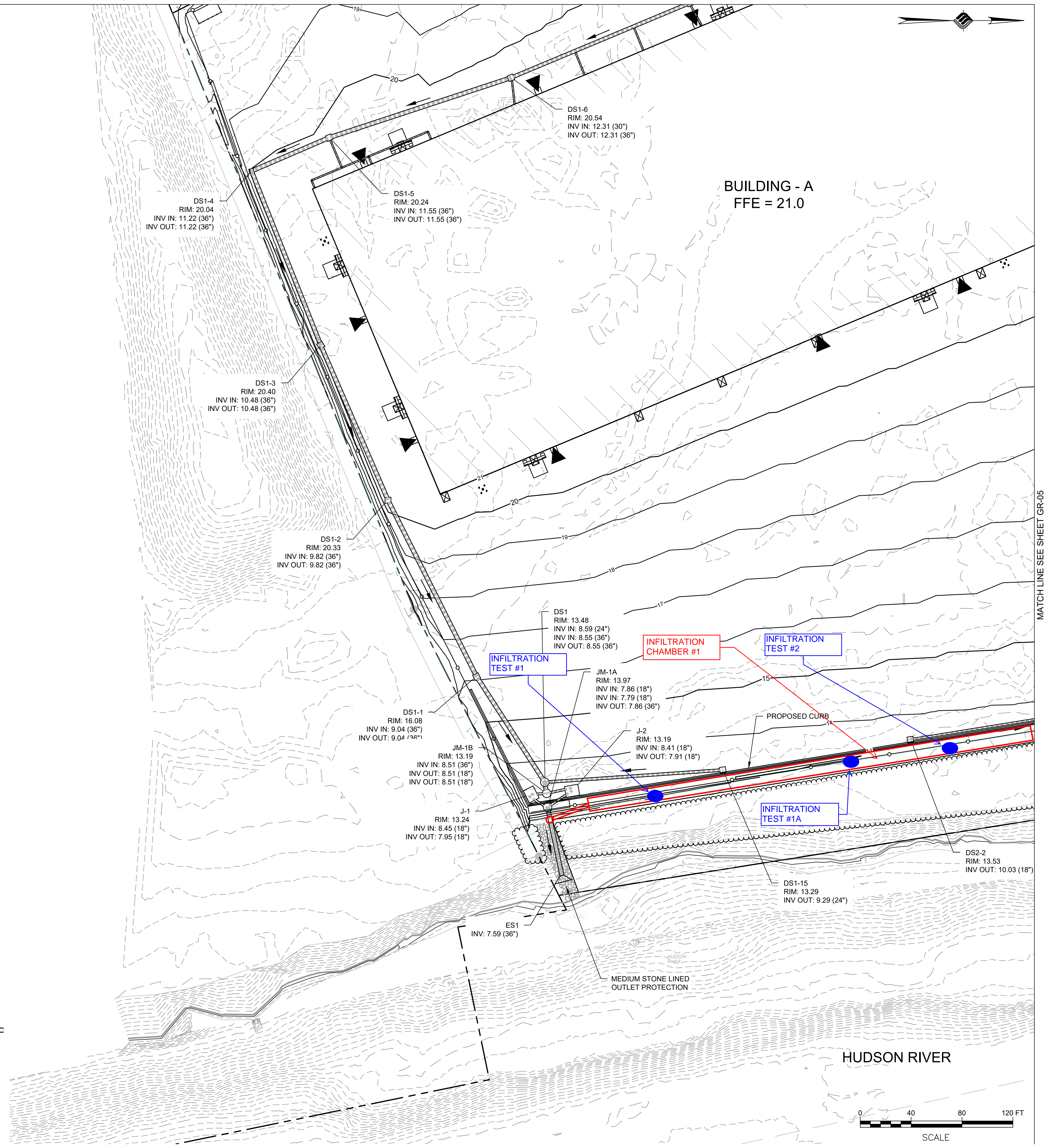
**FOR REVIEW
 NOT FOR
 CONSTRUCTION**

IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECT DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR, TO ALTER AN ITEM IN ANY WAY. IF AN ITEM BEARING THE STAMP OF A LICENSED PROFESSIONAL IS ALTERED, THE ALTERING ENGINEER, ARCHITECT, LANDSCAPE ARCHITECT, OR LAND SURVEYOR SHALL STAMP THE DOCUMENT AND INCLUDE THE NOTATION "ALTERED BY" FOLLOWED BY THEIR SIGNATURE, THE DATE OF SUCH ALTERATION, AND A SPECIFIC DESCRIPTION OF THE ALTERATION.

DRAWING TITLE
GRADING & DRAINAGE

DRAWING NUMBER
GR-04

MATCH LINE SEE SHEET GR-01



LANDS N/F
 PSEG POWER
 L.2701, P.286
 TAX ID#
 98.00-2-10.1

LEGEND

PROPERTY LINE		WETLAND AREA	
BUILDING SETBACK		PROPOSED DRAINAGE PIPE	
EXISTING CONTOUR		PROPOSED RIP RAP	
PROPOSED CONTOUR		MATERIAL STORAGE AREA	
DITCH CENTERLINE		HUDSON RIVER DREDGING	
PROPOSED CHECK DAM		EXCAVATION FOR WHARF	



N:\18641\04 ALBANY PORT EXPANSION\DRAWINGS\GRADING\DRAINAGE\GR-04.DWG

BORING LOG NO. IT-1

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6002° Longitude: -73.7632° Approximate Surface Elev.: 16.6 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	0.3	TOPSOIL	16.5+/-			21	4-11-21-48 N=32		
	3.5	FILL - SILTY SAND (SM) , rootlets, coal, and cinders noted, black, dense to very dense	13+/-			24	42-50-35-17 N=85		
		FILL - COAL ASH , wood and roots noted, black, loose to medium dense		5		21	3-5-4-3 N=9		
						21	3-3-2-4 N=5		
	11.0	Becomes gray w/ crushed stone and slag	5.5+/-	10		22	6-6-17-37 N=23		
		SILT (ML) , shells noted, gray to brown, medium stiff to stiff Silt and clay bands noted 12-14'				19	17-7-9-5 N=16		
	14.0	Boring Terminated at 14 Feet	2.5+/-			19	3-3-2-1 N=5		

Stratification lines are approximate. In-situ, the transition may be gradual.

<p>Advancement Method: 2 1/4" ID HSA</p> <p>Abandonment Method: Boring backfilled with soil cuttings upon completion.</p>	<p>See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any).</p> <p>See Supporting Information for explanation of symbols and abbreviations.</p> <p>Approx. ground surface elev. furnished by client</p>	<p>Notes: Logged by: JCH - 4" PVC infiltration test pipe set at depth of 10.0' alongside test boring</p>						
<p>WATER LEVEL OBSERVATIONS <i>No free water observed</i></p>	<p>30 Corporate Cir Ste 201 Albany, NY</p>	<table style="width: 100%; border: none;"> <tr> <td style="border: none;">Boring Started: 05-11-2022</td> <td style="border: none;">Boring Completed: 05-11-2022</td> </tr> <tr> <td style="border: none;">Drill Rig: CME-750X</td> <td style="border: none;">Driller: J. Lamm</td> </tr> <tr> <td style="border: none;">Project No.: JB215020</td> <td style="border: none;"></td> </tr> </table>	Boring Started: 05-11-2022	Boring Completed: 05-11-2022	Drill Rig: CME-750X	Driller: J. Lamm	Project No.: JB215020	
Boring Started: 05-11-2022	Boring Completed: 05-11-2022							
Drill Rig: CME-750X	Driller: J. Lamm							
Project No.: JB215020								

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-2

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6011° Longitude: -73.7634° Approximate Surface Elev.: 15.3 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (in.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	1.0	TOPSOIL	14.5+/-		X	18	2-3-4-5 N=7		
	2.0	FILL - SANDY SILT (ML) , roots noted, gray, medium stiff	13.5+/-		X		8-8-11-13 N=19		
		FILL - SILTY SAND (SM) , wood, brick, and coal fragments noted, gray, very loose to medium dense		5	X		6-7-7-8 N=14		
					X		6-3-3-2 N=6		
	8.5		7+/-		X		1-2-2-1 N=4		
	10.0	SANDY SILT (ML) , organics and sand seams noted, gray, loose	5.5+/-		X		2-1-1-2 N=2		
		SILT (ML) , gray, soft		10	X				
	12.0	Boring Terminated at 12 Feet	3.5+/-		X				

Stratification lines are approximate. In-situ, the transition may be gradual.

<p>Advancement Method: 2 1/4" ID HSA</p>	<p>See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (if any).</p> <p>See Supporting Information for explanation of symbols and abbreviations.</p> <p>Approx. ground surface elev. furnished by client</p>	<p>Notes: Logged by: JCH - 4" PVC infiltration test pipe set at depth of 9.0' alongside test boring</p>						
<p>Abandonment Method: Boring backfilled with soil cuttings upon completion.</p>								
<p>WATER LEVEL OBSERVATIONS <i>No free water observed</i></p>	<p>30 Corporate Cir Ste 201 Albany, NY</p>	<table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%;">Boring Started: 05-11-2022</td> <td style="width: 50%;">Boring Completed: 05-11-2022</td> </tr> <tr> <td>Drill Rig: CME-750X</td> <td>Driller: J. Lamm</td> </tr> <tr> <td>Project No.: JB215020</td> <td></td> </tr> </table>	Boring Started: 05-11-2022	Boring Completed: 05-11-2022	Drill Rig: CME-750X	Driller: J. Lamm	Project No.: JB215020	
Boring Started: 05-11-2022	Boring Completed: 05-11-2022							
Drill Rig: CME-750X	Driller: J. Lamm							
Project No.: JB215020								

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-3

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6017° Longitude: -73.7636° Approximate Surface Elev.: 10.8 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	0.5	TOPSOIL	-10.5+/-		X	6	1-2-2-2 N=4		
	3.0	FILL - SILTY SAND (SM) , wood chips and organics noted, brown, loose to medium dense	8+/-		X	17	4-3-7-4 N=10		
		SILT (ML) , mottled, occasional sand and clay bands, brown, medium stiff to stiff		5	X	22	3-3-3-3 N=6		
	8.0	Boring Terminated at 8 Feet	3+/-		X	18	3-3-3-3 N=6		

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 4.5' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.
Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-12-2022

Boring Completed: 05-12-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-4

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6022° Longitude: -73.7638° Approximate Surface Elev.: 12.8 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	6.0	FILL - SANDY SILT WITH GRAVEL (ML) , with clayey bands, wood, coal pieces, and roots noted, gray, soft to medium stiff	7+/-		X	14	1-1-2-2 N=3		
	8.0	VARVED SILT AND CLAY (CL-ML) , mottled, rootlets noted, orange to brown, medium stiff	5+/-		X	19	2-3-4-5 N=7		
	10.0	SILT WITH SAND (ML) , sand seams noted, brown, medium stiff	3+/-		X	19	4-3-3-4 N=6		
		SILT WITH SAND (ML) , sand seams noted, brown, medium stiff	5+/-		X	17	4-4-3-3 N=7		
		SILT WITH SAND (ML) , sand seams noted, brown, medium stiff	3+/-		X	18	4-3-3-4 N=6		
		Boring Terminated at 10 Feet							

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 6.5' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-11-2022

Boring Completed: 05-11-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-5

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6027° Longitude: -73.7638° Approximate Surface Elev.: 9.1 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	DEPTH								
	3.0	FILL - SANDY SILT (ML) , pieces of wood noted, gray, soft	6+/-		X	19	1-1-1-2 N=2		
	4.0	SILT (ML) , gray, medium stiff	5+/-		X	18	1-3-5-3 N=8		
	6.0	POORLY GRADED SAND (SP) , brown, loose	3+/-		X	19	2-1-3-3 N=4		
Boring Terminated at 6 Feet									

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method: 2 1/4" ID HSA	See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any). See Supporting Information for explanation of symbols and abbreviations. Approx. ground surface elev. furnished by client	Notes: Logged by: JCH - 4" PVC infiltration test pipe set at depth of 2.5' alongside test boring
Abandonment Method: Boring backfilled with soil cuttings upon completion.		
WATER LEVEL OBSERVATIONS No free water observed	 30 Corporate Cir Ste 201 Albany, NY	Boring Started: 05-11-2022 Drill Rig: CME-750X Project No.: JB215020
		Boring Completed: 05-11-2022 Driller: J. Lamm

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-6

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6034° Longitude: -73.7638° Approximate Surface Elev.: 10.7 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	4.0	SILTY CLAY (CL-ML) , rootlets noted, gray, soft to medium stiff Organics noted 2-4'	6.5+/-		X	14	1-1-2-2 N=3		
	8.0	SILT WITH SAND (ML) , brown, soft to medium stiff			X	19	2-3-4-3 N=7		
		Sand lens from 7-8'	2.5+/-		X	19	2-1-2-2 N=3		
		Boring Terminated at 8 Feet			X	19	3-3-2-3 N=5		

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 4.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-11-2022

Boring Completed: 05-11-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-7

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6041° Longitude: -73.7637° Approximate Surface Elev.: 9.6 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	2.0	VARVED SILT AND CLAY (CL-ML) , rootlets noted, gray, soft	7.5+/-		X	12	WH-1-2-2 N=3		
		SILT (ML) , roots and rootlets noted, brown, medium stiff			X	19	2-2-2-2 N=4		
	5.5		4+/-		X	19	2-2-2-1 N=4		
	6.0	POORLY GRADED SAND (SP) , brown, very loose	3.5+/-						
		Boring Terminated at 6 Feet							

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
WH = Weight of Hammer
- 4" PVC infiltration test pipe set at depth of 3.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-12-2022

Boring Completed: 05-12-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-8

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6069° Longitude: -73.7637° Approximate Surface Elev.: 12.4 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	TOPSOIL		2.5		X	17	1-2-2-4 N=4		
	FILL - SILTY SAND (SM), mottled, trace gravel, brown, medium dense		6.5		X	19	4-6-6-6 N=12		
	SILTY CLAY (CL-ML), rootlets noted, gray to brown, medium stiff		8.0		X	12	7-11-6-6 N=17		
	SILT (ML), gray, medium stiff		10.0		X	19	7-5-3-3 N=8		
	SILT (ML), gray, medium stiff		10.0		X	19	2-3-3-3 N=6		
		Boring Terminated at 10 Feet	10						

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 6.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-10-2022

Boring Completed: 05-10-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-9

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6069° Longitude: -73.7643° Approximate Surface Elev.: 13.6 (Ft.) +/- DEPTH ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
		SILTY SAND (SM) , rootlets and organics noted, brown, very loose to medium dense	5.0	5	X	12	1-1-2-2 N=3		
		SILT WITH SAND (ML) , organics noted, brown, stiff Grades to banded silt with sand	8.5+/-		X	19	3-3-4-4 N=7		
		SILT (ML) , brown, medium stiff	8.0		X	18	7-6-6-7 N=12		
			5.5+/-		X	21	6-7-6-8 N=13		
			10.0		X	24	2-3-2-3 N=5		
		Boring Terminated at 10 Feet	10						

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 7.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-12-2022

Boring Completed: 05-12-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-10

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6070° Longitude: -73.7650° Approximate Surface Elev.: 17.3 (Ft.) +/- DEPTH ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
		No recovery 0-2' SILT WITH SAND (ML) , mottled, trace gravel, rootlets noted, brown, medium stiff to stiff			X	0	1-2-2-2 N=4		
		Silty sand seam noted 5.5-6' Grades to brownish gray	5		X	12	2-3-2-4 N=5		
			5		X	22	5-5-4-6 N=9		
			5		X	19	5-4-5-5 N=9		
			10		X	12	2-3-3-4 N=6		
		SILTY CLAY (CL-ML) , sand lenses noted, gray, medium stiff	10		X	22	3-3-5-5 N=8		
		SILT (ML) , gray, medium stiff	10		X	24	4-4-4-2 N=8		
		Boring Terminated at 14 Feet	14		X				

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 11.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-12-2022

Boring Completed: 05-12-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-11

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6070° Longitude: -73.7656° Approximate Surface Elev.: 15.4 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
		0.5' TOPSOIL	15+/-		X	19	WH-1-2-2 N=3		
		SILT WITH SAND (ML) , rootlets noted, mottled, orange to brown, soft to very stiff			X	21	1-1-2-3 N=3		
		Gravelly seams noted 4-7'	5		X	18	2-3-5-9 N=8		
		7.0' SILT (ML) , gray to brown, medium stiff to very stiff	8.5+/-		X	19	12-17-18-13 N=35		
			10		X	24	4-5-5-5 N=10		
			12.0		X	24	5-4-3-2 N=7		
		Boring Terminated at 12 Feet							

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 9.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-12-2022

Boring Completed: 05-12-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-12

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6084° Longitude: -73.7665° Approximate Surface Elev.: 14 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	0.5	TOPSOIL	13.5+/-		X	12	WH-2-3-4 N=5		
		FILL - SANDY SILT (ML) , shell fragments, wood, and rootlets noted, brown, medium stiff		5					
	7.0	FILL - SILT (ML) , wood and coal fragments noted, gray, medium stiff	7+/-		X	24	3-3-4-7 N=7		
	9.0	Boring Terminated at 9 Feet	5+/-		X	24	4-5-3-7 N=8		

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
WH = Weight of Hammer
- 4" PVC infiltration test pipe set at depth of 6.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-10-2022

Boring Completed: 05-10-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-13

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6085° Longitude: -73.7665° Approximate Surface Elev.: 14.6 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	7.0	SANDY SILT (ML) , trace gravel and rootlets noted, brown, medium stiff	7.5+/-		8		WH-2-4-3 N=6		
	9.0	SILTY SAND (SM) , trace gravel and rootlets noted, gray, loose	5.5+/-		24		3-3-4-4 N=7		
	11.0	SANDY SILT (ML) , trace gravel and wood noted, gray, medium stiff	3.5+/-		18		4-4-5-3 N=9		
		SANDY SILT (ML) , trace gravel and wood noted, gray, medium stiff	3.5+/-		21		1-1-3-4 N=4		
		Boring Terminated at 11 Feet							

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method: 2 1/4" ID HSA	See Exploration and Testing Procedures for a description of field and laboratory procedures used and additional data (If any). See Supporting Information for explanation of symbols and abbreviations. Approx. ground surface elev. furnished by client	Notes: Logged by: JCH WH = Weight of Hammer - 4" PVC infiltration test pipe set at depth of 6.5' alongside test boring
Abandonment Method: Boring backfilled with soil cuttings upon completion.		
WATER LEVEL OBSERVATIONS No free water observed	 30 Corporate Cir Ste 201 Albany, NY	Boring Started: 05-10-2022 Boring Completed: 05-10-2022 Drill Rig: CME-750X Driller: J. Lamm Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-14

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6106° Longitude: -73.7662° Approximate Surface Elev.: 5.8 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	0.5	TOPSOIL	5.5+/-		Hand	12			
	2.0	SANDY SILT (ML) , rootlets noted, brown	4+/-		Hand	12			
	3.0	SILTY CLAY (CL-ML) , roots noted, orange to brown	3+/-						
Boring Terminated at 3 Feet									

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
Hand Auger

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 1.0' alongside test boring

Abandonment Method:
Boring backfilled with excavation spoils upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-12-2022

Boring Completed: 05-12-2022

Drill Rig: Hand Auger

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-15

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6107° Longitude: -73.7662° Approximate Surface Elev.: 5.8 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	0.5	TOPSOIL	5.5+/-		Hand	15			
	1.5	SILT (ML) , rootlets noted, brown	4.5+/-		Hand	12			
	3.0	SILTY CLAY (CL-ML) , sand seams noted, brown	3+/-						
Boring Terminated at 3 Feet									

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
Hand Auger

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 1.0' alongside test boring

Abandonment Method:
Boring backfilled with excavation spoils upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-12-2022

Boring Completed: 05-12-2022

Drill Rig: Hand Auger

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-1A

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6007° Longitude: -73.7634° Approximate Surface Elev.: 14.3 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	3.5	FILL - SILTY SAND WITH GRAVEL (SM) , black, medium dense to very dense	11+/-		X	18	2-3-11-14 N=14		
		FILL - COAL ASH , rootlets noted, black, loose to medium dense		5	X		25-27-25-10 N=52		
	9.0		5.5+/-		X	5	7-5-3-3 N=8		
		FILL - POORLY GRADED SAND (SP) , black, very loose		10	X	19	4-2-3-2 N=5		
	11.0		3.5+/-		X	19	1-1-2-1 N=3		
		Boring Terminated at 11 Feet							

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 8.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-17-2022

Boring Completed: 05-17-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-7A

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6039° Longitude: -73.7638° Approximate Surface Elev.: 11.2 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	2.5	SILTY CLAY (CL-ML) , gray, soft	8.5+/-		X	12	2-1-2-3 N=3		
	8.0	SANDY SILT (ML) , brown, medium stiff	3+/-		X	19	2-3-3-4 N=6		
		Boring Terminated at 8 Feet			X	19	2-2-3-2 N=5		
					X	19	2-3-3-2 N=6		

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 5.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-17-2022

Boring Completed: 05-17-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-8A

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6069° Longitude: -73.7641° Approximate Surface Elev.: 14.8 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
		SILTY SAND (SM) , sand seams noted, brown, very loose to loose	5		X	15	WH-1-1-1 N=2		
		4.5 SILT (ML) , mottled, brown, medium stiff	10.5+/-		X	18	4-4-5-4 N=9		
		6.0 SILTY SAND (SM) , gray clayey bands noted, brown, medium dense	9+/-		X	22	3-2-4-7 N=6		
		8.0 SILT (ML) , gray, soft	7+/-		X	22	12-14-9-10 N=23		
					X	24	1-2-2-2 N=4		
					X	24	3-1-2-1 N=3		
		Boring Terminated at 12 Feet	12.0						

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 7.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-16-2022

Boring Completed: 05-16-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-10A

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6070° Longitude: -73.7650° Approximate Surface Elev.: 17.4 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	0.5	TOPSOIL	17+/-			15	WH/12"-2-3 N=2		
		SANDY SILT (ML) , rootlets noted, brown, soft to stiff				19	4-5-5-6 N=10		
		Gray clayey bands 3-3.5'				24	3-4-4-4 N=8		
		Brown sandy bands 4-6'				21	5-7-6-5 N=13		
	7.5	SILTY CLAY (CL-ML) , gray, soft to stiff	10+/-			24	3-2-4-3 N=6		
		Varved 7.5-8'				24	1-1-2-1 N=3		
		Sand seams noted 12-14'	14.0			24	1-2-2-2 N=4		
		Boring Terminated at 14 Feet	3.5+/-						

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (if any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 11.0' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-16-2022

Boring Completed: 05-16-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-10B

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6070° Longitude: -73.7653° Approximate Surface Elev.: 16.7 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
DEPTH									
	0-2'	No recovery 0-2'			X	0	WH-1-2-3 N=3		
	2-6'	VARVED SILT AND CLAY (CL-ML) , rootlets noted, gray, soft to stiff	10.5+/-		X	14	4-4-5-5 N=9		
	6-10.5'	SANDY SILT (ML) , brown, stiff to very stiff	6+/-		X	21	5-4-5-6 N=9		
	10.5-13.0'	SILT (ML) , mottled, brown, stiff	3.5+/-		X	22	4-6-13-15 N=19		
					X	22	13-9-6-6 N=15		
					X	24	4-5-4-3 N=9		
		Boring Terminated at 13 Feet							

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
2 1/4" ID HSA

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 9.5' alongside test boring

Abandonment Method:
Boring backfilled with soil cuttings upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-16-2022

Boring Completed: 05-16-2022

Drill Rig: CME-750X

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

BORING LOG NO. IT-12A

PROJECT: Proposed Marmen Manufacturing Facility

CLIENT: McFarland Johnson
Saratoga Springs, NY

SITE: River Road
Glenmont, NY

MODEL LAYER	GRAPHIC LOG	LOCATION See Exploration Plan Latitude: 42.6083° Longitude: -73.7665° Approximate Surface Elev.: 12.7 (Ft.) +/- ELEVATION (Ft.)	DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	RECOVERY (In.)	FIELD TEST RESULTS	ORGANIC CONTENT (%)	WATER CONTENT (%)
	0.5	TOPSOIL	12+/-		☞				
	2.0	FILL - SILT WITH SAND (ML) , organics and roots noted, brown	10.5+/-		☞				
	4.0	FILL - SANDY SILT (ML) , brick noted, orange to brown	8.5+/-		☞				
	8.0	SILTY SAND (SM) , mottled, shell fragments and rootlets noted, orange to brown	4.5+/-		☞				
Boring Terminated at 8 Feet									

Stratification lines are approximate. In-situ, the transition may be gradual.

Advancement Method:
Hand Auger

See [Exploration and Testing Procedures](#) for a description of field and laboratory procedures used and additional data (If any).

Notes:

Logged by: JCH
- 4" PVC infiltration test pipe set at depth of 4.0' alongside test boring

Abandonment Method:
Boring backfilled with excavation spoils upon completion.

See [Supporting Information](#) for explanation of symbols and abbreviations.

Approx. ground surface elev. furnished by client

WATER LEVEL OBSERVATIONS

No free water observed



Boring Started: 05-17-2022

Boring Completed: 05-17-2022

Drill Rig: Hand Auger

Driller: J. Lamm

Project No.: JB215020

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. GEO SMART LOG-NO WELL - JB215020 PORT OF ALBANY.MA.GPJ TERRACON_DATATEMPLATE.GDT 6/7/22

Port of Albany Expansion Site
Infiltration Test Summary Table

Test #	Location				EG Elev. * (ft)	Test Depth (ft)	Test Elev.	Test Date	Results ** (in/hr)
	Northing	Easting	Lat	Long					
IT-1	1373126.03	690476.39	N042° 36' 00.83"	W073° 45' 47.69"	16.6	10.0	6.6	5/12/2022	1.7
IT-1A	1373285.45	690441.73	N042° 36' 02.41"	W073° 45' 48.14"	14.3	8.0	6.3	5/18/2022	1.7
IT-2	1373428.1	690427.42	N042° 36' 03.82"	W073° 45' 48.31"	15.3	9.0	6.3	5/12/2022	0
IT-3	1373669.92	690372.95	N042° 36' 06.21"	W073° 45' 49.01"	10.8	4.5	6.3	5/13/2022	0.2
IT-4	1373828.59	690333.82	N042° 36' 07.78"	W073° 45' 49.51"	12.8	6.5	6.3	5/12/2022	0.2
IT-5	1374016.28	690316.2	N042° 36' 09.64"	W073° 45' 49.73"	9.1	2.5	6.6	5/12/2022	-0.2
IT-6	1374286.56	690329.4	N042° 36' 12.31"	W073° 45' 49.52"	10.7	4.0	6.7	5/13/2022	0
IT-7	1374550.28	690339.68	N042° 36' 14.91"	W073° 45' 49.35"	9.6	3.0	6.6	5/13/2022	1.2
IT-7A	1374449.39	690328.11	N042° 36' 13.92"	W073° 45' 49.52"	11.2	5.0	6.2	5/18/2022	0.5
IT-8	1375558.9	690328.24	N042° 36' 24.88"	W073° 45' 49.39"	12.4	6.0	6.4	5/12/2022	2.6
IT-8A	1375555.8	690230.63	N042° 36' 24.86"	W073° 45' 50.69"	14.8	7.0	7.8	5/18/2022	0.4
IT-9	1375569.02	690181.72	N042° 36' 24.99"	W073° 45' 51.35"	13.6	7.0	6.6	5/13/2022	0.1
IT-10	1375581.89	689989.53	N042° 36' 25.13"	W073° 45' 53.91"	17.3	11.0	6.3	5/13/2022	1.2
IT-10A	1375579.21	690067.6	N042° 36' 25.10"	W073° 45' 52.87"	17.4	11.0	6.4	5/18/2022	0
IT-10B	1375586.34	689908.31	N042° 36' 25.18"	W073° 45' 55.00"	16.7	9.5	7.2	5/18/2022	0
IT-11	1375587.41	689824.53	N042° 36' 25.20"	W073° 45' 56.12"	15.4	9.0	6.4	5/12/2022	0.1
IT-12	1376092.03	689570.93	N042° 36' 30.21"	W073° 45' 59.45"	14.0	6.0	8.0	5/13/2022	0.5
IT-12A	1376065.55	689567.77	N042° 36' 29.95"	W073° 45' 59.50"	12.7	4.0	8.7	5/18/2022	8.6
IT-13	1376115.27	689572.99	N042° 36' 30.44"	W073° 45' 59.42"	14.6	6.5	8.1	5/13/2022	0.1
IT-14	1376905.51	689652.3	N042° 36' 38.24"	W073° 45' 58.27"	5.8	1.0	4.8	5/13/2022	12.4
IT-15	1376922.65	689655.08	N042° 36' 38.41"	W073° 45' 58.23"	5.8	1.0	4.8	5/13/2022	>24

* Note EG elevations may have changed from the tree clearing work.

** Represents result of final trial at each location.

INFILTRATION TEST RESULTS					
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO. JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: May 12 and 13, 2022		
WEATHER: M. Sunny 70°-80° F			TESTER: J. Hutchison, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)
IT-1	10.0	1	0.12	60	1.4
		2	0.12	60	1.4
		3	0.15	60	1.8
		4	0.14	60	1.7
		NOTE: Infiltration rate during final trial run = 1.7 inches per hour			
IT-2	9.0	1	0.07	60	0.8
		2	0.00	60	0.0
		3	-	-	-
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.0 inches per hour			
IT-3	4.5	1	0.02	60	0.2
		2	-	-	-
		3	-	-	-
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.2 inches per hour			

Notes:

- 1) Testing was conducted in general accord with the “Infiltration Testing Requirements” outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-1 – Fill (coal ash w/ crushed stone and slag)

Test Location IT-2 – Sandy silt (ML)

Test Location IT-3 – Silt (ML)

INFILTRATION TEST RESULTS					
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO. JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: May 12 and 13, 2022		
WEATHER: M. Sunny 70°-80° F			TESTER: J. Hutchison, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)
IT-4	6.5	1	0.06	60	0.7
		2	0.02	60	0.2
		3	-	-	-
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.2 inches per hour			
IT-5	2.5	1	0.02	60	0.8
		2	-0.02	60	-0.2
		3	-	-	-
		4	-	-	-
		NOTE: Infiltration rate during final trial run = -0.2 inches per hour			
IT-6	4.0	1	0.00	60	0.0
		2	-	-	-
		3	-	-	-
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.0 inches per hour			

Notes:

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-4 – Silt and clay (CL-ML)

Test Location IT-5 – Silt (ML)

Test Location IT-6 – Silt w/ sand (ML)

INFILTRATION TEST RESULTS					
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO. JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: May 12 and 13, 2022		
WEATHER: M. Sunny 70°-80° F			TESTER: J. Hutchison, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)
IT-7	3.0	1	0.14	60	1.7
		2	0.22	60	2.6
		3	0.10	60	1.2
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 1.2 inches per hour			
IT-8	6.0	1	0.29	60	3.5
		2	0.23	60	2.8
		3	0.23	60	2.8
		4	0.22	60	2.6
		NOTE: Infiltration rate during final trial run = 2.6 inches per hour			
IT-9	7.0	1	0.01	60	0.1
		2	0.01	60	0.1
		3	0.01	60	0.1
		4	0.01	60	0.1
		NOTE: Infiltration rate during final trial run = 0.1 inches per hour			

Notes:

- 1) Testing was conducted in general accord with the “Infiltration Testing Requirements” outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-7 – Silt (ML)

Test Location IT-8 – Silty sand (SM)

Test Location IT-9 – Silt with sand (ML)

INFILTRATION TEST RESULTS					
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO. JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: May 12 and 13, 2022		
WEATHER: M. Sunny 70°-80° F			TESTER: J. Hutchison, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)
IT-10	11.0	1	0.28	60	3.4
		2	0.07	60	0.8
		3	0.10	60	1.2
		4	0.10	60	1.2
		NOTE: Infiltration rate during final trial run = 1.2 inches per hour			
IT-11	9.0	1	0.02	60	0.2
		2	0.01	60	0.1
		3	-	-	-
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.1 inches per hour			
IT-12	6.0	1	0.04	60	0.5
		2	0.02	60	0.2
		3	0.04	60	0.5
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.5 inches per hour			

Notes:

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-10 – Silty clay (CL-ML)

Test Location IT-11 – Silt (ML)

Test Location IT-12 – Fill (sandy silt)

INFILTRATION TEST RESULTS					
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO. JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: May 12 and 13, 2022		
WEATHER: M. Sunny 70°-80° F			TESTER: J. Hutchison, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)
IT-13	6.5	1	0.08	60	1.0
		2	0.00	60	0.0
		3	0.01	60	0.1
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.1 inches per hour			
IT-14	1.0	1	1.93	52	> 24
		2	1.93	56	> 24
		3	1.93	64	21.8
		4	1.03	60	12.4
		NOTE: Infiltration rate during final trial run = 12.4 inches per hour			
IT-15	1.0	1	1.80	4	> 24
		2	1.80	7	> 24
		3	1.80	7	> 24
		4	1.80	8	> 24
		NOTE: Infiltration rate during final trial run > 24 inches per hour			

Notes:

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-13 – Sandy silt (ML)
 Test Location IT-14 – Sandy silt (ML)
 Test Location IT-15 – Silt (ML)

INFILTRATION TEST RESULTS					
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO. JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: May 18, 2022		
WEATHER: P. Sunny 68° F			TESTER: J. Lamm, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)
IT-1A	8.0	1	0.10	60	1.2
		2	0.12	60	1.4
		3	0.15	60	1.8
		4	0.14	60	1.7
		NOTE: Infiltration rate during final trial run = 1.7 inches per hour			
IT-7A	5.0	1	0.04	60	0.5
		2	0.02	60	0.2
		3	0.06	60	0.7
		4	0.04	60	0.5
		NOTE: Infiltration rate during final trial run = 0.5 inches per hour			
IT-8A	7.0	1	0.02	60	0.2
		2	0.02	60	0.2
		3	0.02	60	0.2
		4	0.03	60	0.4
		NOTE: Infiltration rate during final trial run = 0.4 inches per hour			

Notes:

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-1A – Fill (coal ash)

Test Location IT-7A – Sandy silt (ML)

Test Location IT-8A – Silty sand (SM)

INFILTRATION TEST RESULTS					
PROJECT: Proposed Marmen Manufacturing Facility			PROJECT NO. JB215020		
PROJECT LOCATION: t/o Bethlehem, NY			TEST DATE: May 18, 2022		
WEATHER: P. Sunny 68° F			TESTER: J. Lamm, et al.		
Test Location	Test Depth (feet)	Trial No.	Water Drop (ft)	Elapsed Time (min)	Infiltration Rate (inches/hour)
IT-10A	11.0	1	0.00	60	0.0
		2	0.00	60	0.0
		3	0.00	60	0.0
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.0 inches per hour			
IT-10B	9.5	1	0.03	60	0.4
		2	0.00	60	0.0
		3	0.00	60	0.0
		4	-	-	-
		NOTE: Infiltration rate during final trial run = 0.0 inches per hour			
IT-12A	4.0	1	0.52	60	6.2
		2	0.54	60	6.5
		3	0.56	60	6.7
		4	0.72	60	8.6
		NOTE: Infiltration rate during final trial run = 8.6 inches per hour			

Notes:

- 1) Testing was conducted in general accord with the "Infiltration Testing Requirements" outlined in Appendix D of the New York State Stormwater Management Design Manual.
- 2) Infiltration tests were located alongside companion test borings numbered correspondingly.

SOIL CLASSIFICATION AT TEST DEPTH

Test Location IT-10A – Silty clay (CL-ML)

Test Location IT-10B – Sandy silt (ML)

Test Location IT-12A – Silty sand (SM)

APPENDIX D

MAINTENANCE INSPECTION CHECKLISTS

Stormwater Pond/Wetland Operation, Maintenance and Management Inspection Checklist

Project _____
 Location: _____
 Site Status: _____

 Date: _____
 Time: _____

 Inspector: _____

Maintenance Item	Satisfactory/ Unsatisfactory	Comments
1. Embankment and emergency spillway (Annual, After Major Storms)		
1. Vegetation and ground cover adequate		
2. Embankment erosion		
3. Animal burrows		
4. Unauthorized planting		
5. Cracking, bulging, or sliding of dam		
a. Upstream face		
b. Downstream face		
c. At or beyond toe		
downstream		
upstream		
d. Emergency spillway		
6. Pond, toe & chimney drains clear and functioning		
7. Seeps/leaks on downstream face		
8. Slope protection or riprap failure		
9. Vertical/horizontal alignment of top of dam "As-Built"		

Maintenance Item	Satisfactory/ Unsatisfactory	Comments
10. Emergency spillway clear of obstructions and debris		
11. Other (specify)		
2. Riser and principal spillway (Annual)		
Type: Reinforced concrete _____ Corrugated pipe _____ Masonry _____		
1. Low flow orifice obstructed		
2. Low flow trash rack. a. Debris removal necessary		
b. Corrosion control		
3. Weir trash rack maintenance a. Debris removal necessary		
b. corrosion control		
4. Excessive sediment accumulation insider riser		
5. Concrete/masonry condition riser and barrels a. cracks or displacement		
b. Minor spalling (<1")		
c. Major spalling (rebars exposed)		
d. Joint failures		
e. Water tightness		
6. Metal pipe condition		
7. Control valve a. Operational/exercised		
b. Chained and locked		
8. Pond drain valve a. Operational/exercised		
b. Chained and locked		
9. Outfall channels functioning		
10. Other (specify)		

Maintenance Item	Satisfactory/ Unsatisfactory	Comments
3. Permanent Pool (Wet Ponds) (monthly)		
1. Undesirable vegetative growth		
2. Floating or floatable debris removal required		
3. Visible pollution		
4. Shoreline problem		
5. Other (specify)		
4. Sediment Forebays		
1. Sedimentation noted		
2. Sediment cleanout when depth < 50% design depth		
5. Dry Pond Areas		
1. Vegetation adequate		
2. Undesirable vegetative growth		
3. Undesirable woody vegetation		
4. Low flow channels clear of obstructions		
5. Standing water or wet spots		
6. Sediment and / or trash accumulation		
7. Other (specify)		
6. Condition of Outfalls (Annual , After Major Storms)		
1. Riprap failures		
2. Slope erosion		
3. Storm drain pipes		
4. Endwalls / Headwalls		
5. Other (specify)		
7. Other (Monthly)		
1. Encroachment on pond, wetland or easement area		

Maintenance Item	Satisfactory/ Unsatisfactory	Comments
2. Complaints from residents		
3. Aesthetics a. Grass growing required		
b. Graffiti removal needed		
c. Other (specify)		
4. Conditions of maintenance access routes.		
5. Signs of hydrocarbon build-up		
6. Any public hazards (specify)		
8. Wetland Vegetation (Annual)		
1. Vegetation healthy and growing Wetland maintaining 50% surface area coverage of wetland plants after the second growing season. (If unsatisfactory, reinforcement plantings needed)		
2. Dominant wetland plants: Survival of desired wetland plant species Distribution according to landscaping plan?		
3. Evidence of invasive species		
4. Maintenance of adequate water depths for desired wetland plant species		
5. Harvesting of emergent plantings needed		
6. Have sediment accumulations reduced pool volume significantly or are plants "choked" with sediment		
7. Eutrophication level of the wetland.		
8. Other (specify)		

Comments:

Actions to be Taken:

Infiltration Trench Operation, Maintenance, and Management Inspection Checklist

Project:
 Location:
 Site Status:

Date:

Time:

Inspector:

MAINTENANCE ITEM	SATISFACTORY / UNSATISFACTORY	COMMENTS
1. Debris Cleanout (Monthly)		
Trench surface clear of debris		
Inflow pipes clear of debris		
Overflow spillway clear of debris		
Inlet area clear of debris		
2. Sediment Traps or Forebays (Annual)		
Obviously trapping sediment		
Greater than 50% of storage volume remaining		
3. Dewatering (Monthly)		
Trench dewaterers between storms		
4. Sediment Cleanout of Trench (Annual)		
No evidence of sedimentation in trench		
Sediment accumulation doesn't yet require cleanout		
5. Inlets (Annual)		

MAINTENANCE ITEM	SATISFACTORY / UNSATISFACTORY	COMMENTS
Good condition		
No evidence of erosion		
6. Outlet/Overflow Spillway (Annual)		
Good condition, no need for repair		
No evidence of erosion		
7. Aggregate Repairs (Annual)		
Surface of aggregate clean		
Top layer of stone does not need replacement		
Trench does not need rehabilitation		

Comments:

Actions to be Taken:

Sand/Organic Filter Operation, Maintenance and Management Inspection Checklist

Project:
Location:
Site Status:

Date:

Time:

Inspector:

MAINTENANCE ITEM	SATISFACTORY / UNSATISFACTORY	COMMENTS
1. Debris Cleanout (Monthly)		
Contributing areas clean of debris		
Filtration facility clean of debris		
Inlet and outlets clear of debris		
2. Oil and Grease (Monthly)		
No evidence of filter surface clogging		
Activities in drainage area minimize oil and grease entry		
3. Vegetation (Monthly)		
Contributing drainage area stabilized		
No evidence of erosion		
Area mowed and clipping removed		
4. Water Retention Where Required (Monthly)		
Water holding chambers at normal pool		
No evidence of leakage		
5. Sediment Deposition (Annual)		

MAINTENANCE ITEM	SATISFACTORY / UNSATISFACTORY	COMMENTS
Filter chamber free of sediments		
Sedimentation chamber not more than half full of sediments		
6. Structural Components (Annual)		
No evidence of structural deterioration		
Any grates are in good condition		
No evidence of spalling or cracking of structural parts		
7. Outlet/Overflow Spillway (Annual)		
Good condition, no need for repairs		
No evidence of erosion (if draining into a natural channel)		
8. Overall Function of Facility (Annual)		
Evidence of flow bypassing facility		
No noticeable odors outside of facility		

Comments:

Actions to be Taken:

Open Channel Operation, Maintenance, and Management Inspection Checklist

Project:
 Location:
 Site Status:

Date:

Time:

Inspector:

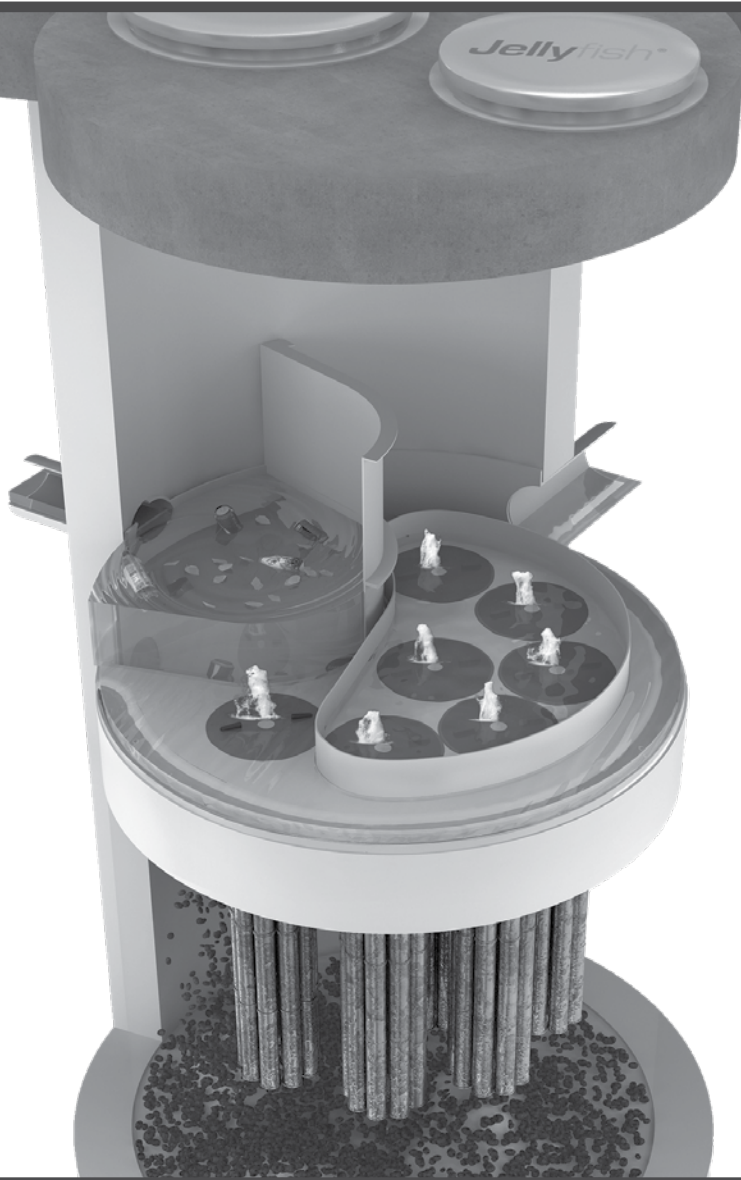
MAINTENANCE ITEM	SATISFACTORY/ UNSATISFACTORY	COMMENTS
1. Debris Cleanout (Monthly)		
Contributing areas clean of debris		
2. Check Dams or Energy Dissipators (Annual, After Major Storms)		
No evidence of flow going around structures		
No evidence of erosion at downstream toe		
Soil permeability		
Groundwater / bedrock		
3. Vegetation (Monthly)		
Mowing done when needed		
Minimum mowing depth not exceeded		
No evidence of erosion		
Fertilized per specification		
4. Dewatering (Monthly)		
Dewaterers between storms		

MAINTENANCE ITEM	SATISFACTORY/ UNSATISFACTORY	COMMENTS
5. Sediment deposition (Annual)		
Clean of sediment		
6. Outlet/Overflow Spillway (Annual)		
Good condition, no need for repairs		
No evidence of erosion		

Comments:

Actions to be Taken:

Jellyfish[®] Filter Maintenance Guide





JELLYFISH® FILTER INSPECTION & MAINTENANCE GUIDE

Jellyfish units are often just one of many structures in a more comprehensive stormwater drainage and treatment system.

In order for maintenance of the Jellyfish filter to be successful, it is imperative that all other components be properly maintained. The maintenance and repair of upstream facilities should be carried out prior to Jellyfish maintenance activities.

In addition to considering upstream facilities, it is also important to correct any problems identified in the drainage area. Drainage area concerns may include: erosion problems, heavy oil loading, and discharges of inappropriate materials.

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1.0 Inspection and Maintenance Overview

The primary purpose of the Jellyfish® Filter is to capture and remove pollutants from stormwater runoff. As with any filtration system, these pollutants must be removed to maintain the filter's maximum treatment performance. Regular inspection and maintenance are required to insure proper functioning of the system.

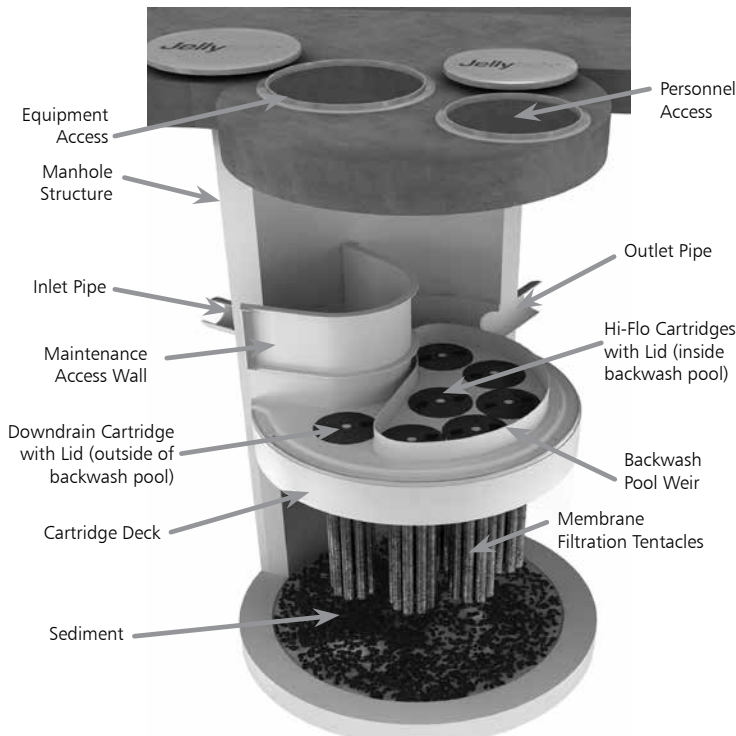
Maintenance frequencies and requirements are site specific and vary depending on pollutant loading. Additional maintenance activities may be required in the event of non-storm event runoff, such as base-flow or seasonal flow, an upstream chemical spill or due to excessive sediment loading from site erosion or extreme runoff events. It is a good practice to inspect the system after major storm events.

Inspection activities are typically conducted from surface observations and include:

- Observe if standing water is present
- Observe if there is any physical damage to the deck or cartridge lids
- Observe the amount of debris in the Maintenance Access Wall (MAW) or inlet bay for vault systems

Maintenance activities include:

- Removal of oil, floatable trash and debris
- Removal of collected sediments
- Rinsing and re-installing the filter cartridges
- Replace filter cartridge tentacles, as needed



Note: Separator Skirt not shown

2.0 Inspection Timing

Inspection of the Jellyfish Filter is key in determining the maintenance requirements for, and to develop a history of, the site's pollutant loading characteristics. In general, inspections should be performed at the times indicated below; *or per the approved project stormwater quality documents (if applicable), whichever is more frequent.*

1. A minimum of quarterly inspections during the first year of operation to assess the sediment and floatable pollutant accumulation, and to ensure proper functioning of the system.
2. Inspection frequency in subsequent years is based on the inspection and maintenance plan developed in the first year of operation. Minimum frequency should be once per year.
3. Inspection is recommended after each major storm event.
4. Inspection is required immediately after an upstream oil, fuel or other chemical spill.

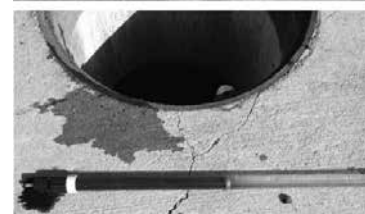
3.0 Inspection Procedure

The following procedure is recommended when performing inspections:

1. Provide traffic control measures as necessary.
2. Inspect the MAW or inlet bay for floatable pollutants such as trash, debris, and oil sheen.
3. Measure oil and sediment depth in several locations, by lowering a sediment probe until contact is made with the floor of the structure. Record sediment depth, and presences of any oil layers.
4. Inspect cartridge lids. Missing or damaged cartridge lids to be replaced.
5. Inspect the MAW (where appropriate), cartridge deck and receptacles, and backwash pool weir, for damaged or broken components.

3.1 Dry weather inspections

- Inspect the cartridge deck for standing water, and/or sediment on the deck.
- No standing water under normal operating conditions.
- Standing water inside the backwash pool, but not outside the backwash pool indicates, that the filter cartridges need to be rinsed.



Inspection Utilizing Sediment Probe

- Standing water outside the backwash pool is not anticipated and may indicate a backwater condition caused by high water elevation in the receiving water body, or possibly a blockage in downstream infrastructure.
- Any appreciable sediment ($\geq 1/16''$) accumulated on the deck surface should be removed.

3.2 Wet weather inspections

- Observe the rate and movement of water in the unit. Note the depth of water above deck elevation within the MAW or inlet bay.
- Less than 6 inches, flow should be exiting the cartridge lids of each of the draindown cartridges (i.e. cartridges located outside the backwash pool).
- Greater than 6 inches, flow should be exiting the cartridge lids of each of the draindown cartridges and each of the hi-flo cartridges (i.e. cartridges located inside the backwash pool), and water should be overflowing the backwash pool weir.
- 18 inches or greater and relatively little flow is exiting the cartridge lids and outlet pipe, this condition indicates that the filter cartridges need to be rinsed.

4.0 Maintenance Requirements

Required maintenance for the Jellyfish Filter is based upon results of the most recent inspection, historical maintenance records, or the site specific water quality management plan; whichever is more frequent. In general, maintenance requires some combination of the following:

1. Sediment removal for depths reaching 12 inches or greater, or within 3 years of the most recent sediment cleaning, whichever occurs sooner.
2. Floatable trash, debris, and oil removal.
3. Deck cleaned and free from sediment.
4. Filter cartridges rinsed and re-installed as required by the most recent inspection results, or within 12 months of the most recent filter rinsing, whichever occurs sooner.
5. Replace tentacles if rinsing does not restore adequate hydraulic capacity, remove accumulated sediment, or if damaged or missing. It is recommended that tentacles should remain in service no longer than 5 years before replacement.
6. Damaged or missing cartridge deck components must be repaired or replaced as indicated by results of the most recent inspection.
7. The unit must be cleaned out and filter cartridges inspected immediately after an upstream oil, fuel, or chemical spill. Filter cartridge tentacles should be replaced if damaged or compromised by the spill.

5.0 Maintenance Procedure

The following procedures are recommended when maintaining the Jellyfish Filter:

1. Provide traffic control measures as necessary.
2. Open all covers and hatches. Use ventilation equipment as required, according to confined space entry procedures.
Caution: Dropping objects onto the cartridge deck may cause damage.

3. Perform Inspection Procedure prior to maintenance activity.
4. To access the cartridge deck for filter cartridge service, descend into the structure and step directly onto the deck. Caution: Do not step onto the maintenance access wall (MAW) or backwash pool weir, as damage may result. Note that the cartridge deck may be slippery.
5. Maximum weight of maintenance crew and equipment on the cartridge deck not to exceed 450 lbs.

5.1 Filter Cartridge Removal

1. Remove a cartridge lid.
2. Remove cartridges from the deck using the lifting loops in the cartridge head plate. Rope or a lifting device (available from Contech) should be used. **Caution: Should a snag occur, do not force the cartridge upward as damage to the tentacles may result. Wet cartridges typically weigh between 100 and 125 lbs.**
3. Replace and secure the cartridge lid on the exposed empty receptacle as a safety precaution. Contech does not recommend exposing more than one empty cartridge receptacle at a time.

5.2 Filter Cartridge Rinsing

1. Remove all 11 tentacles from the cartridge head plate. Take care not to lose or damage the O-ring seal as well as the plastic threaded nut and connector.



Cartridge Removal & Lifting Device



2. Position tentacles in a container (or over the MAW), with the threaded connector (open end) facing down, so rinse water is flushed through the membrane and captured in the container.
3. Using the Jellyfish rinse tool (available from Contech) or a low-pressure garden hose sprayer, direct water spray onto the tentacle membrane, sweeping from top to bottom along the length of the tentacle. Rinse until all sediment is removed from the membrane. **Caution: Do not use a high pressure sprayer or focused stream of water on the membrane. Excessive water pressure may damage the membrane.**

4. Collected rinse water is typically removed by vacuum hose.
5. Reassemble cartridges as detailed later in this document. Reuse O-rings and nuts, ensuring proper placement on each tentacle.

5.3 Sediment and Floatables Extraction

1. Perform vacuum cleaning of the Jellyfish Filter only after filter cartridges have been removed from the system. Access the lower chamber for vacuum cleaning only through the maintenance access wall (MAW) opening. Be careful not to damage the flexible plastic separator skirt that is attached to the underside of the deck on manhole systems. Do not lower the vacuum wand through a cartridge receptacle, as damage to the receptacle will result.
2. Vacuum floatable trash, debris, and oil, from the MAW opening or inlet bay. Alternatively, floatable solids may be removed by a net or skimmer.



Vacuuming Sump Through MAW

3. Pressure wash cartridge deck and receptacles to remove all sediment and debris. Sediment should be rinsed into the sump area. Take care not to flush rinse water into the outlet pipe.
4. Remove water from the sump area. Vacuum or pump equipment should only be introduced through the MAW or inlet bay.
5. Remove the sediment from the bottom of the unit through the MAW or inlet bay opening.



Vacuuming Sump Through MAW

6. For larger diameter Jellyfish Filter manholes (≥ 8 -ft) and some vaults complete sediment removal may be facilitated by removing a cartridge lid from an empty receptacle and inserting a jetting wand (not a vacuum wand) through the receptacle. Use the sprayer to rinse loosened sediment toward the vacuum hose in the MAW opening, being careful not to damage the receptacle.

5.4 Filter Cartridge Reinstallation and Replacement

1. Cartridges should be installed after the deck has been cleaned. It is important that the receptacle surfaces be free from grit and debris.
2. Remove cartridge lid from deck and carefully lower the filter cartridge into the receptacle until head plate gasket is seated squarely in receptacle. **Caution: Do not force the cartridge downward; damage may occur.**
3. Replace the cartridge lid and check to see that both male threads are properly seated before rotating approximately 1/3 of a full rotation until firmly seated. Use of an approved rim gasket lubricant may facilitate installation. See next page for additional details.
4. If rinsing is ineffective in removing sediment from the tentacles, or if tentacles are damaged, provisions must be made to replace the spent or damaged tentacles with new tentacles. Contact Contech to order replacement tentacles.

5.5 Chemical Spills

Caution: If a chemical spill has been captured, do not attempt maintenance. Immediately contact the local hazard response agency and contact Contech.

5.6 Material Disposal

The accumulated sediment found in stormwater treatment and conveyance systems must be handled and disposed of in accordance with regulatory protocols. It is possible for sediments to contain measurable concentrations of heavy metals and organic chemicals (such as pesticides and petroleum products). Areas with the greatest potential for high pollutant loading include industrial areas and heavily traveled roads. Sediments and water must be disposed of in accordance with all applicable waste disposal regulations. When scheduling maintenance, consideration must be made for the disposal of solid and liquid wastes. This typically requires coordination with a local landfill for solid waste disposal. For liquid waste disposal a number of options are available including a municipal vacuum truck decant facility, local waste water treatment plant or on-site treatment and discharge.

Jellyfish Filter Components & Filter Cartridge Assembly and Installation

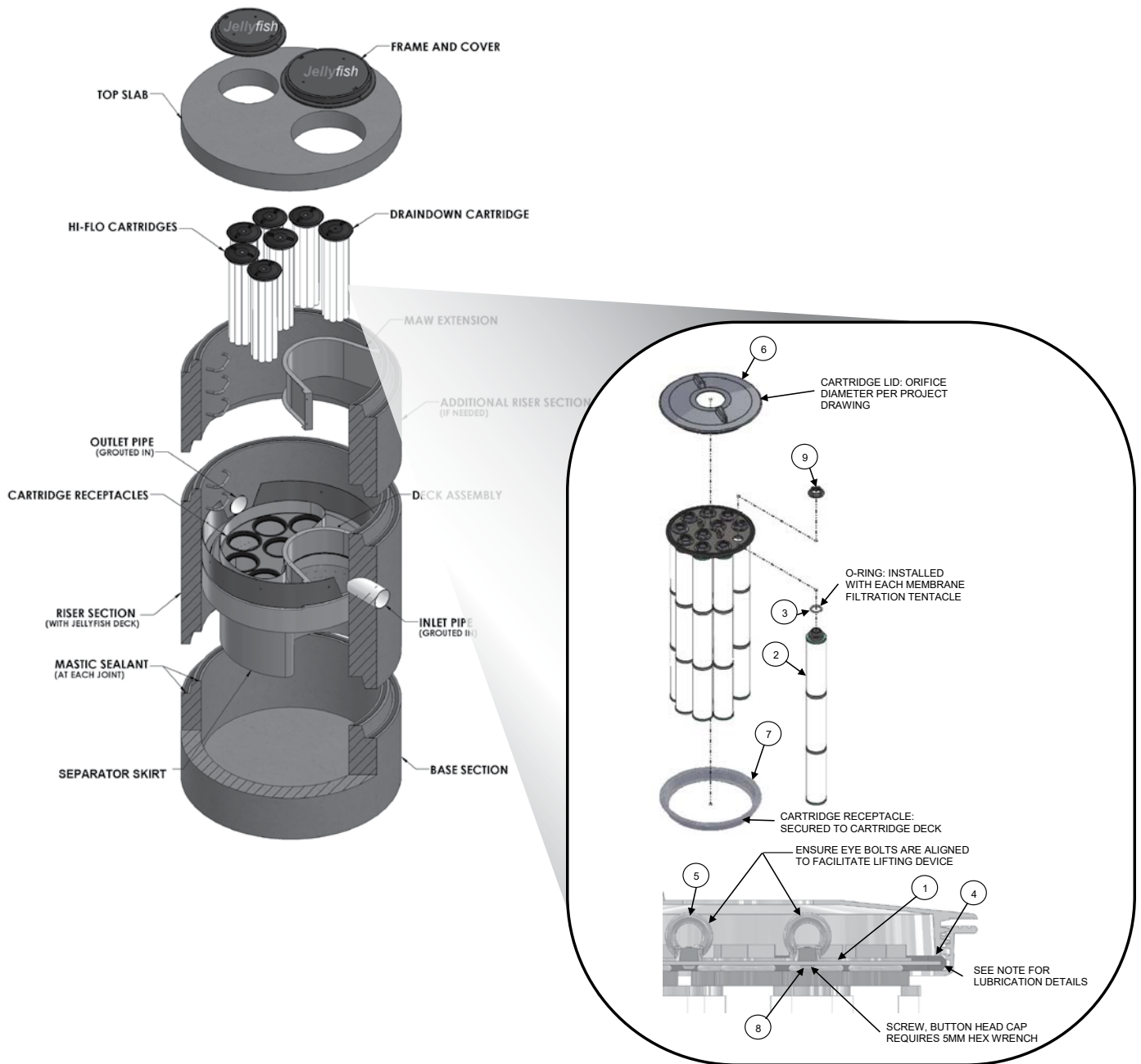


TABLE 1: BOM

ITEM NO.	DESCRIPTION
1	JF HEAD PLATE
2	JF TENTACLE
3	JF O-RING
4	JF HEAD PLATE GASKET
5	JF CARTRIDGE EYELET
6	JF 14IN COVER
7	JF RECEPTACLE
8	BUTTON HEAD CAP SCREW M6X14MM SS
9	JF CARTRIDGE NUT

TABLE 2: APPROVED GASKET LUBRICANTS

PART NO.	MFR	DESCRIPTION
78713	LA-CO	LUBRI-JOINT
40501	HERCULES	DUCK BUTTER
30600	OATEY	PIPE LUBRICANT
PSLUBXL1Q	PROSELECT	PIPE JOINT LUBRICANT

NOTES:

Head Plate Gasket Installation:

Install Head Plate Gasket (Item 4) onto the Head Plate (Item 1) and liberally apply a lubricant from Table 2: Approved Gasket Lubricants onto the gasket where it contacts the Receptacle (Item 7) and Cartridge Lide (Item 6). Follow Lubricant manufacturer's instructions.

Lid Assembly:

Rotate Cartridge Lid counter-clockwise until both male threads drop down and properly seat. Then rotate Cartridge Lid clock-wise approximately one-third of a full rotation until Cartridge Lid is firmly secured, creating a watertight seal.

Jellyfish Filter Inspection and Maintenance Log

Owner:		Jellyfish Model No:	
Location:		GPS Coordinates:	
Land Use:	Commercial:	Industrial:	Service Station:
	Roadway/Highway:	Airport:	Residential:

Date/Time:						
Inspector:						
Maintenance Contractor:						
Visible Oil Present: (Y/N)						
Oil Quantity Removed:						
Floatable Debris Present: (Y/N)						
Floatable Debris Removed: (Y/N)						
Water Depth in Backwash Pool						
Draindown Cartridges externally rinsed and recommissioned: (Y/N)						
New tentacles put on Draindown Cartridges: (Y/N)						
Hi-Flo Cartridges externally rinsed and recommissioned: (Y/N)						
New tentacles put on Hi-Flo Cartridges: (Y/N)						
Sediment Depth Measured: (Y/N)						
Sediment Depth (inches or mm):						
Sediment Removed: (Y/N)						
Cartridge Lids intact: (Y/N)						
Observed Damage:						
Comments:						



Support

- Drawings and specifications are available at www.conteches.com/jellyfish.
- Site-specific design support is available from Contech Engineered Solutions.
- Find a Certified Maintenance Provider at www.conteches.com/ccmp

Jellyfish[®]

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Isolator[®] Row Plus

O&M Manual



The Isolator[®] Row Plus

Introduction

An important component of any Stormwater Pollution Prevention Plan is inspection and maintenance. The StormTech Isolator Row Plus is a technique to inexpensively enhance Total Suspended Solids (TSS) and Total Phosphorus (TP) removal with easy access for inspection and maintenance.

The Isolator Row Plus

The Isolator Row Plus is a row of StormTech chambers, either SC-160, SC-310, SC-310-3, SC-740, DC-780, MC-3500 or MC-7200 models, that is surrounded with filter fabric and connected to a closely located manhole for easy access. The fabric-wrapped chambers provide for sediment settling and filtration as stormwater rises in the Isolator Row Plus and passes through the filter fabric. The open bottom chambers and perforated sidewalls (SC-310, SC-310-3 and SC-740 models) allow stormwater to flow both vertically and horizontally out of the chambers. Sediments are captured in the Isolator Row Plus protecting the adjacent stone and chambers storage areas from sediment accumulation.

ADS geotextile fabric is placed between the stone and the Isolator Row Plus chambers. The woven geotextile provides a media for stormwater filtration, a durable surface for maintenance, prevents scour of the underlying stone and remains intact during high pressure jetting. A non-woven fabric is placed over the chambers to provide a filter media for flows passing through the chamber's sidewall. The non-woven fabric is not required over the SC-160, DC-780, MC-3500 or MC-7200 models as these chambers do not have perforated side walls.

The Isolator Row Plus is designed to capture the "first flush" runoff and offers the versatility to be sized on a volume basis or a flow-rate basis. An upstream manhole provides access to the Isolator Row Plus and includes a high/low concept such that stormwater flow rates or volumes that exceed the capacity of the Isolator Row Plus bypass through a manifold to the other chambers. This is achieved with an elevated bypass manifold or a high-flow weir. This creates a differential between the Isolator Row Plus row of chambers and the manifold to the rest of the system, thus allowing for settlement time in the Isolator Row Plus. After Stormwater flows through the Isolator Row Plus and into the rest of the chamber system it is either exfiltrated into the soils below or passed at a controlled rate through an outlet manifold and outlet control structure.

The Isolator Row FLAMP[™] (patent pending) is a flared end ramp apparatus attached to the inlet pipe on the inside of the chamber end cap. The FLAMP provides a smooth transition from pipe invert to fabric bottom. It is configured to improve chamber function performance by enhancing outflow of solid debris that would otherwise collect at the chamber's end. It also serves to improve the fluid and solid flow into the access pipe during maintenance and cleaning and to guide cleaning and inspection equipment back into the inlet pipe when complete.

The Isolator Row Plus may be part of a treatment train system. The treatment train design and pretreatment device selection by the design engineer is often driven by regulatory requirements. Whether pretreatment is used or not, StormTech recommend using the Isolator Row Plus to minimize maintenance requirements and maintenance costs.

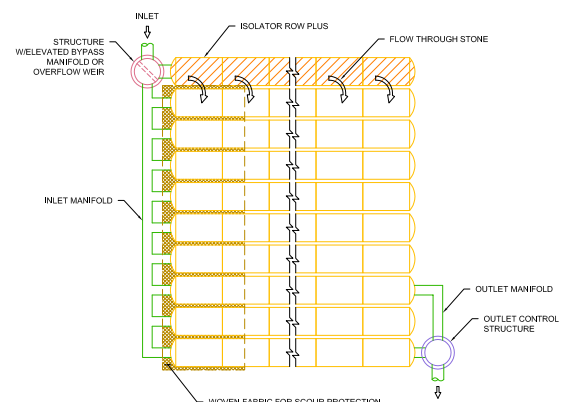
Note: See the StormTech Design Manual for detailed information on designing inlets for a StormTech system, including the Isolator Row Plus.



Looking down the Isolator Row PLUS from the manhole opening, ADS PLUS Fabric is shown between the chamber and stone base.



StormTech Isolator Row PLUS with Overflow Spillway (not to scale)



Isolator Row Plus Inspection/Maintenance

Inspection

The frequency of inspection and maintenance varies by location. A routine inspection schedule needs to be established for each individual location based upon site specific variables. The type of land use (i.e. industrial, commercial, residential), anticipated pollutant load, percent imperviousness, climate, etc. all play a critical role in determining the actual frequency of inspection and maintenance practices.

At a minimum, StormTech recommends annual inspections. Initially, the Isolator Row Plus should be inspected every 6 months for the first year of operation. For subsequent years, the inspection should be adjusted based upon previous observation of sediment deposition.

The Isolator Row Plus incorporates a combination of standard manhole(s) and strategically located inspection ports (as needed). The inspection ports allow for easy access to the system from the surface, eliminating the need to perform a confined space entry for inspection purposes.

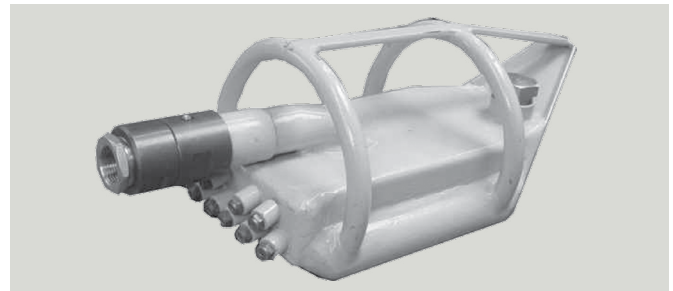
If upon visual inspection it is found that sediment has accumulated, a stadia rod should be inserted to determine the depth of sediment. When the average depth of sediment exceeds 3 inches throughout the length of the Isolator Row Plus, clean-out should be performed.

Maintenance

The Isolator Row Plus was designed to reduce the cost of periodic maintenance. By "isolating" sediments to just one row, costs are dramatically reduced by eliminating the need to clean out each row of the entire storage bed. If inspection indicates the potential need for maintenance, access is provided

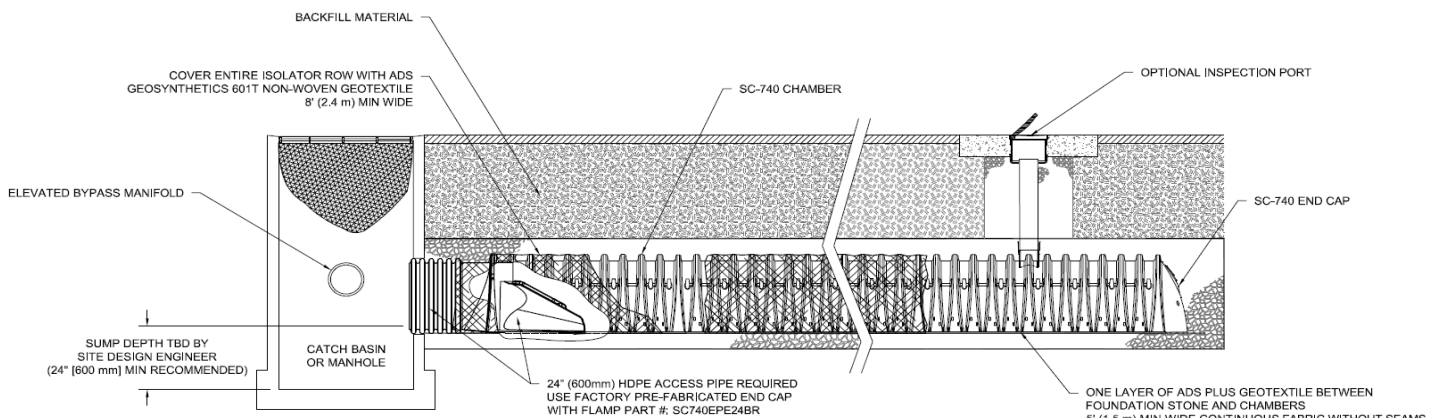
via a manhole(s) located on the end(s) of the row for cleanout. If entry into the manhole is required, please follow local and OSHA rules for a confined space entries.

Maintenance is accomplished with the JetVac process. The JetVac process utilizes a high pressure water nozzle to propel itself down the Isolator Row Plus while scouring and suspending sediments. As the nozzle is retrieved, the captured pollutants are flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/JetVac combination vehicles. Selection of an appropriate JetVac nozzle will improve maintenance efficiency. Fixed nozzles designed for culverts or large diameter pipe cleaning are preferable. Rear facing jets with an effective spread of at least 45" are best. StormTech recommends a maximum nozzle pressure of 2000 psi be utilized during cleaning. JetVac reels can vary in length. For ease of maintenance, ADS recommends Isolator Row Plus lengths up to 200' (61 m). **The JetVac process shall only be performed on StormTech Isolator Row Plus that have ADS Plus Fabric (as specified by StormTech) over their angular base stone.**



StormTech Isolator Row PLUS (not to scale)

Note: Non-woven fabric is only required over the inlet pipe connection into the end cap for SC-160LP, DC-780, MC-3500 and MC-7200 chamber models and is not required over the entire Isolator Row PLUS.



Isolator Row Plus Step By Step Maintenance Procedures

Step 1

Inspect Isolator Row Plus for sediment.

- A) Inspection ports (if present)
 - i. Remove lid from floor box frame
 - ii. Remove cap from inspection riser
 - iii. Using a flashlight and stadia rod, measure depth of sediment and record results on maintenance log.
 - iv. If sediment is at or above 3 inch depth, proceed to Step 2. If not, proceed to Step 3.
- B) All Isolator Row Plus
 - i. Remove cover from manhole at upstream end of Isolator Row Plus
 - ii. Using a flashlight, inspect down Isolator Row Plus through outlet pipe
 - 1. Mirrors on poles or cameras may be used to avoid a confined space entry
 - 2. Follow OSHA regulations for confined space entry if entering manhole
 - iii. If sediment is at or above the lower row of sidewall holes (approximately 3 inches), proceed to Step 2. If not, proceed to Step 3.

Step 2

Clean out Isolator Row Plus using the JetVac process.

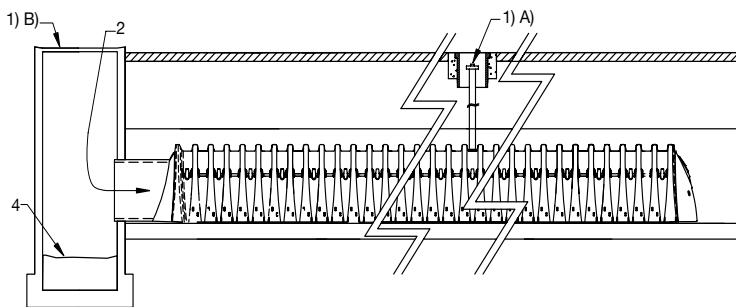
- A) A fixed floor cleaning nozzle with rear facing nozzle spread of 45 inches or more is preferable
- B) Apply multiple passes of JetVac until backflush water is clean
- C) Vacuum manhole sump as required

Step 3

Replace all caps, lids and covers, record observations and actions.

Step 4

Inspect & clean catch basins and manholes upstream of the StormTech system.



Sample Maintenance Log

Date	Stadia Rod Readings		Sedi-ment Depth (1)-(2)	Observations/Actions	Inspector
	Fixed point to chamber bottom (1)	Fixed point to top of sediment (2)			
3/15/11	6.3 ft	none		New installation. Fixed point is CI frame at grade	DJM
9/24/11		6.2	0.1 ft	Some grit felt	SM
6/20/13		5.8	0.5 ft	Mucky feel, debris visible in manhole and in Isolator Row PLUS, maintenance due	NV
7/7/13	6.3 ft		0	System jetted and vacuumed	DJM

adspipe.com

800-821-6710

5.1.6 Soil Restoration

Description

Soil Restoration is a required practice applied across areas of a development site where soils have been disturbed and will be vegetated in order to recover the original properties and porosity of the soil. Healthy soil is vital to a sustainable environment and landscape. A deep, well drained soil, rich in organic matter, absorbs rainwater, helps prevent flooding and soil erosion, filters out water pollutants, and promotes vigorous plant growth that requires less irrigation, pesticides, and fertilizer.

Soil Restoration is applied in the cleanup, restoration, and landscaping phase of construction followed by the permanent establishment of an appropriate, deep-rooted groundcover to help maintain the restored soil structure. Soil restoration includes mechanical decompaction, compost amendment, or both.

Many runoff reduction practices need Soil Restoration measures applied over and adjacent to the practice to achieve runoff reduction performance. (See typical compacted soil in Figure 5.15). Consult individual profile sheets for specific design criteria.

Figure 5.14 Shows typical compacted soils that nearly reach the bulk density of concrete (Schueler et al 2000)



Key Benefits

- More marketable buildings and landscapes
- Less stormwater runoff, better water quality
- Healthier, aesthetically pleasing landscapes
- Increased porosity on redevelopment sites where impervious cover is converted to pervious
- Achieves performance standards on runoff reduction practices
- Decreases runoff volume generated and lowers the demand on runoff control structures
- Enhances direct groundwater recharge
- Promotes successful long-term revegetation by restoring soil organic matter, permeability, drainage and water holding capacity for healthy root system development of trees, shrubs and deep-rooted ground covers, minimizing lawn chemical requirements, plant drowning during wet periods, and burnout during dry periods

Typical Perceived Obstacles and Realities

New York State Stormwater Management Design Manual

Chapter 5: Green Infrastructure Practices

Section 5.1 Planning for Green Infrastructure: Preservation of Natural Features and Conservation Design

- Higher cost due to soil restoration- *application of soil de-compaction and enhancement may have additional initial cost; however, they provide benefit in reducing the need for conveyance structures.*
- Space constraints and obstruction for use of equipment - *post construction space may limit the ability of some of the de-compaction equipment, however, alternative equipment and sensible planning help overcome this obstacle.*

Discussion

Tilling exposes compacted soil devoid of oxygen to air and recreates temporary air space. In addition, research has shown that the incorporation of organic compost, can greatly improve temporary water storage in the soil and subsequent runoff reduction through infiltration and evapotranspiration.

Soils that have a permanent high water table close to the surface (0-12 inches), either influenced by a clay or other highly impervious layer of material, may have bulk densities so naturally high that compaction has little added impact on infiltration (Lacey 2008). However, these soils will still benefit from the addition of compost. The water holding capacity, penetration, structural stability, and fertility of clay soils were improved with compost mixing (Avnimelech and Cohen 1988).

Table 5.3 describes various soil disturbance activities related to land development, soil types and the requirements for soil restoration for each activity. Soil Restoration or modification of curve numbers is a required practice. Restoration is applied across areas of a development site where soils have been compacted and will be vegetated according to the criteria defined in Table 5.3. If Soil Restoration is not applied according to these criteria, designers are required to:

- a) Increase the calculated WQv by factoring in the compacted areas that have not been kept as impervious cover (including areas of cut or fill, heavy traffic areas on site, or Impervious Cover reduction in redevelopment projects unless aeration or full soil restoration is applied, per Table 5.3).
- b) Change by one level the post-construction hydrologic soil group (HSG) to a less permeable group than the original condition. This is applied to all volumetric and discharge rate control computations.

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Table 5.3 Soil Restoration Requirements			
Type of Soil Disturbance	Soil Restoration Requirement		Comments/Examples
No soil disturbance	Restoration not permitted		Preservation of Natural Features
Minimal soil disturbance	Restoration not required		Clearing and grubbing
Areas where topsoil is stripped only - no change in grade	HSG A & B	HSG C&D	Protect area from any ongoing construction activities.
	apply 6 inches of topsoil	Aerate* and apply 6 inches of topsoil	
Areas of cut or fill	HSG A & B	HSG C & D	
	Aerate and apply 6 inches of topsoil	Apply full Soil Restoration **	
Heavy traffic areas on site (especially in a zone 5-25 feet around buildings but not within a 5 foot perimeter around foundation walls)	Apply full Soil Restoration (de-compaction and compost enhancement)		
Areas where Runoff Reduction and/or Infiltration practices are applied	Restoration not required, but may be applied to enhance the reduction specified for appropriate practices.		Keep construction equipment from crossing these areas. To protect newly installed practice from any ongoing construction activities construct a single phase operation fence area
Redevelopment projects	Soil Restoration is required on redevelopment projects in areas where existing impervious area will be converted to pervious area.		

*Aeration includes the use of machines such as tractor-drawn implements with coulters making a narrow slit in the soil, a roller with many spikes making indentations in the soil, or prongs which function like a mini-subsoiler.

** Per “Deep Ripping and De-compaction, DEC 2008”.

Using this Practice

During periods of relatively low to moderate subsoil moisture, the disturbed subsoils are returned to rough grade and the following Soil Restoration steps applied:

- 1) Apply 3 inches of compost over subsoil

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- 2) Till compost into subsoil to a depth of at least 12 inches using a cat-mounted ripper, tractor-mounted disc, or tiller, mixing, and circulating air and compost into subsoils
- 3) Rock-pick until uplifted stone/rock materials of four inches and larger size are cleaned off the site
- 4) Apply topsoil to a depth of 6 inches
- 5) Vegetate as required by approved plan.

At the end of the project an inspector should be able to push a 3/8" metal bar 12 inches into the

soil just with body weight. Figures 5.16 and 5.17 show two attachments used for soil decompaction. Tilling (step 2 above) should not be performed within the drip line of any existing trees or over utility installations that are within 24 inches of the surface.

COMPOST SPECIFICATIONS

Compost shall be aged, from plant derived materials, free of viable weed seeds, have no visible free water or dust produced when handling, pass through a half inch screen and have a pH suitable to grow desired plants.

Maintenance

A simple maintenance agreement should identify where Soil Restoration is applied, where newly restored areas are/cannot be cleared, who the responsible parties are to ensure that routine vegetation improvements are made (i.e., thinning, invasive plant removal, etc.). Soil compost amendments within a filter strip or grass channel should be located in public right of way, or within a dedicated stormwater or drainage easement.

First year maintenance operations includes:

- Initial inspections for the first six months (once after each storm greater than half- inch)

Figure 5.15 Soil aerator implement



Figure 5.16 Soil aerator implement



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- Reseeding to repair bare or eroding areas to assure grass stabilization
- Water once every three days for first month, and then provide a half inch of water per week during first year. Irrigation plan may be adjusted according to the rain event.
- Fertilization may be needed in the fall after the first growing season to increase plant vigor
- Ongoing Maintenance:

Two points help ensure lasting results of decompaction:

- 1) Planting the appropriate ground cover with deep roots to maintain the soil structure
- 2) Keeping the site free of vehicular and foot traffic or other weight loads. Consider pedestrian footpaths. (Sometimes it may be necessary to de-thatch the turf every few years)

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APPENDIX E

SPDES PERMIT



Department of
Environmental
Conservation

NEW YORK STATE
DEPARTMENT OF ENVIRONMENTAL CONSERVATION

SPDES GENERAL PERMIT
FOR STORMWATER DISCHARGES

From

CONSTRUCTION ACTIVITY

Permit No. GP- 0-20-001

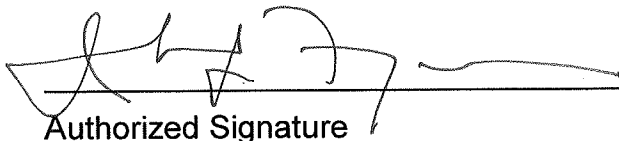
Issued Pursuant to Article 17, Titles 7, 8 and Article 70
of the Environmental Conservation Law

Effective Date: January 29, 2020

Expiration Date: January 28, 2025

John J. Ferguson

Chief Permit Administrator



Authorized Signature

1-23-20

Date

Address: NYS DEC
Division of Environmental Permits
625 Broadway, 4th Floor
Albany, N.Y. 12233-1750

PREFACE

Pursuant to Section 402 of the Clean Water Act (“CWA”), stormwater *discharges* from certain *construction activities* are unlawful unless they are authorized by a *National Pollutant Discharge Elimination System (“NPDES”)* permit or by a state permit program. New York administers the approved State Pollutant Discharge Elimination System (SPDES) program with permits issued in accordance with the New York State Environmental Conservation Law (ECL) Article 17, Titles 7, 8 and Article 70.

An *owner or operator* of a *construction activity* that is eligible for coverage under this permit must obtain coverage prior to the *commencement of construction activity*. Activities that fit the definition of “*construction activity*”, as defined under 40 CFR 122.26(b)(14)(x), (15)(i), and (15)(ii), constitute construction of a *point source* and therefore, pursuant to ECL section 17-0505 and 17-0701, the *owner or operator* must have coverage under a SPDES permit prior to *commencing construction activity*. The *owner or operator* cannot wait until there is an actual *discharge* from the *construction site* to obtain permit coverage.

***Note: The italicized words/phrases within this permit are defined in Appendix A.**

**NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION
SPDES GENERAL PERMIT FOR STORMWATER DISCHARGES FROM
CONSTRUCTION ACTIVITIES**

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Part 1. PERMIT COVERAGE AND LIMITATIONS

A. Permit Application

This permit authorizes stormwater *discharges to surface waters of the State* from the following *construction activities* identified within 40 CFR Parts 122.26(b)(14)(x), 122.26(b)(15)(i) and 122.26(b)(15)(ii), provided all of the eligibility provisions of this permit are met:

1. *Construction activities* involving soil disturbances of one (1) or more acres; including disturbances of less than one acre that are part of a *larger common plan of development or sale* that will ultimately disturb one or more acres of land; excluding *routine maintenance activity* that is performed to maintain the original line and grade, hydraulic capacity or original purpose of a facility;
2. *Construction activities* involving soil disturbances of less than one (1) acre where the Department has determined that a *SPDES* permit is required for stormwater *discharges* based on the potential for contribution to a violation of a *water quality standard* or for significant contribution of *pollutants to surface waters of the State*.
3. *Construction activities* located in the watershed(s) identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.

B. Effluent Limitations Applicable to Discharges from Construction Activities

Discharges authorized by this permit must achieve, at a minimum, the effluent limitations in Part I.B.1. (a) – (f) of this permit. These limitations represent the degree of effluent reduction attainable by the application of best practicable technology currently available.

1. Erosion and Sediment Control Requirements - The *owner or operator* must select, design, install, implement and maintain control measures to *minimize the discharge of pollutants* and prevent a violation of the *water quality standards*. The selection, design, installation, implementation, and maintenance of these control measures must meet the non-numeric effluent limitations in Part I.B.1.(a) – (f) of this permit and be in accordance with the New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016, using sound engineering judgment. Where control measures are not designed in conformance with the design criteria included in the technical standard, the *owner or operator* must include in the *Stormwater Pollution Prevention Plan* (“SWPPP”) the reason(s) for the

deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.

- a. **Erosion and Sediment Controls.** Design, install and maintain effective erosion and sediment controls to *minimize* the *discharge of pollutants* and prevent a violation of the *water quality standards*. At a minimum, such controls must be designed, installed and maintained to:
- (i) *Minimize* soil erosion through application of runoff control and soil stabilization control measure to *minimize pollutant discharges*;
 - (ii) Control stormwater *discharges*, including both peak flowrates and total stormwater volume, to *minimize* channel and *streambank* erosion and scour in the immediate vicinity of the *discharge* points;
 - (iii) *Minimize* the amount of soil exposed during *construction activity*;
 - (iv) *Minimize* the disturbance of *steep slopes*;
 - (v) *Minimize* sediment *discharges* from the site;
 - (vi) Provide and maintain *natural buffers* around surface waters, direct stormwater to vegetated areas and maximize stormwater infiltration to reduce *pollutant discharges*, unless *infeasible*;
 - (vii) *Minimize* soil compaction. Minimizing soil compaction is not required where the intended function of a specific area of the site dictates that it be compacted;
 - (viii) Unless *infeasible*, preserve a sufficient amount of topsoil to complete soil restoration and establish a uniform, dense vegetative cover; and
 - (ix) *Minimize* dust. On areas of exposed soil, *minimize* dust through the appropriate application of water or other dust suppression techniques to control the generation of pollutants that could be discharged from the site.
- b. **Soil Stabilization.** In areas where soil disturbance activity has temporarily or permanently ceased, the application of soil stabilization measures must be initiated by the end of the next business day and completed within fourteen (14) days from the date the current soil disturbance activity ceased. For construction sites that *directly discharge* to one of the 303(d) segments

listed in Appendix E or is located in one of the watersheds listed in Appendix C, the application of soil stabilization measures must be initiated by the end of the next business day and completed within seven (7) days from the date the current soil disturbance activity ceased. See Appendix A for definition of *Temporarily Ceased*.

- c. **Dewatering.** *Discharges* from *dewatering* activities, including *discharges* from *dewatering* of trenches and excavations, must be managed by appropriate control measures.

- d. **Pollution Prevention Measures.** Design, install, implement, and maintain effective pollution prevention measures to *minimize* the *discharge* of *pollutants* and prevent a violation of the *water quality standards*. At a minimum, such measures must be designed, installed, implemented and maintained to:
 - (i) *Minimize* the *discharge* of *pollutants* from equipment and vehicle washing, wheel wash water, and other wash waters. This applies to washing operations that use clean water only. Soaps, detergents and solvents cannot be used;

 - (ii) *Minimize* the exposure of building materials, building products, construction wastes, trash, landscape materials, fertilizers, pesticides, herbicides, detergents, sanitary waste, hazardous and toxic waste, and other materials present on the site to precipitation and to stormwater. Minimization of exposure is not required in cases where the exposure to precipitation and to stormwater will not result in a *discharge* of *pollutants*, or where exposure of a specific material or product poses little risk of stormwater contamination (such as final products and materials intended for outdoor use) ; and

 - (iii) Prevent the *discharge* of *pollutants* from spills and leaks and implement chemical spill and leak prevention and response procedures.

- e. **Prohibited Discharges.** The following *discharges* are prohibited:
 - (i) Wastewater from washout of concrete;

 - (ii) Wastewater from washout and cleanout of stucco, paint, form release oils, curing compounds and other construction materials;

- (iii) Fuels, oils, or other *pollutants* used in vehicle and equipment operation and maintenance;
 - (iv) Soaps or solvents used in vehicle and equipment washing; and
 - (v) Toxic or hazardous substances from a spill or other release.
- f. Surface Outlets. When discharging from basins and impoundments, the outlets shall be designed, constructed and maintained in such a manner that sediment does not leave the basin or impoundment and that erosion at or below the outlet does not occur.

C. Post-construction Stormwater Management Practice Requirements

1. The *owner or operator* of a *construction activity* that requires post-construction stormwater management practices pursuant to Part III.C. of this permit must select, design, install, and maintain the practices to meet the *performance criteria* in the New York State Stormwater Management Design Manual (“Design Manual”), dated January 2015, using sound engineering judgment. Where post-construction stormwater management practices (“SMPs”) are not designed in conformance with the *performance criteria* in the Design Manual, the *owner or operator* must include in the SWPPP the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.
2. The *owner or operator* of a *construction activity* that requires post-construction stormwater management practices pursuant to Part III.C. of this permit must design the practices to meet the applicable *sizing criteria* in Part I.C.2.a., b., c. or d. of this permit.

a. Sizing Criteria for New Development

- (i) Runoff Reduction Volume (“RRv”): Reduce the total Water Quality Volume (“WQv”) by application of RR techniques and standard SMPs with RRv capacity. The total WQv shall be calculated in accordance with the criteria in Section 4.2 of the Design Manual.
- (ii) Minimum RRv and Treatment of Remaining Total WQv: Construction activities that cannot meet the criteria in Part I.C.2.a.(i) of this permit due to site limitations shall direct runoff from all newly constructed impervious areas to a RR technique or standard SMP with RRv capacity unless infeasible. The specific site limitations that prevent the reduction of 100% of the WQv shall be documented in the SWPPP.

For each impervious area that is not directed to a RR technique or standard SMP with RRv capacity, the SWPPP must include documentation which demonstrates that all options were considered and for each option explains why it is considered infeasible.

In no case shall the runoff reduction achieved from the newly constructed impervious areas be less than the Minimum RRv as calculated using the criteria in Section 4.3 of the Design Manual.

The remaining portion of the total WQv that cannot be reduced shall be treated by application of standard SMPs.

- (iii) Channel Protection Volume (“Cpv”): Provide 24 hour extended detention of the post-developed 1-year, 24-hour storm event; remaining after runoff reduction. The Cpv requirement does not apply when:
 - (1) Reduction of the entire Cpv is achieved by application of runoff reduction techniques or infiltration systems, or
 - (2) The site discharges directly to tidal waters, or fifth order or larger streams.

- (iv) *Overbank* Flood Control Criteria (“Qp”): Requires storage to attenuate the post-development 10-year, 24-hour peak discharge rate (Qp) to predevelopment rates. The Qp requirement does not apply when:
 - (1) the site discharges directly to tidal waters or fifth order or larger streams, or
 - (2) A downstream analysis reveals that *overbank* control is not required.

- (v) Extreme Flood Control Criteria (“Qf”): Requires storage to attenuate the post-development 100-year, 24-hour peak discharge rate (Qf) to predevelopment rates. The Qf requirement does not apply when:
 - (1) the site discharges directly to tidal waters or fifth order or larger streams, or
 - (2) A downstream analysis reveals that *overbank* control is not required.

b. Sizing Criteria for New Development in Enhanced Phosphorus Removal Watershed

- (i) Runoff Reduction Volume (RRv): Reduce the total Water Quality Volume (WQv) by application of RR techniques and standard SMPs with RRv capacity. The total WQv is the runoff volume from the 1-year, 24 hour design storm over the post-developed watershed and shall be

calculated in accordance with the criteria in Section 10.3 of the Design Manual.

- (ii) Minimum RRv and Treatment of Remaining Total WQv: *Construction activities* that cannot meet the criteria in Part I.C.2.b.(i) of this permit due to *site limitations* shall direct runoff from all newly constructed *impervious areas* to a RR technique or standard SMP with RRv capacity unless *infeasible*. The specific *site limitations* that prevent the reduction of 100% of the WQv shall be documented in the SWPPP. For each *impervious area* that is not directed to a RR technique or standard SMP with RRv capacity, the SWPPP must include documentation which demonstrates that all options were considered and for each option explains why it is considered *infeasible*.

In no case shall the runoff reduction achieved from the newly constructed *impervious areas* be less than the Minimum RRv as calculated using the criteria in Section 10.3 of the Design Manual. The remaining portion of the total WQv that cannot be reduced shall be treated by application of standard SMPs.

- (iii) Channel Protection Volume (Cpv): Provide 24 hour extended detention of the post-developed 1-year, 24-hour storm event; remaining after runoff reduction. The Cpv requirement does not apply when:
 - (1) Reduction of the entire Cpv is achieved by application of runoff reduction techniques or infiltration systems, or
 - (2) The site *discharges* directly to tidal waters, or fifth order or larger streams.
- (iv) *Overbank* Flood Control Criteria (Qp): Requires storage to attenuate the post-development 10-year, 24-hour peak *discharge* rate (Qp) to predevelopment rates. The Qp requirement does not apply when:
 - (1) the site *discharges* directly to tidal waters or fifth order or larger streams, or
 - (2) A downstream analysis reveals that *overbank* control is not required.
- (v) Extreme Flood Control Criteria (Qf): Requires storage to attenuate the post-development 100-year, 24-hour peak *discharge* rate (Qf) to predevelopment rates. The Qf requirement does not apply when:
 - (1) the site *discharges* directly to tidal waters or fifth order or larger streams, or
 - (2) A downstream analysis reveals that *overbank* control is not required.

c. Sizing Criteria for Redevelopment Activity

- (i) Water Quality Volume (WQv): The WQv treatment objective for *redevelopment activity* shall be addressed by one of the following options. *Redevelopment activities* located in an Enhanced Phosphorus Removal Watershed (see Part III.B.3. and Appendix C of this permit) shall calculate the WQv in accordance with Section 10.3 of the Design Manual. All other *redevelopment activities* shall calculate the WQv in accordance with Section 4.2 of the Design Manual.
- (1) Reduce the existing *impervious cover* by a minimum of 25% of the total disturbed, *impervious area*. The Soil Restoration criteria in Section 5.1.6 of the Design Manual must be applied to all newly created pervious areas, or
 - (2) Capture and treat a minimum of 25% of the WQv from the disturbed, *impervious area* by the application of standard SMPs; or reduce 25% of the WQv from the disturbed, *impervious area* by the application of RR techniques or standard SMPs with RRv capacity., or
 - (3) Capture and treat a minimum of 75% of the WQv from the disturbed, *impervious area* as well as any additional runoff from tributary areas by application of the alternative practices discussed in Sections 9.3 and 9.4 of the Design Manual., or
 - (4) Application of a combination of 1, 2 and 3 above that provide a weighted average of at least two of the above methods. Application of this method shall be in accordance with the criteria in Section 9.2.1(B) (IV) of the Design Manual.

If there is an existing post-construction stormwater management practice located on the site that captures and treats runoff from the *impervious area* that is being disturbed, the WQv treatment option selected must, at a minimum, provide treatment equal to the treatment that was being provided by the existing practice(s) if that treatment is greater than the treatment required by options 1 – 4 above.

- (ii) Channel Protection Volume (Cpv): Not required if there are no changes to hydrology that increase the *discharge* rate from the project site.
- (iii) *Overbank* Flood Control Criteria (Qp): Not required if there are no changes to hydrology that increase the *discharge* rate from the project site.
- (iv) Extreme Flood Control Criteria (Qf): Not required if there are no changes to hydrology that increase the *discharge* rate from the project site

d. Sizing Criteria for Combination of Redevelopment Activity and New Development

Construction projects that include both New Development and Redevelopment Activity shall provide post-construction stormwater management controls that meet the sizing criteria calculated as an aggregate of the Sizing Criteria in Part I.C.2.a. or b. of this permit for the New Development portion of the project and Part I.C.2.c of this permit for Redevelopment Activity portion of the project.

D. Maintaining Water Quality

The Department expects that compliance with the conditions of this permit will control *discharges* necessary to meet applicable *water quality standards*. It shall be a violation of the *ECL* for any discharge to either cause or contribute to a violation of *water quality standards* as contained in Parts 700 through 705 of Title 6 of the Official Compilation of Codes, Rules and Regulations of the State of New York, such as:

1. There shall be no increase in turbidity that will cause a substantial visible contrast to natural conditions;
2. There shall be no increase in suspended, colloidal or settleable solids that will cause deposition or impair the waters for their best usages; and
3. There shall be no residue from oil and floating substances, nor visible oil film, nor globules of grease.

If there is evidence indicating that the stormwater *discharges* authorized by this permit are causing, have the reasonable potential to cause, or are contributing to a violation of the *water quality standards*; the *owner or operator* must take appropriate corrective action in accordance with Part IV.C.5. of this general permit and document in accordance with Part IV.C.4. of this general permit. To address the *water quality standard* violation the *owner or operator* may need to provide additional information, include and implement appropriate controls in the SWPPP to correct the problem, or obtain an individual SPDES permit.

If there is evidence indicating that despite compliance with the terms and conditions of this general permit it is demonstrated that the stormwater *discharges* authorized by this permit are causing or contributing to a violation of *water quality standards*, or if the Department determines that a modification of the permit is necessary to prevent a violation of *water quality standards*, the authorized *discharges* will no longer be eligible for coverage under this permit. The Department may require the *owner or operator* to obtain an individual SPDES permit to continue discharging.

E. Eligibility Under This General Permit

1. This permit may authorize all *discharges* of stormwater from *construction activity* to *surface waters of the State* and *groundwaters* except for ineligible *discharges* identified under subparagraph F. of this Part.
2. Except for non-stormwater *discharges* explicitly listed in the next paragraph, this permit only authorizes stormwater *discharges*; including stormwater runoff, snowmelt runoff, and surface runoff and drainage, from *construction activities*.
3. Notwithstanding paragraphs E.1 and E.2 above, the following non-stormwater discharges are authorized by this permit: those listed in 6 NYCRR 750-1.2(a)(29)(vi), with the following exception: “Discharges from firefighting activities are authorized only when the firefighting activities are emergencies/unplanned”; waters to which other components have not been added that are used to control dust in accordance with the SWPPP; and uncontaminated *discharges* from *construction site* de-watering operations. All non-stormwater discharges must be identified in the SWPPP. Under all circumstances, the *owner or operator* must still comply with *water quality standards* in Part I.D of this permit.
4. The *owner or operator* must maintain permit eligibility to *discharge* under this permit. Any *discharges* that are not compliant with the eligibility conditions of this permit are not authorized by the permit and the *owner or operator* must either apply for a separate permit to cover those ineligible *discharges* or take steps necessary to make the *discharge* eligible for coverage.

F. Activities Which Are Ineligible for Coverage Under This General Permit

All of the following are **not** authorized by this permit:

1. *Discharges* after *construction activities* have been completed and the site has undergone *final stabilization*;
2. *Discharges* that are mixed with sources of non-stormwater other than those expressly authorized under subsection E.3. of this Part and identified in the SWPPP required by this permit;
3. *Discharges* that are required to obtain an individual SPDES permit or another SPDES general permit pursuant to Part VII.K. of this permit;
4. *Construction activities* or *discharges* from *construction activities* that may adversely affect an *endangered or threatened species* unless the *owner or*

operator has obtained a permit issued pursuant to 6 NYCRR Part 182 for the project or the Department has issued a letter of non-jurisdiction for the project. All documentation necessary to demonstrate eligibility shall be maintained on site in accordance with Part II.D.2 of this permit;

5. *Discharges* which either cause or contribute to a violation of *water quality standards* adopted pursuant to the *ECL* and its accompanying regulations;
6. *Construction activities* for residential, commercial and institutional projects:
 - a. Where the *discharges* from the *construction activities* are tributary to waters of the state classified as AA or AA-s; and
 - b. Which are undertaken on land with no existing *impervious cover*; and
 - c. Which disturb one (1) or more acres of land designated on the current United States Department of Agriculture (“USDA”) Soil Survey as Soil Slope Phase “D”, (provided the map unit name is inclusive of slopes greater than 25%), or Soil Slope Phase “E” or “F” (regardless of the map unit name), or a combination of the three designations.
7. *Construction activities* for linear transportation projects and linear utility projects:
 - a. Where the *discharges* from the *construction activities* are tributary to waters of the state classified as AA or AA-s; and
 - b. Which are undertaken on land with no existing *impervious cover*; and
 - c. Which disturb two (2) or more acres of land designated on the current USDA Soil Survey as Soil Slope Phase “D” (provided the map unit name is inclusive of slopes greater than 25%), or Soil Slope Phase “E” or “F” (regardless of the map unit name), or a combination of the three designations.

8. *Construction activities* that have the potential to affect an *historic property*, unless there is documentation that such impacts have been resolved. The following documentation necessary to demonstrate eligibility with this requirement shall be maintained on site in accordance with Part II.D.2 of this permit and made available to the Department in accordance with Part VII.F of this permit:
- a. Documentation that the *construction activity* is not within an archeologically sensitive area indicated on the sensitivity map, and that the *construction activity* is not located on or immediately adjacent to a property listed or determined to be eligible for listing on the National or State Registers of Historic Places, and that there is no new permanent building on the *construction site* within the following distances from a building, structure, or object that is more than 50 years old, or if there is such a new permanent building on the *construction site* within those parameters that NYS Office of Parks, Recreation and Historic Preservation (OPRHP), a Historic Preservation Commission of a Certified Local Government, or a qualified preservation professional has determined that the building, structure, or object more than 50 years old is not historically/archeologically significant.
 - 1-5 acres of disturbance - 20 feet
 - 5-20 acres of disturbance - 50 feet
 - 20+ acres of disturbance - 100 feet, or
 - b. DEC consultation form sent to OPRHP, and copied to the NYS DEC Agency Historic Preservation Officer (APO), and
 - (i) the State Environmental Quality Review (SEQR) Environmental Assessment Form (EAF) with a negative declaration or the Findings Statement, with documentation of OPRHP's agreement with the resolution; or
 - (ii) documentation from OPRHP that the *construction activity* will result in No Impact; or
 - (iii) documentation from OPRHP providing a determination of No Adverse Impact; or
 - (iv) a Letter of Resolution signed by the owner/operator, OPRHP and the DEC APO which allows for this *construction activity* to be eligible for coverage under the general permit in terms of the State Historic Preservation Act (SHPA); or
 - c. Documentation of satisfactory compliance with Section 106 of the National Historic Preservation Act for a coterminous project area:

- (i) No Affect
- (ii) No Adverse Affect
- (iii) Executed Memorandum of Agreement, or

d. Documentation that:

- (i) SHPA Section 14.09 has been completed by NYS DEC or another state agency.
9. *Discharges from construction activities* that are subject to an existing SPDES individual or general permit where a SPDES permit for *construction activity* has been terminated or denied; or where the *owner or operator* has failed to renew an expired individual permit.

Part II. PERMIT COVERAGE

A. How to Obtain Coverage

1. An *owner or operator* of a *construction activity* that is not subject to the requirements of a regulated, traditional land use control MS4 must first prepare a SWPPP in accordance with all applicable requirements of this permit and then submit a completed Notice of Intent (NOI) to the Department to be authorized to discharge under this permit.
2. An *owner or operator* of a *construction activity* that is subject to the requirements of a *regulated, traditional land use control MS4* must first prepare a SWPPP in accordance with all applicable requirements of this permit and then have the SWPPP reviewed and accepted by the *regulated, traditional land use control MS4* prior to submitting the NOI to the Department. The *owner or operator* shall have the “MS4 SWPPP Acceptance” form signed in accordance with Part VII.H., and then submit that form along with a completed NOI to the Department.
3. The requirement for an *owner or operator* to have its SWPPP reviewed and accepted by the *regulated, traditional land use control MS4* prior to submitting the NOI to the Department does not apply to an *owner or operator* that is obtaining permit coverage in accordance with the requirements in Part II.F. (Change of *Owner or Operator*) or where the *owner or operator* of the *construction activity* is the *regulated, traditional land use control MS4* . This exemption does not apply to *construction activities* subject to the New York City Administrative Code.

B. Notice of Intent (NOI) Submittal

1. Prior to December 21, 2020, an owner or operator shall use either the electronic (eNOI) or paper version of the NOI that the Department prepared. Both versions of the NOI are located on the Department's website (<http://www.dec.ny.gov/>). The paper version of the NOI shall be signed in accordance with Part VII.H. of this permit and submitted to the following address:

**NOTICE OF INTENT
NYS DEC, Bureau of Water Permits
625 Broadway, 4th Floor
Albany, New York 12233-3505**

2. Beginning December 21, 2020 and in accordance with EPA's 2015 NPDES Electronic Reporting Rule (40 CFR Part 127), the *owner or operator* must submit the NOI electronically using the *Department's* online NOI.
3. The *owner or operator* shall have the SWPPP preparer sign the "SWPPP Preparer Certification" statement on the NOI prior to submitting the form to the Department.
4. As of the date the NOI is submitted to the Department, the *owner or operator* shall make the NOI and SWPPP available for review and copying in accordance with the requirements in Part VII.F. of this permit.

C. Permit Authorization

1. An *owner or operator* shall not *commence construction activity* until their authorization to *discharge* under this permit goes into effect.
2. Authorization to *discharge* under this permit will be effective when the *owner or operator* has satisfied all of the following criteria:
 - a. project review pursuant to the State Environmental Quality Review Act ("SEQRA") have been satisfied, when SEQRA is applicable. See the Department's website (<http://www.dec.ny.gov/>) for more information,
 - b. where required, all necessary Department permits subject to the *Uniform Procedures Act ("UPA")* (see 6 NYCRR Part 621), or the equivalent from another New York State agency, have been obtained, unless otherwise notified by the Department pursuant to 6 NYCRR 621.3(a)(4). *Owners or operators of construction activities* that are required to obtain *UPA* permits

must submit a preliminary SWPPP to the appropriate DEC Permit Administrator at the Regional Office listed in Appendix F at the time all other necessary *UPA* permit applications are submitted. The preliminary SWPPP must include sufficient information to demonstrate that the *construction activity* qualifies for authorization under this permit,

- c. the final SWPPP has been prepared, and
 - d. a complete NOI has been submitted to the Department in accordance with the requirements of this permit.
3. An *owner or operator* that has satisfied the requirements of Part II.C.2 above will be authorized to *discharge* stormwater from their *construction activity* in accordance with the following schedule:
- a. For *construction activities* that are not subject to the requirements of a *regulated, traditional land use control MS4*:
 - (i) Five (5) business days from the date the Department receives a complete electronic version of the NOI (eNOI) for *construction activities* with a SWPPP that has been prepared in conformance with the design criteria in the technical standard referenced in Part III.B.1 and the *performance criteria* in the technical standard referenced in Parts III.B., 2 or 3, for *construction activities* that require post-construction stormwater management practices pursuant to Part III.C.; or
 - (ii) Sixty (60) business days from the date the Department receives a complete NOI (electronic or paper version) for *construction activities* with a SWPPP that has not been prepared in conformance with the design criteria in technical standard referenced in Part III.B.1. or, for *construction activities* that require post-construction stormwater management practices pursuant to Part III.C., the *performance criteria* in the technical standard referenced in Parts III.B., 2 or 3, or;
 - (iii) Ten (10) business days from the date the Department receives a complete paper version of the NOI for *construction activities* with a SWPPP that has been prepared in conformance with the design criteria in the technical standard referenced in Part III.B.1 and the *performance criteria* in the technical standard referenced in Parts III.B., 2 or 3, for *construction activities* that require post-construction stormwater management practices pursuant to Part III.C.

- b. For *construction activities* that are subject to the requirements of a *regulated, traditional land use control MS4*:
 - (i) Five (5) business days from the date the Department receives both a complete electronic version of the NOI (eNOI) and signed “MS4 SWPPP Acceptance” form, or
 - (ii) Ten (10) business days from the date the Department receives both a complete paper version of the NOI and signed “MS4 SWPPP Acceptance” form.
4. Coverage under this permit authorizes stormwater *discharges* from only those areas of disturbance that are identified in the NOI. If an *owner or operator* wishes to have stormwater *discharges* from future or additional areas of disturbance authorized, they must submit a new NOI that addresses that phase of the development, unless otherwise notified by the Department. The *owner or operator* shall not *commence construction activity* on the future or additional areas until their authorization to *discharge* under this permit goes into effect in accordance with Part II.C. of this permit.

D. General Requirements For Owners or Operators With Permit Coverage

1. The *owner or operator* shall ensure that the provisions of the SWPPP are implemented from the *commencement of construction activity* until all areas of disturbance have achieved *final stabilization* and the Notice of Termination (“NOT”) has been submitted to the Department in accordance with Part V. of this permit. This includes any changes made to the SWPPP pursuant to Part III.A.4. of this permit.
2. The *owner or operator* shall maintain a copy of the General Permit (GP-0-20-001), NOI, *NOI Acknowledgment Letter*, SWPPP, MS4 SWPPP Acceptance form, inspection reports, responsible contractor’s or subcontractor’s certification statement (see Part III.A.6.), and all documentation necessary to demonstrate eligibility with this permit at the *construction site* until all disturbed areas have achieved *final stabilization* and the NOT has been submitted to the Department. The documents must be maintained in a secure location, such as a job trailer, on-site construction office, or mailbox with lock. The secure location must be accessible during normal business hours to an individual performing a compliance inspection.
3. The *owner or operator of a construction activity* shall not disturb greater than five (5) acres of soil at any one time without prior written authorization from the Department or, in areas under the jurisdiction of a *regulated, traditional land*

- use control MS4, the regulated, traditional land use control MS4 (provided the regulated, traditional land use control MS4 is not the owner or operator of the construction activity). At a minimum, the owner or operator must comply with the following requirements in order to be authorized to disturb greater than five (5) acres of soil at any one time:*
- a. The *owner or operator* shall have a *qualified inspector* conduct **at least two** (2) site inspections in accordance with Part IV.C. of this permit every seven (7) calendar days, for as long as greater than five (5) acres of soil remain disturbed. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
 - b. In areas where soil disturbance activity has temporarily or permanently ceased, the application of soil stabilization measures must be initiated by the end of the next business day and completed within seven (7) days from the date the current soil disturbance activity ceased. The soil stabilization measures selected shall be in conformance with the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016.
 - c. The *owner or operator* shall prepare a phasing plan that defines maximum disturbed area per phase and shows required cuts and fills.
 - d. The *owner or operator* shall install any additional site-specific practices needed to protect water quality.
 - e. The *owner or operator* shall include the requirements above in their SWPPP.
4. In accordance with statute, regulations, and the terms and conditions of this permit, the Department may suspend or revoke an *owner's or operator's* coverage under this permit at any time if the Department determines that the SWPPP does not meet the permit requirements or consistent with Part VII.K..
 5. Upon a finding of significant non-compliance with the practices described in the SWPPP or violation of this permit, the Department may order an immediate stop to all activity at the site until the non-compliance is remedied. The stop work order shall be in writing, describe the non-compliance in detail, and be sent to the *owner or operator*.
 6. For *construction activities* that are subject to the requirements of a *regulated, traditional land use control MS4*, the *owner or operator* shall notify the

regulated, traditional land use control MS4 in writing of any planned amendments or modifications to the post-construction stormwater management practice component of the SWPPP required by Part III.A. 4. and 5. of this permit. Unless otherwise notified by the *regulated, traditional land use control MS4*, the *owner or operator* shall have the SWPPP amendments or modifications reviewed and accepted by the *regulated, traditional land use control MS4* prior to commencing construction of the post-construction stormwater management practice.

E. Permit Coverage for Discharges Authorized Under GP-0-15-002

1. Upon renewal of SPDES General Permit for Stormwater Discharges from *Construction Activity* (Permit No. GP-0-15-002), an *owner or operator* of a *construction activity* with coverage under GP-0-15-002, as of the effective date of GP- 0-20-001, shall be authorized to *discharge* in accordance with GP- 0-20-001, unless otherwise notified by the Department.

An *owner or operator* may continue to implement the technical/design components of the post-construction stormwater management controls provided that such design was done in conformance with the technical standards in place at the time of initial project authorization. However, they must comply with the other, non-design provisions of GP-0-20-001.

F. Change of Owner or Operator

1. When property ownership changes or when there is a change in operational control over the construction plans and specifications, the original *owner or operator* must notify the new *owner or operator*, in writing, of the requirement to obtain permit coverage by submitting a NOI with the Department. For *construction activities* subject to the requirements of a *regulated, traditional land use control MS4*, the original *owner or operator* must also notify the MS4, in writing, of the change in ownership at least 30 calendar days prior to the change in ownership.
2. Once the new *owner or operator* obtains permit coverage, the original *owner or operator* shall then submit a completed NOT with the name and permit identification number of the new *owner or operator* to the Department at the address in Part II.B.1. of this permit. If the original *owner or operator* maintains ownership of a portion of the *construction activity* and will disturb soil, they must maintain their coverage under the permit.
3. Permit coverage for the new *owner or operator* will be effective as of the date the Department receives a complete NOI, provided the original *owner or*

operator was not subject to a sixty (60) business day authorization period that has not expired as of the date the Department receives the NOI from the new *owner or operator*.

Part III. STORMWATER POLLUTION PREVENTION PLAN (SWPPP)

A. General SWPPP Requirements

1. A SWPPP shall be prepared and implemented by the *owner or operator* of each *construction activity* covered by this permit. The SWPPP must document the selection, design, installation, implementation and maintenance of the control measures and practices that will be used to meet the effluent limitations in Part I.B. of this permit and where applicable, the post-construction stormwater management practice requirements in Part I.C. of this permit. The SWPPP shall be prepared prior to the submittal of the NOI. The NOI shall be submitted to the Department prior to the *commencement of construction activity*. A copy of the completed, final NOI shall be included in the SWPPP.
2. The SWPPP shall describe the erosion and sediment control practices and where required, post-construction stormwater management practices that will be used and/or constructed to reduce the *pollutants* in stormwater *discharges* and to assure compliance with the terms and conditions of this permit. In addition, the SWPPP shall identify potential sources of pollution which may reasonably be expected to affect the quality of stormwater *discharges*.
3. All SWPPPs that require the post-construction stormwater management practice component shall be prepared by a *qualified professional* that is knowledgeable in the principles and practices of stormwater management and treatment.
4. The *owner or operator* must keep the SWPPP current so that it at all times accurately documents the erosion and sediment controls practices that are being used or will be used during construction, and all post-construction stormwater management practices that will be constructed on the site. At a minimum, the *owner or operator* shall amend the SWPPP, including construction drawings:
 - a. whenever the current provisions prove to be ineffective in minimizing *pollutants* in stormwater *discharges* from the site;

- b. whenever there is a change in design, construction, or operation at the *construction site* that has or could have an effect on the *discharge* of *pollutants*;
 - c. to address issues or deficiencies identified during an inspection by the *qualified inspector*, the Department or other regulatory authority; and
 - d. to document the final construction conditions.
5. The Department may notify the *owner or operator* at any time that the SWPPP does not meet one or more of the minimum requirements of this permit. The notification shall be in writing and identify the provisions of the SWPPP that require modification. Within fourteen (14) calendar days of such notification, or as otherwise indicated by the Department, the *owner or operator* shall make the required changes to the SWPPP and submit written notification to the Department that the changes have been made. If the *owner or operator* does not respond to the Department's comments in the specified time frame, the Department may suspend the *owner's or operator's* coverage under this permit or require the *owner or operator* to obtain coverage under an individual SPDES permit in accordance with Part II.D.4. of this permit.
6. Prior to the *commencement of construction activity*, the *owner or operator* must identify the contractor(s) and subcontractor(s) that will be responsible for installing, constructing, repairing, replacing, inspecting and maintaining the erosion and sediment control practices included in the SWPPP; and the contractor(s) and subcontractor(s) that will be responsible for constructing the post-construction stormwater management practices included in the SWPPP. The *owner or operator* shall have each of the contractors and subcontractors identify at least one person from their company that will be responsible for implementation of the SWPPP. This person shall be known as the *trained contractor*. The *owner or operator* shall ensure that at least one *trained contractor* is on site on a daily basis when soil disturbance activities are being performed.

The *owner or operator* shall have each of the contractors and subcontractors identified above sign a copy of the following certification statement below before they commence any *construction activity*:

"I hereby certify under penalty of law that I understand and agree to comply with the terms and conditions of the SWPPP and agree to implement any corrective actions identified by the *qualified inspector* during a site inspection. I also understand that the *owner or operator* must comply with

the terms and conditions of the most current version of the New York State Pollutant Discharge Elimination System ("SPDES") general permit for stormwater *discharges* from *construction activities* and that it is unlawful for any person to cause or contribute to a violation of *water quality standards*. Furthermore, I am aware that there are significant penalties for submitting false information, that I do not believe to be true, including the possibility of fine and imprisonment for knowing violations"

In addition to providing the certification statement above, the certification page must also identify the specific elements of the SWPPP that each contractor and subcontractor will be responsible for and include the name and title of the person providing the signature; the name and title of the *trained contractor* responsible for SWPPP implementation; the name, address and telephone number of the contracting firm; the address (or other identifying description) of the site; and the date the certification statement is signed. The *owner or operator* shall attach the certification statement(s) to the copy of the SWPPP that is maintained at the *construction site*. If new or additional contractors are hired to implement measures identified in the SWPPP after construction has commenced, they must also sign the certification statement and provide the information listed above.

7. For projects where the Department requests a copy of the SWPPP or inspection reports, the *owner or operator* shall submit the documents in both electronic (PDF only) and paper format within five (5) business days, unless otherwise notified by the Department.

B. Required SWPPP Contents

1. Erosion and sediment control component - All SWPPPs prepared pursuant to this permit shall include erosion and sediment control practices designed in conformance with the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016. Where erosion and sediment control practices are not designed in conformance with the design criteria included in the technical standard, the *owner or operator* must demonstrate *equivalence* to the technical standard. At a minimum, the erosion and sediment control component of the SWPPP shall include the following:
 - a. Background information about the scope of the project, including the location, type and size of project

- b. A site map/construction drawing(s) for the project, including a general location map. At a minimum, the site map shall show the total site area; all improvements; areas of disturbance; areas that will not be disturbed; existing vegetation; on-site and adjacent off-site surface water(s); floodplain/floodway boundaries; wetlands and drainage patterns that could be affected by the *construction activity*; existing and final contours ; locations of different soil types with boundaries; material, waste, borrow or equipment storage areas located on adjacent properties; and location(s) of the stormwater *discharge(s)*;
- c. A description of the soil(s) present at the site, including an identification of the Hydrologic Soil Group (HSG);
- d. A construction phasing plan and sequence of operations describing the intended order of *construction activities*, including clearing and grubbing, excavation and grading, utility and infrastructure installation and any other activity at the site that results in soil disturbance;
- e. A description of the minimum erosion and sediment control practices to be installed or implemented for each *construction activity* that will result in soil disturbance. Include a schedule that identifies the timing of initial placement or implementation of each erosion and sediment control practice and the minimum time frames that each practice should remain in place or be implemented;
- f. A temporary and permanent soil stabilization plan that meets the requirements of this general permit and the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016, for each stage of the project, including initial land clearing and grubbing to project completion and achievement of *final stabilization*;
- g. A site map/construction drawing(s) showing the specific location(s), size(s), and length(s) of each erosion and sediment control practice;
- h. The dimensions, material specifications, installation details, and operation and maintenance requirements for all erosion and sediment control practices. Include the location and sizing of any temporary sediment basins and structural practices that will be used to divert flows from exposed soils;
- i. A maintenance inspection schedule for the contractor(s) identified in Part III.A.6. of this permit, to ensure continuous and effective operation of the erosion and sediment control practices. The maintenance inspection

schedule shall be in accordance with the requirements in the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016;

- j. A description of the pollution prevention measures that will be used to control litter, construction chemicals and construction debris from becoming a *pollutant* source in the stormwater *discharges*;
 - k. A description and location of any stormwater *discharges* associated with industrial activity other than construction at the site, including, but not limited to, stormwater *discharges* from asphalt plants and concrete plants located on the *construction site*; and
 - l. Identification of any elements of the design that are not in conformance with the design criteria in the technical standard, New York State Standards and Specifications for Erosion and Sediment Control, dated November 2016. Include the reason for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.
2. Post-construction stormwater management practice component – The *owner or operator* of any construction project identified in Table 2 of Appendix B as needing post-construction stormwater management practices shall prepare a SWPPP that includes practices designed in conformance with the applicable *sizing criteria* in Part I.C.2.a., c. or d. of this permit and the *performance criteria* in the technical standard, New York State Stormwater Management Design Manual dated January 2015

Where post-construction stormwater management practices are not designed in conformance with the *performance criteria* in the technical standard, the *owner or operator* must include in the SWPPP the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the technical standard.

The post-construction stormwater management practice component of the SWPPP shall include the following:

- a. Identification of all post-construction stormwater management practices to be constructed as part of the project. Include the dimensions, material specifications and installation details for each post-construction stormwater management practice;

- b. A site map/construction drawing(s) showing the specific location and size of each post-construction stormwater management practice;
- c. A Stormwater Modeling and Analysis Report that includes:
 - (i) Map(s) showing pre-development conditions, including watershed/subcatchments boundaries, flow paths/routing, and design points;
 - (ii) Map(s) showing post-development conditions, including watershed/subcatchments boundaries, flow paths/routing, design points and post-construction stormwater management practices;
 - (iii) Results of stormwater modeling (i.e. hydrology and hydraulic analysis) for the required storm events. Include supporting calculations (model runs), methodology, and a summary table that compares pre and post-development runoff rates and volumes for the different storm events;
 - (iv) Summary table, with supporting calculations, which demonstrates that each post-construction stormwater management practice has been designed in conformance with the *sizing criteria* included in the Design Manual;
 - (v) Identification of any *sizing criteria* that is not required based on the requirements included in Part I.C. of this permit; and
 - (vi) Identification of any elements of the design that are not in conformance with the *performance criteria* in the Design Manual. Include the reason(s) for the deviation or alternative design and provide information which demonstrates that the deviation or alternative design is *equivalent* to the Design Manual;
- d. Soil testing results and locations (test pits, borings);
- e. Infiltration test results, when required; and
- f. An operations and maintenance plan that includes inspection and maintenance schedules and actions to ensure continuous and effective operation of each post-construction stormwater management practice. The plan shall identify the entity that will be responsible for the long term operation and maintenance of each practice.

3. Enhanced Phosphorus Removal Standards - All construction projects identified in Table 2 of Appendix B that are located in the watersheds identified in Appendix C shall prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the applicable *sizing criteria* in Part I.C.2. b., c. or d. of this permit and the *performance criteria*, Enhanced Phosphorus Removal Standards included in the Design Manual. At a minimum, the post-construction stormwater management practice component of the SWPPP shall include items 2.a - 2.f. above.

C. Required SWPPP Components by Project Type

Unless otherwise notified by the Department, *owners or operators of construction activities* identified in Table 1 of Appendix B are required to prepare a SWPPP that only includes erosion and sediment control practices designed in conformance with Part III.B.1 of this permit. *Owners or operators of the construction activities* identified in Table 2 of Appendix B shall prepare a SWPPP that also includes post-construction stormwater management practices designed in conformance with Part III.B.2 or 3 of this permit.

Part IV. INSPECTION AND MAINTENANCE REQUIREMENTS

A. General Construction Site Inspection and Maintenance Requirements

1. The *owner or operator* must ensure that all erosion and sediment control practices (including pollution prevention measures) and all post-construction stormwater management practices identified in the SWPPP are inspected and maintained in accordance with Part IV.B. and C. of this permit.
2. The terms of this permit shall not be construed to prohibit the State of New York from exercising any authority pursuant to the ECL, common law or federal law, or prohibit New York State from taking any measures, whether civil or criminal, to prevent violations of the laws of the State of New York or protect the public health and safety and/or the environment.

B. Contractor Maintenance Inspection Requirements

1. The *owner or operator* of each *construction activity* identified in Tables 1 and 2 of Appendix B shall have a *trained contractor* inspect the erosion and sediment control practices and pollution prevention measures being implemented within the active work area daily to ensure that they are being maintained in effective operating condition at all times. If deficiencies are identified, the contractor shall

begin implementing corrective actions within one business day and shall complete the corrective actions in a reasonable time frame.

2. For construction sites where soil disturbance activities have been temporarily suspended (e.g. winter shutdown) and *temporary stabilization* measures have been applied to all disturbed areas, the *trained contractor* can stop conducting the maintenance inspections. The *trained contractor* shall begin conducting the maintenance inspections in accordance with Part IV.B.1. of this permit as soon as soil disturbance activities resume.
3. For construction sites where soil disturbance activities have been shut down with partial project completion, the *trained contractor* can stop conducting the maintenance inspections if all areas disturbed as of the project shutdown date have achieved *final stabilization* and all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational.

C. Qualified Inspector Inspection Requirements

The *owner or operator* shall have a *qualified inspector* conduct site inspections in conformance with the following requirements:

[Note: The *trained contractor* identified in Part III.A.6. and IV.B. of this permit **cannot** conduct the *qualified inspector* site inspections unless they meet the *qualified inspector* qualifications included in Appendix A. In order to perform these inspections, the *trained contractor* would have to be a:

- licensed Professional Engineer,
 - Certified Professional in Erosion and Sediment Control (CPESC),
 - New York State Erosion and Sediment Control Certificate Program holder
 - Registered Landscape Architect, or
 - someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided they have received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity].
1. A *qualified inspector* shall conduct site inspections for all *construction activities* identified in Tables 1 and 2 of Appendix B, with the exception of:
 - a. the construction of a single family residential subdivision with 25% or less *impervious cover* at total site build-out that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres and is not located

in one of the watersheds listed in Appendix C and not directly discharging to one of the 303(d) segments listed in Appendix E;

- b. the construction of a single family home that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres and is not located in one of the watersheds listed in Appendix C and not directly discharging to one of the 303(d) segments listed in Appendix E;
 - c. construction on agricultural property that involves a soil disturbance of one (1) or more acres of land but less than five (5) acres; and
 - d. *construction activities* located in the watersheds identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.
2. Unless otherwise notified by the Department, the *qualified inspector* shall conduct site inspections in accordance with the following timetable:
- a. For construction sites where soil disturbance activities are on-going, the *qualified inspector* shall conduct a site inspection at least once every seven (7) calendar days.
 - b. For construction sites where soil disturbance activities are on-going and the *owner or operator* has received authorization in accordance with Part II.D.3 to disturb greater than five (5) acres of soil at any one time, the *qualified inspector* shall conduct at least two (2) site inspections every seven (7) calendar days. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
 - c. For construction sites where soil disturbance activities have been temporarily suspended (e.g. winter shutdown) and *temporary stabilization* measures have been applied to all disturbed areas, the *qualified inspector* shall conduct a site inspection at least once every thirty (30) calendar days. The *owner or operator* shall notify the DOW Water (SPDES) Program contact at the Regional Office (see contact information in Appendix F) or, in areas under the jurisdiction of a *regulated, traditional land use control MS4*, the *regulated, traditional land use control MS4* (provided the *regulated, traditional land use control MS4* is not the *owner or operator* of the *construction activity*) in writing prior to reducing the frequency of inspections.

- d. For construction sites where soil disturbance activities have been shut down with partial project completion, the *qualified inspector* can stop conducting inspections if all areas disturbed as of the project shutdown date have achieved *final stabilization* and all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational. The *owner or operator* shall notify the DOW Water (SPDES) Program contact at the Regional Office (see contact information in Appendix F) or, in areas under the jurisdiction of a *regulated, traditional land use control MS4*, the *regulated, traditional land use control MS4* (provided the *regulated, traditional land use control MS4* is not the *owner or operator* of the *construction activity*) in writing prior to the shutdown. If soil disturbance activities are not resumed within 2 years from the date of shutdown, the *owner or operator* shall have the *qualified inspector* perform a final inspection and certify that all disturbed areas have achieved *final stabilization*, and all temporary, structural erosion and sediment control measures have been removed; and that all post-construction stormwater management practices have been constructed in conformance with the SWPPP by signing the “*Final Stabilization*” and “*Post-Construction Stormwater Management Practice*” certification statements on the NOT. The *owner or operator* shall then submit the completed NOT form to the address in Part II.B.1 of this permit.
 - e. For construction sites that directly *discharge* to one of the 303(d) segments listed in Appendix E or is located in one of the watersheds listed in Appendix C, the *qualified inspector* shall conduct at least two (2) site inspections every seven (7) calendar days. The two (2) inspections shall be separated by a minimum of two (2) full calendar days.
3. At a minimum, the *qualified inspector* shall inspect all erosion and sediment control practices and pollution prevention measures to ensure integrity and effectiveness, all post-construction stormwater management practices under construction to ensure that they are constructed in conformance with the SWPPP, all areas of disturbance that have not achieved *final stabilization*, all points of *discharge* to natural surface waterbodies located within, or immediately adjacent to, the property boundaries of the *construction site*, and all points of *discharge* from the *construction site*.
 4. The *qualified inspector* shall prepare an inspection report subsequent to each and every inspection. At a minimum, the inspection report shall include and/or address the following:

- a. Date and time of inspection;
- b. Name and title of person(s) performing inspection;
- c. A description of the weather and soil conditions (e.g. dry, wet, saturated) at the time of the inspection;
- d. A description of the condition of the runoff at all points of *discharge* from the *construction site*. This shall include identification of any *discharges* of sediment from the *construction site*. Include *discharges* from conveyance systems (i.e. pipes, culverts, ditches, etc.) and overland flow;
- e. A description of the condition of all natural surface waterbodies located within, or immediately adjacent to, the property boundaries of the *construction site* which receive runoff from disturbed areas. This shall include identification of any *discharges* of sediment to the surface waterbody;
- f. Identification of all erosion and sediment control practices and pollution prevention measures that need repair or maintenance;
- g. Identification of all erosion and sediment control practices and pollution prevention measures that were not installed properly or are not functioning as designed and need to be reinstalled or replaced;
- h. Description and sketch of areas with active soil disturbance activity, areas that have been disturbed but are inactive at the time of the inspection, and areas that have been stabilized (temporary and/or final) since the last inspection;
- i. Current phase of construction of all post-construction stormwater management practices and identification of all construction that is not in conformance with the SWPPP and technical standards;
- j. Corrective action(s) that must be taken to install, repair, replace or maintain erosion and sediment control practices and pollution prevention measures; and to correct deficiencies identified with the construction of the post-construction stormwater management practice(s);
- k. Identification and status of all corrective actions that were required by previous inspection; and

- I. Digital photographs, with date stamp, that clearly show the condition of all practices that have been identified as needing corrective actions. The *qualified inspector* shall attach paper color copies of the digital photographs to the inspection report being maintained onsite within seven (7) calendar days of the date of the inspection. The *qualified inspector* shall also take digital photographs, with date stamp, that clearly show the condition of the practice(s) after the corrective action has been completed. The *qualified inspector* shall attach paper color copies of the digital photographs to the inspection report that documents the completion of the corrective action work within seven (7) calendar days of that inspection.
5. Within one business day of the completion of an inspection, the *qualified inspector* shall notify the *owner or operator* and appropriate contractor or subcontractor identified in Part III.A.6. of this permit of any corrective actions that need to be taken. The contractor or subcontractor shall begin implementing the corrective actions within one business day of this notification and shall complete the corrective actions in a reasonable time frame.
6. All inspection reports shall be signed by the *qualified inspector*. Pursuant to Part II.D.2. of this permit, the inspection reports shall be maintained on site with the SWPPP.

Part V. TERMINATION OF PERMIT COVERAGE

A. Termination of Permit Coverage

1. An *owner or operator* that is eligible to terminate coverage under this permit must submit a completed NOT form to the address in Part II.B.1 of this permit. The NOT form shall be one which is associated with this permit, signed in accordance with Part VII.H of this permit.
2. An *owner or operator* may terminate coverage when one or more the following conditions have been met:
 - a. Total project completion - All *construction activity* identified in the SWPPP has been completed; and all areas of disturbance have achieved *final stabilization*; and all temporary, structural erosion and sediment control measures have been removed; and all post-construction stormwater management practices have been constructed in conformance with the SWPPP and are operational;

- b. Planned shutdown with partial project completion - All soil disturbance activities have ceased; and all areas disturbed as of the project shutdown date have achieved *final stabilization*; and all temporary, structural erosion and sediment control measures have been removed; and all post-construction stormwater management practices required for the completed portion of the project have been constructed in conformance with the SWPPP and are operational;
 - c. A new *owner or operator* has obtained coverage under this permit in accordance with Part II.F. of this permit.
 - d. The *owner or operator* obtains coverage under an alternative SPDES general permit or an individual SPDES permit.
3. For *construction activities* meeting subdivision 2a. or 2b. of this Part, the *owner or operator* shall have the *qualified inspector* perform a final site inspection prior to submitting the NOT. The *qualified inspector* shall, by signing the “*Final Stabilization*” and “*Post-Construction Stormwater Management Practice certification statements*” on the NOT, certify that all the requirements in Part V.A.2.a. or b. of this permit have been achieved.
4. For *construction activities* that are subject to the requirements of a *regulated, traditional land use control MS4* and meet subdivision 2a. or 2b. of this Part, the *owner or operator* shall have the *regulated, traditional land use control MS4* sign the “*MS4 Acceptance*” statement on the NOT in accordance with the requirements in Part VII.H. of this permit. The *regulated, traditional land use control MS4* official, by signing this statement, has determined that it is acceptable for the *owner or operator* to submit the NOT in accordance with the requirements of this Part. The *regulated, traditional land use control MS4* can make this determination by performing a final site inspection themselves or by accepting the *qualified inspector’s* final site inspection certification(s) required in Part V.A.3. of this permit.
5. For *construction activities* that require post-construction stormwater management practices and meet subdivision 2a. of this Part, the *owner or operator* must, prior to submitting the NOT, ensure one of the following:
 - a. the post-construction stormwater management practice(s) and any right-of-way(s) needed to maintain such practice(s) have been deeded to the municipality in which the practice(s) is located,

- b. an executed maintenance agreement is in place with the municipality that will maintain the post-construction stormwater management practice(s),
- c. for post-construction stormwater management practices that are privately owned, the *owner or operator* has a mechanism in place that requires operation and maintenance of the practice(s) in accordance with the operation and maintenance plan, such as a deed covenant in the *owner or operator's* deed of record,
- d. for post-construction stormwater management practices that are owned by a public or private institution (e.g. school, university, hospital), government agency or authority, or public utility; the *owner or operator* has policy and procedures in place that ensures operation and maintenance of the practices in accordance with the operation and maintenance plan.

Part VI. REPORTING AND RETENTION RECORDS

A. Record Retention

The *owner or operator* shall retain a copy of the NOI, NOI Acknowledgment Letter, SWPPP, MS4 SWPPP Acceptance form and any inspection reports that were prepared in conjunction with this permit for a period of at least five (5) years from the date that the Department receives a complete NOT submitted in accordance with Part V. of this general permit.

B. Addresses

With the exception of the NOI, NOT, and MS4 SWPPP Acceptance form (which must be submitted to the address referenced in Part II.B.1 of this permit), all written correspondence requested by the Department, including individual permit applications, shall be sent to the address of the appropriate DOW Water (SPDES) Program contact at the Regional Office listed in Appendix F.

Part VII. STANDARD PERMIT CONDITIONS

A. Duty to Comply

The *owner or operator* must comply with all conditions of this permit. All contractors and subcontractors associated with the project must comply with the terms of the SWPPP. Any non-compliance with this permit constitutes a violation of the Clean Water

Act (CWA) and the ECL and is grounds for an enforcement action against the *owner or operator* and/or the contractor/subcontractor; permit revocation, suspension or modification; or denial of a permit renewal application. Upon a finding of significant non-compliance with this permit or the applicable SWPPP, the Department may order an immediate stop to all *construction activity* at the site until the non-compliance is remedied. The stop work order shall be in writing, shall describe the non-compliance in detail, and shall be sent to the *owner or operator*.

If any human remains or archaeological remains are encountered during excavation, the *owner or operator* must immediately cease, or cause to cease, all *construction activity* in the area of the remains and notify the appropriate Regional Water Engineer (RWE). *Construction activity* shall not resume until written permission to do so has been received from the RWE.

B. Continuation of the Expired General Permit

This permit expires five (5) years from the effective date. If a new general permit is not issued prior to the expiration of this general permit, an *owner or operator* with coverage under this permit may continue to operate and *discharge* in accordance with the terms and conditions of this general permit, if it is extended pursuant to the State Administrative Procedure Act and 6 NYCRR Part 621, until a new general permit is issued.

C. Enforcement

Failure of the *owner or operator*, its contractors, subcontractors, agents and/or assigns to strictly adhere to any of the permit requirements contained herein shall constitute a violation of this permit. There are substantial criminal, civil, and administrative penalties associated with violating the provisions of this permit. Fines of up to \$37,500 per day for each violation and imprisonment for up to fifteen (15) years may be assessed depending upon the nature and degree of the offense.

D. Need to Halt or Reduce Activity Not a Defense

It shall not be a defense for an *owner or operator* in an enforcement action that it would have been necessary to halt or reduce the *construction activity* in order to maintain compliance with the conditions of this permit.

E. Duty to Mitigate

The *owner or operator* and its contractors and subcontractors shall take all reasonable steps to *minimize* or prevent any *discharge* in violation of this permit which has a reasonable likelihood of adversely affecting human health or the environment.

F. Duty to Provide Information

The *owner or operator* shall furnish to the Department, within a reasonable specified time period of a written request, all documentation necessary to demonstrate eligibility and any information to determine compliance with this permit or to determine whether cause exists for modifying or revoking this permit, or suspending or denying coverage under this permit, in accordance with the terms and conditions of this permit. The NOI, SWPPP and inspection reports required by this permit are public documents that the *owner or operator* must make available for review and copying by any person within five (5) business days of the *owner or operator* receiving a written request by any such person to review these documents. Copying of documents will be done at the requester's expense.

G. Other Information

When the *owner or operator* becomes aware that they failed to submit any relevant facts, or submitted incorrect information in the NOI or in any of the documents required by this permit, or have made substantive revisions to the SWPPP (e.g. the scope of the project changes significantly, the type of post-construction stormwater management practice(s) changes, there is a reduction in the sizing of the post-construction stormwater management practice, or there is an increase in the disturbance area or *impervious area*), which were not reflected in the original NOI submitted to the Department, they shall promptly submit such facts or information to the Department using the contact information in Part II.A. of this permit. Failure of the *owner or operator* to correct or supplement any relevant facts within five (5) business days of becoming aware of the deficiency shall constitute a violation of this permit.

H. Signatory Requirements

1. All NOIs and NOTs shall be signed as follows:
 - a. For a corporation these forms shall be signed by a responsible corporate officer. For the purpose of this section, a responsible corporate officer means:

- (i) a president, secretary, treasurer, or vice-president of the corporation in charge of a principal business function, or any other person who performs similar policy or decision-making functions for the corporation; or
 - (ii) the manager of one or more manufacturing, production or operating facilities, provided the manager is authorized to make management decisions which govern the operation of the regulated facility including having the explicit or implicit duty of making major capital investment recommendations, and initiating and directing other comprehensive measures to assure long term environmental compliance with environmental laws and regulations; the manager can ensure that the necessary systems are established or actions taken to gather complete and accurate information for permit application requirements; and where authority to sign documents has been assigned or delegated to the manager in accordance with corporate procedures;
 - b. For a partnership or sole proprietorship these forms shall be signed by a general partner or the proprietor, respectively; or
 - c. For a municipality, State, Federal, or other public agency these forms shall be signed by either a principal executive officer or ranking elected official. For purposes of this section, a principal executive officer of a Federal agency includes:
 - (i) the chief executive officer of the agency, or
 - (ii) a senior executive officer having responsibility for the overall operations of a principal geographic unit of the agency (e.g., Regional Administrators of EPA).
2. The SWPPP and other information requested by the Department shall be signed by a person described in Part VII.H.1. of this permit or by a duly authorized representative of that person. A person is a duly authorized representative only if:
- a. The authorization is made in writing by a person described in Part VII.H.1. of this permit;
 - b. The authorization specifies either an individual or a position having responsibility for the overall operation of the regulated facility or activity, such as the position of plant manager, operator of a well or a well field,

superintendent, position of *equivalent* responsibility, or an individual or position having overall responsibility for environmental matters for the company. (A duly authorized representative may thus be either a named individual or any individual occupying a named position) and,

- c. The written authorization shall include the name, title and signature of the authorized representative and be attached to the SWPPP.
3. All inspection reports shall be signed by the *qualified inspector* that performs the inspection.
4. The MS4 SWPPP Acceptance form shall be signed by the principal executive officer or ranking elected official from the *regulated, traditional land use control MS4*, or by a duly authorized representative of that person.

It shall constitute a permit violation if an incorrect and/or improper signatory authorizes any required forms, SWPPP and/or inspection reports.

I. Property Rights

The issuance of this permit does not convey any property rights of any sort, nor any exclusive privileges, nor does it authorize any injury to private property nor any invasion of personal rights, nor any infringement of Federal, State or local laws or regulations. *Owners or operators* must obtain any applicable conveyances, easements, licenses and/or access to real property prior to *commencing construction activity*.

J. Severability

The provisions of this permit are severable, and if any provision of this permit, or the application of any provision of this permit to any circumstance, is held invalid, the application of such provision to other circumstances, and the remainder of this permit shall not be affected thereby.

K. Requirement to Obtain Coverage Under an Alternative Permit

1. The Department may require any owner or operator authorized by this permit to apply for and/or obtain either an individual SPDES permit or another SPDES general permit. When the Department requires any discharger authorized by a general permit to apply for an individual SPDES permit, it shall notify the discharger in writing that a permit application is required. This notice shall

include a brief statement of the reasons for this decision, an application form, a statement setting a time frame for the owner or operator to file the application for an individual SPDES permit, and a deadline, not sooner than 180 days from owner or operator receipt of the notification letter, whereby the authorization to discharge under this general permit shall be terminated. Applications must be submitted to the appropriate Permit Administrator at the Regional Office. The Department may grant additional time upon demonstration, to the satisfaction of the Department, that additional time to apply for an alternative authorization is necessary or where the Department has not provided a permit determination in accordance with Part 621 of this Title.

2. When an individual SPDES permit is issued to a discharger authorized to *discharge* under a general SPDES permit for the same *discharge(s)*, the general permit authorization for outfalls authorized under the individual SPDES permit is automatically terminated on the effective date of the individual permit unless termination is earlier in accordance with 6 NYCRR Part 750.

L. Proper Operation and Maintenance

The *owner or operator* shall at all times properly operate and maintain all facilities and systems of treatment and control (and related appurtenances) which are installed or used by the *owner or operator* to achieve compliance with the conditions of this permit and with the requirements of the SWPPP.

M. Inspection and Entry

The *owner or operator* shall allow an authorized representative of the Department, EPA, applicable county health department, or, in the case of a *construction site* which *discharges* through an *MS4*, an authorized representative of the *MS4* receiving the discharge, upon the presentation of credentials and other documents as may be required by law, to:

1. Enter upon the owner's or operator's premises where a regulated facility or activity is located or conducted or where records must be kept under the conditions of this permit;
2. Have access to and copy at reasonable times, any records that must be kept under the conditions of this permit; and

3. Inspect at reasonable times any facilities or equipment (including monitoring and control equipment), practices or operations regulated or required by this permit.
4. Sample or monitor at reasonable times, for purposes of assuring permit compliance or as otherwise authorized by the Act or ECL, any substances or parameters at any location.

N. Permit Actions

This permit may, at any time, be modified, suspended, revoked, or renewed by the Department in accordance with 6 NYCRR Part 621. The filing of a request by the *owner or operator* for a permit modification, revocation and reissuance, termination, a notification of planned changes or anticipated noncompliance does not limit, diminish and/or stay compliance with any terms of this permit.

O. Definitions

Definitions of key terms are included in Appendix A of this permit.

P. Re-Opener Clause

1. If there is evidence indicating potential or realized impacts on water quality due to any stormwater discharge associated with construction activity covered by this permit, the owner or operator of such discharge may be required to obtain an individual permit or alternative general permit in accordance with Part VII.K. of this permit or the permit may be modified to include different limitations and/or requirements.
2. Any Department initiated permit modification, suspension or revocation will be conducted in accordance with 6 NYCRR Part 621, 6 NYCRR 750-1.18, and 6 NYCRR 750-1.20.

Q. Penalties for Falsification of Forms and Reports

In accordance with 6NYCRR Part 750-2.4 and 750-2.5, any person who knowingly makes any false material statement, representation, or certification in any application, record, report or other document filed or required to be maintained under this permit, including reports of compliance or noncompliance shall, upon conviction, be punished in accordance with ECL §71-1933 and or Articles 175 and 210 of the New York State Penal Law.

R. Other Permits

Nothing in this permit relieves the *owner or operator* from a requirement to obtain any other permits required by law.

APPENDIX A – Acronyms and Definitions

Acronyms

APO – Agency Preservation Officer

BMP – Best Management Practice

CPESC – Certified Professional in Erosion and Sediment Control

Cpv – Channel Protection Volume

CWA – Clean Water Act (or the Federal Water Pollution Control Act, 33 U.S.C. §1251 et seq)

DOW – Division of Water

EAF – Environmental Assessment Form

ECL - Environmental Conservation Law

EPA – U. S. Environmental Protection Agency

HSG – Hydrologic Soil Group

MS4 – Municipal Separate Storm Sewer System

NOI – Notice of Intent

NOT – Notice of Termination

NPDES – National Pollutant Discharge Elimination System

OPRHP – Office of Parks, Recreation and Historic Places

Qf – Extreme Flood

Qp – Overbank Flood

RRv – Runoff Reduction Volume

RWE – Regional Water Engineer

SEQR – State Environmental Quality Review

SEQRA - State Environmental Quality Review Act

SHPA – State Historic Preservation Act

SPDES – State Pollutant Discharge Elimination System

SWPPP – Stormwater Pollution Prevention Plan

TMDL – Total Maximum Daily Load

UPA – Uniform Procedures Act

USDA – United States Department of Agriculture

WQv – Water Quality Volume

Definitions

All definitions in this section are solely for the purposes of this permit.

Agricultural Building – a structure designed and constructed to house farm implements, hay, grain, poultry, livestock or other horticultural products; excluding any structure designed, constructed or used, in whole or in part, for human habitation, as a place of employment where agricultural products are processed, treated or packaged, or as a place used by the public.

Agricultural Property – means the land for construction of a barn, *agricultural building*, silo, stockyard, pen or other structural practices identified in Table II in the “Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State” prepared by the Department in cooperation with agencies of New York Nonpoint Source Coordinating Committee (dated June 2007).

Alter Hydrology from Pre to Post-Development Conditions - means the post-development peak flow rate(s) has increased by more than 5% of the pre-developed condition for the design storm of interest (e.g. 10 yr and 100 yr).

Combined Sewer - means a sewer that is designed to collect and convey both “sewage” and “stormwater”.

Commence (Commencement of) Construction Activities - means the initial disturbance of soils associated with clearing, grading or excavation activities; or other construction related activities that disturb or expose soils such as demolition, stockpiling of fill material, and the initial installation of erosion and sediment control practices required in the SWPPP. See definition for “*Construction Activity(ies)*” also.

Construction Activity(ies) - means any clearing, grading, excavation, filling, demolition or stockpiling activities that result in soil disturbance. Clearing activities can include, but are not limited to, logging equipment operation, the cutting and skidding of trees, stump removal and/or brush root removal. Construction activity does not include routine maintenance that is performed to maintain the original line and grade, hydraulic capacity, or original purpose of a facility.

Construction Site – means the land area where *construction activity(ies)* will occur. See definition for “*Commence (Commencement of) Construction Activities*” and “*Larger Common Plan of Development or Sale*” also.

Dewatering – means the act of draining rainwater and/or groundwater from building foundations, vaults or excavations/trenches.

Direct Discharge (to a specific surface waterbody) - means that runoff flows from a *construction site* by overland flow and the first point of discharge is the specific surface waterbody, or runoff flows from a *construction site* to a separate storm sewer system

and the first point of discharge from the separate storm sewer system is the specific surface waterbody.

Discharge(s) - means any addition of any pollutant to waters of the State through an outlet or *point source*.

Embankment – means an earthen or rock slope that supports a road/highway.

Endangered or Threatened Species – see 6 NYCRR Part 182 of the Department’s rules and regulations for definition of terms and requirements.

Environmental Conservation Law (ECL) - means chapter 43-B of the Consolidated Laws of the State of New York, entitled the Environmental Conservation Law.

Equivalent (Equivalence) – means that the practice or measure meets all the performance, longevity, maintenance, and safety objectives of the technical standard and will provide an equal or greater degree of water quality protection.

Final Stabilization - means that all soil disturbance activities have ceased and a uniform, perennial vegetative cover with a density of eighty (80) percent over the entire pervious surface has been established; or other equivalent stabilization measures, such as permanent landscape mulches, rock rip-rap or washed/crushed stone have been applied on all disturbed areas that are not covered by permanent structures, concrete or pavement.

General SPDES permit - means a SPDES permit issued pursuant to 6 NYCRR Part 750-1.21 and Section 70-0117 of the ECL authorizing a category of discharges.

Groundwater(s) - means waters in the saturated zone. The saturated zone is a subsurface zone in which all the interstices are filled with water under pressure greater than that of the atmosphere. Although the zone may contain gas-filled interstices or interstices filled with fluids other than water, it is still considered saturated.

Historic Property – means any building, structure, site, object or district that is listed on the State or National Registers of Historic Places or is determined to be eligible for listing on the State or National Registers of Historic Places.

Impervious Area (Cover) - means all impermeable surfaces that cannot effectively infiltrate rainfall. This includes paved, concrete and gravel surfaces (i.e. parking lots, driveways, roads, runways and sidewalks); building rooftops and miscellaneous impermeable structures such as patios, pools, and sheds.

Infeasible – means not technologically possible, or not economically practicable and achievable in light of best industry practices.

Larger Common Plan of Development or Sale - means a contiguous area where multiple separate and distinct *construction activities* are occurring, or will occur, under one plan. The term “plan” in “larger common plan of development or sale” is broadly defined as any announcement or piece of documentation (including a sign, public notice or hearing, marketing plan, advertisement, drawing, permit application, State Environmental Quality Review Act (SEQRA) environmental assessment form or other documents, zoning request, computer design, etc.) or physical demarcation (including boundary signs, lot stakes, surveyor markings, etc.) indicating that *construction activities* may occur on a specific plot.

For discrete construction projects that are located within a larger common plan of development or sale that are at least 1/4 mile apart, each project can be treated as a separate plan of development or sale provided any interconnecting road, pipeline or utility project that is part of the same “common plan” is not concurrently being disturbed.

Minimize – means reduce and/or eliminate to the extent achievable using control measures (including best management practices) that are technologically available and economically practicable and achievable in light of best industry practices.

Municipal Separate Storm Sewer (MS4) - a conveyance or system of conveyances (including roads with drainage systems, municipal streets, catch basins, curbs, gutters, ditches, man-made channels, or storm drains):

- (i) Owned or operated by a State, city, town, borough, county, parish, district, association, or other public body (created by or pursuant to State law) having jurisdiction over disposal of sewage, industrial wastes, stormwater, or other wastes, including special districts under State law such as a sewer district, flood control district or drainage district, or similar entity, or an Indian tribe or an authorized Indian tribal organization, or a designated and approved management agency under section 208 of the CWA that discharges to surface waters of the State;
- (ii) Designed or used for collecting or conveying stormwater;
- (iii) Which is not a *combined sewer*, and
- (iv) Which is not part of a Publicly Owned Treatment Works (POTW) as defined at 40 CFR 122.2.

National Pollutant Discharge Elimination System (NPDES) - means the national system for the issuance of wastewater and stormwater permits under the Federal Water Pollution Control Act (Clean Water Act).

Natural Buffer – means an undisturbed area with natural cover running along a surface water (e.g. wetland, stream, river, lake, etc.).

New Development – means any land disturbance that does not meet the definition of Redevelopment Activity included in this appendix.

New York State Erosion and Sediment Control Certificate Program – a certificate program that establishes and maintains a process to identify and recognize individuals who are capable of developing, designing, inspecting and maintaining erosion and sediment control plans on projects that disturb soils in New York State. The certificate program is administered by the New York State Conservation District Employees Association.

NOI Acknowledgment Letter - means the letter that the Department sends to an owner or operator to acknowledge the Department's receipt and acceptance of a complete Notice of Intent. This letter documents the owner's or operator's authorization to discharge in accordance with the general permit for stormwater discharges from *construction activity*.

Nonpoint Source - means any source of water pollution or pollutants which is not a discrete conveyance or *point source* permitted pursuant to Title 7 or 8 of Article 17 of the Environmental Conservation Law (see ECL Section 17-1403).

Overbank –means flow events that exceed the capacity of the stream channel and spill out into the adjacent floodplain.

Owner or Operator - means the person, persons or legal entity which owns or leases the property on which the *construction activity* is occurring; an entity that has operational control over the construction plans and specifications, including the ability to make modifications to the plans and specifications; and/or an entity that has day-to-day operational control of those activities at a project that are necessary to ensure compliance with the permit conditions.

Performance Criteria – means the design criteria listed under the “Required Elements” sections in Chapters 5, 6 and 10 of the technical standard, New York State Stormwater Management Design Manual, dated January 2015. It does not include the Sizing Criteria (i.e. WQv, RRv, Cpv, Qp and Qf) in Part I.C.2. of the permit.

Point Source - means any discernible, confined and discrete conveyance, including but not limited to any pipe, ditch, channel, tunnel, conduit, well, discrete fissure, container, rolling stock, concentrated animal feeding operation, vessel or other floating craft, or landfill leachate collection system from which *pollutants* are or may be discharged.

Pollutant - means dredged spoil, filter backwash, solid waste, incinerator residue, sewage, garbage, sewage sludge, munitions, chemical wastes, biological materials, radioactive materials, heat, wrecked or discarded equipment, rock, sand and industrial, municipal, agricultural waste and ballast discharged into water; which may cause or might reasonably be expected to cause pollution of the waters of the state in contravention of the standards or guidance values adopted as provided in 6 NYCRR Parts 700 et seq .

Qualified Inspector - means a person that is knowledgeable in the principles and practices of erosion and sediment control, such as a licensed Professional Engineer, Certified Professional in Erosion and Sediment Control (CPESC), Registered Landscape Architect, New York State Erosion and Sediment Control Certificate Program holder or other Department endorsed individual(s).

It can also mean someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided that person has training in the principles and practices of erosion and sediment control. Training in the principles and practices of erosion and sediment control means that the individual working under the direct supervision of the licensed Professional Engineer or Registered Landscape Architect has received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity. After receiving the initial training, the individual working under the direct supervision of the licensed Professional Engineer or Registered Landscape Architect shall receive four (4) hours of training every three (3) years.

It can also mean a person that meets the *Qualified Professional* qualifications in addition to the *Qualified Inspector* qualifications.

Note: Inspections of any post-construction stormwater management practices that include structural components, such as a dam for an impoundment, shall be performed by a licensed Professional Engineer.

Qualified Professional - means a person that is knowledgeable in the principles and practices of stormwater management and treatment, such as a licensed Professional Engineer, Registered Landscape Architect or other Department endorsed individual(s). Individuals preparing SWPPPs that require the post-construction stormwater management practice component must have an understanding of the principles of hydrology, water quality management practice design, water quantity control design, and, in many cases, the principles of hydraulics. All components of the SWPPP that involve the practice of engineering, as defined by the NYS Education Law (see Article 145), shall be prepared by, or under the direct supervision of, a professional engineer licensed to practice in the State of New York.

Redevelopment Activity(ies) – means the disturbance and reconstruction of existing impervious area, including impervious areas that were removed from a project site within five (5) years of preliminary project plan submission to the local government (i.e. site plan, subdivision, etc.).

Regulated, Traditional Land Use Control MS4 - means a city, town or village with land use control authority that is authorized to discharge under New York State DEC's

SPDES General Permit For Stormwater Discharges from Municipal Separate Stormwater Sewer Systems (MS4s) or the City of New York's Individual SPDES Permit for their Municipal Separate Storm Sewer Systems (NY-0287890).

Routine Maintenance Activity - means *construction activity* that is performed to maintain the original line and grade, hydraulic capacity, or original purpose of a facility, including, but not limited to:

- Re-grading of gravel roads or parking lots,
- Cleaning and shaping of existing roadside ditches and culverts that maintains the approximate original line and grade, and hydraulic capacity of the ditch,
- Cleaning and shaping of existing roadside ditches that does not maintain the approximate original grade, hydraulic capacity and purpose of the ditch if the changes to the line and grade, hydraulic capacity or purpose of the ditch are installed to improve water quality and quantity controls (e.g. installing grass lined ditch),
- Placement of aggregate shoulder backing that stabilizes the transition between the road shoulder and the ditch or *embankment*,
- Full depth milling and filling of existing asphalt pavements, replacement of concrete pavement slabs, and similar work that does not expose soil or disturb the bottom six (6) inches of subbase material,
- Long-term use of equipment storage areas at or near highway maintenance facilities,
- Removal of sediment from the edge of the highway to restore a previously existing sheet-flow drainage connection from the highway surface to the highway ditch or *embankment*,
- Existing use of Canal Corp owned upland disposal sites for the canal, and
- Replacement of curbs, gutters, sidewalks and guide rail posts.

Site limitations – means site conditions that prevent the use of an infiltration technique and or infiltration of the total WQv. Typical site limitations include: seasonal high groundwater, shallow depth to bedrock, and soils with an infiltration rate less than 0.5 inches/hour. The existence of site limitations shall be confirmed and documented using actual field testing (i.e. test pits, soil borings, and infiltration test) or using information from the most current United States Department of Agriculture (USDA) Soil Survey for the County where the project is located.

Sizing Criteria – means the criteria included in Part I.C.2 of the permit that are used to size post-construction stormwater management control practices. The criteria include; Water Quality Volume (WQv), Runoff Reduction Volume (RRv), Channel Protection Volume (Cpv), *Overbank Flood* (Qp), and *Extreme Flood* (Qf).

State Pollutant Discharge Elimination System (SPDES) - means the system established pursuant to Article 17 of the ECL and 6 NYCRR Part 750 for issuance of permits authorizing discharges to the waters of the state.

Steep Slope – means land area designated on the current United States Department of Agriculture (“USDA”) Soil Survey as Soil Slope Phase “D”, (provided the map unit name is inclusive of slopes greater than 25%) , or Soil Slope Phase E or F, (regardless of the map unit name), or a combination of the three designations.

Streambank – as used in this permit, means the terrain alongside the bed of a creek or stream. The bank consists of the sides of the channel, between which the flow is confined.

Stormwater Pollution Prevention Plan (SWPPP) – means a project specific report, including construction drawings, that among other things: describes the construction activity(ies), identifies the potential sources of pollution at the *construction site*; describes and shows the stormwater controls that will be used to control the pollutants (i.e. erosion and sediment controls; for many projects, includes post-construction stormwater management controls); and identifies procedures the *owner or operator* will implement to comply with the terms and conditions of the permit. See Part III of the permit for a complete description of the information that must be included in the SWPPP.

Surface Waters of the State - shall be construed to include lakes, bays, sounds, ponds, impounding reservoirs, springs, rivers, streams, creeks, estuaries, marshes, inlets, canals, the Atlantic ocean within the territorial seas of the state of New York and all other bodies of surface water, natural or artificial, inland or coastal, fresh or salt, public or private (except those private waters that do not combine or effect a junction with natural surface waters), which are wholly or partially within or bordering the state or within its jurisdiction. Waters of the state are further defined in 6 NYCRR Parts 800 to 941.

Temporarily Ceased – means that an existing disturbed area will not be disturbed again within 14 calendar days of the previous soil disturbance.

Temporary Stabilization - means that exposed soil has been covered with material(s) as set forth in the technical standard, New York Standards and Specifications for Erosion and Sediment Control, to prevent the exposed soil from eroding. The materials can include, but are not limited to, mulch, seed and mulch, and erosion control mats (e.g. jute twisted yarn, excelsior wood fiber mats).

Total Maximum Daily Loads (TMDLs) - A TMDL is the sum of the allowable loads of a single pollutant from all contributing point and *nonpoint sources*. It is a calculation of the maximum amount of a pollutant that a waterbody can receive on a daily basis and still meet *water quality standards*, and an allocation of that amount to the pollutant's sources. A TMDL stipulates wasteload allocations (WLAs) for *point source* discharges, load allocations (LAs) for *nonpoint sources*, and a margin of safety (MOS).

Trained Contractor - means an employee from the contracting (construction) company, identified in Part III.A.6., that has received four (4) hours of Department endorsed

training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity. After receiving the initial training, the *trained contractor* shall receive four (4) hours of training every three (3) years.

It can also mean an employee from the contracting (construction) company, identified in Part III.A.6., that meets the *qualified inspector* qualifications (e.g. licensed Professional Engineer, Certified Professional in Erosion and Sediment Control (CPESC), Registered Landscape Architect, New York State Erosion and Sediment Control Certificate Program holder, or someone working under the direct supervision of, and at the same company as, the licensed Professional Engineer or Registered Landscape Architect, provided they have received four (4) hours of Department endorsed training in proper erosion and sediment control principles from a Soil and Water Conservation District, or other Department endorsed entity).

The *trained contractor* is responsible for the day to day implementation of the SWPPP.

Uniform Procedures Act (UPA) Permit - means a permit required under 6 NYCRR Part 621 of the Environmental Conservation Law (ECL), Article 70.

Water Quality Standard - means such measures of purity or quality for any waters in relation to their reasonable and necessary use as promulgated in 6 NYCRR Part 700 et seq.

APPENDIX B – Required SWPPP Components by Project Type

Table 1
Construction Activities that Require the Preparation of a SWPPP That Only Includes Erosion and Sediment Controls

<p>The following construction activities that involve soil disturbances of one (1) or more acres of land, but less than five (5) acres:</p> <ul style="list-style-type: none">• Single family home <u>not</u> located in one of the watersheds listed in Appendix C or <u>not directly discharging</u> to one of the 303(d) segments listed in Appendix E• Single family residential subdivisions with 25% or less impervious cover at total site build-out and <u>not</u> located in one of the watersheds listed in Appendix C and <u>not</u> directly discharging to one of the 303(d) segments listed in Appendix E• Construction of a barn or other <i>agricultural building</i>, silo, stock yard or pen.
<p>The following construction activities that involve soil disturbances between five thousand (5000) square feet and one (1) acre of land:</p> <p>All construction activities located in the watersheds identified in Appendix D that involve soil disturbances between five thousand (5,000) square feet and one (1) acre of land.</p>
<p>The following construction activities that involve soil disturbances of one (1) or more acres of land:</p> <ul style="list-style-type: none">• Installation of underground, linear utilities; such as gas lines, fiber-optic cable, cable TV, electric, telephone, sewer mains, and water mains• Environmental enhancement projects, such as wetland mitigation projects, stormwater retrofits and stream restoration projects• Pond construction• Linear bike paths running through areas with vegetative cover, including bike paths surfaced with an impervious cover• Cross-country ski trails and walking/hiking trails• Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are not part of residential, commercial or institutional development;• Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that include incidental shoulder or curb work along an existing highway to support construction of the sidewalk, bike path or walking path.• Slope stabilization projects• Slope flattening that changes the grade of the site, but does not significantly change the runoff characteristics

Table 1 (Continued) CONSTRUCTION ACTIVITIES THAT REQUIRE THE PREPARATION OF A SWPPP THAT ONLY INCLUDES EROSION AND SEDIMENT CONTROLS

The following construction activities that involve soil disturbances of one (1) or more acres of land:

- Spoil areas that will be covered with vegetation
- Vegetated open space projects (i.e. recreational parks, lawns, meadows, fields, downhill ski trails) excluding projects that *alter hydrology from pre to post development* conditions,
- Athletic fields (natural grass) that do not include the construction or reconstruction of *impervious area* and do not *alter hydrology from pre to post development* conditions
- Demolition project where vegetation will be established, and no redevelopment is planned
- Overhead electric transmission line project that does not include the construction of permanent access roads or parking areas surfaced with *impervious cover*
- Structural practices as identified in Table II in the “Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State”, excluding projects that involve soil disturbances of greater than five acres and construction activities that include the construction or reconstruction of impervious area
- Temporary access roads, median crossovers, detour roads, lanes, or other temporary impervious areas that will be restored to pre-construction conditions once the construction activity is complete

Table 2
CONSTRUCTION ACTIVITIES THAT REQUIRE THE PREPARATION OF A SWPPP THAT INCLUDES
POST-CONSTRUCTION STORMWATER MANAGEMENT PRACTICES

The following construction activities that involve soil disturbances of one (1) or more acres of land:

- Single family home located in one of the watersheds listed in Appendix C or *directly discharging* to one of the 303(d) segments listed in Appendix E
- Single family home that disturbs five (5) or more acres of land
- Single family residential subdivisions located in one of the watersheds listed in Appendix C or *directly discharging* to one of the 303(d) segments listed in Appendix E
- Single family residential subdivisions that involve soil disturbances of between one (1) and five (5) acres of land with greater than 25% impervious cover at total site build-out
- Single family residential subdivisions that involve soil disturbances of five (5) or more acres of land, and single family residential subdivisions that involve soil disturbances of less than five (5) acres that are part of a larger common plan of development or sale that will ultimately disturb five or more acres of land
- Multi-family residential developments; includes duplexes, townhomes, condominiums, senior housing complexes, apartment complexes, and mobile home parks
- Airports
- Amusement parks
- Breweries, cideries, and wineries, including establishments constructed on agricultural land
- Campgrounds
- Cemeteries that include the construction or reconstruction of impervious area (>5% of disturbed area) or *alter the hydrology from pre to post development* conditions
- Commercial developments
- Churches and other places of worship
- Construction of a barn or other *agricultural building* (e.g. silo) and structural practices as identified in Table II in the "Agricultural Management Practices Catalog for Nonpoint Source Pollution in New York State" that include the construction or reconstruction of *impervious area*, excluding projects that involve soil disturbances of less than five acres.
- Golf courses
- Institutional development; includes hospitals, prisons, schools and colleges
- Industrial facilities; includes industrial parks
- Landfills
- Municipal facilities; includes highway garages, transfer stations, office buildings, POTW's, water treatment plants, and water storage tanks
- Office complexes
- Playgrounds that include the construction or reconstruction of impervious area
- Sports complexes
- Racetracks; includes racetracks with earthen (dirt) surface
- Road construction or reconstruction, including roads constructed as part of the construction activities listed in Table 1

Table 2 (Continued)

CONSTRUCTION ACTIVITIES THAT REQUIRE THE PREPARATION OF A SWPPP THAT INCLUDES POST-CONSTRUCTION STORMWATER MANAGEMENT PRACTICES

The following construction activities that involve soil disturbances of one (1) or more acres of land:

- Parking lot construction or reconstruction, including parking lots constructed as part of the construction activities listed in Table 1
- Athletic fields (natural grass) that include the construction or reconstruction of impervious area (>5% of disturbed area) or *alter the hydrology from pre to post development* conditions
- Athletic fields with artificial turf
- Permanent access roads, parking areas, substations, compressor stations and well drilling pads, surfaced with *impervious cover*, and constructed as part of an over-head electric transmission line project, wind-power project, cell tower project, oil or gas well drilling project, sewer or water main project or other linear utility project
- Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are part of a residential, commercial or institutional development
- Sidewalk, bike path or walking path projects, surfaced with an impervious cover, that are part of a highway construction or reconstruction project
- All other construction activities that include the construction or reconstruction of *impervious area* or *alter the hydrology from pre to post development* conditions, and are not listed in Table 1

APPENDIX C – Watersheds Requiring Enhanced Phosphorus Removal

Watersheds where *owners or operators* of construction activities identified in Table 2 of Appendix B must prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the Enhanced Phosphorus Removal Standards included in the technical standard, New York State Stormwater Management Design Manual (“Design Manual”).

- Entire New York City Watershed located east of the Hudson River - Figure 1
- Onondaga Lake Watershed - Figure 2
- Greenwood Lake Watershed -Figure 3
- Oscawana Lake Watershed – Figure 4
- Kinderhook Lake Watershed – Figure 5

Figure 1 - New York City Watershed East of the Hudson

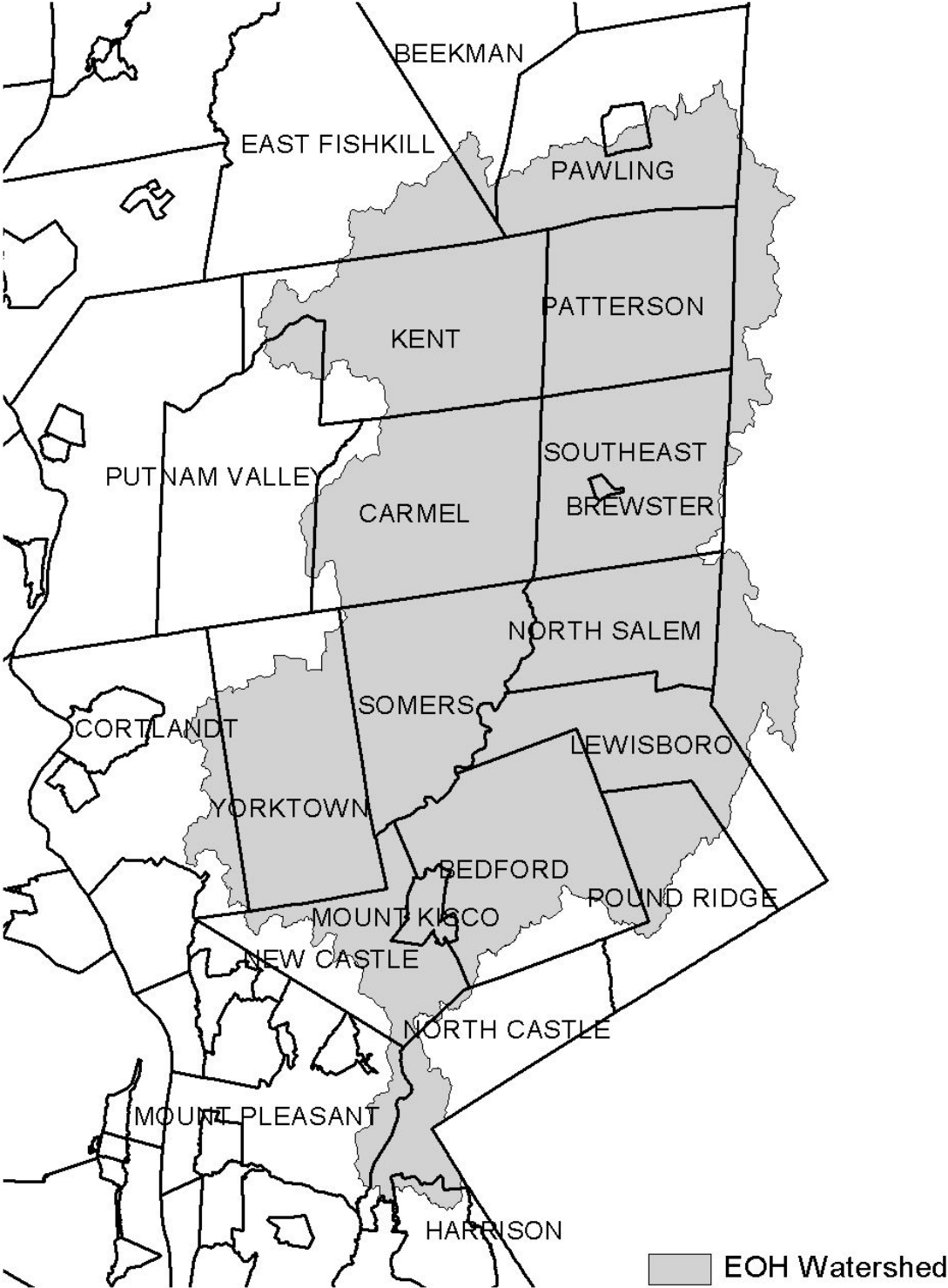


Figure 2 - Onondaga Lake Watershed



Figure 3 - Greenwood Lake Watershed

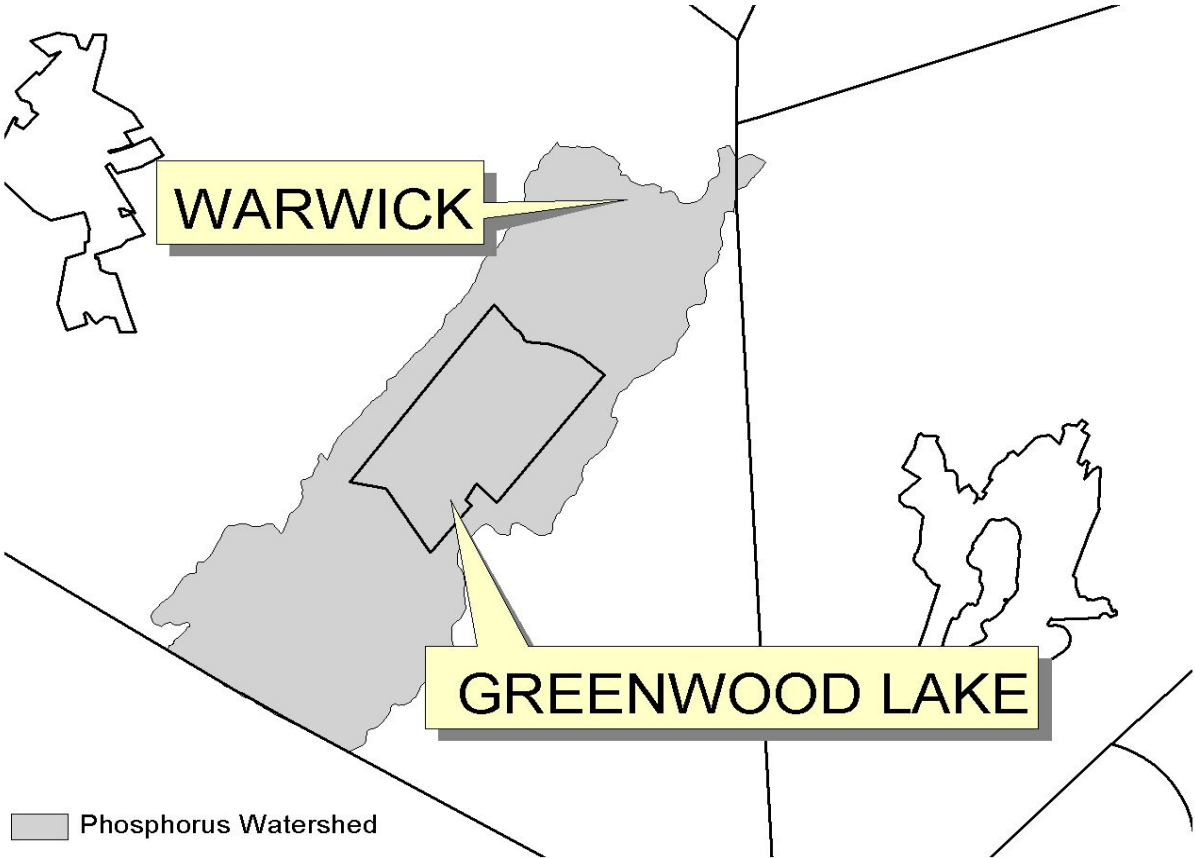


Figure 4 - Oscawana Lake Watershed

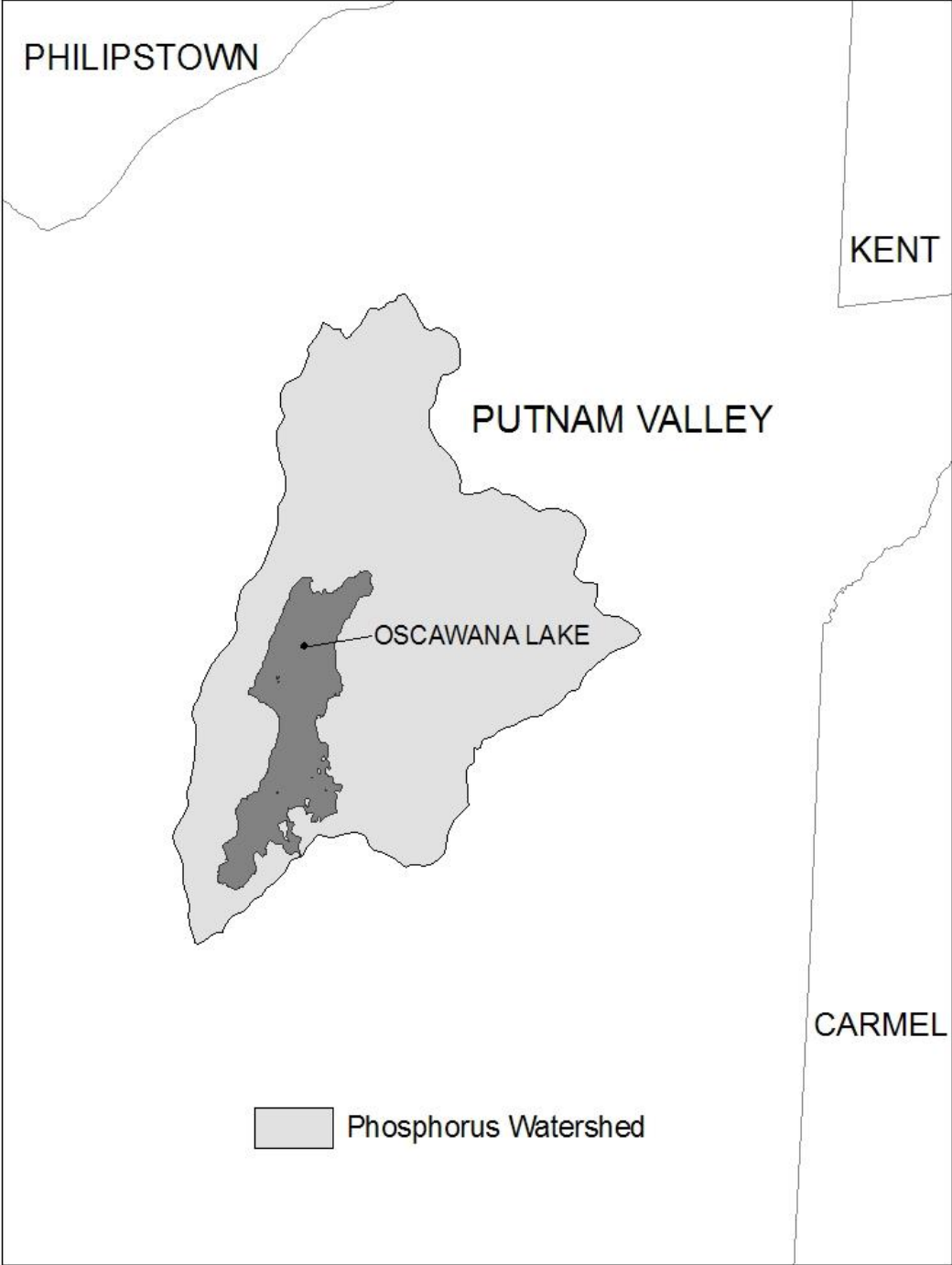
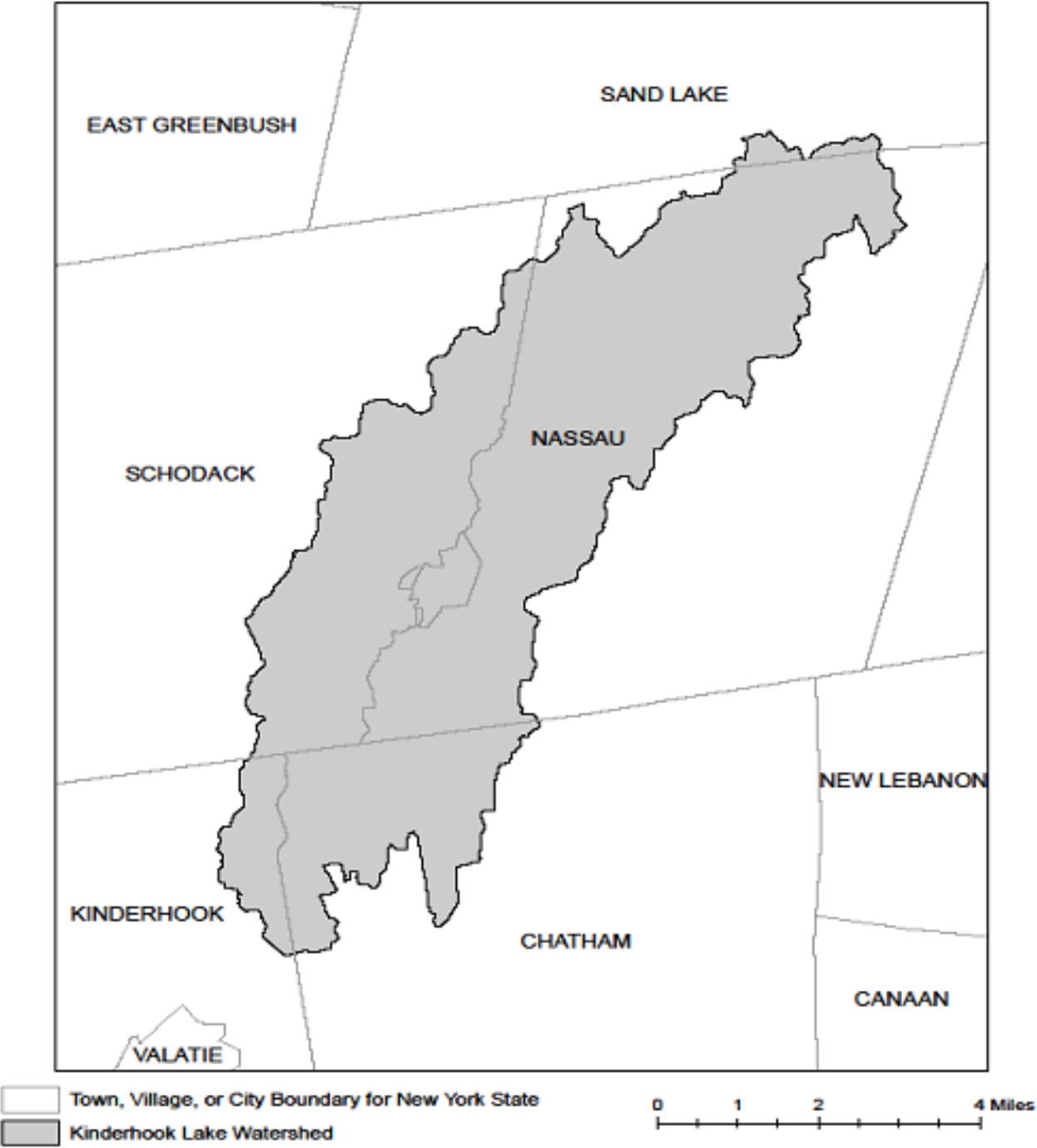


Figure 5 - Kinderhook Lake Watershed



APPENDIX D – Watersheds with Lower Disturbance Threshold

Watersheds where *owners or operators* of construction activities that involve soil disturbances between five thousand (5000) square feet and one (1) acre of land must obtain coverage under this permit.

Entire New York City Watershed that is located east of the Hudson River - See Figure 1 in Appendix C

APPENDIX E – 303(d) Segments Impaired by Construction Related Pollutant(s)

List of 303(d) segments impaired by pollutants related to *construction activity* (e.g. silt, sediment or nutrients). The list was developed using "The Final New York State 2016 Section 303(d) List of Impaired Waters Requiring a TMDL/Other Strategy" dated November 2016. *Owners or operators* of single family home and single family residential subdivisions with 25% or less total impervious cover at total site build-out that involve soil disturbances of one or more acres of land, but less than 5 acres, and *directly discharge* to one of the listed segments below shall prepare a SWPPP that includes post-construction stormwater management practices designed in conformance with the New York State Stormwater Management Design Manual ("Design Manual"), dated January 2015.

COUNTY	WATERBODY	POLLUTANT
Albany	Ann Lee (Shakers) Pond, Stump Pond	Nutrients
Albany	Basic Creek Reservoir	Nutrients
Allegany	Amity Lake, Saunders Pond	Nutrients
Bronx	Long Island Sound, Bronx	Nutrients
Bronx	Van Cortlandt Lake	Nutrients
Broome	Fly Pond, Deer Lake, Sky Lake	Nutrients
Broome	Minor Tribs to Lower Susquehanna (north)	Nutrients
Broome	Whitney Point Lake/Reservoir	Nutrients
Cattaraugus	Allegheny River/Reservoir	Nutrients
Cattaraugus	Beaver (Alma) Lake	Nutrients
Cattaraugus	Case Lake	Nutrients
Cattaraugus	Linlyco/Club Pond	Nutrients
Cayuga	Duck Lake	Nutrients
Cayuga	Little Sodus Bay	Nutrients
Chautauqua	Bear Lake	Nutrients
Chautauqua	Chadakoin River and tribs	Nutrients
Chautauqua	Chautauqua Lake, North	Nutrients
Chautauqua	Chautauqua Lake, South	Nutrients
Chautauqua	Findley Lake	Nutrients
Chautauqua	Hulburt/Clymer Pond	Nutrients
Clinton	Great Chazy River, Lower, Main Stem	Silt/Sediment
Clinton	Lake Champlain, Main Lake, Middle	Nutrients
Clinton	Lake Champlain, Main Lake, North	Nutrients
Columbia	Kinderhook Lake	Nutrients
Columbia	Robinson Pond	Nutrients
Cortland	Dean Pond	Nutrients

303(d) Segments Impaired by Construction Related Pollutant(s)

Dutchess	Fall Kill and tribs	Nutrients
Dutchess	Hillside Lake	Nutrients
Dutchess	Wappingers Lake	Nutrients
Dutchess	Wappingers Lake	Silt/Sediment
Erie	Beeman Creek and tribs	Nutrients
Erie	Ellicott Creek, Lower, and tribs	Silt/Sediment
Erie	Ellicott Creek, Lower, and tribs	Nutrients
Erie	Green Lake	Nutrients
Erie	Little Sister Creek, Lower, and tribs	Nutrients
Erie	Murder Creek, Lower, and tribs	Nutrients
Erie	Rush Creek and tribs	Nutrients
Erie	Scajaquada Creek, Lower, and tribs	Nutrients
Erie	Scajaquada Creek, Middle, and tribs	Nutrients
Erie	Scajaquada Creek, Upper, and tribs	Nutrients
Erie	South Branch Smoke Cr, Lower, and tribs	Silt/Sediment
Erie	South Branch Smoke Cr, Lower, and tribs	Nutrients
Essex	Lake Champlain, Main Lake, South	Nutrients
Essex	Lake Champlain, South Lake	Nutrients
Essex	Willsboro Bay	Nutrients
Genesee	Bigelow Creek and tribs	Nutrients
Genesee	Black Creek, Middle, and minor tribs	Nutrients
Genesee	Black Creek, Upper, and minor tribs	Nutrients
Genesee	Bowen Brook and tribs	Nutrients
Genesee	LeRoy Reservoir	Nutrients
Genesee	Oak Orchard Cr, Upper, and tribs	Nutrients
Genesee	Tonawanda Creek, Middle, Main Stem	Nutrients
Greene	Schoharie Reservoir	Silt/Sediment
Greene	Sleepy Hollow Lake	Silt/Sediment
Herkimer	Steele Creek tribs	Silt/Sediment
Herkimer	Steele Creek tribs	Nutrients
Jefferson	Moon Lake	Nutrients
Kings	Hendrix Creek	Nutrients
Kings	Prospect Park Lake	Nutrients
Lewis	Mill Creek/South Branch, and tribs	Nutrients
Livingston	Christie Creek and tribs	Nutrients
Livingston	Conesus Lake	Nutrients
Livingston	Mill Creek and minor tribs	Silt/Sediment
Monroe	Black Creek, Lower, and minor tribs	Nutrients
Monroe	Buck Pond	Nutrients
Monroe	Cranberry Pond	Nutrients

303(d) Segments Impaired by Construction Related Pollutant(s)

Monroe	Lake Ontario Shoreline, Western	Nutrients
Monroe	Long Pond	Nutrients
Monroe	Mill Creek and tribs	Nutrients
Monroe	Mill Creek/Blue Pond Outlet and tribs	Nutrients
Monroe	Minor Tribs to Irondequoit Bay	Nutrients
Monroe	Rochester Embayment - East	Nutrients
Monroe	Rochester Embayment - West	Nutrients
Monroe	Shipbuilders Creek and tribs	Nutrients
Monroe	Thomas Creek/White Brook and tribs	Nutrients
Nassau	Beaver Lake	Nutrients
Nassau	Camaans Pond	Nutrients
Nassau	East Meadow Brook, Upper, and tribs	Silt/Sediment
Nassau	East Rockaway Channel	Nutrients
Nassau	Grant Park Pond	Nutrients
Nassau	Hempstead Bay	Nutrients
Nassau	Hempstead Lake	Nutrients
Nassau	Hewlett Bay	Nutrients
Nassau	Hog Island Channel	Nutrients
Nassau	Long Island Sound, Nassau County Waters	Nutrients
Nassau	Massapequa Creek and tribs	Nutrients
Nassau	Milburn/Parsonage Creeks, Upp, and tribs	Nutrients
Nassau	Reynolds Channel, west	Nutrients
Nassau	Tidal Tribs to Hempstead Bay	Nutrients
Nassau	Tribs (fresh) to East Bay	Nutrients
Nassau	Tribs (fresh) to East Bay	Silt/Sediment
Nassau	Tribs to Smith/Halls Ponds	Nutrients
Nassau	Woodmere Channel	Nutrients
New York	Harlem Meer	Nutrients
New York	The Lake in Central Park	Nutrients
Niagara	Bergholtz Creek and tribs	Nutrients
Niagara	Hyde Park Lake	Nutrients
Niagara	Lake Ontario Shoreline, Western	Nutrients
Niagara	Lake Ontario Shoreline, Western	Nutrients
Oneida	Ballou, Nail Creeks and tribs	Nutrients
Onondaga	Harbor Brook, Lower, and tribs	Nutrients
Onondaga	Ley Creek and tribs	Nutrients
Onondaga	Minor Tribs to Onondaga Lake	Nutrients
Onondaga	Ninemile Creek, Lower, and tribs	Nutrients
Onondaga	Onondaga Creek, Lower, and tribs	Nutrients
Onondaga	Onondaga Creek, Middle, and tribs	Nutrients

303(d) Segments Impaired by Construction Related Pollutant(s)

Onondaga	Onondaga Lake, northern end	Nutrients
Onondaga	Onondaga Lake, southern end	Nutrients
Ontario	Great Brook and minor tribs	Silt/Sediment
Ontario	Great Brook and minor tribs	Nutrients
Ontario	Hemlock Lake Outlet and minor tribs	Nutrients
Ontario	Honeoye Lake	Nutrients
Orange	Greenwood Lake	Nutrients
Orange	Monhagen Brook and tribs	Nutrients
Orange	Orange Lake	Nutrients
Orleans	Lake Ontario Shoreline, Western	Nutrients
Orleans	Lake Ontario Shoreline, Western	Nutrients
Oswego	Lake Neatahwanta	Nutrients
Oswego	Pleasant Lake	Nutrients
Putnam	Bog Brook Reservoir	Nutrients
Putnam	Boyd Corners Reservoir	Nutrients
Putnam	Croton Falls Reservoir	Nutrients
Putnam	Diverting Reservoir	Nutrients
Putnam	East Branch Reservoir	Nutrients
Putnam	Lake Carmel	Nutrients
Putnam	Middle Branch Reservoir	Nutrients
Putnam	Oscawana Lake	Nutrients
Putnam	Palmer Lake	Nutrients
Putnam	West Branch Reservoir	Nutrients
Queens	Bergen Basin	Nutrients
Queens	Flushing Creek/Bay	Nutrients
Queens	Jamaica Bay, Eastern, and tribs (Queens)	Nutrients
Queens	Kissena Lake	Nutrients
Queens	Meadow Lake	Nutrients
Queens	Willow Lake	Nutrients
Rensselaer	Nassau Lake	Nutrients
Rensselaer	Snyders Lake	Nutrients
Richmond	Grasmere Lake/Bradys Pond	Nutrients
Rockland	Congers Lake, Swartout Lake	Nutrients
Rockland	Rockland Lake	Nutrients
Saratoga	Ballston Lake	Nutrients
Saratoga	Dwaas Kill and tribs	Silt/Sediment
Saratoga	Dwaas Kill and tribs	Nutrients
Saratoga	Lake Lonely	Nutrients
Saratoga	Round Lake	Nutrients
Saratoga	Tribs to Lake Lonely	Nutrients

303(d) Segments Impaired by Construction Related Pollutant(s)

Schenectady	Collins Lake	Nutrients
Schenectady	Duane Lake	Nutrients
Schenectady	Mariaville Lake	Nutrients
Schoharie	Engleville Pond	Nutrients
Schoharie	Summit Lake	Nutrients
Seneca	Reeder Creek and tribs	Nutrients
St.Lawrence	Black Lake Outlet/Black Lake	Nutrients
St.Lawrence	Fish Creek and minor tribs	Nutrients
Steuben	Smith Pond	Nutrients
Suffolk	Agawam Lake	Nutrients
Suffolk	Big/Little Fresh Ponds	Nutrients
Suffolk	Canaan Lake	Silt/Sediment
Suffolk	Canaan Lake	Nutrients
Suffolk	Flanders Bay, West/Lower Sawmill Creek	Nutrients
Suffolk	Fresh Pond	Nutrients
Suffolk	Great South Bay, East	Nutrients
Suffolk	Great South Bay, Middle	Nutrients
Suffolk	Great South Bay, West	Nutrients
Suffolk	Lake Ronkonkoma	Nutrients
Suffolk	Long Island Sound, Suffolk County, West	Nutrients
Suffolk	Mattituck (Marratooka) Pond	Nutrients
Suffolk	Meetinghouse/Terrys Creeks and tribs	Nutrients
Suffolk	Mill and Seven Ponds	Nutrients
Suffolk	Millers Pond	Nutrients
Suffolk	Moriches Bay, East	Nutrients
Suffolk	Moriches Bay, West	Nutrients
Suffolk	Peconic River, Lower, and tidal tribs	Nutrients
Suffolk	Quantuck Bay	Nutrients
Suffolk	Shinnecock Bay and Inlet	Nutrients
Suffolk	Tidal tribs to West Moriches Bay	Nutrients
Sullivan	Bodine, Montgomery Lakes	Nutrients
Sullivan	Davies Lake	Nutrients
Sullivan	Evens Lake	Nutrients
Sullivan	Pleasure Lake	Nutrients
Tompkins	Cayuga Lake, Southern End	Nutrients
Tompkins	Cayuga Lake, Southern End	Silt/Sediment
Tompkins	Owasco Inlet, Upper, and tribs	Nutrients
Ulster	Ashokan Reservoir	Silt/Sediment
Ulster	Esopus Creek, Upper, and minor tribs	Silt/Sediment
Warren	Hague Brook and tribs	Silt/Sediment

303(d) Segments Impaired by Construction Related Pollutant(s)

Warren	Huddle/Finkle Brooks and tribs	Silt/Sediment
Warren	Indian Brook and tribs	Silt/Sediment
Warren	Lake George	Silt/Sediment
Warren	Tribs to L.George, Village of L George	Silt/Sediment
Washington	Cossayuna Lake	Nutrients
Washington	Lake Champlain, South Bay	Nutrients
Washington	Tribs to L.George, East Shore	Silt/Sediment
Washington	Wood Cr/Champlain Canal and minor tribs	Nutrients
Wayne	Port Bay	Nutrients
Westchester	Amawalk Reservoir	Nutrients
Westchester	Blind Brook, Upper, and tribs	Silt/Sediment
Westchester	Cross River Reservoir	Nutrients
Westchester	Lake Katonah	Nutrients
Westchester	Lake Lincolndale	Nutrients
Westchester	Lake Meahagh	Nutrients
Westchester	Lake Mohegan	Nutrients
Westchester	Lake Shenorock	Nutrients
Westchester	Long Island Sound, Westchester (East)	Nutrients
Westchester	Mamaroneck River, Lower	Silt/Sediment
Westchester	Mamaroneck River, Upper, and minor tribs	Silt/Sediment
Westchester	Muscoot/Upper New Croton Reservoir	Nutrients
Westchester	New Croton Reservoir	Nutrients
Westchester	Peach Lake	Nutrients
Westchester	Reservoir No.1 (Lake Isle)	Nutrients
Westchester	Saw Mill River, Lower, and tribs	Nutrients
Westchester	Saw Mill River, Middle, and tribs	Nutrients
Westchester	Sheldrake River and tribs	Silt/Sediment
Westchester	Sheldrake River and tribs	Nutrients
Westchester	Silver Lake	Nutrients
Westchester	Teatown Lake	Nutrients
Westchester	Titicus Reservoir	Nutrients
Westchester	Truesdale Lake	Nutrients
Westchester	Wallace Pond	Nutrients
Wyoming	Java Lake	Nutrients
Wyoming	Silver Lake	Nutrients

APPENDIX F – List of NYS DEC Regional Offices

<u>Region</u>	<u>COVERING THE FOLLOWING COUNTIES:</u>	<u>DIVISION OF ENVIRONMENTAL PERMITS (DEP) PERMIT ADMINISTRATORS</u>	<u>DIVISION OF WATER (DOW) WATER (SPDES) PROGRAM</u>
1	NASSAU AND SUFFOLK	50 CIRCLE ROAD STONY BROOK, NY 11790 TEL. (631) 444-0365	50 CIRCLE ROAD STONY BROOK, NY 11790-3409 TEL. (631) 444-0405
2	BRONX, KINGS, NEW YORK, QUEENS AND RICHMOND	1 HUNTERS POINT PLAZA, 47-40 21ST ST. LONG ISLAND CITY, NY 11101-5407 TEL. (718) 482-4997	1 HUNTERS POINT PLAZA, 47-40 21ST ST. LONG ISLAND CITY, NY 11101-5407 TEL. (718) 482-4933
3	DUTCHESS, ORANGE, PUTNAM, ROCKLAND, SULLIVAN, ULSTER AND WESTCHESTER	21 SOUTH PUTT CORNERS ROAD NEW PALTZ, NY 12561-1696 TEL. (845) 256-3059	100 HILLSIDE AVENUE, SUITE 1W WHITE PLAINS, NY 10603 TEL. (914) 428 - 2505
4	ALBANY, COLUMBIA, DELAWARE, GREENE, MONTGOMERY, OTSEGO, RENSSELAER, SCHENECTADY AND SCHOHARIE	1150 NORTH WESTCOTT ROAD SCHENECTADY, NY 12306-2014 TEL. (518) 357-2069	1130 NORTH WESTCOTT ROAD SCHENECTADY, NY 12306-2014 TEL. (518) 357-2045
5	CLINTON, ESSEX, FRANKLIN, FULTON, HAMILTON, SARATOGA, WARREN AND WASHINGTON	1115 STATE ROUTE 86, Po Box 296 RAY BROOK, NY 12977-0296 TEL. (518) 897-1234	232 GOLF COURSE ROAD WARRENSBURG, NY 12885-1172 TEL. (518) 623-1200
6	HERKIMER, JEFFERSON, LEWIS, ONEIDA AND ST. LAWRENCE	STATE OFFICE BUILDING 317 WASHINGTON STREET WATERTOWN, NY 13601-3787 TEL. (315) 785-2245	STATE OFFICE BUILDING 207 GENESEE STREET UTICA, NY 13501-2885 TEL. (315) 793-2554
7	BROOME, CAYUGA, CHENANGO, CORTLAND, MADISON, ONONDAGA, OSWEGO, TIOGA AND TOMPKINS	615 ERIE BLVD. WEST SYRACUSE, NY 13204-2400 TEL. (315) 426-7438	615 ERIE BLVD. WEST SYRACUSE, NY 13204-2400 TEL. (315) 426-7500
8	CHEMUNG, GENESEE, LIVINGSTON, MONROE, ONTARIO, ORLEANS, SCHUYLER, SENECA, STEUBEN, WAYNE AND YATES	6274 EAST AVON-LIMA ROADAVON, NY 14414-9519 TEL. (585) 226-2466	6274 EAST AVON-LIMA RD. AVON, NY 14414-9519 TEL. (585) 226-2466
9	ALLEGANY, CATTARAUGUS, CHAUTAUQUA, ERIE, NIAGARA AND WYOMING	270 MICHIGAN AVENUE BUFFALO, NY 14203-2999 TEL. (716) 851-7165	270 MICHIGAN AVENUE BUFFALO, NY 14203-2999 TEL. (716) 851-7070

APPENDIX F

NEW YORK STATE HISTORIC PRESERVATION OFFICE
(SHPO) "NO EFFECT LETTER"



**Parks, Recreation,
and Historic Preservation**

ANDREW M. CUOMO
Governor

ERIK KULLESEID
Commissioner

September 13, 2019

Mr. Andrew Dangler
USACE Update Regulatory Field Office
1 Buffington Street
Building 10, 3rd Floor North
Watervliet, NY 12819

Re: USACE
Albany Port District Commission Industrial Park Project
City of Albany, Town of Bethlehem, Albany County, NY
18PR07273

Dear Mr. Dangler:

Thank you for requesting the comments of the New York State Historic Preservation Office (SHPO). We have reviewed the visual simulation and the August 6, 2019 McFarland Johnson letter noting that the proposed building height has changed and could reach 85 feet in accordance with Section 106 of the National Historic Preservation Act of 1966. These comments are those of the SHPO and relate only to Historic/Cultural resources.

The visual simulation of the proposed building shows that the roof will be visible from the National Register eligible Papscaenee Island Historic District. As noted in our November 2009 Determination of Eligibility for Papscaenee Island, "Papscaenee Island is historically and archaeologically significant for its association with the Upper Hudson Valley's predominate native people, the Mohican..." "The rich soil along the flats and on Papscaenee Island were flooded annually and generations of Mohicans cleared and cultivated these areas."

While some buildings have been introduced into the landscape, these buildings are not directly across from one of the few remaining cultivated areas on the Island. Since only the top of the building will be visible, the SHPO continues to recommend that this undertaking will have **No Adverse Effect** on historic properties with the **condition** that non-reflective, earth toned roofing materials are utilized. Maintaining a non-reflective roof will minimize any visual intrusions and help maintain the agricultural setting of the Papscaenee Island Historic District.

If you have any questions, I can be reached at (518) 268-2179.

Sincerely,

Nancy Herter
Archaeology Unit Program Coordinator



**Parks, Recreation,
and Historic Preservation**

KATHY HOCHUL
Governor

ERIK KULLESEID
Commissioner

December 9, 2021

Jordan Tate
Environmental Analyst
McFarland Johnson
60 Railroad Place
Suite 402
Saratoga Springs, NY 12866

Re: USACE
Marmen/Welcon Offshore Wind Tower Manufacturing Plant
Town of Bethlehem, Albany County, NY
21PR04693

Dear Jordan Tate:

Thank you for requesting the comments of the New York State Historic Preservation Office (SHPO). We have reviewed the provided documentation in accordance with Section 106 of the National Historic Preservation Act of 1966. These comments are those of the SHPO and relate only to Historic/Cultural resources.

SHPO has reviewed the proposed cut/fill plan and construction depths, and the visual simulation from the Papscaanee Island shoreline. We have no archaeological concerns with the proposed ground disturbing activities that will occur during this project. Based on the visual simulation, the SHPO concurs with the Stockbridge Munsee Community (SMC) THPO that the Marmen/Welcon Offshore Wind Tower Manufacturing Plant will have an adverse visual effect on the National Register eligible Papscaanee Island Historic District (08303.000130).

SHPO will provide additional comments once the Acoustic Noise Assessment has been completed to measure the proposed project's noise impacts at the Papscaanee Island Historic District and the SMC THPO's comments regarding noise impacts have been provided.

If you have any questions, I can be reached at Jessica.Schreyer@parks.ny.gov.

Sincerely,

Jessica Schreyer
Scientist Archaeology

Stockbridge-Munsee Tribal Historic Preservation

Arvid E. Miller Library Museum
N8510 Mohheconnuck Road
Bowler, WI 54416

Extension Office
86 Spring Street
Williamstown, MA 01267

March 3, 2022

Andrew Dangler
Biologist/Senior Project Manager
Upstate New York Section
DEPARTMENT OF THE ARMY
US Army Corps of Engineers, ATTN: CENAN-OP-RU
1 Buffington St., Bldg. 10, 3rd Fl. North
Watervliet, NY 12189
Via email only

**Re: Port of Albany Expansion Project, Town of Bethlehem, Albany Co., NY
SHPO #18PR07273 /21PR04693**

Dear Mr. Dangler:

I am writing regarding the aforementioned project as part of our continuing Government-to-Government Section 106 consultation.

In review of the project's designs and the additional visual and auidial assessments, Stockbridge-Munsee Community feels that its cultural resource concerns have now been satisfactorily addressed.

Our determination is that the Port of Albany project will have **No Adverse Effect** to Historic Properties. No further consultation is required unless the designs should change further.

If you have any questions, please feel free to contact our office.

Respectfully,



Bonney Hartley
Tribal Historic Preservation Manager
Stockbridge-Munsee Community

Cc: John Eddins, ACHP *Via email only*
Jessica Schreyer, NY SHPO *via email only*
David Witt, Charles Vandrei, NY DEC, *via email only*
Robert Leslie, Town of Bethlehem, *via email only*
Megan Daly, Port of Albany, *via email only*
Steve Boisfort, David Rosa, Jordan Tate- Mc Farland Johnson, *via email only*

(413) 884-6048

Email: thpo@mohican-nsn.gov



**Parks, Recreation,
and Historic Preservation**

KATHY HOCHUL
Governor

ERIK KULLESEID
Commissioner

March 25, 2022

Jordan Tate
Environmental Analyst
McFarland Johnson
60 Railroad Place
Suite 402
Saratoga Springs, NY 12866

Re: USACE
Marmen/Welcon Offshore Wind Tower Manufacturing Plant
Town of Bethlehem, Albany County, NY
21PR04693

Dear Jordan Tate:

Thank you for requesting the comments of the New York State Historic Preservation Office (SHPO). We have reviewed the provided documentation in accordance with Section 106 of the National Historic Preservation Act of 1966. These comments are those of the SHPO and relate only to Historic/Cultural resources.

SHPO has reviewed the Noise Assessment and updated Visual Simulations (provided via email, McFarland Johnson, Inc., 2/18/22) to evaluate the project's effects on the National Register eligible Papscaenee Island Historic District (08303.000130) and the Site Plan (McFarland Johnson, Inc., 3/18/22) showing the proposed 3.30-acre deed restricted area containing the vegetated area along the Hudson River shoreline. The vegetated area will provide a visual and acoustic buffer between the Papscaenee Island Historic District and the proposed manufacturing plant.

We note that the Stockbridge Munsee Community has issued their opinion (letter, dated 3/2/22) that this project will have No Adverse Effect on Historic Resources.

Based on this review, it is the opinion of the SHPO that no historic properties, including archaeological and/or historic resources, will be Adversely Affected by this undertaking with the condition that a Restrictive Deed Covenant is filed to protect and maintain the vegetated buffer along the Hudson River shoreline.

If you have any questions, I can be reached at Jessica.Schreyer@parks.ny.gov.

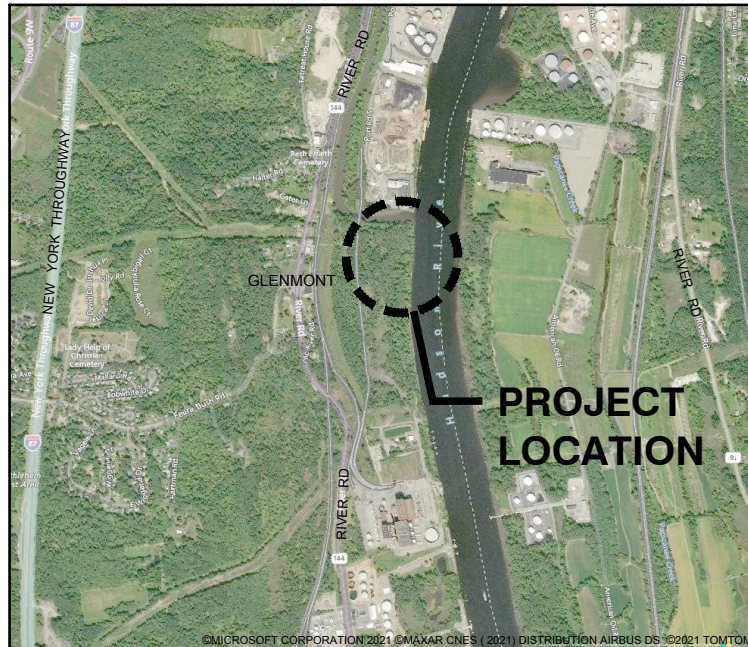
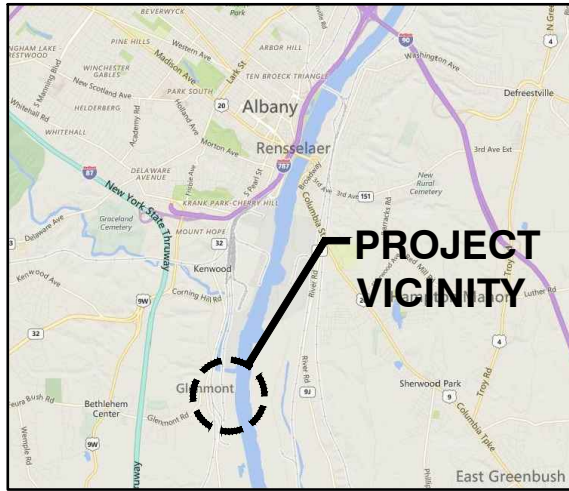
Sincerely,

Jessica Schreyer
Scientist Archaeology

APPENDIX G

DRAFT WHARF AND DREDGING E&SC PLANS

File: Q:\IN\10949-01\20 CADD\ Active\ Permits\1094901\IP-01 - Plotted: 10/12/2021 3:17 PM by: COKER, MAEVE ; Saved: 10/12/2021 2:59 PM by: MCCOKER



VICINITY AND LOCATION MAP

SCALE: N.T.S.

NOTES:

1. HORIZONTAL CONTROL REFERENCED TO NORTH AMERICAN DATUM OF 1983, STATE PLANE COORDINATE SYSTEM, NEW YORK, EAST ZONE, IN FEET.
2. WATER LEVEL DATUM IS BASED ON NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88), AS FOLLOWS:
 - MEAN HIGHER HIGH WATER LEVEL (MHHW) = +3.78 (NAVD88)
 - MEAN HIGH WATER LEVEL (MHW) = +3.40 (NAVD88)
 - MEAN TIDE LEVEL (MTL) = +0.91 (NAVD88)
 - MEAN LOW WATER LEVEL (MLW) = -1.59 (NAVD88)
 - MEAN LOWER LOW WATER LEVEL (MLLW) = -1.81 (NAVD88)

PURPOSE: WHARF CONSTRUCTION
 PERMIT SUBMITTAL-NOT TO BE USED
 FOR CONSTRUCTION
 DATUM: NAVD88



OWNER/APPLICANT:
 ALBANY PORT DISTRICT COMMISSION
 PORT OF ALBANY

IN: HUDSON RIVER
 NEAR: SOUTH OF ALBANY
 LOCATION: PORT OF ALBANY
 106 SMITH BOULEVARD
 ALBANY, NEW YORK 12202

WHARF DREDGING AND CONSTRUCTION

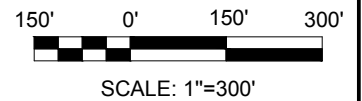
VICINITY AND LOCATION

SHEET 1 OF 5 DATE: (REV1) 2021-10-11

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PLAN - EXISTING CONDITIONS



PURPOSE: WHARF CONSTRUCTION
 PERMIT SUBMITTAL-NOT TO BE USED
 FOR CONSTRUCTION
 DATUM: NAVD88



OWNER/APPLICANT:
 ALBANY PORT DISTRICT COMMISSION
 PORT OF ALBANY

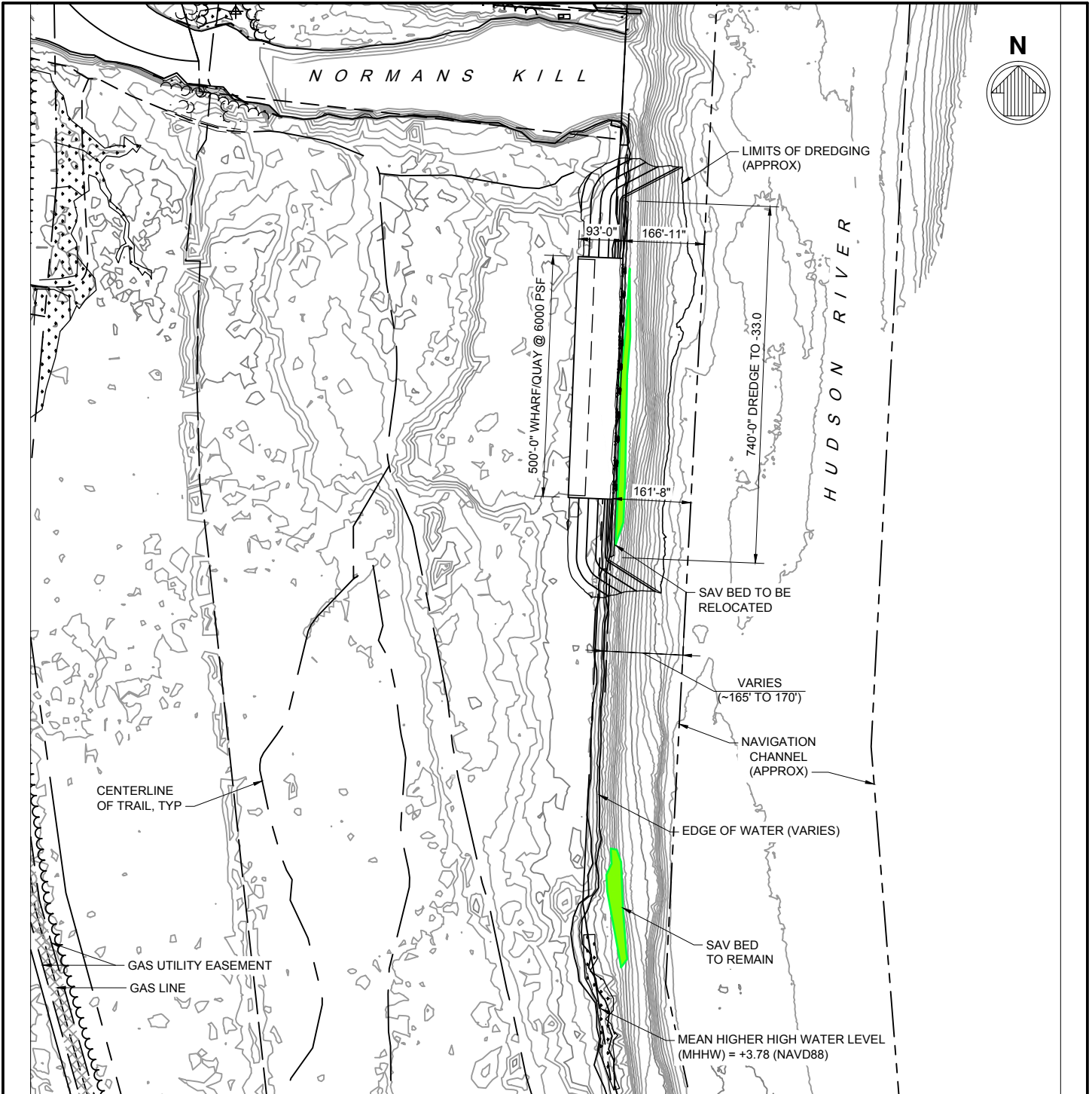
IN: HUDSON RIVER
 NEAR: SOUTH OF ALBANY
 LOCATION: PORT OF ALBANY
 106 SMITH BOULEVARD
 ALBANY, NEW YORK 12202

WHARF DREDGING AND CONSTRUCTION

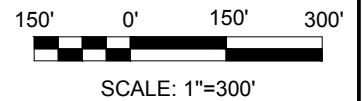
PLAN - EXISTING CONDITIONS

SHEET 2 OF 5 DATE: (REV1) 2021-10-11

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PLAN - PROPOSED CONDITIONS



PURPOSE: WHARF CONSTRUCTION
 PERMIT SUBMITTAL-NOT TO BE USED
 FOR CONSTRUCTION
 DATUM: NAVD88



OWNER/APPLICANT:
 ALBANY PORT DISTRICT COMMISSION
 PORT OF ALBANY

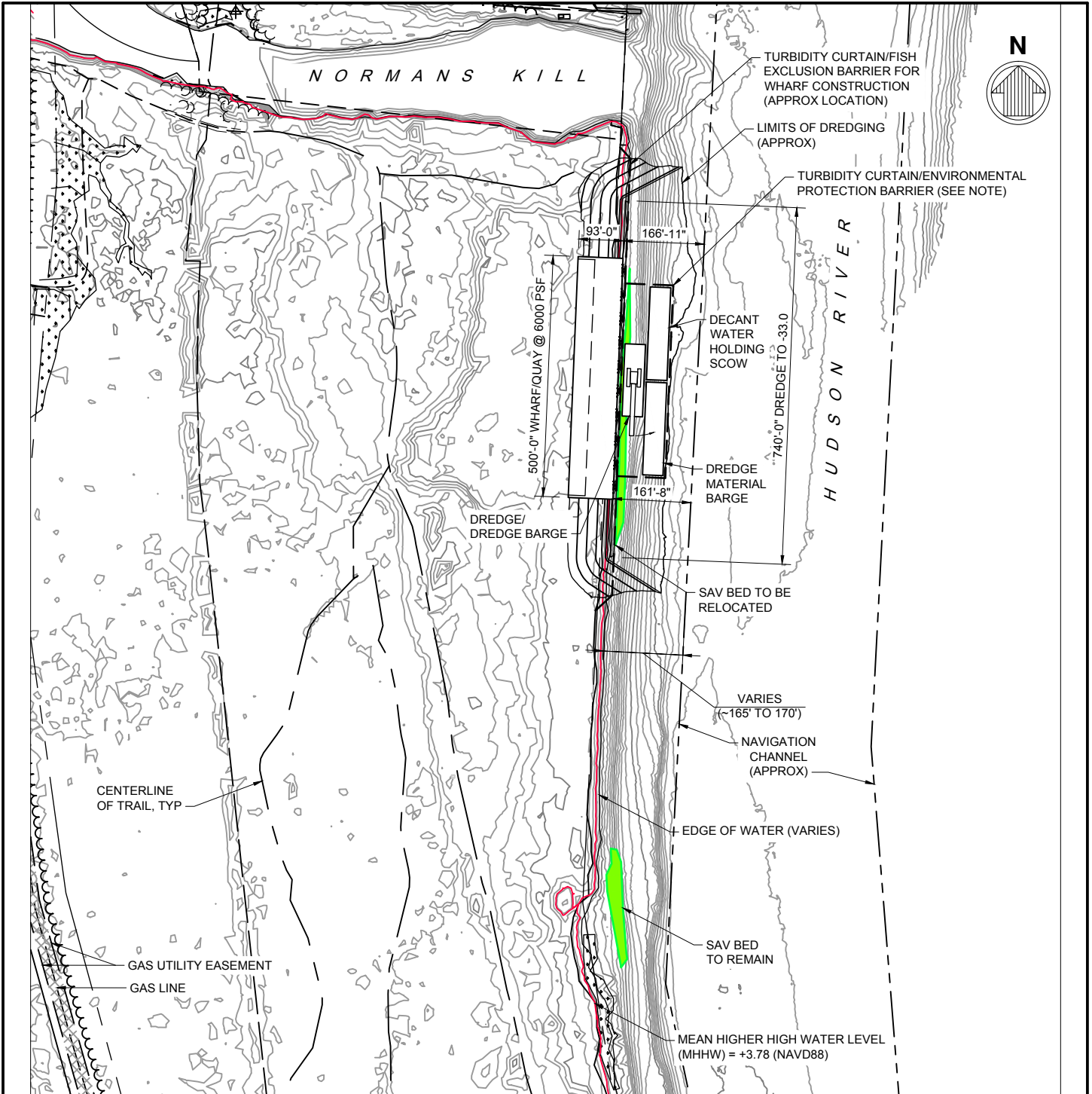
IN: HUDSON RIVER
 NEAR: SOUTH OF ALBANY
 LOCATION: PORT OF ALBANY
 106 SMITH BOULEVARD
 ALBANY, NEW YORK 12202

WHARF DREDGING AND CONSTRUCTION

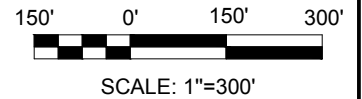
PLAN - PROPOSED CONDITIONS

SHEET 3 OF 5 DATE: (REV1) 2021-10-11

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PLAN - PROPOSED TEMPORARY ENVIRONMENTAL PROTECTION



NOTE: DREDGE EQUIPMENT AND ASSOCIATED TURBIDITY CURTAIN/ ENVIRONMENTAL PROTECTION BARRIER LOCATIONS VARY.

PURPOSE: WHARF CONSTRUCTION PERMIT SUBMITTAL-NOT TO BE USED FOR CONSTRUCTION
 DATUM: NAVD88



m & n engineering, p.c.

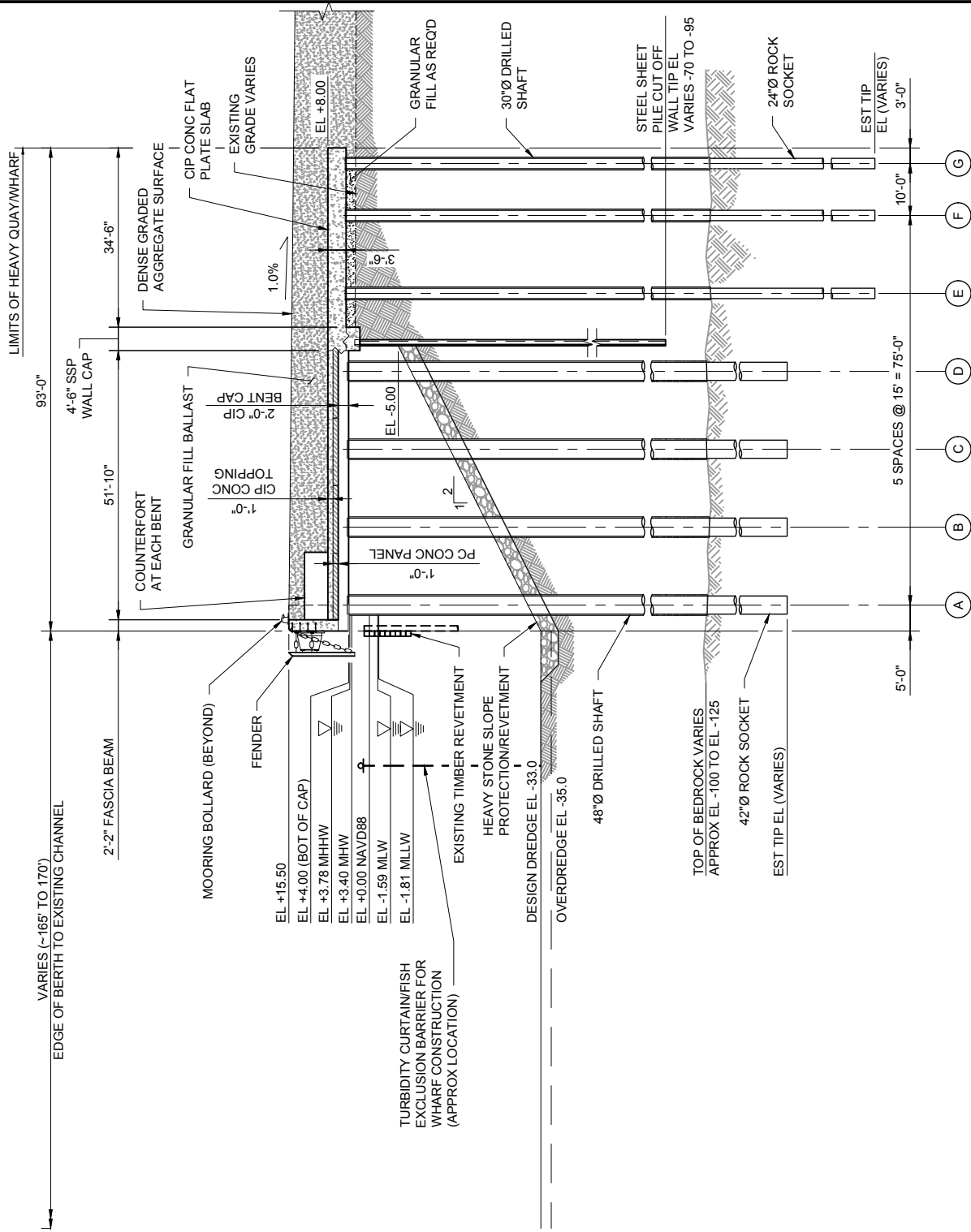
OWNER/APPLICANT:
 ALBANY PORT DISTRICT COMMISSION
 PORT OF ALBANY

IN: HUDSON RIVER
 NEAR: SOUTH OF ALBANY
 LOCATION: PORT OF ALBANY
 106 SMITH BOULEVARD
 ALBANY, NEW YORK 12202

WHARF DREDGING AND CONSTRUCTION

PLAN - PROPOSED TEMPORARY ENVIRONMENTAL PROTECTION

SHEET 4 OF 5 DATE: (REV1) 2021-10-11



SECTION - WHARF AND DREDGING

SCALE: N.T.S.

NOTE: WATER SURFACE AND DREDGE ELEVATIONS ARE REFERENCED TO NAVD88.

PURPOSE: WHARF CONSTRUCTION
 PERMIT SUBMITTAL-NOT TO BE USED
 FOR CONSTRUCTION
 DATUM: NAVD88



OWNER/APPLICANT:
 ALBANY PORT DISTRICT COMMISSION
 PORT OF ALBANY

IN: HUDSON RIVER
 NEAR: SOUTH OF ALBANY
 LOCATION: PORT OF ALBANY
 106 SMITH BOULEVARD
 ALBANY, NEW YORK 12202

WHARF DREDGING AND CONSTRUCTION

SECTION - WHARF AND DREDGING

SHEET 5 OF 5 DATE: (REV1) 2021-10-11

APPENDIX H

SOIL MANAGEMENT PLAN



ATLANTIC TESTING LABORATORIES

WBE certified company

Albany
22 Corporate Drive
Clifton Park, NY 12065
518-383-9144 (T)
atlantictesting.com

October 23, 2020

McFarland Johnson, Inc.
60 Railroad Place, Suite 402
Saratoga Springs, New York 12866

Attn: David Rosa

Re: Soil Management Plan
Port of Albany Expansion Project
Beacon Island Parcel
Bethlehem, Albany County, New York
MJ Project No. 18641.02
ATL Report No. AT5596CE-05-10-20

Ladies/Gentlemen:

Enclosed is a copy of the **Soil Management Plan** prepared for the referenced site. This report was completed in accordance with the standard form of agreement between McFarland Johnson, Inc., and Atlantic Testing Laboratories, Limited.

Please contact our office should you have any questions, or if we may be of further assistance.

Sincerely,
ATLANTIC TESTING LABORATORIES, Limited

Cheyenne J. Dashnaw, P.E.
Senior Engineer

CJD/cjd

Enclosures

cc: Georgie Nugent, McFarland Johnson, Inc.

SOIL MANAGEMENT PLAN

**PORT OF ALBANY EXPANSION PROJECT
BEACON ISLAND PARCEL
BETHLEHEM, ALBANY COUNTY, NEW YORK**



WBE certified company

PREPARED BY:

**ATLANTIC TESTING LABORATORIES, LIMITED
22 Corporate Drive
Clifton Park, New York 12065**

PREPARED FOR:

**McFarland Johnson, Inc.
60 Railroad Place, Suite 402
Saratoga Springs, New York 12866
*MJ Project No. 18641.02***

**Albany Port District Commission
106 Smith Boulevard
Albany, New York 12202**

ATL REPORT NO. AT5596CE-05-10-20

October 23, 2020

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1.0 INTRODUCTION

1.1 Purpose

Atlantic Testing Laboratories, Limited (ATL) was retained by McFarland Johnson, Inc., on behalf of the Albany Port District Commission, to prepare a Soil Management Plan that can be used to address areas at the Beacon Island parcel that are impacted with ash material and related debris. The purpose of this Soil Management Plan is to summarize procedures to implement for planned excavation activities, installation of a soil cover system in areas of ash material or other potential impacted fill, and management of waste soil and/or groundwater. This Soil Management Plan also addresses protocol for monitoring and sampling and analysis during excavation and site work, and recommendations for installation of vapor barrier systems beneath proposed buildings.

1.2 Site Description

The project site is the Beacon Island parcel located to the east of River Road (County Route 144) and along the west side of the Hudson River, in the Town of Bethlehem, Albany County, New York. The Beacon Island parcel is comprised of approximately 80 acres, and is the site of a planned expansion for the Port of Albany. A Site Location Map, showing the approximate location of the subject site, is included in Appendix A.

Information provided to ATL by McFarland Johnson, Inc., indicates that planned redevelopment for the site includes land clearing, excavation and backfill operations, dredging sediment for the area along the Hudson River, and construction of facilities to be associated with the Port of Albany.

1.3 Plan Contents and Organization

This Soil Management Plan includes an introductory section (Section 1), a summary of information obtained from prior investigations (Section 2), pertinent coordination items when work is scheduled for impacted areas (Section 4) and a description of procedures that may be warranted for various site work activities (Section 3), a description of procedures to be implemented during specific site work activities (Sections 5 through 12), and a description of reports and records that should be maintained for work completed at the subject site (Section 13). Appendices are included to provide supplemental information that is considered pertinent to the items described in the Soil Management Plan and are referenced where applicable.

This Soil Management Plan is organized in a manner to allow for site representatives to review and identify applicable measures to be implemented for different areas of work and types of work activities being performed. Section 1.4 describes different areas of work and the associated work activities that may be applicable. A Soil Management Plan Flow Chart, contained in Appendix B, is provided to outline tasks to be implemented for management of existing on-site soil and soil that may be imported for use as fill.

1.4 Applicability

1.4.1 Areas to be Developed with Buildings/Structures

Areas to be developed with buildings or other structures will require appropriate soil management procedures, in association with the excavation, backfill, and grading for the

installation of foundation systems, and with the construction of slabs-on-grade for buildings. Following is a summary of the soil management procedures to be implemented, with reference to applicable sections of this Soil Management Plan.

- Excavation for foundations in areas of known/suspect impacts from ash: Refer to **Section 5** and **Item A** of Soil Management Plan Flow Chart (Appendix B)
- Excavation for foundations in areas without known/suspect impacts from ash: Refer to **Section 6** and **Item B** of Soil Management Plan Flow Chart (Appendix B)
- Backfill in areas of construction: Refer to **Section 11** and **Items E and F** of Soil Management Plan Flow Chart (Appendix B)
- Construction of slabs-on-grade for buildings: Refer to **Section 9** and **Item E** of Soil Management Plan Flow Chart (Appendix B)

1.4.2 Areas to be Developed with Asphalt/Concrete Surfaces

Areas to be developed with asphalt or concrete surfaces (e.g., driveways, parking lots, walking paths) will require appropriate soil management procedures, in association with the excavation, backfill, and grading prior to installation of the asphalt or concrete surface cover. Following is a summary of the soil management procedures to be implemented, with reference to applicable sections of this Soil Management Plan.

- Excavation and site preparation in areas of known/suspect impacts from ash: Refer to **Section 5** and **Item A** of Soil Management Plan Flow Chart (Appendix B)
- Excavation and site preparation in areas without known/suspect impacts from ash: Refer to **Section 6** and **Item B** of Soil Management Plan Flow Chart (Appendix B)
- Backfill in areas of construction: Refer to **Section 11** and **Items E and F** of Soil Management Plan Flow Chart (Appendix B)

1.4.3 Areas to be Developed with Lawn/Landscaping

Areas to be redeveloped with lawn or landscaping will require appropriate soil management procedures, in association with the excavation, backfill, grading, and soil cover system installation. Following is a summary of the soil management procedures to be implemented, with reference to applicable sections of this Soil Management Plan.

- Excavation and site preparation in areas of known/suspect impacts from ash: Refer to **Section 5** and **Item A** of Soil Management Plan Flow Chart (Appendix B)
- Excavation and site preparation in areas without known/suspect impacts from ash: Refer to **Section 6** and **Item B** of Soil Management Plan Flow Chart (Appendix B)
- Backfill and soil cover system in areas of lawns and landscaping: Refer to **Sections 8 and 11** and **Items E and F** of Soil Management Plan Flow Chart (Appendix B)

1.4.4 Areas to Remain Wooded

Areas of the subject site that are currently wooded and are planned to remain wooded will not require implementation of specific soil management procedures at this time. In the event that these areas are scheduled for redevelopment in the future, or if there are any ground intrusive activities performed, appropriate soil management procedures should then be provided.

1.4.5 Areas to be Dredged

Management of areas where sediment is planned for dredging is described in general for this Soil Management Plan; however, additional planning and coordination with the New York State Department of Environmental Conservation (NYSDEC), United States Army Corps of Engineers (USACE), and other applicable regulatory agencies will be necessary prior to performing the dredging operations and the handling and reuse or disposal of dredged sediments. Refer to **Section 10** and **Item D** of the Soil Management Plan Flow Chart (Appendix B).

2.0 BACKGROUND INFORMATION AND AREAS OF CONCERN

2.1 Summary of Previous Investigations

ATL performed sediment sampling at the subject site in June 2019 and August 2020, and a subsurface investigation and soil sampling in September 2020. Additionally, ATL was provided with a draft Phase II Environmental Site Assessment report prepared by Bergmann Associates for the Port of Albany and dated April 6, 2017.

The sediment sampling conducted by ATL in June 2019 included the advancement of 5 cores, and the sediment sampling conducted by ATL in August 2020 included the advancement of 10 cores. The cores were advanced in the areas scheduled for dredging as part of planned redevelopment for the site. Sediment samples were collected from the core locations and submitted for subsequent laboratory analysis. Laboratory analysis parameters for the June 2019 sampling event were selected to include compounds described in NYSDEC Technical and Operational Guidance Series (TOGS) 5.1.9, whereas the samples collected in August 2020 were analyzed for parameters to evaluate potential reuse options in addition to the NYSDEC TOGS 5.1.9 parameters. A complete summary of findings for the previously completed sediment sampling and analysis are provided in ATL Report No. CD4644CE-01-07-19, dated July 15, 2019, ATL Report No. CD4644CE-01-07-19 Addendum 1, dated August 2, 2019, and ATL Report No. AT5596CE-03-09-20 dated September 24, 2020.

The subsurface investigation and soil sampling conducted by ATL in September 2020 included the advancement of 45 probes. The probes were advanced in accessible areas throughout the site, to assess the presence or absence of ash material. Additionally, soil samples were collected from locations without ash material to evaluate potential reuse options for consideration during site redevelopment. The subsurface investigation identified multiple locations where ash material is present, but did not identify obvious visual or olfactive evidence of petroleum or chemical-related contamination. Soil samples were collected from areas without ash material, including 22 samples for analysis of volatile organic compounds (VOC), and 11 samples for analysis of semi-VOC, polychlorinated biphenyls (PCB), pesticides, metals, and cyanide. With a few exceptions, laboratory analysis results for the soil samples collected from areas without ash material were below 6 NYCRR Part 360 fill material pre-determined beneficial use criteria and below NYSDEC Unrestricted Use Soil Cleanup Objectives (SCO) listed in 6 NYCRR Part 375 and/or NYSDEC CP-51 document. A general summary of the findings for the subsurface investigation previously completed by ATL is provided as Table C-1 in Appendix C. A complete summary of findings is provided in ATL Report No. AT5596CE-04-10-20, dated October 22, 2020.

The Phase II ESA conducted by Bergmann Associates in February 2017 included the advancement of 12 test pits and 8 borings, and the installation of temporary monitor wells at 3 of the boring locations. Information in the draft Phase II ESA report indicates that coal ash was observed throughout the depths for 3 of the test pits and a fourth test pit exhibited the presence of railroad ties covered in a black tar-like substance at depths of 8 to 12 feet below ground surface. Of the 8 borings advanced during this investigation, 7 exhibited evidence of coal ash. A surface soil sample was collected from the initial 2 inches for each boring. Subsurface soil samples were also collected from the borings at varying depths. There were 3 temporary monitor wells installed for collection of groundwater samples. The soil and groundwater samples were laboratory analyzed for VOC, semi-VOC, cyanide, pesticides, PCB, and target compound list (TCL) metals. With the exception of metals, target compounds for the referenced analytical parameters were non-detect for each of the soil and groundwater samples. A general summary of the findings for the subsurface investigation previously completed by Bergmann Associates is provided as Tables C-2 and C-3 in Appendix C. The report prepared by Bergmann Associates and dated April 6, 2017, should be referenced for additional details pertaining to the findings of the subsurface investigation.

2.2 Known Locations of Impacted Soil

Data and information from the previous subsurface investigation activities indicates that ash material is present at the site in a widespread condition. The ash material has been predominantly observed on the west side of the subject site. No obvious visual or olfactive evidence of petroleum or chemical-related contamination was observed at the locations investigated.

The Aerial Overview of Affected Locations, contained in Appendix D, shows approximate locations for the borings, test pits, and probes previously advanced at the subject site, along with an indication of which exhibited the presence of ash material. The referenced drawing also shows an approximate delineation of areas where ash material is expected to be present, areas where ash material is not expected, and areas that are considered to potentially contain ash material. The areas shown on the drawing are based on existing available data and not intended to represent an exact delineation for the locations of ash material.

3.0 COORDINATION OF WORK

3.1 Roles and Responsibilities

The soil management procedures described herein should be coordinated and conducted by firms and individuals who are familiar with the conditions of the Soil Management Plan, have an understanding of the known or suspected conditions in different areas of the subject site, and have related experience and capabilities to implement the applicable work activities. While the Owner of the property has responsibility for the implementation of the Soil Management Plan, it is anticipated that performance of work activities associated with the Soil Management Plan would be coordinated and completed by design professionals, contractors, and environmental consultants who are retained by the Owner. The following table provides a summary of the primary roles and responsibilities for implementation of the Soil Management Plan.

Role	Responsibilities
Owner	<ul style="list-style-type: none"> • Retain and coordinate with Design Professionals, Contractors, and Environmental Consultants for performance of site work pursuant to conditions of the Soil Management Plan • Maintain site records and documentation for work completed pursuant to Soil Management Plan
Design Professionals	<ul style="list-style-type: none"> • Incorporate applicable provisions of the Soil Management Plan into design plans and specifications for planned site redevelopment • Coordinate with Owner, Contractors, and Environmental Consultants during design and construction phases to confirm work is completed as planned
Contractors	<ul style="list-style-type: none"> • Correspond with NYSDEC (and other regulatory agencies, as applicable) for notifications of work activities • Perform site work activities, including, but not limited to, excavation, grading, placement and compaction of backfill, dust control, groundwater management, soil cover system installation, vapor barrier system installation, construction, and waste transport and disposal
Environmental Consultants	<ul style="list-style-type: none"> • Provide guidance and assistance with implementation of the Soil Management Plan • Correspond with NYSDEC (and other regulatory agencies, as applicable) to discuss clarifications or modifications to conditions of the Soil Management Plan • Conduct monitoring and soil screening during performance of work activities that affect impacted or contaminated soil • Conduct air monitoring during ground intrusive activities that affect impacted or contaminated soil • Perform soil sampling and laboratory analysis for waste materials, fill materials, and excavation areas

3.2 Project Notifications

Within 14 days, and no less than 3 days, prior to commencing work activities that may affect areas of the subject site that are impacted with ash, the NYSDEC should be notified of the planned work. This notification should be performed by the Owner and/or Contractor performing the site work. The Design Professional and Environmental Consultant should also be similarly notified.

3.3 Spill Reporting/Administration

The subject site is known to have areas impacted with ash and related debris. Other types of contamination (i.e., petroleum, chemical) have not been encountered at locations of past investigations. The NYSDEC must be notified in the event that petroleum- or chemical-related contaminated soil is discovered on the project site. This notification will need to be provided directly to the NYSDEC Spill Hotline (telephone number 1-800-457-7362).

4.0 GENERAL SITE WORK AND SOIL MANAGEMENT PLAN CONDITIONS

4.1 Health and Safety

In addition to construction site health and safety, site personnel should be aware of the contaminants of concern associated with the ash material (metals) and utilize appropriate control methods, personal protective clothing, and personal protective equipment during the handling and management of impacted materials. Contractors working at the subject site should perform work pursuant to a health and safety plan that is specific to their scope of work and associated hazards or potential hazards.

4.2 Groundwater Removal and Management (If Applicable)

In the event that there is significant groundwater inflow in a zone of contaminated soil, a vacuum truck should be provided to remove the infiltrated groundwater as the excavation progresses or at the completion of excavation activities. Alternatively, groundwater can be pumped into a frac tank(s) or other appropriate receptacles and temporarily stored on-site prior to on-site treatment and discharge or transfer and disposal off-site.

4.3 Dust Control and Air Monitoring

Fugitive dust and vapors should be minimized or mitigated during the excavation and handling of contaminated soil, if encountered. In the event that particulates and/or vapors represent a potential concern for the work area and/or surrounding areas, particulates and/or vapors should be monitored during ground intrusive activities associated with contaminated soil by setting up real-time instrumentation at locations upwind and downwind of the project area. Assessment for airborne dust would be performed using particulate monitors capable of measuring particulate matter less than 10 microns (PM10). Assessment for vapors (applicable to areas where petroleum- or chemical-related contamination is encountered) would be performed using a photoionization detector (PID) to screen the ambient air for the measurable presence of VOC.

If air monitoring for particulates is conducted, an action level of 0.15 milligrams per cubic meter (mg/m^3) should be used for PM10 concentrations associated with the project work area. If screening is performed for ambient airborne VOC concentrations, an action level of 5 parts per million (ppm) should be used for the project work area. These action levels are consistent with the NYSDEC DER-10 "Technical Guidance for Site Investigation and Remediation" and the New York State Department of Health (NYSDOH) "Generic Community Air Monitoring Plan."

In the event that the PM10 action level is exceeded for the work site (downwind monitoring station), the upwind background level should be immediately confirmed and it should be determined whether the work site (downwind) level exceeds the upwind background by greater than $0.1 \text{ mg}/\text{m}^3$. For any such exceedance, work activities should temporarily cease and dust suppression techniques should be implemented. Dust suppression techniques may include some or all of the following (as cited from Appendix 1B of the NYSDEC DER-10):

- Applying water on haul roads
- Wetting equipment and excavation faces
- Spraying water on buckets during excavation and dumping
- Hauling materials in properly tarped or watertight containers

- Restricting vehicle speeds to 10 mph
- Covering excavated areas and material after excavation activity ceases
- Reducing the excavation size and/or number of excavations

In the event that the VOC action level is exceeded for the work site (downwind monitoring station), the upwind background level should be immediately confirmed and it should be determined whether the work site (downwind) level exceeds the upwind background by greater than 5 ppm. For any such exceedance, work activities should temporarily cease while monitoring continues. If the concentrations readily decrease below 5 ppm over background, work activities can resume. If the concentrations do not readily decrease and a definitive source can not be eliminated, the work site and on-site work activities would require further evaluation to determine an appropriate course of action.

4.4 Personnel and Equipment Decontamination

Equipment that is in contact with contaminated soil should be decontaminated, as necessary to prevent cross-contamination to other areas. Equipment and tools can be decontaminated by initially scrubbing the bulk material from the item, cleaning with a phosphate-free detergent and tap water wash, rinsing with tap water, and rinsing with distilled water. In order to contain decontamination liquids, a decontamination pad, of sufficient size to accommodate the affected portions of equipment, can be constructed using double layers of polyethylene sheeting as a base and a suitable material (i.e., lumber, clean soil, hay bales) for a perimeter berm. A more durable setup would be necessary if larger, heavier items need to be decontaminated. The polyethylene sheeting should be wrapped around the perimeter berm. Wastewater generated from decontamination activities shall be disposed of pursuant to applicable local, state and federal requirements.

5.0 EXCAVATION IN AREAS IMPACTED WITH ASH AND DEBRIS

5.1 Soil Removal and Stockpile

Soil that is impacted with ash and requires excavation for planned site redevelopment activities will need to be transported off-site for disposal. In consideration of the ash materials being widespread at various locations of the subject site, and the soil cover system that will be implemented as described in other sections of this Soil Management Plan, the areal extent of excavation for ash and debris wastes will be only as necessary to complete the scheduled site redevelopment. It is intended that the depths of removal be similarly limited to scheduled depths of excavations; however, if existing available information suggests that waste ash/debris exists at only a limited distance below scheduled depths of excavations, removal of the additional material should be conducted to limit the amount of material that would remain below permanent structures or site features to be constructed.

Excavated soil should be field examined for the visual and/or olfactive indicators of the presence of ash and debris materials or the potential presence of petroleum- or chemical-related impacts. In the event that petroleum- or chemical-related impacts are identified, procedures described in Section 7 should be implemented.

Excavated soil should be segregated between soil that is impacted with ash and overburden soil that does not exhibit visual evidence of these wastes. The impacted soil should be stockpiled or directly loaded for subsequent transport and disposal. The

overburden soil can be processed for reuse on-site, provided applicable conditions are satisfied (reference Section 11).

For impacted soil that is stockpiled on-site, the selected location(s) should be an area not susceptible to flooding or inundation of water during precipitation events, readily accessible to equipment that will be utilized for loading and hauling the material, and located away from stormwater or site drainage components. Any contaminated soil stockpile would need to be placed on and covered with 6-mil polyethylene sheeting or other comparable impervious material that can be readily removed and disposed of. The following items should be applicable to stockpiles for contaminated soil materials.

- Polyethylene sheeting or other impervious membrane used for the base of the soil stockpile should be placed with sheets overlapping a minimum of 1 foot.
- The base of the soil stockpile should be bermed at the perimeter to contain the soil stockpile and potential runoff during precipitation events. The berm materials, which can be comprised of mounds of clean soil material, hay bales, lumber, or other readily available suitable materials, should be placed along the perimeter and wrapped with the polyethylene sheeting or other impervious membrane that is used for the base of the soil stockpile. To minimize extraneous handling of materials and the size of the completed soil stockpile area, the berm perimeter can initially be constructed along 2 sides, and the remaining 2 sides can be constructed after all soil material is placed in the stockpile or temporarily bermed at the end of each workday.
- The height and slopes of the soil stockpile should be limited such that slope stability is not compromised during storage or the loading process.
- The soil stockpile should be covered with the polyethylene sheeting upon placement of all impacted soil material or at the end of each workday. Seams should be overlapped a minimum of 1 foot. The stockpile cover should be sufficiently weighted to contain the stored soil and resist damage from wind. Materials used to weigh down and stabilize the stockpile cover should consist of readily available materials that will not tend to damage the cover upon placement (e.g., clean soil material, sand bags, tires).
- Any temporary on-site soil stockpiles should be periodically inspected to ensure that material continues to be contained and is not released to the surrounding environment. The temporary on-site soil stockpiles will need to be properly protected and maintained until removal and off-site disposal. Polyethylene sheeting should be repaired or replaced as needed.
- Water from precipitation events that ponds on the surface of the stockpile cover should be removed upon discovery. The ponded water can be discharged on-site provided there is no contact with the petroleum-contaminated soil, and provided such activities are compliant with any stormwater discharge permits that may be applicable for the site or active construction work. Water that contacts the petroleum-impacted soil shall be properly containerized and managed as impacted waste water.
- Stockpiles with impacted soil should not remain on-site in excess of 60 days.

5.2 Excavation Monitoring and Soil Sampling

A representative of the Environmental Consultant should be on-site during excavation activities in the known or suspect areas of ash materials, to examine exposed soil for the presence of ash. The on-site representative should assist with determinations for the segregation of soil material that is considered relatively clean overburden to be reused

and soil material that would be classified as contaminated for off-site disposal. The on-site representative would also be available to provide guidance relative to the management of the contaminated subsurface materials.

Since it is planned to manage ash materials in-place for various locations at the subject site, soil samples are not proposed for excavation area(s) where waste ash/debris is removed, unless other potential contaminants of concern are encountered or suspected. If soil samples are to be collected from these excavation areas, the Environmental Consultant should coordinate with the NYSDEC to confirm analytical parameters, sampling locations, and quantity of samples.

5.3 Soil Reuse or Disposal

Overburden soil scheduled for reuse should be managed pursuant to procedures described in Section 11. Waste soil materials scheduled for disposal should be managed pursuant to procedures described in Section 12.

6.0 EXCAVATION IN NON-IMPACTED AREAS

6.1 Soil Removal and Stockpile

Soil that is excavated from areas without known or suspect impacts from ash can be removed and handled pursuant to routine construction and site work methods. Contractors performing the excavation work should be cognizant of the potential for impacted soil and should visually monitor the soil as removed to determine if it may be potentially affected. If ash material is identified, the excavation and soil management procedures should transition to the methods described in Section 5. In the event that petroleum- or chemical-related impacts are identified, procedures described in Section 7 should be implemented.

6.2 Excavation Monitoring

As indicated in Section 6.1, a representative of the Contractor should examine exposed soil for visual and/or olfactive indicators of potential contamination. If suspect impacted materials are encountered, a representative of the Environmental Consultant should be on-site for further assessment and monitoring in the affected area.

Unless suspect contamination is encountered, soil samples are not proposed for the excavations. If soil samples are to be collected from these excavation areas, the Environmental Consultant should coordinate with the NYSDEC to confirm analytical parameters, sampling locations, and quantity of samples.

6.3 Soil Reuse or Disposal

The excavated soil that is scheduled for reuse should be managed pursuant to procedures described in Section 11. In the event that the soil materials need to be disposed of, transport and disposal should be performed pursuant to procedures described in Section 12.

7.0 EXCAVATION IN AREAS OF PETROLEUM/CHEMICAL SPILLS

7.1 Soil Removal and Stockpile

If petroleum- or chemical-related contamination is encountered during site work, a spill will need to be reported (reference Section 3.3) and contaminated soil will need to be removed for disposal. The areal extent and depths of excavation for material affected by a spill should be inclusive of the entirety of the contaminated material, if feasible and practical. If the affected materials cannot be completely removed, an alternate approach to site remediation should be coordinated through the NYSDEC.

Excavated soil should be field examined for the visual and/or olfactive indicators of the petroleum- or chemical-related impacts, and field screened for the measurable presence of VOC with a photoionization detector (PID), equipped with the 10.6 eV lamp. In general, soil exhibiting obvious visual or olfactive evidence of contamination and/or greater than 10 ppm via ambient PID screening should be removed from the excavation, and processed for subsequent disposal. Overburden soil that does not exhibit these characteristics should be stockpiled on-site for subsequent sampling and evaluation of reuse options.

For petroleum-contaminated soil that is stockpiled on-site, the selected location(s) should be an area not susceptible to flooding or inundation of water during precipitation events, readily accessible to equipment that will be utilized for loading and hauling the material, and located away from stormwater or site drainage components. Any contaminated soil stockpile would need to be placed on and covered with 6-mil polyethylene sheeting or other comparable impervious material that can be readily removed and disposed of. The following items should be applicable to stockpiles for contaminated soil materials.

- Polyethylene sheeting or other impervious membrane used for the base of the soil stockpile should be placed with sheets overlapping a minimum of 1 foot.
- The base of the soil stockpile should be bermed at the perimeter to contain the soil stockpile and potential runoff during precipitation events. The berm materials, which can be comprised of mounds of clean soil material, hay bales, lumber, or other readily available suitable materials, should be placed along the perimeter and wrapped with the polyethylene sheeting or other impervious membrane that is used for the base of the soil stockpile. To minimize extraneous handling of materials and the size of the completed soil stockpile area, the berm perimeter can initially be constructed along 2 sides, and the remaining 2 sides can be constructed after all soil material is placed in the stockpile or temporarily bermed at the end of each workday.
- The height and slopes of the soil stockpile should be limited such that slope stability is not compromised during storage or the loading process.
- The soil stockpile should be covered with the polyethylene sheeting upon placement of all impacted soil material or at the end of each workday. Seams should be overlapped a minimum of 1 foot. The stockpile cover should be sufficiently weighted to contain the stored soil and resist damage from wind. Materials used to weigh down and stabilize the stockpile cover should consist of readily available materials that will not tend to damage the cover upon placement (e.g., clean soil material, sand bags, tires).
- Any temporary on-site soil stockpiles should be periodically inspected to ensure that material continues to be contained and is not released to the surrounding environment. The temporary on-site soil stockpiles will need to be properly

protected and maintained until removal and off-site disposal. Polyethylene sheeting should be repaired or replaced as needed.

- Water from precipitation events that ponds on the surface of the stockpile cover should be removed upon discovery. The ponded water can be discharged on-site provided there is no contact with the petroleum-contaminated soil, and provided such activities are compliant with any stormwater discharge permits that may be applicable for the site or active construction work. Water that contacts the petroleum-impacted soil shall be properly containerized and managed as impacted waste water.
- Stockpiles with impacted soil should not remain on-site in excess of 60 days.

7.2 Excavation Monitoring and Sampling

A representative of the Environmental Consultant should be on-site during excavation activities in the areas affected by a petroleum- or chemical-related spill, to examine exposed soil for visual and/or olfactive indicators of petroleum- or chemical-related impacts. Additionally, field screening for the measurable presence of VOC should be performed at the time of the excavation activities, using a portable PID, equipped with a 10.6 eV lamp.

The on-site representative should assist with determinations for the segregation of soil material that is considered relatively clean overburden to be reused and soil material that would be classified as contaminated for off-site disposal. The on-site representative would also be available to provide guidance relative to the management of the contaminated subsurface materials.

Post-excavation soil samples should be collected from the walls and floor of the excavation area(s) where petroleum- or chemical-contaminated soil is removed. The quantities of soil samples to be collected from these excavation areas should be selected pursuant to the following criteria:

- For excavations with a perimeter of less than 20 feet, 1 bottom and 1 sidewall sample should be collected.
- For excavations with a perimeter between 20 and 300 feet, samples from sidewalls should be collected at a frequency of 1 per 30 linear feet and samples from the bottom should be collected at a frequency of 1 per 900 square feet.
- For excavations with a perimeter of greater than 300 linear feet, the quantity of samples to be collected should be coordinated through the NYSDEC, or selected pursuant to the same criteria specified for an excavation perimeter between 20 and 300 feet.

The post-excavation soil samples should be laboratory analyzed for VOC, in accordance with EPA Method 8260; and semi-VOC, in accordance with EPA Method 8270 (base/neutral extractables).

7.3 Soil Reuse or Disposal

Overburden soil scheduled for reuse should be managed pursuant to procedures described in Section 11. Waste soil materials scheduled for disposal should be managed pursuant to procedures described in Section 12.

8.0 SOIL COVER SYSTEM INSTALLATION

A soil cover should be installed in areas of the site that are impacted with ash material and will be utilized as lawn or landscaped areas. The following criteria should be applicable to the soil cover system.

- The upper 6 inches of the soil cover should be suitable to sustain growth of appropriate vegetation at the ground surface.
- A minimum of 1 foot of soil cover should be placed above the ash material.
- The upper 1 foot of the soil cover should not have concentrations of contaminants that exceed the Restricted Residential Soil Cleanup Objectives (SCO) set forth in 6 NYCRR Part 375-6.
- Fill that is placed at a depth below the upper 1 foot of soil cover should not have concentrations of contaminants that exceed the Commercial SCO set forth in 6 NYCRR Part 375-6.
- A demarcation layer should be provided between the soil cover layer and underlying impacted soil, unless approval is obtained from the NYSDEC to forego installation of a demarcation layer.
- In the event that the soil cover system is breached, penetrated, or temporarily removed, restoration to original conditions (or equivalent) should be performed.
- Areas with a soil cover should be inspected at least annually, to assess existing conditions and determine if any restoration or repairs are necessary. Inspections should also be performed after severe weather events or significant site operations that may have adversely affected the soil cover system.

9.0 VAPOR BARRIER SYSTEM INSTALLATION

A vapor barrier system could be considered as an option for buildings that are constructed at the subject site, especially for buildings that would be occupied on a routine basis. While risks with vapor migration from contaminants associated with ash material is relatively low, installation of a vapor barrier system is generally an inexpensive addition to the construction of a new building. A vapor barrier system could consist of a gas permeable layer (i.e., crushed stone) and a soil gas retarder membrane (i.e., polyethylene or polyolefin sheeting) between the gas permeable layer and concrete slab. Soil gas collector pipes could also be installed in the gas permeable layer, and established as a passive system, active system, or passive with capability to be transitioned to an active system. If the Owner opts for installation of a vapor barrier system for buildings, the vapor barrier system should be incorporated into design plans and specifications for the specific building(s) being constructed.

10.0 DREDGING OF SEDIMENT

10.1 Sediment Removal and Management

Dredging of sediment would need to be conducted pursuant to conditions of applicable permits, as determined through the joint application for permits process with state agencies and the USACE. A dredging plan should also be developed to identify the dredging methods and management options. Direct coordination with the NYSDEC and reference to NYSDEC TOGS 5.1.9 would be necessary to ensure that necessary criteria for the dredging operations are addressed.

10.2 Sediment Reuse or Disposal

6 NYCRR Part 360.12(c)(1)(iv) describes conditions for pre-determined beneficial use of navigational dredged material; however, laboratory analysis data for previously collected samples at the site are not indicative of the sediment material meeting the requisite criteria. For navigational dredged material that does not meet the pre-determined beneficial use criteria, a petition for a case-specific beneficial use determination (BUD) could be considered.

Laboratory analysis results from previously collected sediment samples have identified elevated concentrations for metals and PCB, and as such, dredged sediment (or affected portions thereof) should be disposed of at a permitted solid waste management facility. If reuse is desired for portions that may exhibit lesser contaminant concentrations, a plan would need to be developed for segregation and sampling and analysis, along with submitting the petition for a case-specific BUD.

11.0 BACKFILL AND SOIL REUSE

11.1 Suitable On-Site Soil

Laboratory analysis results for samples previously collected from locations on the subject site not impacted with ash indicate that concentrations of contaminants generally do not exceed the 6 NYCRR Part 375 Commercial SCO and the 6 NYCRR Part 360 fill material pre-determined beneficial use criteria. This material should be suitable for on-site reuse below the upper 1 foot of soil cover. Additional sampling and analysis may be needed for areas not previously investigated and for previously sampled areas where exceedances were identified relative to the 6 NYCRR Part 375 Commercial SCO and/or the 6 NYCRR Part 360 fill material pre-determined beneficial use criteria. If additional sampling and analysis is performed, the quantity of samples and analytical parameters should be selected pursuant to the Sampling and Analysis Schedule for Fill in Appendix E.

11.2 Imported Fill

Fill material may need to be imported to the site, for use as the upper 1 foot of soil cover system or for other areas specific types of fill material. Imported fill material should be sampled and analyzed prior to delivery to the site, to confirm the material satisfies criteria established for use as a soil cover (reference Section 8) or criteria for use as general fill, restricted use fill, or limited use fill per 6 NYCRR Part 360.13. The quantity of samples and analytical parameters for imported fill should be selected pursuant to the Sampling and Analysis Schedule for Fill in Appendix E.

12.0 WASTE TRANSPORT AND DISPOSAL

The Contractor should provide for loading and transporting contaminated soil to a permitted solid waste management facility. Transport of waste materials will require use of trucks with applicable permits pursuant to 6 NYCRR Part 364 criteria. The disposal of waste soil materials should be documented via waste manifests and/or copies of waste disposal receipts.

Waste characterization soil samples should be collected and laboratory analyzed from the impacted material, pursuant to requirements of the selected disposal facility. The selected disposal facility should be contacted prior to excavation work to identify applicable

laboratory analysis parameters and quantity of samples, and to process waste profile documentation.

13.0 REPORTING AND RECORDKEEPING

Reports and records of site work should be maintained, as needed to document site conditions and soil management procedures that are completed. Reports and records to be maintained in association with this Soil Management Plan include, but may not be limited to, the following:

- As-built plans
- Waste manifests and/or disposal receipts for ash, soil, and groundwater
- Air monitoring data
- Excavation monitoring data
- Soil sampling and laboratory analysis data
- Site observation reports

APPENDIX A
Site Location Map



Site Location Map

Drawn by:
TSP

Scale:
Not to scale

Project No.:
AT5596

Date:
May 2020

**Beacon Island Parcel
Bethlehem, Albany County, New York**

ATLANTIC TESTING LABORATORIES, Limited

Albany, NY
Poughkeepsie,

Binghamton, NY
Syracuse, NY

Canton, NY
Rochester, NY

Elmira, NY
Utica, NY

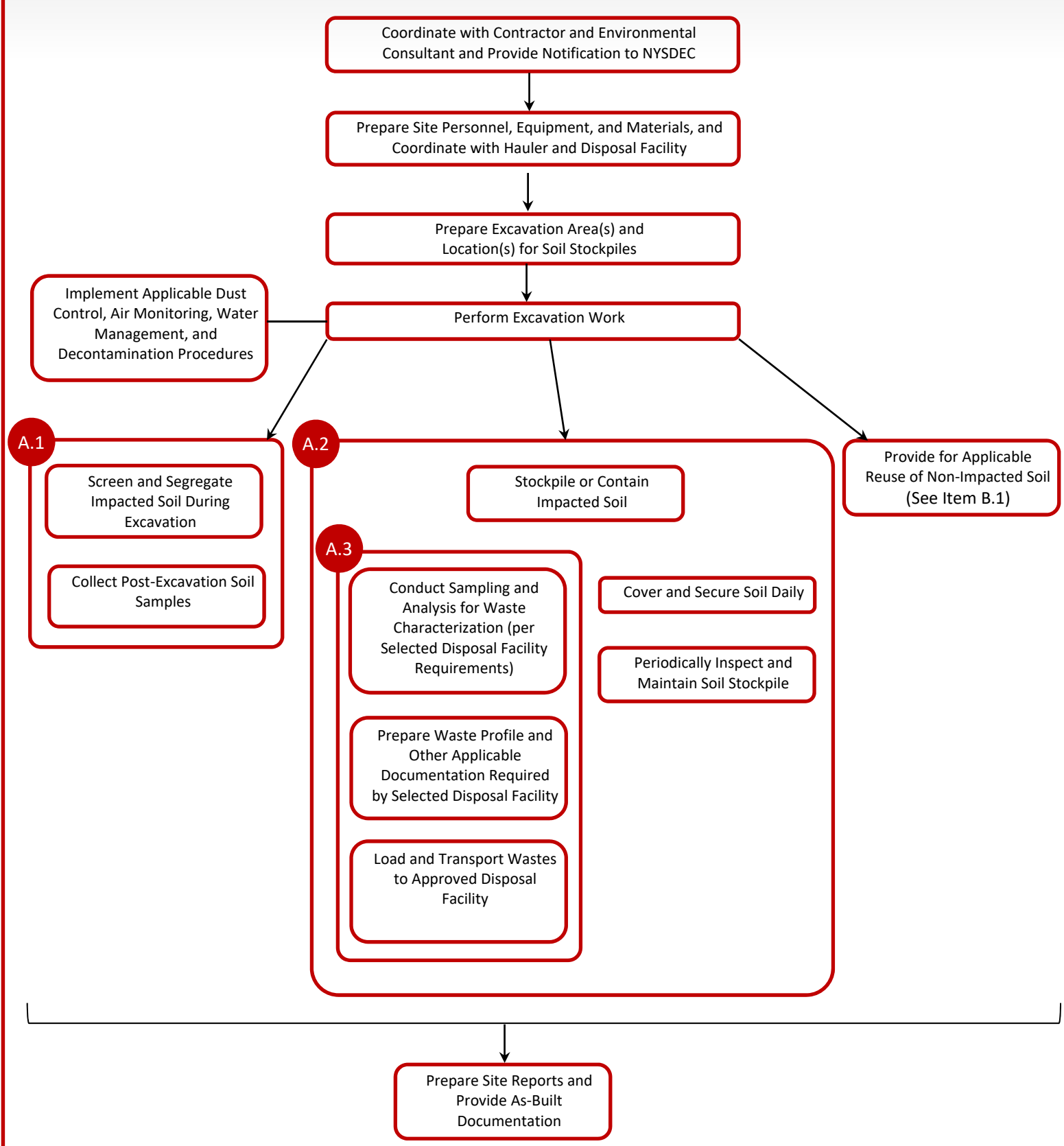
Plattsburgh, NY
Watertown, NY

APPENDIX B

Soil Management Plan Flow Chart

A

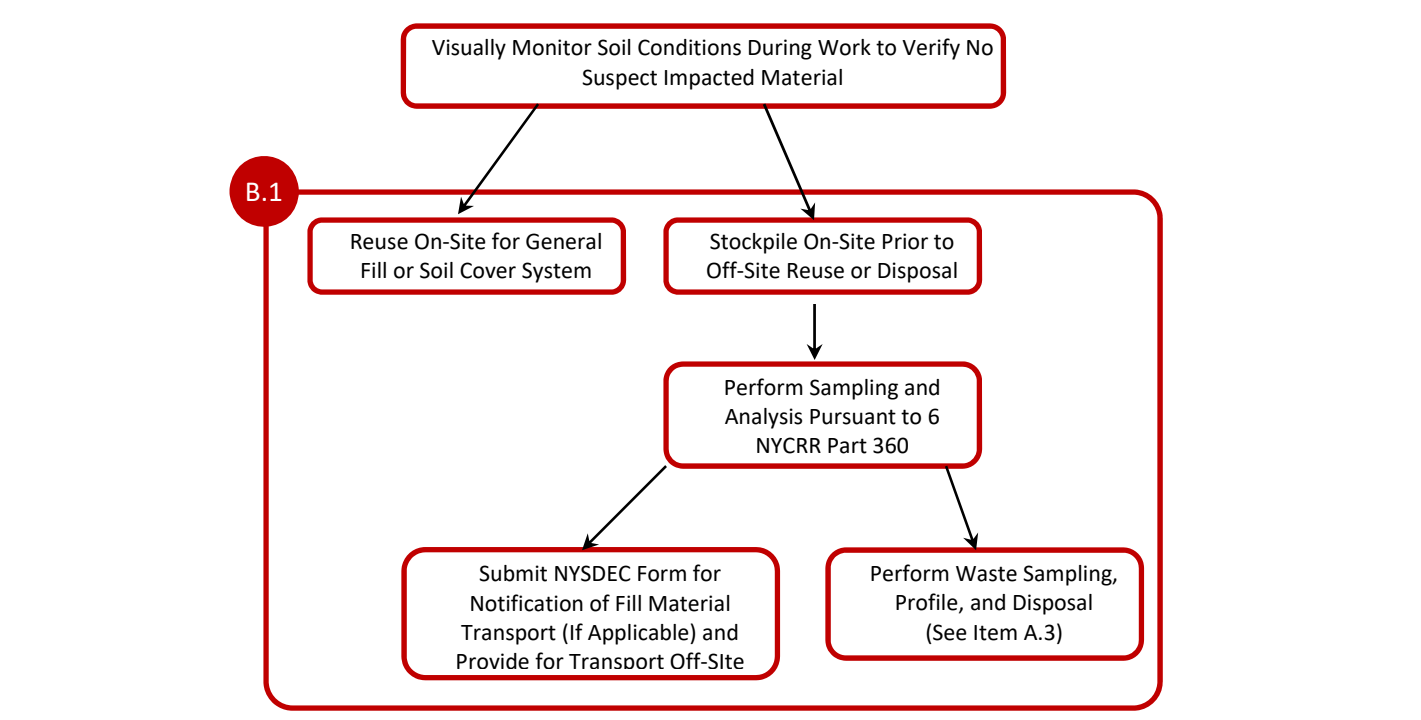
Soil Excavation/Ground Disturbance Activities – Areas of Known/Suspect Impacts from Ash/Debris



- 1. If petroleum/chemical spill or contamination is encountered, implement soil management procedures described in Item C.
- 2. Reference Items D and E for procedures pertaining to site backfill/soil cover system and assessment for imported fill.

B

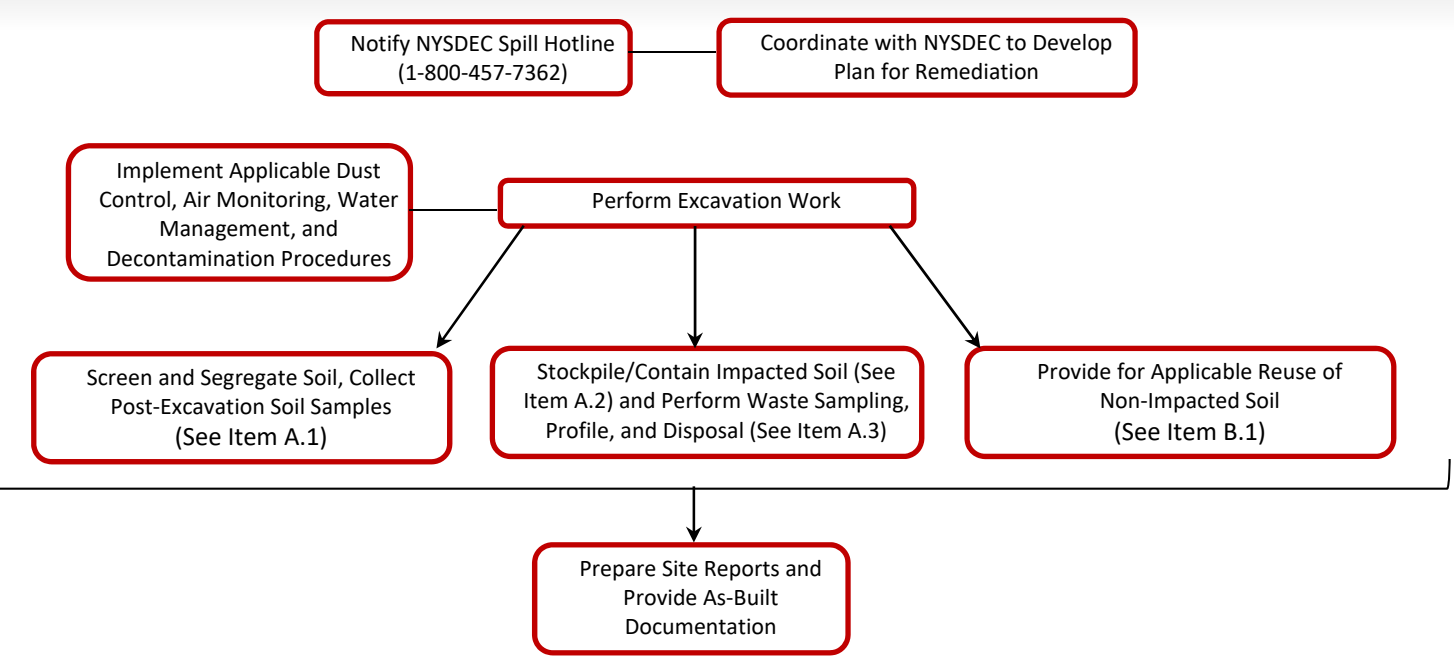
Soil Excavation/Ground Disturbance Activities – Areas without Known/Suspect Impacts from Ash/Debris



- 1. If ash/debris material is encountered, implement soil management procedures described in Item A.
- 2. If petroleum/chemical spill or contamination is encountered, implement soil management procedures described in Item C.
- 3. Reference Items D and E for procedures pertaining to site backfill/soil cover system and assessment for imported fill.

C

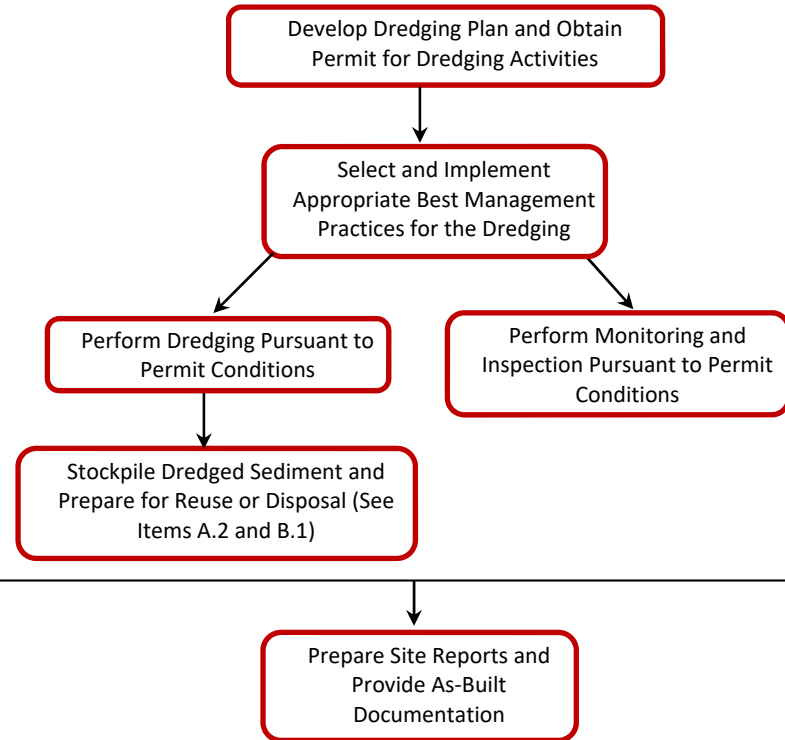
Soil Excavation/Ground Disturbance Activities – Petroleum/Chemical Spill or Contamination Encountered



Prepare Site Reports and Provide As-Built Documentation

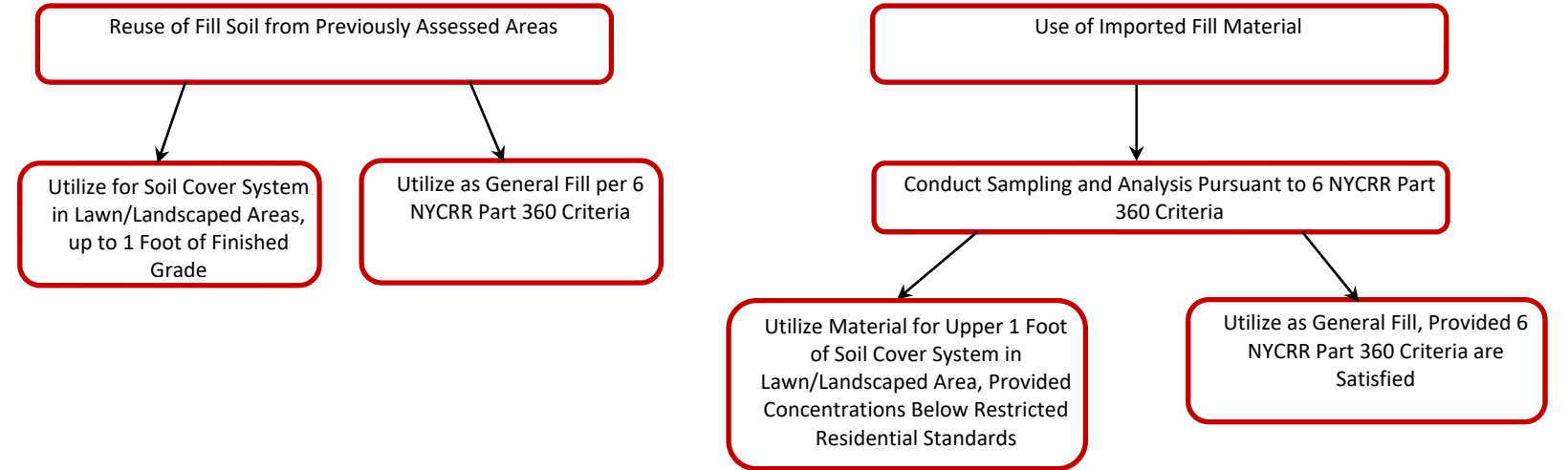
D

Sediment Dredging



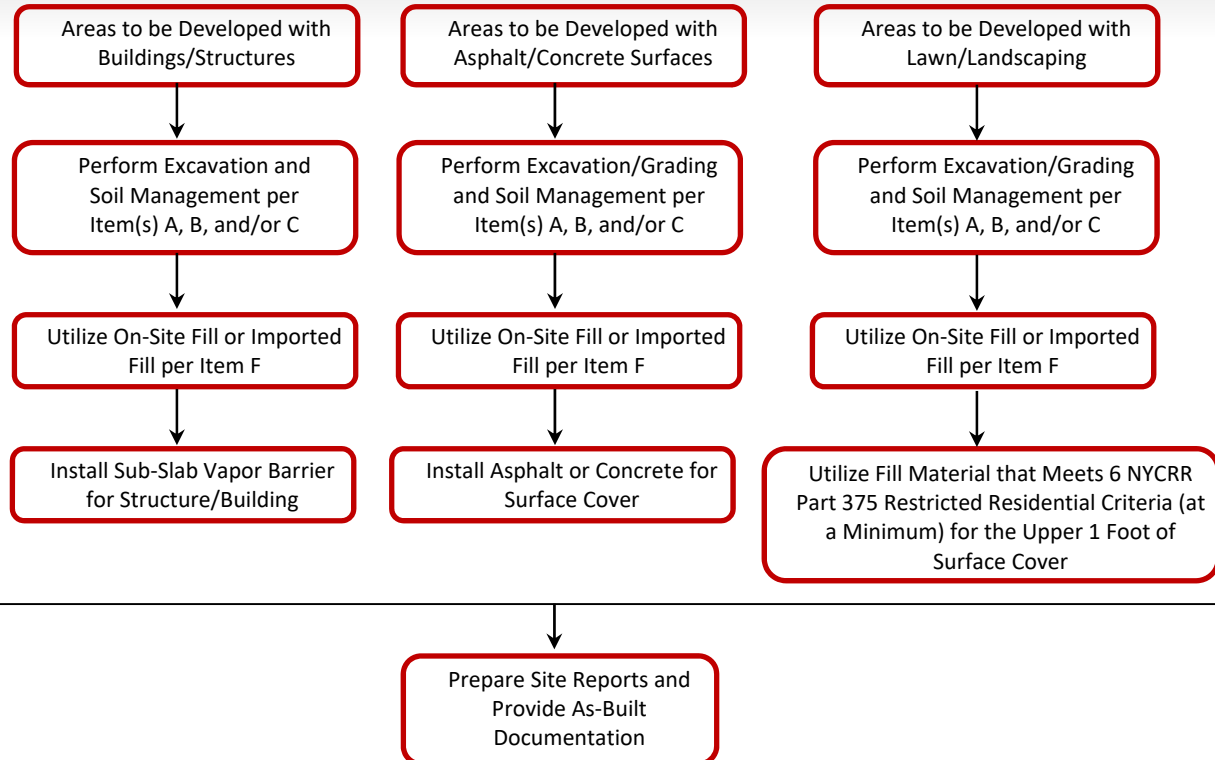
F

Reuse of Previously Assessed On-Site Fill and Assessment and Use of Imported Fill



E

Installation of Soil Cover System/ Ground Surface Cover Conditions



APPENDIX C

Summary of Data from Previous Investigations

Table C-1
Summary of Information from September 2020 Investigation – Probes
(Information Available from Environmental Subsurface Investigation and Soil Sampling Report prepared by ATL and dated October 22, 2020)

Probe ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Samples Collected for Analysis of VOC	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO	Samples Collected for Analysis of Semi-VOC, PCB, Metals, Pesticides, and Cyanide	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO
B-1	20'	Coal Ash @ 0.5 – 2'	ND				
B-2	20'	Coal Ash @ 0' – 20'	ND				
B-3	20'	Coal Ash @ 0' – 20'	ND				
B-4	20'	Coal Ash @ 0' – 18'	ND				
B-5	20'		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-6 and B-8)	Iron
B-6	20'		ND	Soil @ 10' – 15'		Soil @ 0' – 20' (Composite with B-5 and B-8)	See B-5
B-7	20'	Coal Ash @ 0' – 11'	ND				
B-8	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-5 and B-6)	See B-5
B-9	20'	Coal Ash @ 0.5' – 2.5'	ND – 18.2				
B-10	20'		ND			Soil @ 0' – 20' (Composite with B-11 and B-12)	4,4'-DDD, Arsenic, Iron, Vanadium
B-11	20'	Coal Ash @ 8' – 11.5'	ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-10 and B-12)	See B-10

Table C-1 (continued)
Summary of Information from September 2020 Investigation – Probes
(Information Available from Environmental Subsurface Investigation and Soil Sampling Report prepared by ATL and dated October 22, 2020)

Probe ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Samples Collected for Analysis of VOC	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO	Samples Collected for Analysis of Semi-VOC, PCB, Metals, Pesticides, and Cyanide	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO
B-12	20'		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-10 and B-11)	See B-10
B-13	20'		ND	Soil @ 10' – 15'	Acetone	Soil @ 0' – 20' (Composite with B-15 and B-16)	Iron, Vanadium
B-14	20'		ND				
B-15	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-13 and B-16)	See B-13
B-16	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-13 and B-15)	See B-13
B-17	20'		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-18 and B-19)	Iron, Vanadium
B-18	20'		ND	Soil @ 10' – 15'		Soil @ 0' – 20' (Composite with B-17 and B-19)	See B-17
B-19	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-17 and B-18)	See B-17
B-20	20'	Coal Ash @ 0' – 2'	ND				
B-21	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-22 and B-23)	Iron
B-22	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-21 and B-23)	See B-21
B-23	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-21 and B-22)	See B-21
B-24	20'		ND			Soil @ 0' – 20' (Composite with B-25)	Aluminum, Iron
B-25	20'		ND			Soil @ 0' – 20' (Composite with B-24)	See B-24
B-26	5.1' (Refusal)		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-27)	Iron
B-27	20'		ND			Soil @ 0' – 20' (Composite with B-26)	See B-26
B-28	20'		ND	Soil @ 10' – 15'		Soil @ 0' – 20' (Composite with B-29)	Iron

Table C-1 (continued)
Summary of Information from September 2020 Investigation – Probes
(Information Available from Environmental Subsurface Investigation and Soil Sampling Report prepared by ATL and dated October 22, 2020)

Probe ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Samples Collected for Analysis of VOC	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO	Samples Collected for Analysis of Semi-VOC, PCB, Metals, Pesticides, and Cyanide	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO
B-29	20'		ND			Soil @ 0' – 20' (Composite with B-28)	See B-28
B-30	10' (Refusal)		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-31)	Iron
B-31	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-30)	See B-30
B-32	20'		ND				
B-33	20'		ND				
B-34	20'		ND				
B-35	20'	Coal Ash @ 0' – 12.5'	ND				
B-36	20'	Coal Ash @ 0.5' – 6'	ND				
B-37	20'	Coal Ash @ 0.5' – 7.5'	ND				
B-38	20'	Coal Ash @ 0' – 11.5'	ND				
B-39	20'	Coal Ash @ 0' – 15'	ND				
B-40	20'	Coal Ash @ 0.5' – 20'	ND				
B-41	20'		ND	Soil @ 5' – 10'		Soil @ 0' – 20' (Composite with B-43)	4,4'-DDE, 4,4'-DDD, Aluminum, Calcium, Iron
B-42	20'	Coal Ash @ 0' – 8'	ND				
B-43	20'		ND	Soil @ 15' – 20'		Soil @ 0' – 20' (Composite with B-41)	See B-41

Table C-1 (continued)
Summary of Information from September 2020 Investigation – Probes
(Information Available from Environmental Subsurface Investigation and Soil Sampling Report prepared by ATL and dated October 22, 2020)

Probe ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Samples Collected for Analysis of VOC	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO	Samples Collected for Analysis of Semi-VOC, PCB, Metals, Pesticides, and Cyanide	Compounds Exceeding 6 NYCRR Part 375 Unrestricted Use SCO
B-44	20'		ND	Soil @ 0' – 5'		Soil @ 0' – 20' (Composite with B-45)	Iron
B-45	20'		ND	Soil @ 10' – 15'	Acetone	Soil @ 0' – 20' (Composite with B-44)	See B-44
** Approximate locations of probes are shown on the <i>Aerial Overview of Affected Locations</i> plan in Appendix D.							

Table C-2

Summary of Information from February 2017 Investigation – Borings/Monitor Wells

(Information Available from Draft Phase II Environmental Site Assessment Report prepared by Bergmann Associates and dated April 6, 2017)

Boring/ Monitor Well ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)	Groundwater Observations	Samples Collected for Metals Analysis	Metals Exceeding 6 NYCRR Part 375 Unrestricted Use Soil Cleanup Objectives
B-1	100' (environmental assessment to 12')	Coal Ash @ 0' – 12'	0.0	Water @ 12.9'	0" – 2" (Soil)	Arsenic, Barium, Nickel
					10' – 12' (Soil)	Arsenic, Barium
B-2	50' (environmental assessment to 10')	Coal Ash @ 0' – 10'	0.0 – 2.9	Water @ 6'	0" – 2" (Soil)	Arsenic, Barium, Silver
					4' – 6' (Soil)	Arsenic, Barium, Chromium, Selenium, Silver
B-3/ MW- 1	150' (environmental assessment to 16')	Coal Ash @ 0' – 6'	0.0 – 13.7	Water @ 14.9'	0" – 2" (Soil)	Nickel
					2' – 4' (Soil)	Silver
					Groundwater (Screened @ 12' – 22')	Iron, Manganese
B-4/ MW- 3	100' (environmental assessment to 12')	Coal Ash @ 0' – 12'	0.0 – 0.9		0" – 2" (Soil)	Arsenic, Barium, Mercury
					2' – 4' (Soil)	Arsenic, Barium, Mercury
					Groundwater (Screened @ 5' – 15')	Iron, Sodium
B-5/ MW- 2	50' (environmental assessment to 14')		2.9 – 22.9		0" – 2" (Soil)	Arsenic, Barium, Silver
					4' – 6' (Soil)	Arsenic, Selenium, Silver
					Groundwater (Screened @ 11' – 21')	Iron, Manganese
B-6	50' (environmental assessment to 14')	Coal Ash @ 0' – 14'	0.0 – 0.2	Water @ 7.8'	0" – 2" (Soil)	Arsenic, Barium, Chromium, Nickel, Silver
					4' – 6' (Soil)	Arsenic, Barium, Nickel
B-7	50' (environmental assessment to 20')	Coal Ash @ 0' – 18'	0.1 – 0.2	Water @ 2.5'	0" – 2" (Soil)	Arsenic, Barium, Nickel, Silver
					1' – 4' (Soil)	Arsenic, Barium, Chromium, Mercury, Nickel
B-8	50' (environmental assessment to 18')	Coal Ash @ 6' – 18'	0.1 – 0.6		0" – 2" (Soil)	
					6' – 8' (Soil)	

** Approximate locations of borings are shown on the *Aerial Overview of Affected Locations* plan in Appendix D.

Table C-3

Summary of Information from February 2017 Investigation – Test Pits

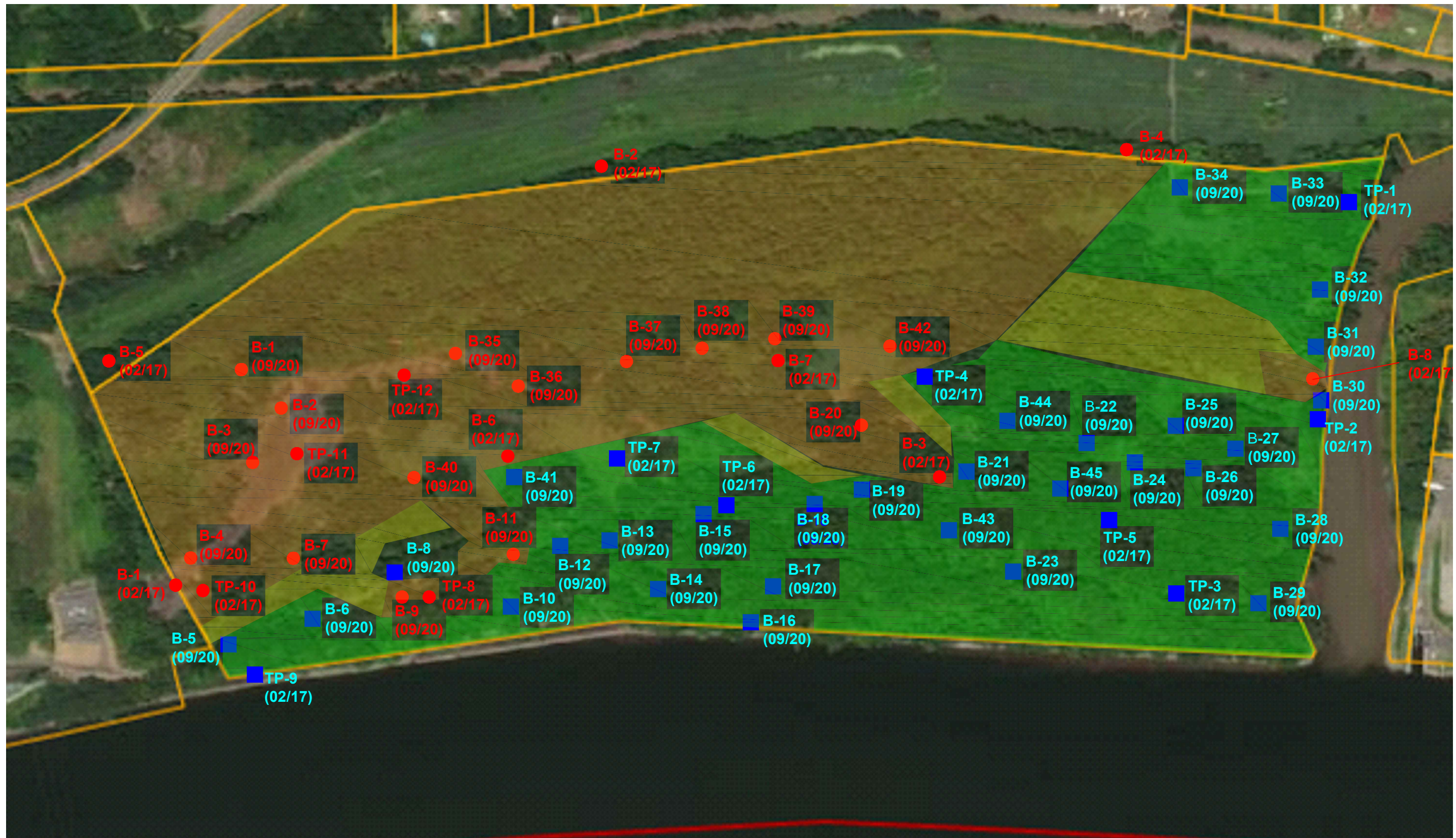
(Information Available from Draft Phase II Environmental Site Assessment Report prepared by Bergmann Associates and dated April 6, 2017)

Test Pit ID**	Depth Advanced	Coal Ash/Debris Observations	VOC Field Screening (ppm)
TP-1	12'		0.0 – 0.1
TP-2	12'		0.0 – 0.1
TP-3	12'		0.0 – 0.2
TP-4	12'		0.1 – 0.2
TP-5	12'		0.0 – 0.1
TP-6	12'		0.0
TP-7	12'		0.0
TP-8	12'	Railroad ties covered in black tar-like substance @ 8' – 12'	0.0 – 10.1
TP-9	10'		0.0
TP-10	12'	Coal Ash @ 0' – 12'	0.1
TP-11	12'	Coal Ash @ 0' – 12'	0.0 – 0.1
TP-12	12'	Coal Ash @ 0' – 12'	0.1



** Approximate locations of test pits are shown on the *Aerial Overview of Affected Locations* plan in Appendix D.



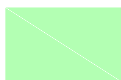
APPENDIX D


Aerial Overview of Affected Locations



LEGEND :

-  **B-5**
 (02/17) Approximate Location of Previous Boring or Test Pit with or Debris Ash Material Present (and Month/Year of Investigation)
-  **TP-4**
 (02/17) Approximate Location of Previous Boring or Test Pit without Ash Material Present (and Month/Year of Investigation)

-  Approximate Extents of Area Expected to have Ash Material Present
-  Approximate Extents of Area with Potential to have Ash Material Present
-  Approximate Extents of Area Not Expected to have Ash Material Present

AERIAL OVERVIEW OF AFFECTED LOCATIONS	Drawn By: CJD	Drawing: 1 of 1	Scale: As Noted	Project No.: AT5596	Date : October 2020
	Beacon Island Parcel Bethlehem, Albany County, New York		 ATLANTIC TESTING LABORATORIES, Limited Albany, NY Binghamton, NY Canton, NY Elmira, NY Poughkeepsie, NY Plattsburgh, NY Rochester, NY Syracuse, NY Utica, NY Watertown, NY <small>WBE Certified Company www.AtlanticTesting.com</small>		

APPENDIX E

Sampling and Analysis Schedule for Fill

Sampling Criteria for Fill Material per 6 NYCRR Part 360.13(e)

Soil Quantity (cubic yards)	Number of Discrete Samples	Number of Composite Samples ¹
	Volatile Organic Compounds (VOC)	Semi-VOC, Inorganics, Polychlorinated Biphenyls (PCB), and Pesticides
0 – 300	2	1
300 – 1,000	4	2
1,000 – 10,000	6	3
>10,000	2 for every additional 10,000 cubic yards	1 for every additional 10,000 cubic yards
Notes: ¹ Each composite sample will be comprised of 3 to 5 discrete samples from different locations within the fill material.		

APPENDIX I

SEDIMENT BASIN CALCULATIONS

TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

Computed by NSO Date 1/20/22 Checked by _____ Date _____
Project Port of Albany Basin # 1/ WQv Pond #2
Location Expansion Site Total Area draining to basin (≤ 50 Ac.) 5.3 Acres

BASIN SIZE DESIGN

1. Sediment storage zone volume = 1,000 cu. ft. x number of disturbed acres = 5,300 cu. ft., Top of Zone Elev. _____
2. Dewatering zone volume = 3,600 cu. ft. x number of drainage area acres = 19,080 cu. ft., Top of Zone Elev. _____
3. Length to width ratio = 3.6:1
4. A. Cleanout at 50% of sediment storage zone volume, Elev. _____
B. Distance below top of riser _____ feet
5. Minimum surface area is larger of $0.01 Q_{(10)}$ 0.15 or, $0.015 DA$ = 0.08 use 0.15 acres

DESIGN OF SPILLWAYS & ELEVATIONS

Runoff

6. $Q_{p(10)}$ = 14.96 cfs (Attach runoff computation sheets)

Pipe Spillway (Q_{ps})

7. Min. pipe spillway cap., $Q_{ps} = 0.2 \times$ _____ Drainage Area, acres = _____ cfs
Note: If there is no emergency spillway, then required $Q_{ps} = Q_{p(10)} =$ _____ cfs.
8. H, head = _____ ft. Barrel length = _____ ft
9. Barrel: Diam. _____ inches; $Q_{ps} = (Q)$ _____ x (cor.fac.) _____ = _____ cfs.
10. Riser: Diam. _____ inches; Length _____ ft.; h = _____ ft. Crest Elev. _____
11. Trash Rack: Diameter = _____ inches; H, height = _____ inches

*Basin 1 (WQv Pond #2) has adequate storage and surface area to function as a temporary sediment basin. All pipes and structures within basin are to be covered with filter fabric during construction. Sediment cleanout is to take place once final stabilization is reached.

Emergency Spillway Design

12. Emergency Spillway Flow, $Q_{es} = Q_p - Q_{ps} =$ _____ - _____ = _____ cfs.
13. Width _____ ft.; H_p _____ ft. Crest elevation _____; Design High Water Elev. _____
Entrance channel slope _____% ; Top of Dam Elev. _____
Exit channel slope _____%

ANTI-SEEP COLLAR/SEEPAGE DIAPHRAGM DESIGN

Collars:

14. $y =$ _____ ft.; $z =$ _____ :1; pipe slope = _____ %, $L_s =$ _____ ft.
Use _____ collars, _____ - _____ inches square; projection = _____ ft.

Diaphragms:

_____ width _____ ft. height _____ ft.

DEWATERING ORIFICE SIZING

(Determined from the Dewatering Device Standard)

15. Dewatering orifice diameter = _____ inches. Skimmer ____ or Riser ____ (check one)
16. Design dewatering time _____ days (Min. 2 days required)

TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

Computed by NSO Date 1/20/22 Checked by _____ Date _____
Project Port of Albany Basin # 2
Location Expansion Site Total Area draining to basin (≤ 50 Ac.) 15.2 Acres

BASIN SIZE DESIGN

- Sediment storage zone volume = 1,000 cu. ft. x number of disturbed acres = 15,200 cu. ft., Top of Zone Elev. 7.5
- Dewatering zone volume = 3,600 cu. ft. x number of drainage area acres = 54,720 cu. ft., Top of Zone Elev. 11.0
- Length to width ratio = 9.2:1
- A. Cleanout at 50% of sediment storage zone volume, Elev. 6.75'
B. Distance below top of riser 4.25 feet
- Minimum surface area is larger of $0.01 Q_{(10)}$ 0.57 or, $0.015 DA$ = 0.23 use 0.57 acres

DESIGN OF SPILLWAYS & ELEVATIONS

Runoff

- $Q_{p(10)}$ = 56.95 cfs (Attach runoff computation sheets)

Pipe Spillway (Q_{ps})

- Min. pipe spillway cap., $Q_{ps} = 0.2 \times$ 15.2 Drainage Area, acres = 3.04 cfs
Note: If there is no emergency spillway, then required $Q_{ps} = Q_{p(10)} =$ - cfs.
- H, head = 5 ft. Barrel length = 115 ft
- Barrel: Diam. 12 inches; $Q_{ps} = (Q)$ 4.41 x (cor.fac.) 0.86 = 3.79 cfs.
- Riser: Diam. 15 inches; Length 4.5 ft.; h = 1 ft. Crest Elev. 11.0
- Trash Rack: Diameter = 21 inches; H, height = 7 inches

Emergency Spillway Design

- Emergency Spillway Flow, $Q_{es} = Q_p - Q_{ps} =$ 56.95 - 3.79 = 53.16 cfs.
- Width 15 ft.; H_p 1 ft Crest elevation 12.0; Design High Water Elev. 13.0
Entrance channel slope 1 % ; Top of Dam Elev. 14.0
Exit channel slope 3 %

ANTI-SEEP COLLAR/SEEPAGE DIAPHRAGM DESIGN

Collars:

- $y =$ 4.5 ft.; $z =$ 2 :1; pipe slope = 0.5 %, $L_s =$ 27 ft.
Use 2 collars, 4 - 0 inches square; projection = 1.4 ft.

Diaphragms:

_____ width _____ ft. height _____ ft.

DEWATERING ORIFICE SIZING

(Determined from the Dewatering Device Standard)

- Dewatering orifice diameter = 5 inches. Skimmer X or Riser _____ (check one)
- Design dewatering time 2 days (Min. 2 days required)

TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

Computed by NSO Date 1/20/22 Checked by _____ Date _____
Project Port of Albany Basin # 3
Location Expansion Site Total Area draining to basin (≤ 50 Ac.) 33.0 Acres

BASIN SIZE DESIGN

- Sediment storage zone volume = 1,000 cu. ft. x number of disturbed acres = 33,000 cu. ft., Top of Zone Elev. 7.5
- Dewatering zone volume = 3,600 cu. ft. x number of drainage area acres = 118,800 cu. ft., Top of Zone Elev. 11.0
- Length to width ratio = 11.6:1
- A. Cleanout at 50% of sediment storage zone volume, Elev. 6.75
B. Distance below top of riser 4.25 feet
- Minimum surface area is larger of $0.01 Q_{(10)}$ 1.11 or, $0.015 DA$ = .49 use 1.11 acres

DESIGN OF SPILLWAYS & ELEVATIONS

Runoff

- $Q_{p(10)}$ = 110.93 cfs (Attach runoff computation sheets)

Pipe Spillway (Q_{ps})

- Min. pipe spillway cap., $Q_{ps} = 0.2 \times$ 33 Drainage Area, acres = 6.6 cfs
Note: If there is no emergency spillway, then required $Q_{ps} = Q_{p(10)} =$ - cfs.
- H, head = 5 ft. Barrel length = 115 ft
- Barrel: Diam. 15 inches; $Q_{ps} = (Q)$ 7.78 x (cor.fac.) 0.85 = 6.61 cfs.
- Riser: Diam. 18 inches; Length 4.5 ft.; h = 1 ft. Crest Elev. 11.0
- Trash Rack: Diameter = 27 inches; H, height = 8 inches

Emergency Spillway Design

- Emergency Spillway Flow, $Q_{es} = Q_p - Q_{ps} =$ 110.93 - 6.61 = 104.32 cfs.
- Width 30 ft.; H_p 1 ft Crest elevation 12.0; Design High Water Elev. 13.0
Entrance channel slope 1 % ; Top of Dam Elev. 14.0
Exit channel slope 3 %

ANTI-SEEP COLLAR/SEEPAGE DIAPHRAGM DESIGN

Collars:

- $y =$ 4.5 ft.; $z =$ 3 :1; pipe slope = 0.5 %, $L_s =$ 31.5 ft.
Use 2 collars, 4 - 3 inches square; projection = 1.6 ft.

Diaphragms:

_____ width _____ ft. height _____ ft.

DEWATERING ORIFICE SIZING

(Determined from the Dewatering Device Standard)

- Dewatering orifice diameter = 7 inches. Skimmer or Riser _____ (check one)
- Design dewatering time 2 days (Min. 2 days required)

18641.00-Construction Activity

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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DA1: (new Subcat)

Runoff = 14.96 cfs @ 12.07 hrs, Volume= 0.906 af, Depth> 2.05"

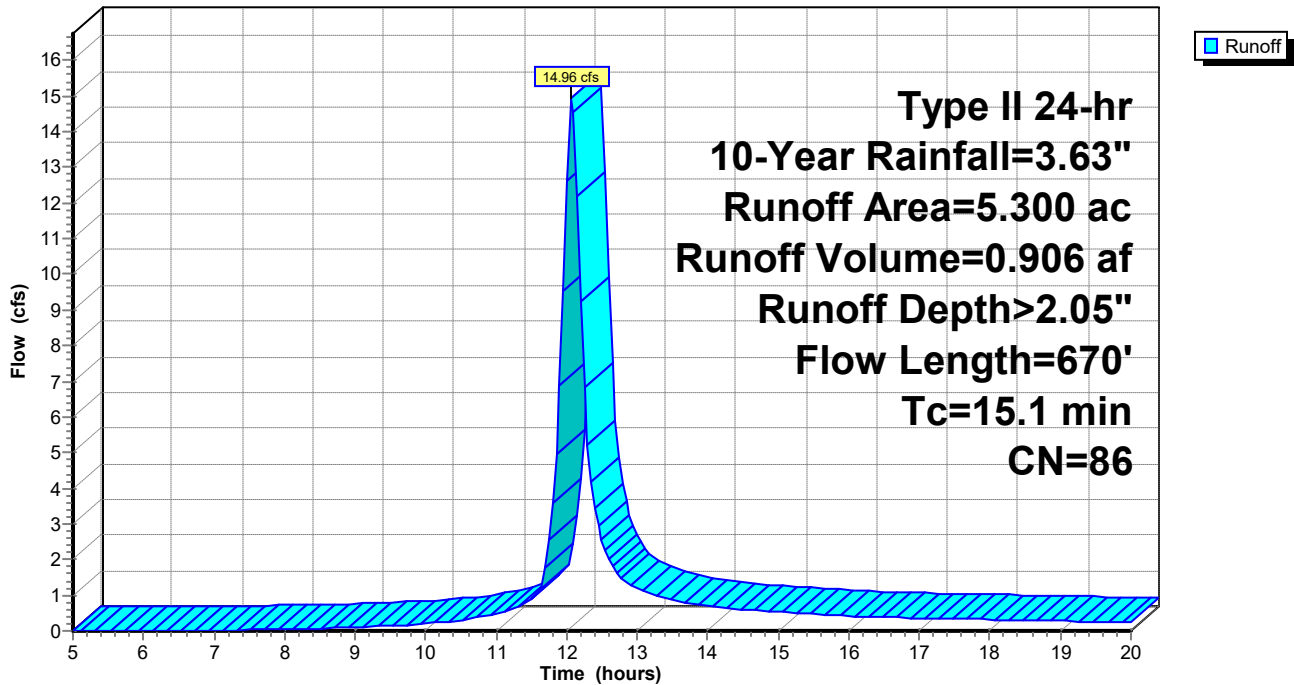
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
0.850	96	Gravel surface, HSG D
2.200	80	>75% Grass cover, Good, HSG D
2.250	89	Dirt roads, HSG D
5.300	86	Weighted Average
5.300		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.5	150	0.0200	0.72		Sheet Flow, n= 0.023 P2= 2.40"
11.6	520	0.0025	0.75		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
15.1	670	Total			

Subcatchment DA1: (new Subcat)

Hydrograph



18641.00-Construction Activity

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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DA2: (new Subcat)

Runoff = 56.95 cfs @ 12.04 hrs, Volume= 3.393 af, Depth> 2.68"

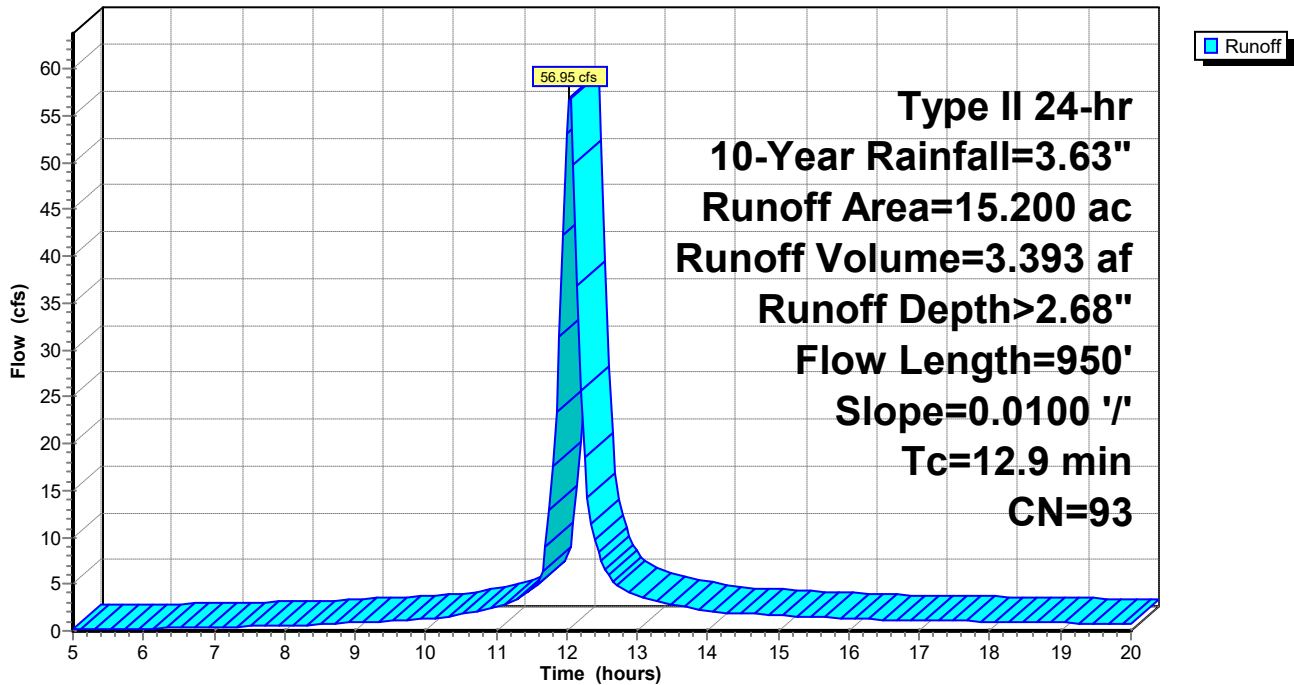
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 6.900	98	Bldg A
8.300	89	Dirt roads, HSG D
15.200	93	Weighted Average
8.300		54.61% Pervious Area
6.900		45.39% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.6	150	0.0100	0.54		Sheet Flow, n= 0.023 P2= 2.40"
8.3	800	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
12.9	950	Total			

Subcatchment DA2: (new Subcat)

Hydrograph



18641.00-Construction Activity

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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Subcatchment DA3: (new Subcat)

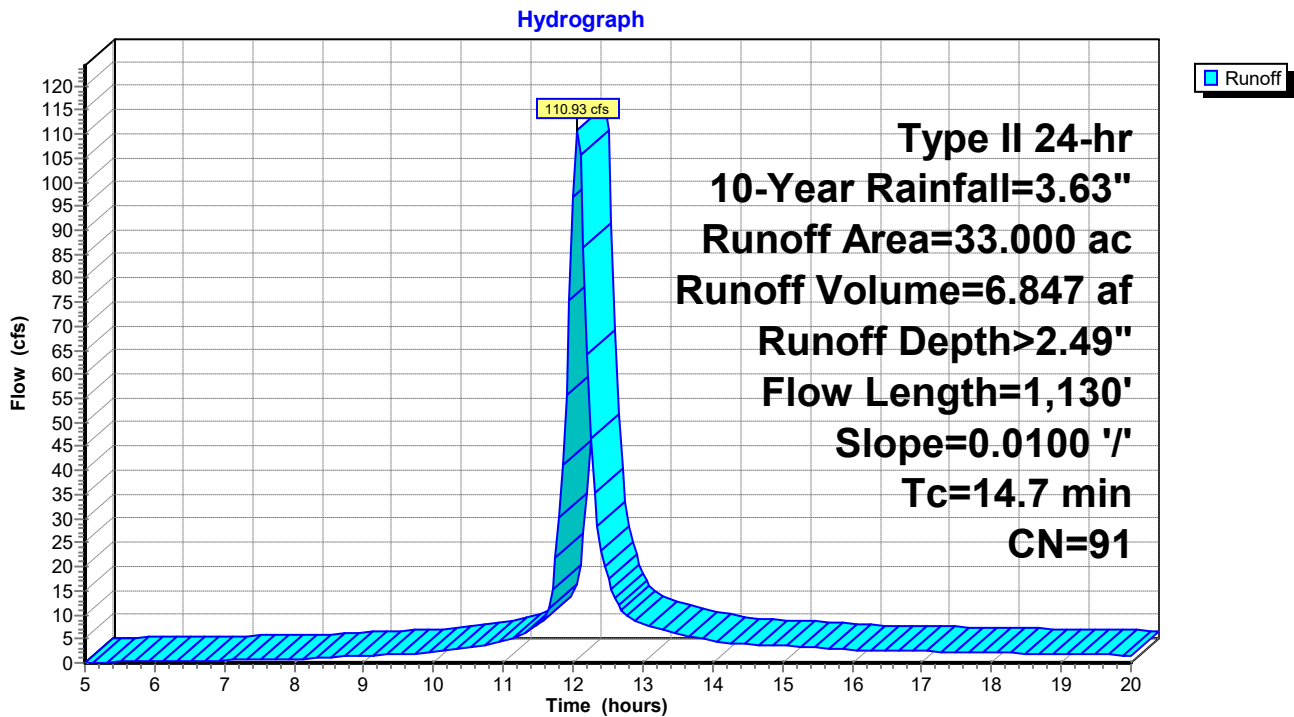
Runoff = 110.93 cfs @ 12.06 hrs, Volume= 6.847 af, Depth> 2.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-Year Rainfall=3.63"

Area (ac)	CN	Description
* 7.000	98	Bldg B C D
26.000	89	Dirt roads, HSG D
33.000	91	Weighted Average
26.000		78.79% Pervious Area
7.000		21.21% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.6	150	0.0100	0.54		Sheet Flow, n= 0.023 P2= 2.40"
10.1	980	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
14.7	1,130	Total			

Subcatchment DA3: (new Subcat)



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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Pond 2P: (new Pond)

Volume	Invert	Avail.Storage	Storage Description			
#1	6.00'	71,786 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
6.00	9,449	976.0	0	0	9,449	
7.00	11,415	988.9	10,417	10,417	11,693	
7.50	12,407	995.0	5,954	16,370	12,776	
11.00	19,527	1,039.0	55,416	71,786	20,738	

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Type II 24-hr 10-Year Rainfall=3.63"

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Summary for Pond 3p: (new Pond)

Volume	Invert	Avail.Storage	Storage Description			
#1	6.00'	156,085 cf	Custom Stage Data (Irregular) Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
6.00	21,679	1,328.0	0	0	21,679	
6.50	23,679	1,338.0	11,336	11,336	23,903	
7.00	25,694	1,347.0	12,340	23,676	25,940	
7.50	27,044	1,353.0	13,183	36,859	27,395	
11.00	41,606	1,419.0	119,226	156,085	42,740	

APPENDIX J

DRAFT NOI

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NOI for coverage under Stormwater General Permit for Construction Activity

version 1.35

(Submission #: HPE-0QXG-AE8EZ, version 1)

Details

Originally Started By Natalie Olivieri
Alternate Identifier Marmen-Welcon Tower Manufacturing Plant
Submission ID HPE-0QXG-AE8EZ
Submission Reason New
Status Draft
Active Steps Form Submitted

Form Input

Owner/Operator Information

Owner/Operator Name (Company/Private Owner/Municipality/Agency/Institution, etc.)

Albany Port District Commission

Owner/Operator Contact Person Last Name (NOT CONSULTANT)

Hendrick

Owner/Operator Contact Person First Name

Richard

Owner/Operator Mailing Address

106 Smith Boulevard

City

Albany

State

New York

Zip

12205

Phone

5184638763

Email

rhendrick@portofalbany.us

Federal Tax ID

14-6002520

Project Location

Project/Site Name

Marmen-Welcon Tower Manufacturing Plant

Street Address (Not P.O. Box)

309 River Road

Side of Street

East

City/Town/Village (THAT ISSUES BUILDING PERMIT)

Town of Bethlehem

State

NY

Zip

12077

DEC Region

4

County

ALBANY

Name of Nearest Cross Street

Old River Road

Distance to Nearest Cross Street (Feet)

970

Project In Relation to Cross Street

South

Tax Map Numbers Section-Block-Parcel

98.00-2-10.23

Tax Map Numbers

98.01-2-1.0

1. Coordinates

Provide the Geographic Coordinates for the project site. The two methods are:

- Navigate to the project location on the map (below) and click to place a marker and obtain the XY coordinates.
- The "Find Me" button will provide the lat/long for the person filling out this form. Then pan the map to the correct location and click the map to place a marker and obtain the XY coordinates.

Navigate to your location and click on the map to get the X,Y coordinates

42.602283629058164,-73.76555834600738

Project Details**2. What is the nature of this project?**

New Construction

3. Select the predominant land use for both pre and post development conditions.**Pre-Development Existing Landuse**

Forest

Post-Development Future Land Use

Industrial

3a. If Single Family Subdivision was selected in question 3, enter the number of subdivision lots.

NONE PROVIDED

4. In accordance with the larger common plan of development or sale, enter the total project site acreage, the acreage to be disturbed and the future impervious area (acreage)within the disturbed area.

*** ROUND TO THE NEAREST TENTH OF AN ACRE. ***

Total Site Area (acres)

108.6

Total Area to be Disturbed (acres)

72.7

Existing Impervious Area to be Disturbed (acres)

5.2

Future Impervious Area Within Disturbed Area (acres)

65.9

5. Do you plan to disturb more than 5 acres of soil at any one time?

Yes

6. Indicate the percentage (%) of each Hydrologic Soil Group(HSG) at the site.

A (%)

3.2

B (%)

0

C (%)

0

D (%)

96.8

7. Is this a phased project?

Yes

8. Enter the planned start and end dates of the disturbance activities.

Start Date

6/1/2022

End Date

9/1/2023

9. Identify the nearest surface waterbody(ies) to which construction site runoff will discharge.

Hudson River, Normans Kill, Wetland

9a. Type of waterbody identified in question 9?

Wetland/Federal Jurisdiction On Site (Answer 9b)

River On Site

Stream/Creek On Site

Other Waterbody Type Off Site Description

NONE PROVIDED

9b. If "wetland" was selected in 9A, how was the wetland identified?

Delineated by Consultant

10. Has the surface waterbody(ies) in question 9 been identified as a 303(d) segment in Appendix E of GP-0-20-001?

No

11. Is this project located in one of the Watersheds identified in Appendix C of GP-0-20-001?

No

12. Is the project located in one of the watershed areas associated with AA and AA-S classified waters?

No

If No, skip question 13.

13. Does this construction activity disturb land with no existing impervious cover and where the Soil Slope Phase is identified as D (provided the map unit name is inclusive of slopes greater than 25%), E or F on the USDA Soil Survey?

NONE PROVIDED

If Yes, what is the acreage to be disturbed?

NONE PROVIDED

14. Will the project disturb soils within a State regulated wetland or the protected 100 foot adjacent area?

Yes

15. Does the site runoff enter a separate storm sewer system (including roadside drains, swales, ditches, culverts, etc)?

No

16. What is the name of the municipality/entity that owns the separate storm sewer system?

NONE PROVIDED

17. Does any runoff from the site enter a sewer classified as a Combined Sewer?

No

18. Will future use of this site be an agricultural property as defined by the NYS Agriculture and Markets Law?

No

19. Is this property owned by a state authority, state agency, federal government or local government?

Yes

20. Is this a remediation project being done under a Department approved work plan? (i.e. CERCLA, RCRA, Voluntary Cleanup Agreement, etc.)

No

Required SWPPP Components

21. Has the required Erosion and Sediment Control component of the SWPPP been developed in conformance with the current NYS Standards and Specifications for Erosion and Sediment Control (aka Blue Book)?

Yes

22. Does this construction activity require the development of a SWPPP that includes the post-construction stormwater management practice component (i.e. Runoff Reduction, Water Quality and Quantity Control practices/techniques)?

Yes

If you answered No in question 22, skip question 23 and the Post-construction Criteria and Post-construction SMP Identification sections.

23. Has the post-construction stormwater management practice component of the SWPPP been developed in conformance with the current NYS Stormwater Management Design Manual?

No

24. The Stormwater Pollution Prevention Plan (SWPPP) was prepared by:

Professional Engineer (P.E.)

SWPPP Preparer

Adam Frosino

Contact Name (Last, Space, First)

Frosino, Adam

Mailing Address

60 Railroad Place, Suite 402

City

Saratoga Springs

State

NY

Zip

12866

Phone

5185809380

Email

afrosino@mjjinc.com

Download SWPPP Preparer Certification Form

Please take the following steps to prepare and upload your preparer certification form:

- 1) Click on the link below to download a blank certification form
- 2) The certified SWPPP preparer should sign this form
- 3) Scan the signed form
- 4) Upload the scanned document

[Download SWPPP Preparer Certification Form](#)**Please upload the SWPPP Preparer Certification**

SWPPP Preparer Cert_Signed.pdf - 05/24/2022 10:45 AM

Comment

NONE PROVIDED

Erosion & Sediment Control Criteria**25. Has a construction sequence schedule for the planned management practices been prepared?**

Yes

26. Select all of the erosion and sediment control practices that will be employed on the project site:**Temporary Structural**

Check Dams
 Construction Road Stabilization
 Dust Control
 Perimeter Dike/Swale
 Sediment Basin
 Sediment Traps
 Silt Fence
 Stabilized Construction Entrance
 Storm Drain Inlet Protection

Biotechnical

None

Vegetative Measures

Mulching
 Seeding
 Temporary Swale
 Topsoiling

Permanent Structural

Lined Waterway (Rock)
 Land Grading
 Retaining Wall
 Rock Outlet Protection
 Streambank Protection

Other

NONE PROVIDED

Post-Construction Criteria

*** IMPORTANT: Completion of Questions 27-39 is not required if response to Question 22 is No.**

27. Identify all site planning practices that were used to prepare the final site plan/layout for the project.

Preservation of Undisturbed Area
Preservation of Buffers
Reduction of Clearing and Grading

27a. Indicate which of the following soil restoration criteria was used to address the requirements in Section 5.1.6("Soil Restoration") of the Design Manual (2010 version).

All disturbed areas will be restored in accordance with the Soil Restoration requirements in Table 5.3 of the Design Manual (see page 5-22).

28. Provide the total Water Quality Volume (WQv) required for this project (based on final site plan/layout). (Acre-feet)
6.29

29. Post-construction SMP Identification

Use the Post-construction SMP Identification section to identify the RR techniques (Area Reduction), RR techniques (Volume Reduction) and Standard SMPs with RRv Capacity that were used to reduce the Total WQv Required (#28).

Identify the SMPs to be used by providing the total impervious area that contributes runoff to each technique/practice selected. For the Area Reduction Techniques, provide the total contributing area (includes pervious area) and, if applicable, the total impervious area that contributes runoff to the technique/practice.

Note: Redevelopment projects shall use the Post-Construction SMP Identification section to identify the SMPs used to treat and/or reduce the WQv required. If runoff reduction techniques will not be used to reduce the required WQv, skip to question 33a after identifying the SMPs.

30. Indicate the Total RRv provided by the RR techniques (Area/Volume Reduction) and Standard SMPs with RRv capacity identified in question 29. (acre-feet)

1.45

31. Is the Total RRv provided (#30) greater than or equal to the total WQv required (#28)?

No

If Yes, go to question 36. If No, go to question 32.

32. Provide the Minimum RRv required based on HSG. [Minimum RRv Required = (P) (0.95) (Ai) / 12, Ai=(s) (Aic)] (acre-feet)

1.32

32a. Is the Total RRv provided (#30) greater than or equal to the Minimum RRv Required (#32)?

Yes

If Yes, go to question 33.

Note: Use the space provided in question #39 to summarize the specific site limitations and justification for not reducing 100% of WQv required (#28). A detailed evaluation of the specific site limitations and justification for not reducing 100% of the WQv required (#28) must also be included in the SWPPP.

If No, sizing criteria has not been met; therefore, NOI can not be processed. SWPPP preparer must modify design to meet sizing criteria.

33. SMPs

Use the Post-construction SMP Identification section to identify the Standard SMPs and, if applicable, the Alternative SMPs to be used to treat the remaining total WQv (=Total WQv Required in #28 - Total RRv Provided in #30).

Also, provide the total impervious area that contributes runoff to each practice selected.

NOTE: Use the Post-construction SMP Identification section to identify the SMPs used on Redevelopment projects.

33a. Indicate the Total WQv provided (i.e. WQv treated) by the SMPs identified in question #33 and Standard SMPs with RRv Capacity identified in question #29. (acre-feet)

4.85

Note: For the standard SMPs with RRv capacity, the WQv provided by each practice = the WQv calculated using the contributing drainage area to the practice - provided by the practice. (See Table 3.5 in Design Manual)

34. Provide the sum of the Total RRv provided (#30) and the WQv provided (#33a).

6.31

35. Is the sum of the RRv provided (#30) and the WQv provided (#33a) greater than or equal to the total WQv required (#28)?

Yes

If Yes, go to question 36.

If No, sizing criteria has not been met; therefore, NOI can not be processed. SWPPP preparer must modify design to meet sizing criteria.

36. Provide the total Channel Protection Storage Volume (CPv required and provided or select waiver (#36a), if applicable.

CPv Required (acre-feet)

0.93

CPv Provided (acre-feet)

1.17

36a. The need to provide channel protection has been waived because:

NONE PROVIDED

37. Provide the Overbank Flood (Qp) and Extreme Flood (Qf) control criteria or select waiver (#37a), if applicable.

Overbank Flood Control Criteria (Qp)

Pre-Development (CFS)

73.24

Post-Development (CFS)

12.46

Total Extreme Flood Control Criteria (Qf)

Pre-Development (CFS)

163.60

Post-Development (CFS)

30.97

37a. The need to meet the Qp and Qf criteria has been waived because:

NONE PROVIDED

38. Has a long term Operation and Maintenance Plan for the post-construction stormwater management practice(s) been developed?

Yes

If Yes, Identify the entity responsible for the long term Operation and Maintenance

Albany Port District Commission

39. Use this space to summarize the specific site limitations and justification for not reducing 100% of WQv required (#28). (See question #32a) This space can also be used for other pertinent project information.

The proposed Facility requires 85 acres of usable manufacturing and storage space along the Hudson River. This site was chosen given it is located adjacent to the existing Port of Albany and is directly on the Hudson River. However, the usable portion of the site adjacent to the Hudson River, is only 66-acre area. Therefore, the entirety of the site is needed for the OSW manufacturing process, with an ancillary receiving site located at 700 Smith Boulevard.

Responses to questions 36 and 37 are related only to Analysis Point #1A. Analysis Points #1, #2, and #3 have direct discharge to tidal waters and therefore are waived from meeting the CPv, Qp, and Qf requirements.

Post-Construction SMP Identification

Runoff Reduction (RR) Techniques, Standard Stormwater Management Practices (SMPs) and Alternative SMPs
Identify the Post-construction SMPs to be used by providing the total impervious area that contributes runoff to each technique/practice selected. For the Area Reduction Techniques, provide the total contributing area (includes pervious area) and, if applicable, the total impervious area that contributes runoff to the technique/practice.

RR Techniques (Area Reduction)

Round to the nearest tenth

Total Contributing Acres for Conservation of Natural Area (RR-1)

4.0

Total Contributing Impervious Acres for Conservation of Natural Area (RR-1)

0

Total Contributing Acres for Sheetflow to Riparian Buffers/Filter Strips (RR-2)

NONE PROVIDED

Total Contributing Impervious Acres for Sheetflow to Riparian Buffers/Filter Strips (RR-2)

NONE PROVIDED

Total Contributing Acres for Tree Planting/Tree Pit (RR-3)

NONE PROVIDED

Total Contributing Impervious Acres for Tree Planting/Tree Pit (RR-3)

NONE PROVIDED

Total Contributing Acres for Disconnection of Rooftop Runoff (RR-4)

NONE PROVIDED

RR Techniques (Volume Reduction)

Total Contributing Impervious Acres for Disconnection of Rooftop Runoff (RR-4)

NONE PROVIDED

Total Contributing Impervious Acres for Vegetated Swale (RR-5)

NONE PROVIDED

Total Contributing Impervious Acres for Rain Garden (RR-6)

NONE PROVIDED

Total Contributing Impervious Acres for Stormwater Planter (RR-7)

NONE PROVIDED

Total Contributing Impervious Acres for Rain Barrel/Cistern (RR-8)

NONE PROVIDED

Total Contributing Impervious Acres for Porous Pavement (RR-9)

NONE PROVIDED

Total Contributing Impervious Acres for Green Roof (RR-10)

NONE PROVIDED

Standard SMPs with RRv Capacity

Total Contributing Impervious Acres for Infiltration Trench (I-1)

NONE PROVIDED

Total Contributing Impervious Acres for Infiltration Basin (I-2)

1

Total Contributing Impervious Acres for Dry Well (I-3)

NONE PROVIDED

Total Contributing Impervious Acres for Underground Infiltration System (I-4)

23.7

Total Contributing Impervious Acres for Bioretention (F-5)

NONE PROVIDED

Total Contributing Impervious Acres for Dry Swale (O-1)

0.05

Standard SMPs

Total Contributing Impervious Acres for Micropool Extended Detention (P-1)

5.1

Total Contributing Impervious Acres for Wet Pond (P-2)

NONE PROVIDED

Total Contributing Impervious Acres for Wet Extended Detention (P-3)

NONE PROVIDED

Total Contributing Impervious Acres for Multiple Pond System (P-4)

NONE PROVIDED

Total Contributing Impervious Acres for Pocket Pond (P-5)

NONE PROVIDED

Total Contributing Impervious Acres for Surface Sand Filter (F-1)

NONE PROVIDED

Total Contributing Impervious Acres for Underground Sand Filter (F-2)

NONE PROVIDED

Total Contributing Impervious Acres for Perimeter Sand Filter (F-3)

NONE PROVIDED

Total Contributing Impervious Acres for Organic Filter (F-4)

NONE PROVIDED

Total Contributing Impervious Acres for Shallow Wetland (W-1)

NONE PROVIDED

Total Contributing Impervious Acres for Extended Detention Wetland (W-2)

NONE PROVIDED

Total Contributing Impervious Acres for Pond/Wetland System (W-3)

NONE PROVIDED

Total Contributing Impervious Acres for Pocket Wetland (W-4)

NONE PROVIDED

Total Contributing Impervious Acres for Wet Swale (O-2)

NONE PROVIDED

Alternative SMPs (DO NOT INCLUDE PRACTICES BEING USED FOR PRETREATMENT ONLY)

Total Contributing Impervious Area for Hydrodynamic

NONE PROVIDED

Total Contributing Impervious Area for Wet Vault

NONE PROVIDED

Total Contributing Impervious Area for Media Filter

NONE PROVIDED

"Other" Alternative SMP?

Contech Jellyfish Filter

Total Contributing Impervious Area for "Other"

54.7

Provide the name and manufacturer of the alternative SMPs (i.e. proprietary practice(s)) being used for WQv treatment.

Note: Redevelopment projects which do not use RR techniques, shall use questions 28, 29, 33 and 33a to provide SMPs used, total WQv required and total WQv provided for the project.

Manufacturer of Alternative SMP

Contech

Name of Alternative SMP

Jellyfish Filter

Other Permits

40. Identify other DEC permits, existing and new, that are required for this project/facility.

Endangered or Threatened Species (Incidental Take Permit)

If SPDES Multi-Sector GP, then give permit ID

NONE PROVIDED

If Other, then identify

Wetland Joint Permit, Air State Facility Permit

41. Does this project require a US Army Corps of Engineers Wetland Permit?

Yes

If "Yes," then indicate Size of Impact, in acres, to the nearest tenth

0.9

42. If this NOI is being submitted for the purpose of continuing or transferring coverage under a general permit for stormwater runoff from construction activities, please indicate the former SPDES number assigned.

NONE PROVIDED

MS4 SWPPP Acceptance

43. Is this project subject to the requirements of a regulated, traditional land use control MS4?

Yes - Please attach the MS4 Acceptance form below

If No, skip question 44

44. Has the "MS4 SWPPP Acceptance" form been signed by the principal executive officer or ranking elected official and submitted along with this NOI?

NONE PROVIDED

MS4 SWPPP Acceptance Form Download

Download form from the link below. Complete, sign, and upload.

[MS4 SWPPP Acceptance Form](#)

MS4 Acceptance Form Upload

NONE PROVIDED

Comment

NONE PROVIDED

Owner/Operator Certification

Owner/Operator Certification Form Download

Download the certification form by clicking the link below. Complete, sign, scan, and upload the form.
[Owner/Operator Certification Form \(PDF, 45KB\)](#)

Upload Owner/Operator Certification Form

POA - eNOI Owner Cert_Signed.pdf - 05/24/2022 11:52 AM

Comment

NONE PROVIDED

Attachments

Date	Attachment Name	Context	User
5/24/2022 11:52 AM	POA - eNOI Owner Cert_Signed.pdf	Attachment	Natalie Olivieri
5/24/2022 10:45 AM	SWPPP Preparer Cert_Signed.pdf	Attachment	Natalie Olivieri

Status History

	User	Processing Status
12/16/2021 1:10:48 PM	Natalie Olivieri	Draft

Processing Steps

Step Name	Assigned To/Completed By	Date Completed
Form Submitted		
Under Review	DAVID GASPER	
Under Review	Daniel von Schilgen	

APPENDIX K

UNIFORM PROCEDURES ACT EXCEPTION LETTER

NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION

Division of Environmental Permits

625 Broadway, 4th Floor, Albany, New York 12233-1750
P: (518) 402-9167 | F: (518) 402-9168 | deppermitting@dec.ny.gov
www.dec.ny.gov

March 30, 2022

VIA EMAIL

Richard Hendrick
Albany Port District Commission
106 Smith Boulevard
Albany, NY 12202
rhendrick@portofalbany.us

RE: SPDES GP-0-20-001 - Commencement of Limited Construction Activities
Port of Albany Expansion Project
Beacon Island Parcel, Bethlehem NY, Albany County
DEC # 4-0122-00322/00002

Dear Mr. Hendrick:

By letter dated March 25, 2022, Albany Port District Commission (APDC) requested to commence limited construction activities (i.e., tree clearing), and authorization to discharge pursuant to the Stormwater State Pollutant Discharge Elimination System (SPDES) General Permit for Construction Activity (GP-0-20-001), for the Port of Albany Expansion Project (Project) prior to obtaining all necessary permits from New York State Department of Environmental Conservation (NYSDEC or Department). APDC has not obtained an Air State Facility (ASF) permit, individual SPDES permit, Part 182 permit, Protection of Waters permits and Water Quality Certification (WQC) ("Uniform Procedures Act (UPA) Permits").¹ APDC asserts in its request that good cause exists based on its committed construction schedule and specific requirements for site preparation, construction, and operational components. Pursuant to 6 NYCRR 621.3(a)(4), based on permitting considerations and the specific circumstances presented here, NYSDEC reviewed the March 25, 2022 request from APDC and determined that there is good cause to allow the commencement of limited construction activities² as further described herein, without all UPA Permits having been obtained.

¹According to Part II(C)(1) of GP-0-20-001, an owner or operator shall not commence any construction activity in any location until the authorization to discharge under the General Permit goes into effect. Additionally, under Part II(C)(2)(b) of GP-0-20-001, authorization to discharge under the permit will be effective, among other requirements, when the owner or operator has obtained, "all necessary Department permits subject to the Uniform Procedures Act ("UPA") (see 6 NYCRR Part 621), or the equivalent from another New York State agency" unless otherwise notified by the Department pursuant to 6 NYCRR 621.3(a)(4).

² Construction [Activities] are defined in GP-0-20-001 as, "any clearing, grading, excavation, filling, demolition or stockpiling activities that result in soil disturbance. Clearing activities can include, but are not limited to, logging equipment operation, the cutting and skidding of trees, stump removal and/or brush root removal. Construction activity does not include routine maintenance that is performed to maintain the original line and grade, hydraulic capacity, or original purpose of a facility."

Demonstration of Good Cause

In evaluating whether there is good cause for NYSDEC to grant an exception to the authorization criterion contained in Part II(C)(2)(b) of SPDES GP-0-20-0001, and allow authorization to discharge and the commencement of limited construction activities prior to obtaining all other necessary UPA permits, NYSDEC has considered the following factors:

- Pursuant to UPA regulations, Section 621.3(a)(4), APDC has submitted all applications for UPA Permits for the Project.
- The requirements of the State Environmental Quality Review Act (SEQR - Article 8 of the ECL) have been satisfied,³ as follows: (i) The Town of Bethlehem Planning Board was established as SEQR Lead Agency (Lead Agency) and a positive declaration was issued requiring a Draft Generic Environmental Impact Statement (GEIS) for the Project; (ii) a Final GEIS was accepted as complete and a SEQR Findings Statement was adopted by the Lead Agency on June 2, 2020 for the Project; (iii) the Lead Agency determined the Project may have potential to create one or more significant adverse environmental impacts not evaluated within the Final GEIS and issued a Positive Declaration requiring a Supplemental Draft EIS on July 6, 2021; and (iv) a Supplemental Final EIS was accepted as complete and a SEQR Findings Statement was adopted by the Lead Agency on March 15, 2022 for the Project.
- The requirements of the State Historic Preservation Act (SHPA),⁴ have been complied with for the Project, as follows:
 - The Stockbridge Munsee Community issued their opinion in a March 2, 2022 letter that the Project will have No Adverse Effect on Historic Resources.
 - The New York State Historic Preservation Office (SHPO) issued a letter on March 25, 2022, stating that that no historic properties, including archaeological and/or historic resources, will be Adversely Affected by the Project, provided that a Restrictive Deed Covenant is filed to protect and maintain the vegetated buffer along the Hudson River shoreline.
- APDC has prepared a Stormwater Pollution Prevention Plan (SWPPP) for tree clearing activities.
- On March 29, 2022, the Town of Bethlehem as a regulated, traditional land use control Municipal Separate Stormwater Sewer Systems (MS4) accepted the SWPPP for tree clearing activities.
- APDC has indicated that to meet its contractual obligations with Equinor to be operational by December 1, 2023, tree clearing must take place by mid-April 2022 to facilitate site preparation, including implementation of a 3-month surcharge program to address poor soils and settlement concerns.
- APDC has indicated that the UPA Permits for the operational components of the Project (ASF and individual SPDES permits) require selection of manufacturing and processing equipment that must follow the Port of Albany procurement process and therefore, not all information is available prior to the construction bid. This information is required for NYSDEC to issue the ASF and individual SPDES permits.

³ See Part II.C(2)(a) of SPDES GP-0-20-001

⁴ See Part I.F(8)(b)(iv) of SPDES GP-0-20-001

Commencement of Limited Construction Activities

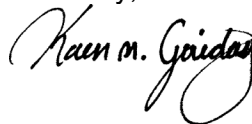
In consideration of the factors identified above, NYSDEC is hereby granting a limited exception to the authorization criterion contained in Part II(C)(2)(b) of SPDES GP-0-20-001. Upon submission of a complete eNOI, APDC would be authorized to commence limited construction activities, (i.e., tree clearing), under SPDES GP-0-20-001 and pursuant to the SWPPP approved by the Town of Bethlehem on March 29, 2022, subject to the following limitations:

1. No permanent construction, including building supports and foundations, can commence until the Air State Facility permit is obtained.⁵
2. No construction of the Project's wastewater treatment facility can commence until the individual SPDES permit is issued and plan approval for the wastewater treatment facility has been obtained from NYSDEC.
3. No excavation, fill, or dredging activities can commence in any wetlands or other waters of the U.S., including the Hudson River, Normans Kill, and federally regulated wetlands, until the following Permits are issued: Part 182, Protection of Waters, and WQC.
4. If tree clearing is conducted within federal wetlands, it must only be done using hand equipment and no stumps shall be removed.
5. No trees shall be removed within the vegetated buffer area, located along the Hudson River, in contravention of the Restrictive Deed Covenant that APDC has agreed to establish.
6. If any bats are observed flying from a tree that will be cut, work activities shall be stopped immediately and NYSDEC shall be contacted for guidance (see #5 in the following link: <https://www.dec.ny.gov/animals/106090.html>).
7. All other applicable terms and conditions of SPDES GP-0-20-001 are satisfied and complied with.

This exception to Part II(C)(2)(b) of SPDES GP-0-20-001 for the limited construction activities (i.e., tree clearing) is only authorized until May 15, 2022, or until NYSDEC issues all UPA Permits, whichever comes first. Please also note that granting of this exception does not guarantee issuance of the individual permits identified above as the permits are still subject to public review and comment, and other applicable provisions of 6 NYCRR Part 621. Further, this exception does not apply to construction activities that would be commenced beyond tree clearing. As a result, APDC assumes all risks in commencing construction.

Please contact me at karen.gaidasz@dec.ny.gov if you have any questions or concerns.

Sincerely,



Karen M. Gaidasz, Chief
Offshore Wind & Hydroelectric Section
Bureau of Energy Project Management

⁵ NYCRR 201-2.1(b)(9), specifically excludes site clearing and excavation activities, it states, "[t]he initiation of physical on-site construction activities which are of a permanent nature excluding site clearing and excavation. Such activities include, but are not limited to, installation of building supports and foundations, laying underground pipework and construction of permanent storage structures."

APPENDIX L

5 ACRE WAIVER REQUEST



May 20, 2022

Paul Penman, P.E.
Town Engineer, Deputy Commissioner of Public Works
Town of Bethlehem
445 Delaware Avenue
Delmar, New York 12054

Re: SPDES General Permit for Storm Water Discharges from Construction Activity –
Marmen-Welcon Tower Manufacturing Plant

Mr. Penman,

We are hereby requesting approval to disturb more than 5 acres of soil at a time for the Marmen-Welcon Tower Manufacturing Plant project.

Activities related to the above construction site will comply with all other requirements under GP-0-20-001. As such, SWPPP inspections will be conducted twice weekly while more than 5 acres of soil are disturbed.

The project has been split into five (5) phases spanning 20 months as shown on the project's Erosion and Sediment Control plans. The maximum soil disturbance at one time is anticipated to be around 12-15 acres as partial disturbance in two phases may occur simultaneously for short durations given the nature of the project. The anticipated soil disturbance areas and durations for each phase are as follows:

SOIL DISTURBANCE PHASING		
PHASE	DISTURBANCE AREA	DURATION
1	8.5 ACRES	2 MONTHS
2	11.3 ACRES	
3	11.0 ACRES MAX	6 MONTHS
3A	9.7 ACRES	
3B	9.6 ACRES	
3C	10.0 ACRES	
3D	10.1 ACRES	
3E	10.0 ACRES	
3F	3.5 ACRES	
4	NO NEW AREAS	4 MONTHS
5	5.1 ACRES	8 MONTHS

Disturbances associated with Phases 1 and 2 are expected to take place concurrently over a 2-month period. During these phases the construction entrance (including rock hammering), staging area, and site access roads will be established, as well as temporary sediment basins #1, #2, and #3. Any additional sediment controls not installed during the site tree cutting are to be installed during this phase.

During Phase 3 the site will be grubbed, and mass site grading will occur in preparation for the stone aggregate surcharging. Approximately 98,000 CY of on-site cut material will be used as fill to balance out the site. In addition, approximately 150,000-200,000 CY of suitable fill will be brought in to bring the site up to the sub-grade elevation.

The large grubbing area as well as the large amount of mass grading required resulted in breaking up Phase 3 into sub-phases of roughly 10 acres each. The sub-phases were determined based on overall project sequencing to start at the south end with Building A preparation, as well as establishing approximate areas where borrowing and fill will occur within each sub-area. Limits of disturbance to be minimized in each sub-phase by stabilizing areas within 2 days of achieving final grade. The sub-phase areas will be disturbed and stabilized in a rolling operation as the earthwork progresses from the south end of the site to the north end with disturbance ranging from 8-11 acres. The disturbance envelope ranges from 700 feet initially to 400 feet as earthwork progresses. To avoid stockpiling, available cut material from one sub-phase area that no longer requires any additional fill may be deposited and stabilized within another sub-phase area; however, the overall total disturbed area during Phase 3 shall not exceed 11.0 acres. Fine earthwork grading and subgrade preparation under the surcharge areas in accordance with the project's geotechnical report will also occur during this phase. In accordance with the SWPPP, all areas which are not active will be temporarily stabilized.

During Phase 4, approximately 700,000 CY of stone aggregate will be imported and stockpiled on the proposed building pads as a temporary building pad surcharge and will be used as the future stone yard area. It is anticipated that the subbase stone will begin to be brought into the site as the building footprint subgrade is completed for each sub-phase of Phase 3. As the stone aggregate is brought onto the site and placed in the surcharge areas it will act as permanent stabilization therefore decreasing the disturbed area. Given the volume of material to be brought into the site, this will take some time and will be completed in a rolling fashion in a similar fashion to Phase 3. The first building's surcharge import (Building A) will be completed to enable the surcharging compaction timeframe to start prior to placing the stone aggregate surcharge on the next building pad. Any peripheral subgrade areas previously disturbed or disturbed as part of the surcharge operations and no longer active will be temporarily stabilized in accordance with the SWPPP.

Phase 5 includes spreading the stone aggregate surcharge material to establish the stone yard area and all remaining construction on the project. Once the proposed drainage system and second pond have been installed and are operational, the temporary sediment basins will be removed as well as the conversion and installation of the permanent stormwater ponds. All

previously disturbed areas that are to remain pervious will need to achieve final stabilization during this phase prior to issuance of the Notice of Termination.

The attached Phasing Plans demonstrates the intended construction sequence for the Marmen-Welcon Tower Manufacturing Plant project.

If you have any questions, or require anything further, please let us know. Thank you.

Sincerely,
McFarland-Johnson, Inc.




Adam J. Frosino, PE, PTOE
Project Manager

cc: Robert Leslie, Town of Bethlehem
Richard Hendrick, Port of Albany
Megan Daly, Port of Albany
Steve Boisvert, McFarland-Johnson

APPENDIX M

NATIONAL GRID ENVIRONMENTAL GUIDANCE

 National Grid Environmental Guidance	Doc No.:	EG-501NYN
	Rev. No.:	5
	Page No.:	1 of 2
	Date:	03/05/2020
SUBJECT Release Notifications in New York North	REFERENCE EP-5	

Purpose / Objective: This guidance document provides instructions for reporting a release of oil, chemical, or hazardous material.

Who: All National Grid employees and contractors working on National Grid projects or properties.

What to Do:

Report all releases to the National Grid Regional Control Center (RCC) immediately, regardless of the volume or location.

EASTERN RCC (518) 356-6471

CENTRAL RCC (315) 460-2796

WESTERN RCC (716) 398-5308

Provide the following information to the RCC concerning the release:


- Name and contact information
- Time of discovery
- Location (be specific)
- Material and quantity
- Source (vehicle number, transformer, gas meter, HVAC unit, tank number, etc.)
- Cause (i.e., equipment malfunction, motor vehicle accident, storm, human factor, other)
- Description of impacted area and resources (land, water, air)
- Request cleanup crew

REGIONAL CONTROL CENTER:

1. Upon notification of a release, contact New York State Spill Hotline (1-800-457-7362) within 2 hours (of discovery time).
2. If release is reported at an Environmental SIR Site, contact Environmental immediately (see below).
3. Record release in the Incident Management System (IMS).
4. Contact Divisional Environmental Engineer, as applicable.

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ENVIRONMENTAL MANAGEMENT:

1. Communicate with RCC and/or field crews regarding additional reporting requirements (e.g., releases to water and PCB releases require reporting to the National Response Center (1-800-424-8802).
2. In IMS categorize the release as Category 1 or Category 2 (EG-1502) and classify/complete/close out the incident.
3. Confirm clean up, provide additional information to state agency to close out the release as requested.

RELEASE REPORTING ON NEW YORK SIR MGP SITES

Environmental Site Investigation and Remediation has entered into Consent Orders with the New York State Department of Environmental Conservation (NYSDEC) to evaluate and, where necessary, remediate former manufactured gas plant (MGP) sites. These sites are managed by a National Grid project manager (PM). As agreed to with NYSDEC, in the event of an accidental release or spill of material at an MGP site which will require subsurface excavation work for cleanup:


- Report release using procedures above.
- The National Grid PM must be notified as soon as possible to coordinate work.
- The National Grid PM would document the release in IMS.

HELP: Contact the local Environmental Representative if you have questions.

EASTERN:	Matt Root	518-227-7508
CENTRAL:	Rich Fox	315-546-4011
WESTERN:	Lisa Montesano	716-479-5339

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	Date:	03/06/2020
SUBJECT Release Clean Up in New York North	REFERENCE EP-5; Release Response	

Purpose / Objective:

The purpose of this guidance document is to provide instructions in the clean-up of oil and other chemical releases.

Who:

This guidance applies to New York North National Grid personnel who may be assigned to respond and/or clean up a release.

What To Do:

Immediate Actions:

- Secure the area
- Attempt to contain release. Utilize release kit contained on most company vehicles.
- Use absorbent/containment materials to minimize or eliminate the spread of contamination.
- Do not walk through or touch the released material; step away from the release area.
- Using physical barriers, visible warnings (i.e., caution tape, cones, etc.), or other means, restrict access to the release area. Prevent unauthorized persons from entering the area.

Note: *Large releases should be cleaned up by qualified Hazardous Materials personnel. If the release is large and/or PCB containing, or has reached a water body, contact Regional Control or the Divisional Environmental Engineer for assistance in obtaining help with the clean-up.*

Clean up Requirements:

Assess the release. Determine material released. If hazardous material such as mercury, acid or PCB oil, contact Regional Control for help in securing Hazardous Materials personnel or release contractor.


Don personnel protective equipment (PPE) as necessary. PPE may include, but not be limited to gloves, hardhats, safety glasses, steel toed shoes, coveralls, etc. If working near roadway, appropriate cones shall be placed, and high visibility clothing shall be worn. Follow all Safety procedures.

Note: *All releases are unique. The clean-up methodology employed will depend upon the nature of the release, the amount released, location, etc. The guidance listed below is meant to be general and not prescriptive.*

Non-PCB oil releases to land:

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Non-PCB oil releases include non-PCB labeled transformers, hydraulic oil, diesel fuel and motor oil. Clean up requires removal of visible stained oil from the surface. Soil removal, use of oil sorbent pads, Speedi Dri, and use of a water-based cleaner may all be used for release clean-up.

- Remove all visible traces of oil.
- Document clean-up efforts and provide to divisional environmental engineer.
- Containerize waste in appropriate containers and label.

Note: *NYS DEC guidance and clean up criteria vary between Regions in NYS. Effort shall be made to clean the area to as close as possible to pre-release conditions.*

Unlabeled transformer oil releases to land:

If an unlabeled transformer has released, obtain a sample of the oil from the unit and conduct a field PCB test using a CLOR-N-OIL kit. Collect an additional sample for laboratory analysis. If results reveal ≥ 50 ppm, waste clean-up debris must be handled as PCB contaminated and labeled as such until laboratory results determine otherwise. If CLOR-N-OIL results reveal < 50 ppm, the oil and waste may be handled as non-PCB until laboratory results are received. If no oil is left in the unit or a sample cannot be obtained, collect oily soil or debris and send to laboratory for analysis.

- Clean up release as noted above.
- Collect additional soil sample or wipe samples to verify clean up.
- Containerize waste and label appropriately.
- Document clean up and provide to divisional environmental engineer.
- Clean up should be completed within 48 hours. Otherwise, fully document reason for the delay.
- Clean up all reusable equipment using rags and/or cleaners as necessary.
- If PCB results confirm that the oil release was PCB contaminated or PCB oil, an EPA Identification Number may be required prior to disposal of material. Contact the Divisional Engineer for assistance.

Divisional Environmental Engineer Contacts


Western	Lisa Montesano	716-479-5339
Central	Rich Fox	315-546-4011
Eastern	Matt Root	518-227-7508

Documentation

Official record of all releases is maintained in the Incident Management System (IMS.)

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Regional Control centers will initiate the IMS report upon notification from the field and document time of incident, notification from field time, regulatory notification time, release details (material released, amount, location, response measures). Regional control follows National Grid Distribution Control Center System Operations Operating Guide 3.7 "Oil Release Reporting."

If the release is of sensitive or serious nature (based on public exposure, environmental impact, or public relations issue) such as those involving bodies of water or public buildings in addition to immediate notification to the divisional engineer, notify and document in the Shift Supervisor log book.

Document remediation efforts including release area and property items/materials impacted amount of clean up necessary. Submit documentation to Divisional Environmental Engineer.

Any contact with members of the public, emergency agencies or regulatory personnel should be documented by the response crew.

Divisional Environmental Engineers shall maintain and complete the release documentation in the IMS system and ensure release is closed out.

HELP:

Contact the local Environmental Representative if you have questions.